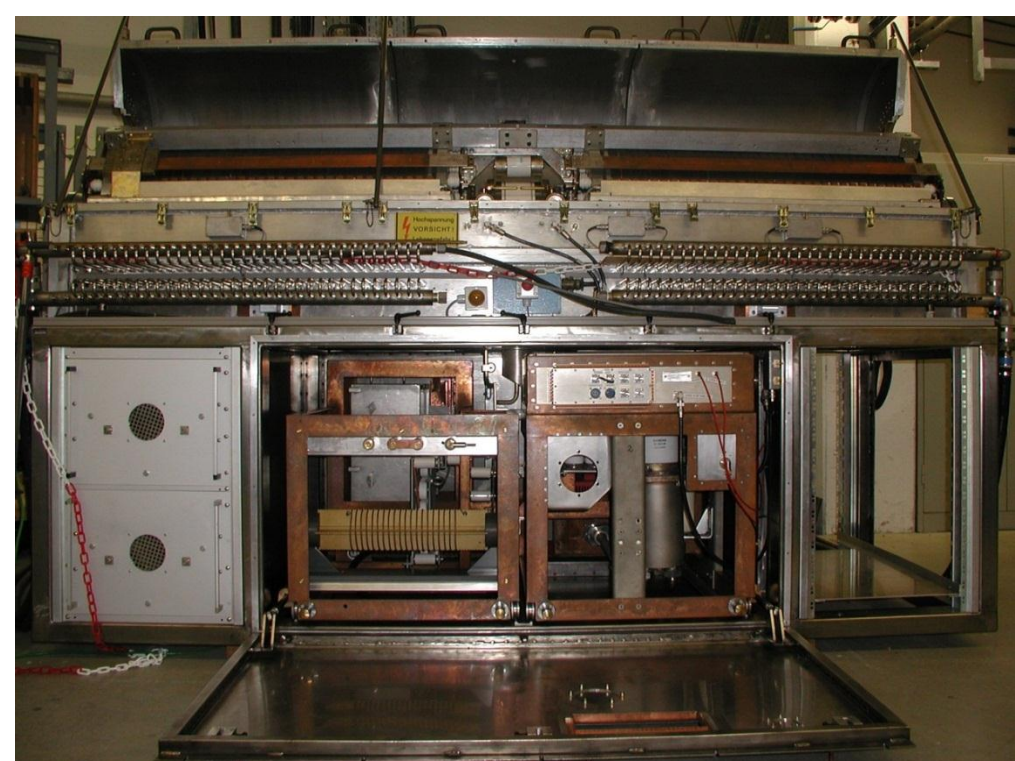


Eigenmode Computation for Biased Ferrite-Loaded Cavity Resonators*

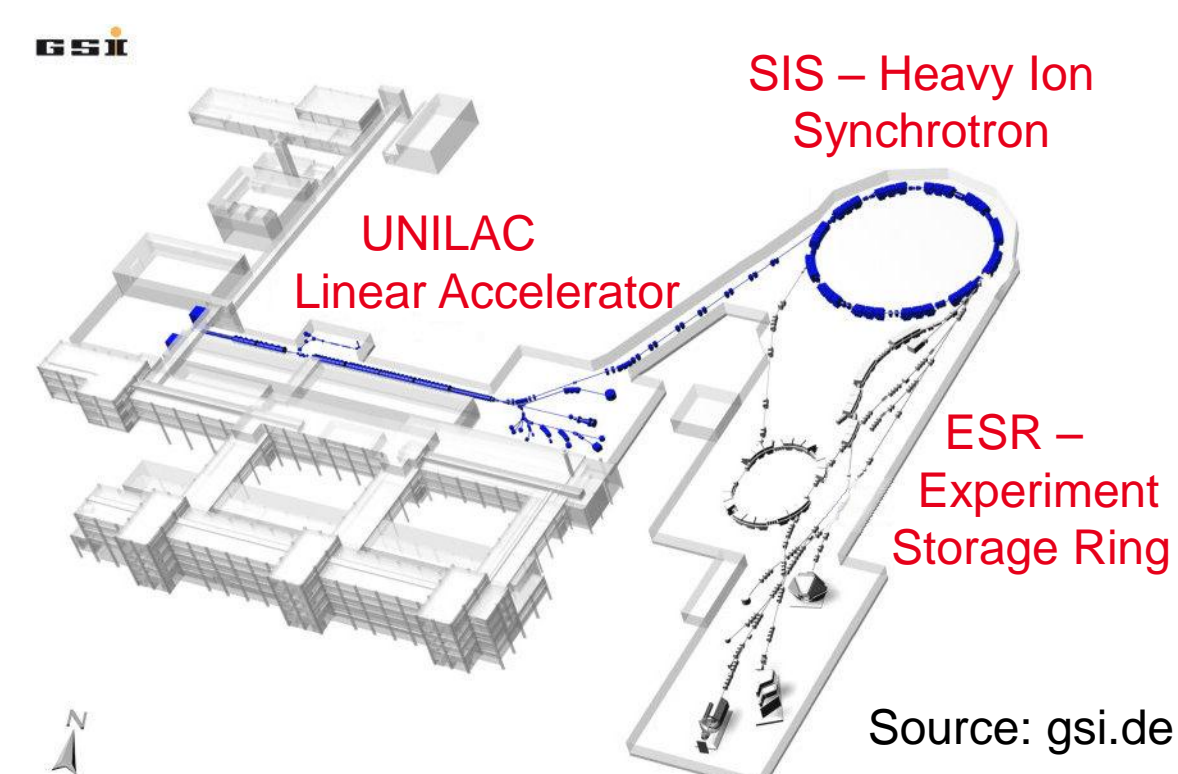
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SIS 18 Ferrite Cavity of GSI

For acceleration of heavy ions at the synchrotron SIS18 of the GSI Helmholtzzentrum für Schwerionenforschung in Darmstadt two biased ferrite-loaded cavity resonators are installed.



SIS 18 ferrite cavity. Source: GSI, A. Zschau

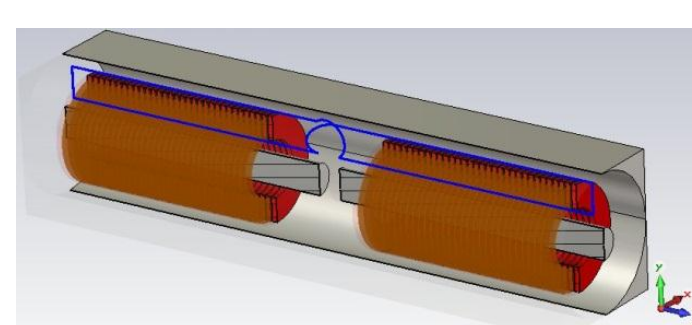


Source: gsi.de

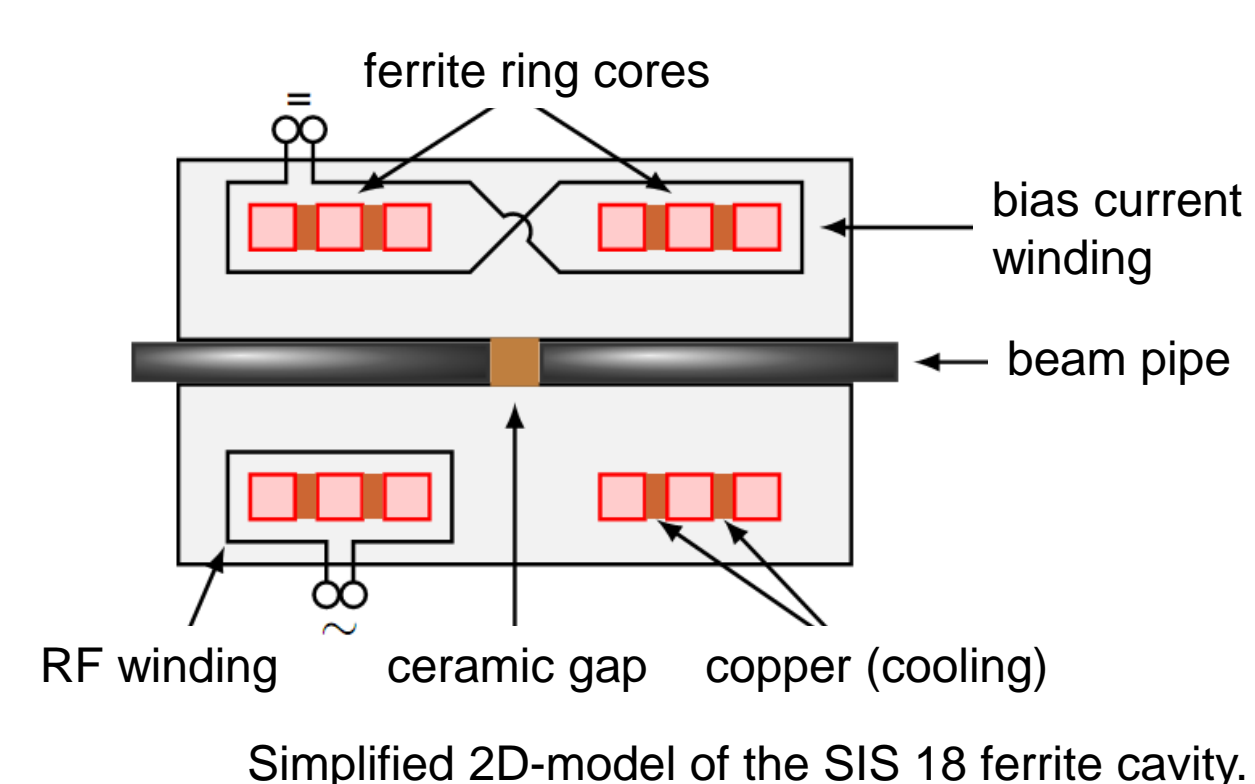
Cavity Parameters

Length	3 m
Max. gap voltage	16 kV
Resonance frequency	~ 0.8 – 5.4 MHz
Max. bias current	~ 500 A

During the acceleration phase the resonance frequency has to be adjusted to reflect the increasing speed of the heavy ions.



Simplified 3D-model of the SIS 18 ferrite cavity.

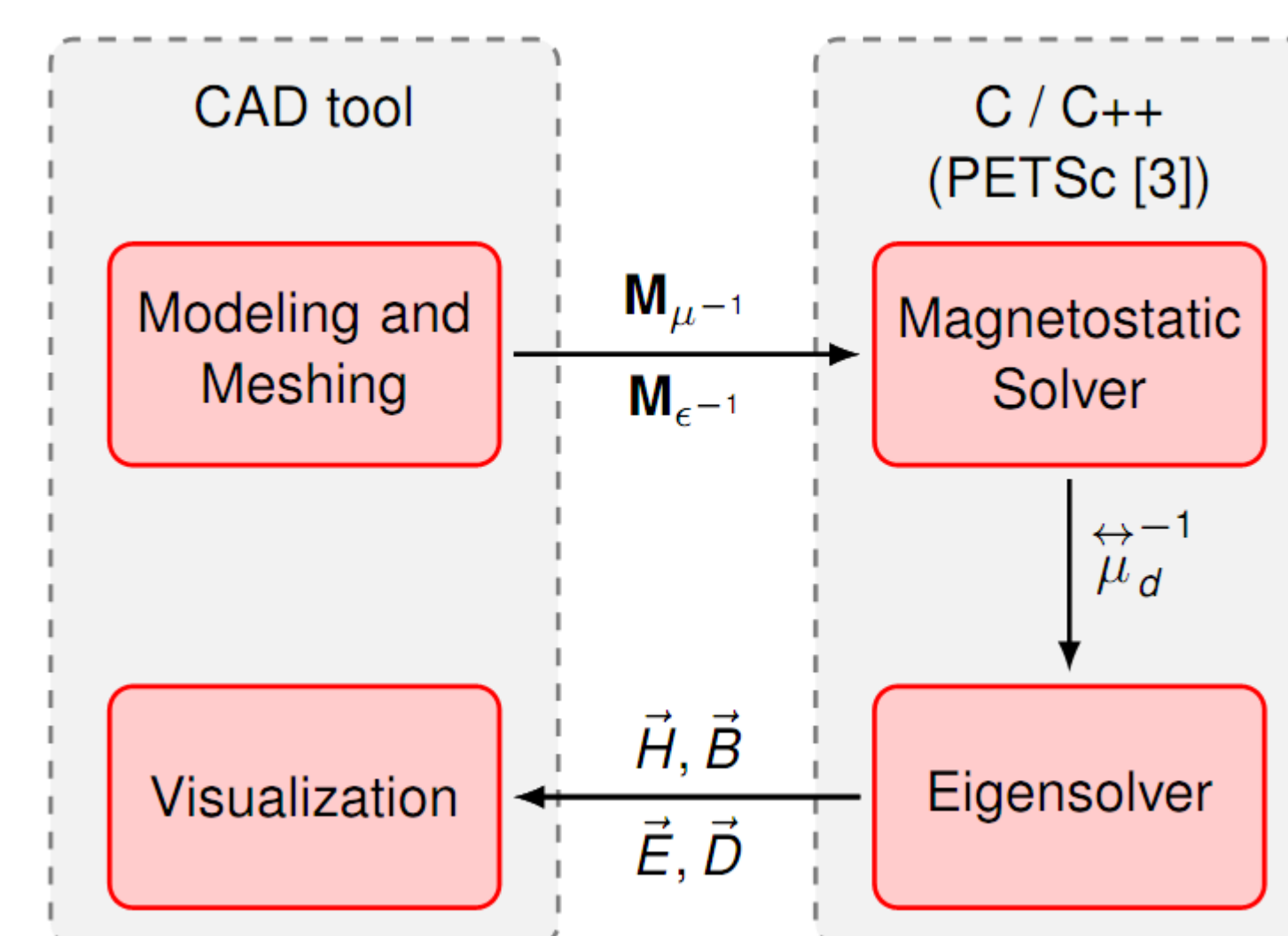


Simplified 2D-model of the SIS 18 ferrite cavity.

Computational Model

Implementation

The current implementation is based on the Finite Integration Technique [2] using a hexahedral staircase mesh.



Magnetostatic field problem

Helmholtz decomposition of H -field
 $\vec{H} = \vec{H}_i + \vec{H}_h$ with
 $\nabla \times \vec{H}_i = \vec{J}$ and $\vec{H}_h = -\nabla\varphi$
(bias) current density

Jacobi-Davidson algorithm

The nonlinear eigenvalue problem is iteratively solved as a sequence of linearized eigenproblems.

General requirements

The solver should support nonlinear and lossy material.
The implementation aims at efficient distributed computing (scalability).

[2] T. Weiland, "A Discretization Method for the Solution of Maxwell's Equations for Six-Component Fields", Electr. and Comm. AEUE, vol. 31, no. 3, pp. 116-120, 1977.
[3] S. Balay et al., "PETSc Users Manual", ANL-95/11 - Revision 3.2, Argonne National Laboratory, 2011.

Resonance Frequency Tuning

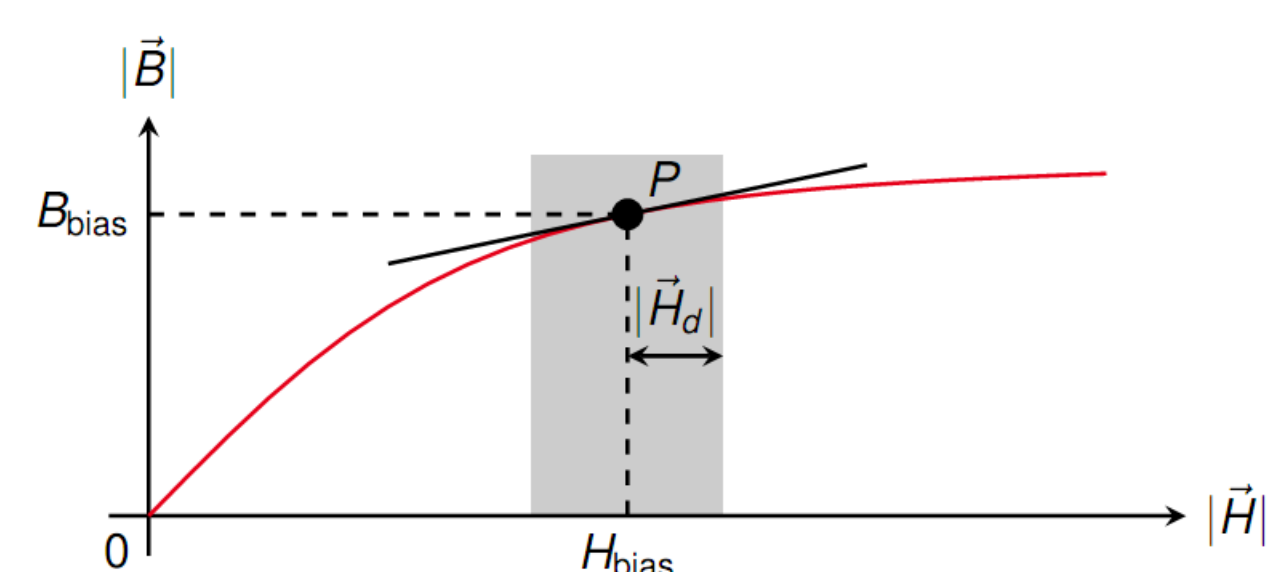
The magnetic induction inside the accelerating cavity can be decomposed into

$$\vec{B}(t) = \mu_0 \mu_{\text{bias}} \vec{H}_{\text{bias}} + \mu_0 \hat{\mu}_d \text{Re}(\vec{H}_d \cdot e^{-i\omega t}).$$

The eigenvectors are calculated under the assumptions that $|\vec{H}_d| \ll |\vec{H}_{\text{bias}}|$ and that effects of hysteresis are negligible. This allows a linearization of the constitutive equation at the working point.

Modification of bias current

- ⇒ Modification of differential permeability
- ⇒ Adjustment of eigenfrequency



Fundamental Relations

Eigenvalue formulation

$$\epsilon^{-1} \nabla \times (\mu_0^{-1} \hat{\mu}_d^{-1} \nabla \times \vec{E}(\vec{r}, t)) = \omega^2 \vec{E}(\vec{r}, t), \quad \vec{r} \in \Omega,$$

$$\vec{n} \times \vec{E}(\vec{r}, t) = 0, \quad \vec{r} \in \partial\Omega.$$

Properties of the differential permeability tensor $\hat{\mu}_d$

- Fully occupied (3x3) – tensor, which for a bias magnetic field aligned with the z -axis reduces to the well-known Polder tensor [1]

$$\hat{\mu}_d = \begin{pmatrix} \mu_1 & i\mu_2 & 0 \\ -i\mu_2 & \mu_1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad \text{with} \quad \mu_{1,2} = \mu_{1,2}(\vec{H}_{\text{bias}}, \omega).$$

- Non-Hermitian if magnetic losses are taken into account, i.e. $\text{Im}(\mu_{1,2}) \neq 0$.

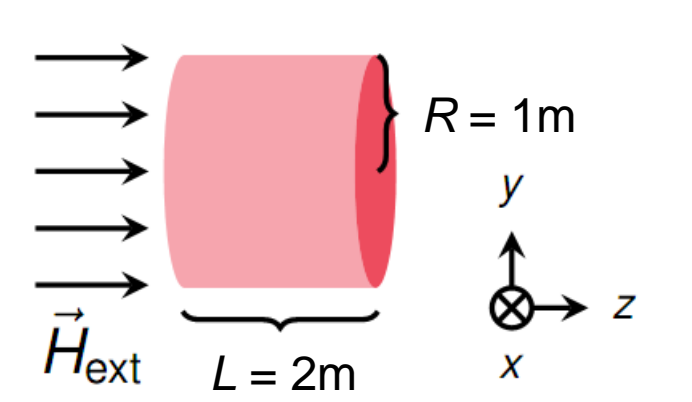
[1] D. Polder, Phil. Mag., 40, p. 99, 1949.

Numerical Examples

Biased cylinder

For verification of the nonlinear eigensolver the following model is considered:

Lossless, ferrite-filled cylindrical cavity resonator, longitudinally biased by a homogeneous magnetic field



Parameters	
$ \vec{H}_{\text{ext}} $	2750 A/m
μ_r	7
ϵ_r	1

A characteristic equation determining the resonance frequencies can be formulated analytically [4].

[4] G. C. Chinn, L.W. Epp and G.M. Wilkins, IEEE Transactions on Microwave Theory Techniques, 43, May 1995.

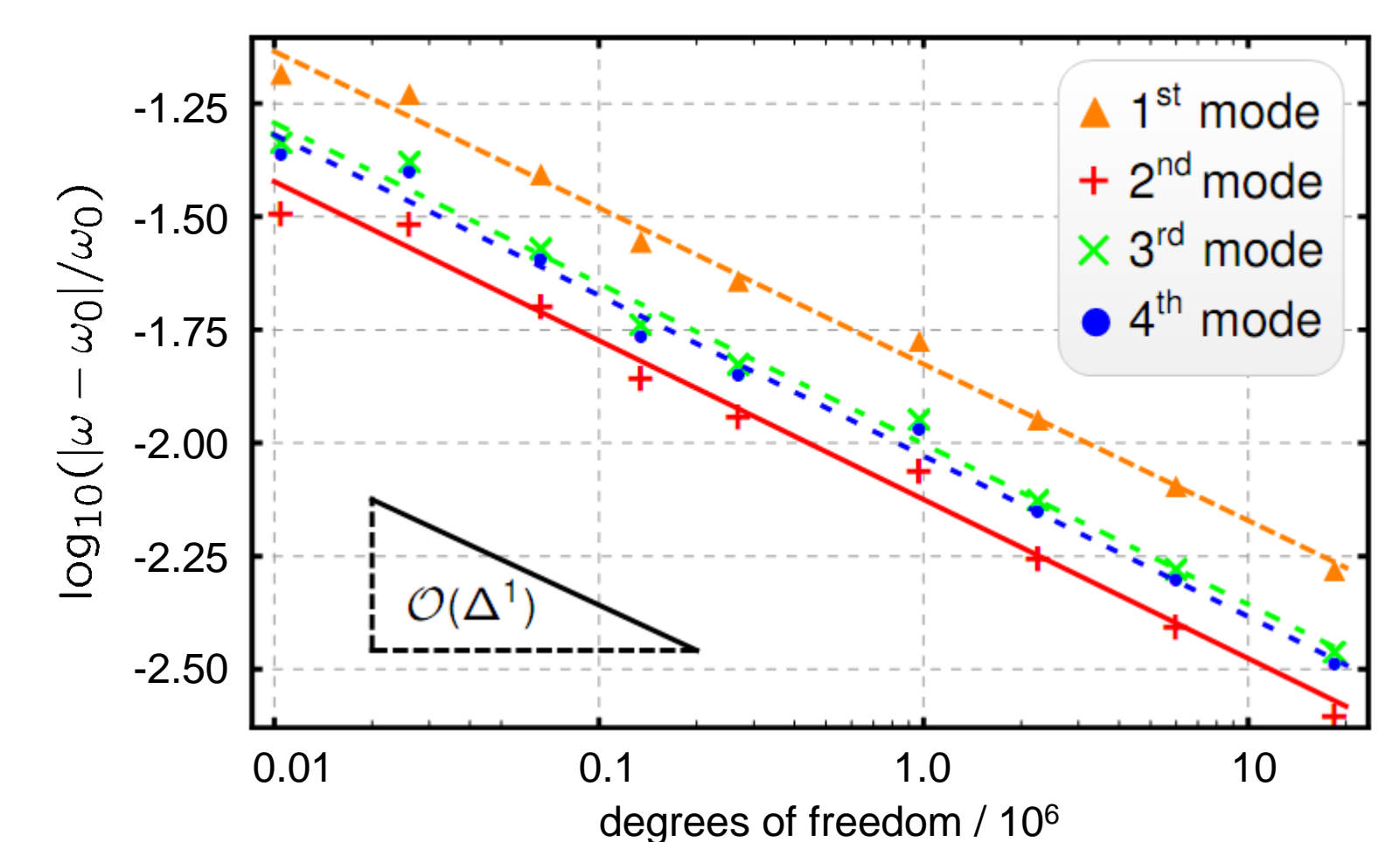


Figure: Relative deviation of the numerically obtained value ω to the analytical result ω_0 as a function of the degrees of freedom.

Biased cavity with ferrite ring cores

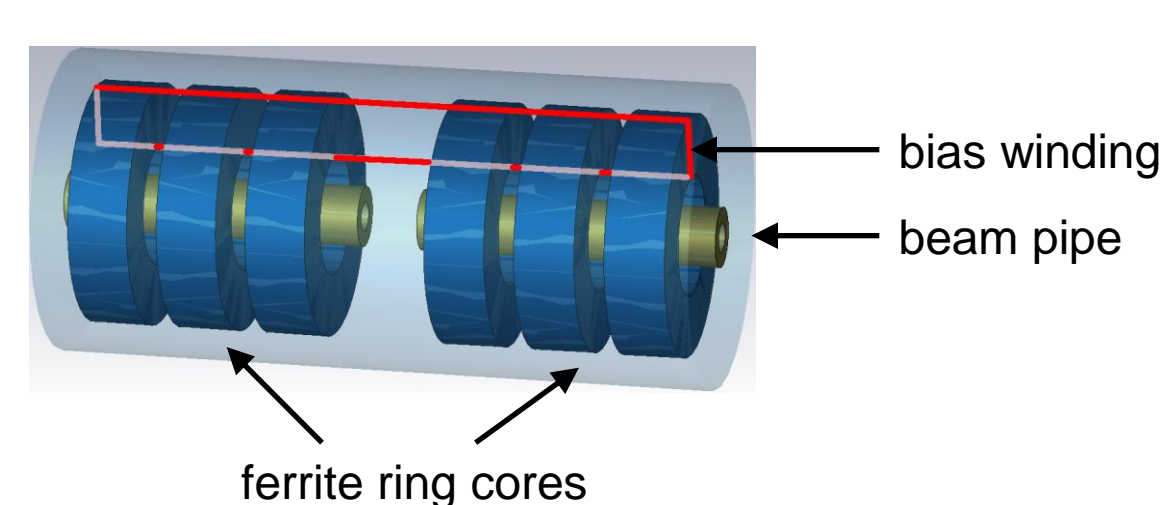
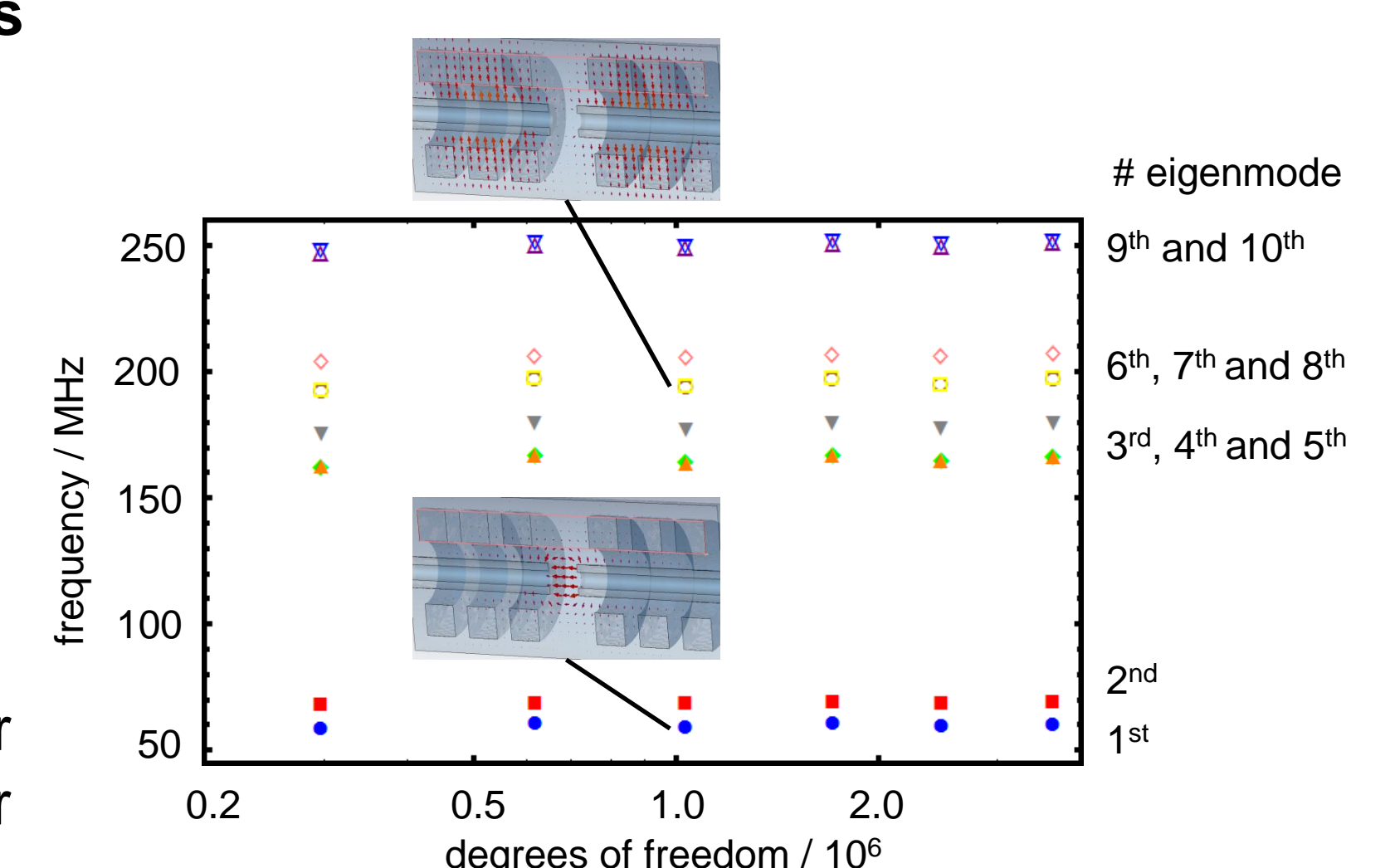


Figure: Results of fully nonlinear computation for lossless resonator



* Work supported by GSI

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