Power Converter Course, Warrington

12.05.2005



## **High Power Active Devices**





Eric Carroll, ABB Switzerland



## INTRODUCTION



#### **Electronic Switches**

#### Thyristor

Can be turned **on** by gate signal but can only be turned **off** by reversal of the anode current

#### Gate Turn-Off Thyristor (GTO)

Can be turned **on** and **off** by the gate signal but requires large capacitor (snubber) across device to limit dv/dt

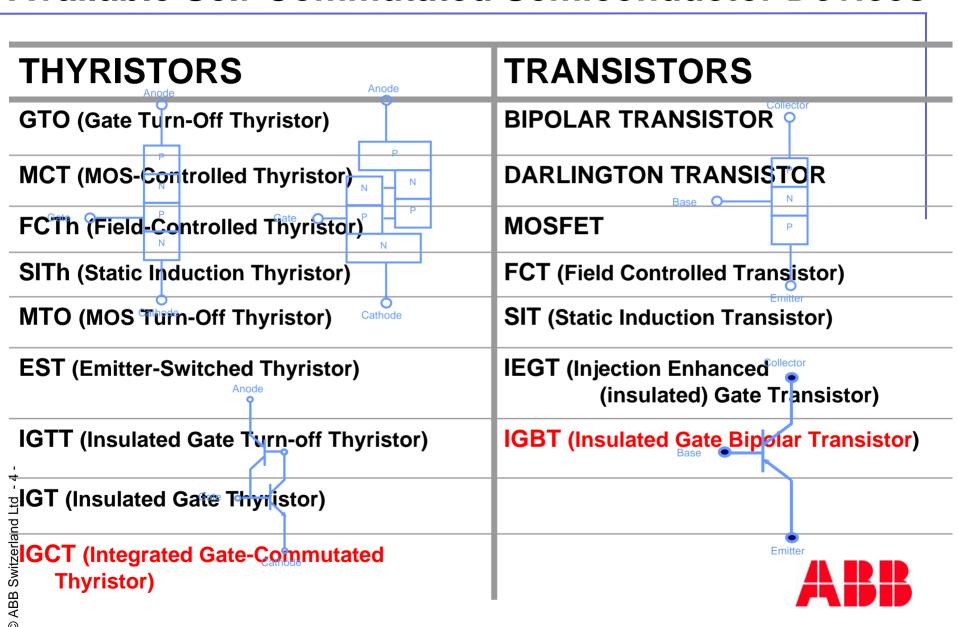
#### ■ Transistor (transitional resistor)

Can be turned **on** and **off** by the gate (or base) signal but has high conduction losses (its an amplifier, not a switch)

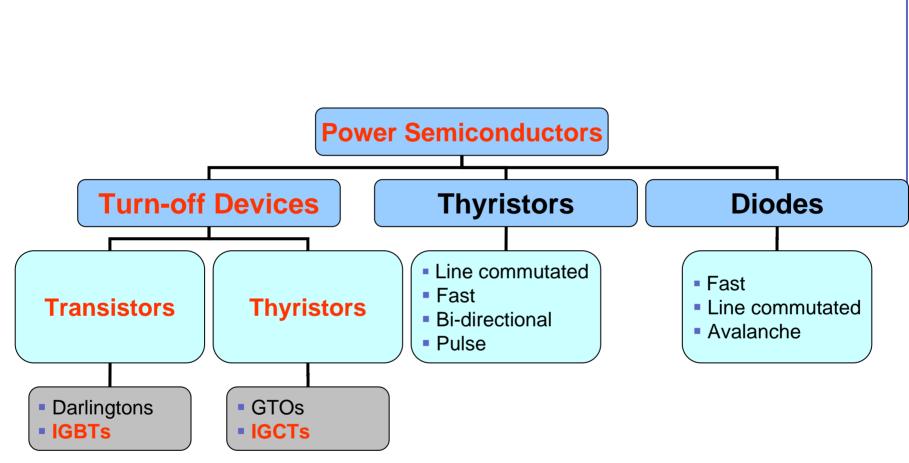
#### Integrated Gate Commutated Thyristor (IGCT)

Can be turned *on* and *off* by the gate signal, has low conduction loss and requires no dv/dt snubber

#### **Available Self-Commutated Semiconductor Devices**



#### **High Power Turn-off Devices**

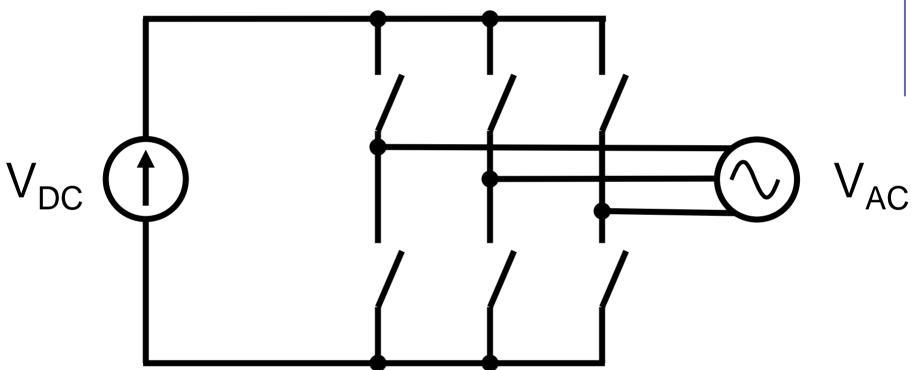




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#### Power Semiconductors ...

are switches....

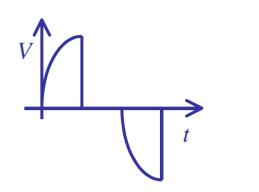


....for converting electrical energy

#### **Turn-on Switches (Thyristors)**

#### **Thyristors (PCTs)**

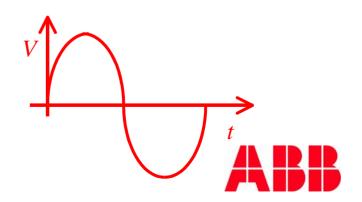
thyristors produce voltage distortion in phase control mode



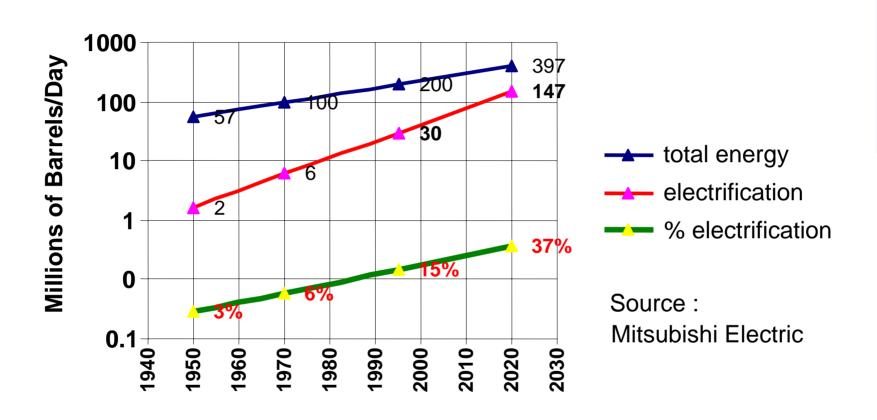
will ultimately be replaced by ToDs, except...

in AC configuration for:

- transfer switches
- tap changers
- line interrupters



#### World Energy Consumption ...



... drives the need for high power electronics



#### **Energy trend**

#### By 2020:

- Energy consumption will double
- Electricity generation will double
- Electrification of end-consumption will quintuple

Today, only 15% of electricity flows via electronics

Medium Voltage conversion has only been economically possible in the last 10 years

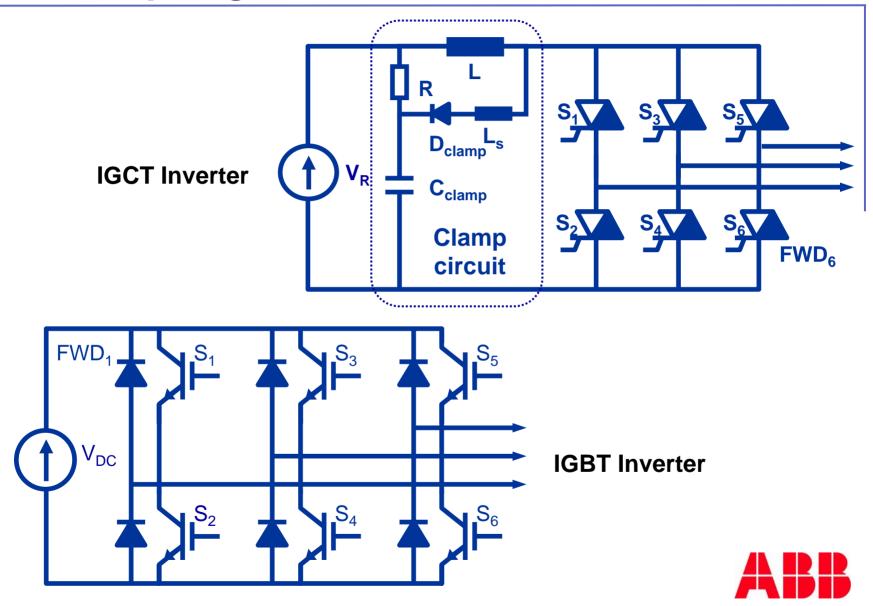
Power conversion at MV levels set to grow faster than LV (20% p.a.)



## SELF- COMMUTATED INVERTERS



#### **Basic Topologies**



#### Turn-on waveforms for IGCTs and IGBTs

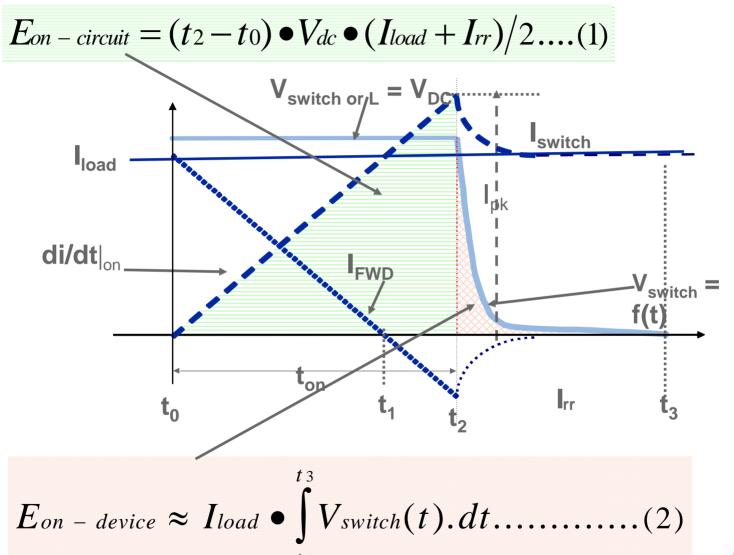




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## **DEVICES**



## **IGBTs**



#### **IGBTs** – key features

- Transistors with insulated gate
- Allow dv/dt and di/dt control via gate signal (losses)
- High on-state voltage (transistor)
- High turn-on losses (no snubber)
- Low gate power requirements (voltage control)
- No passives required (independant dv/dt and di/dt control)



#### **HiPak**<sup>TM</sup> **High Power IGBT Modules**



	Voltage	Current	Type	Part Number	$V_{ce}$	$V_{F}$	Eoff	Eon	Vdc
	_				125°C	125°C	125°C	125°C	
	2500V	1200A	Single	5SNA 1200E250100	3.1V	1.8V	1.25J	1.15J	1250V
	3300V	1200A	Single	5SNA 1200E330100	3.8V	2.35V	1.95J	1.89J	1800V
	3300V	1200A	Single	5SNA 1200G330100*	3.8V	2.35V	1.95J	1.89J	1800V
-1	6500V	600A	Single	5SNA 0600G650100*	4.7V	4.0V	3.5J	4.0J	3600V

<sup>\*</sup> High voltage version



#### StakPak<sup>TM</sup> - stackable press-packs (collector side)

StakPak-H4: 2.5 kV/1300 to 3000 A







StakPak-J6: 4.5 kV/2000 to 3000 A



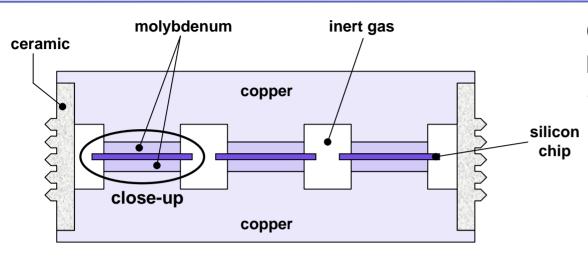


StakPak-H6: 2.5 kV/ 2000A to 3000 A



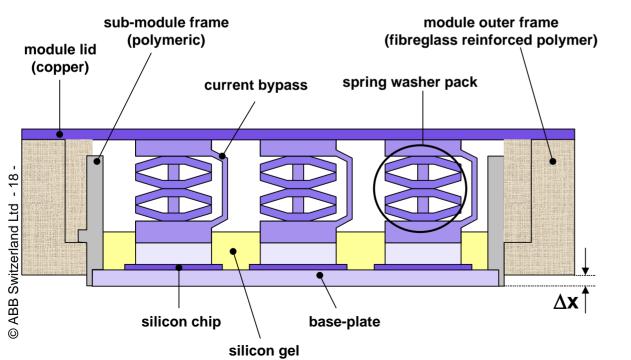
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#### **IGBT Press-packs**



Conventional IGBT presspack:

requires tight mechanical tolerances



StakPak™ IGBT presspack with individual springs:

suitable for long stacks with compounded tolerances



#### StakPak™ HVDC Valve

Long stacks would require very tight mechanical tolerances to ensure identical force on each chip in each housing:

- on assembly
- over time
- with temperature cycling
- with shock and vibration





## **IGBT Trends**

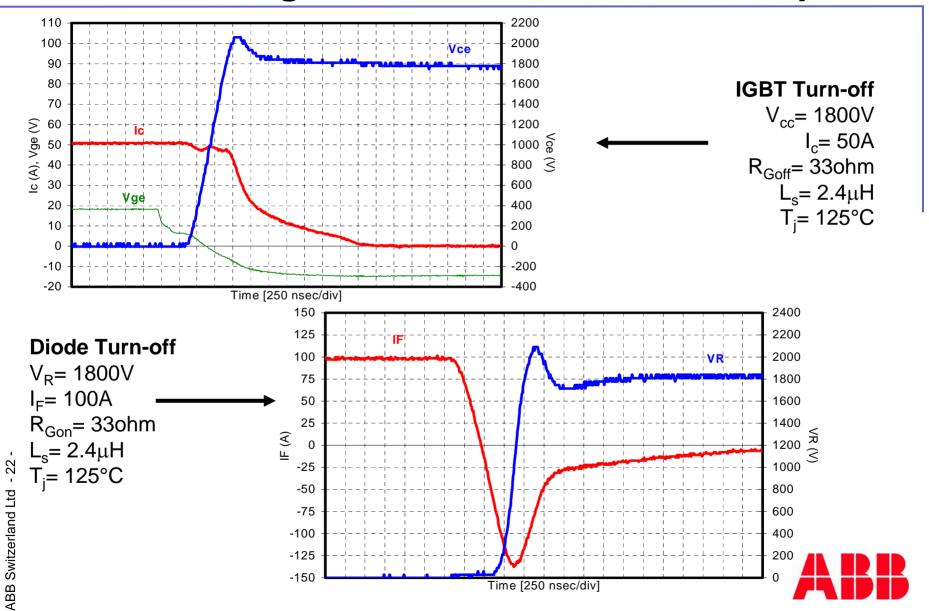


#### **IGBT Trends**

- Higher voltages
- Higher Safe Operating Area (SOA)
- Softer (controlled) switching

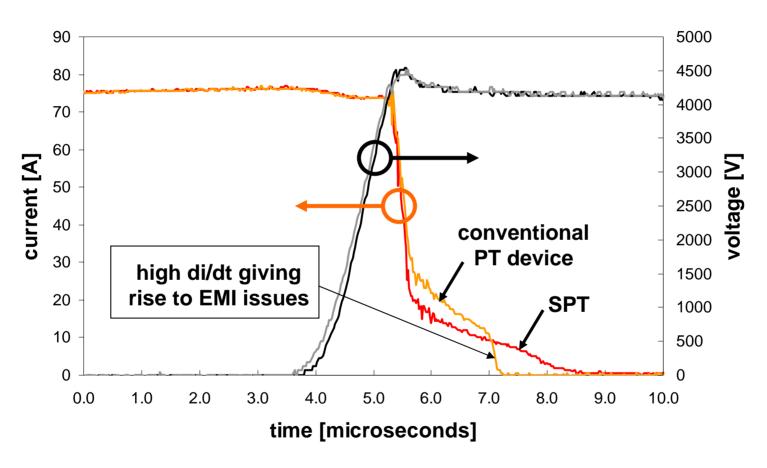


#### Soft switching: 3.3kV SPT\* IGBT/Diode chip-set



\* Soft Punch Through

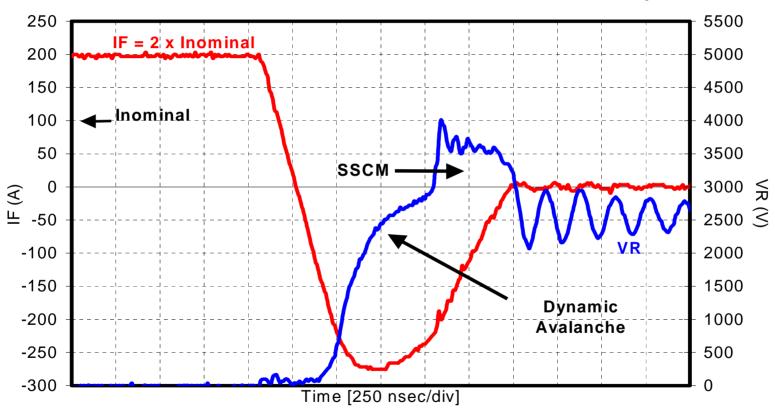
#### Soft switching: 8 kV IGBT PT vs SPT





#### 3.3kV Diode RBSOA Performance

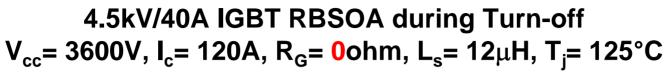
## 3.3kV/100A Diode RBSOA during Reverse Recovery $V_R$ = 2500V, $I_F$ = 200A, di/dt=1000A/ $\mu$ s, $L_s$ = 2.4 $\mu$ H, $T_j$ = 125°C

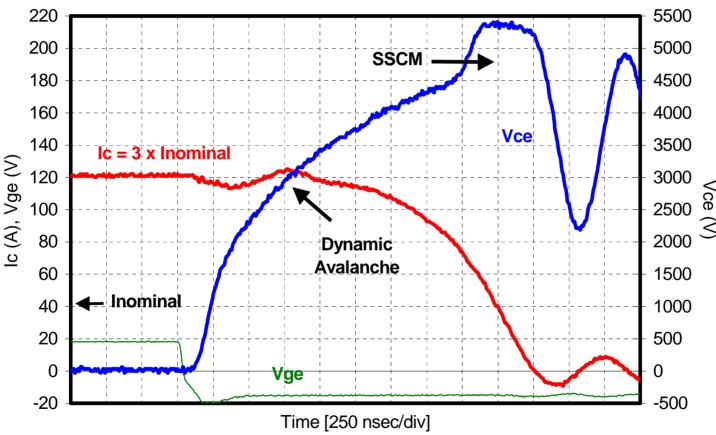


Peak Power = 0.8 MW/cm<sup>2</sup>
No clamp, no snubber



#### 4.5kV IGBT RBSOA Performance





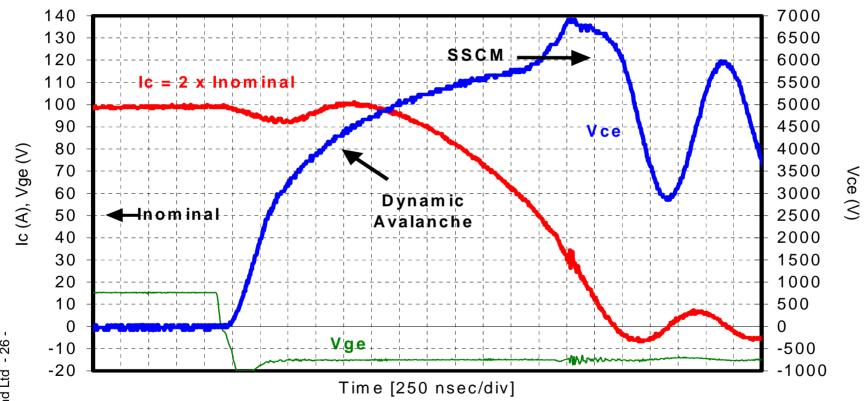
Peak Power = 0.5 MW/cm<sup>2</sup>
No Clamp, No Snubbers



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#### 6.5kV IGBT RBSOA Performance

6.5kV/2x25A IGBT RBSOA during Turn-off  $V_{cc}$ = 4500V,  $I_c$ = 100A,  $R_G$ = 0ohm,  $L_s$ = 20 $\mu$ H,  $T_j$ = 125°C



Peak Power = 0.25 MW/cm<sup>2</sup>
No Clamp, No Snubbers

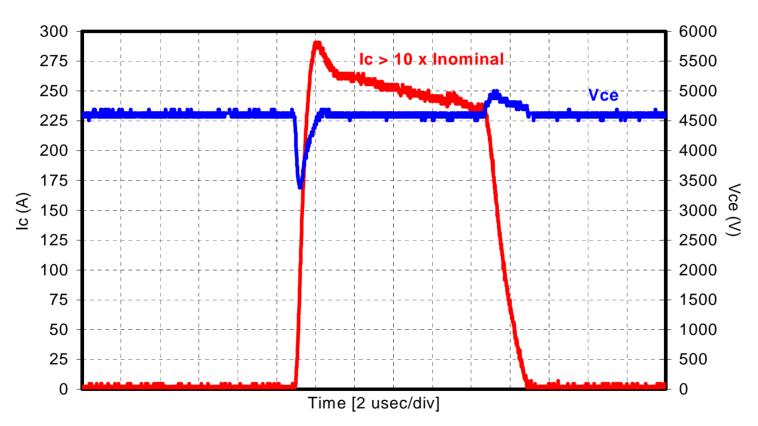


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#### **6.5kV IGBT Short Circuit Performance**

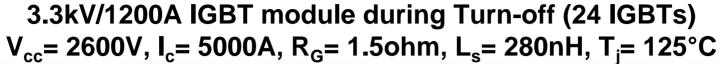
6.5kV/25A IGBT SCSOA during Short Circuit  $V_{cc}$ = 4500V,  $I_{cpeak}$ = 290A,  $V_{GE}$ = 18V,  $L_s$ = 2.4 $\mu$ H,  $T_j$ = 25°C

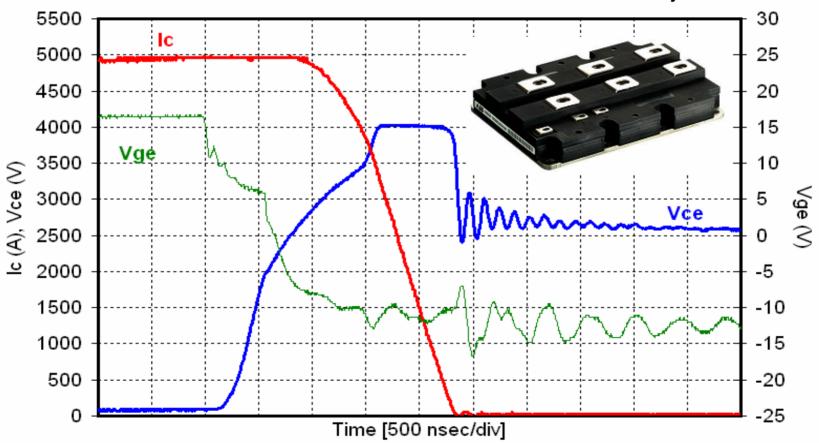


Peak Power = 1.35 MW/cm<sup>2</sup>
No Clamp, No Snubbers



#### 3.3kV IGBT Module RBSOA Performance







## **IGCTs**

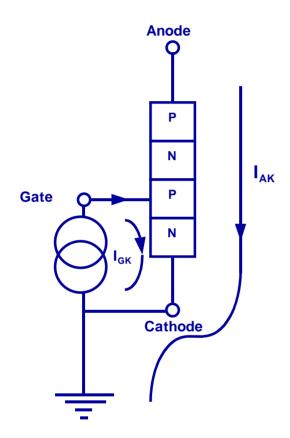


#### **IGCTs** – key features

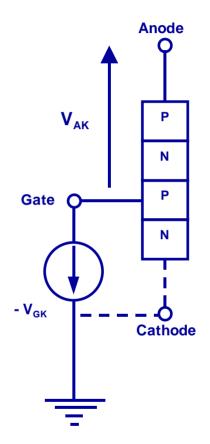
- Thyristor with integrated gate unit
- Low on-state voltage (thyristor)
- Negligible turn-on losses (turn-on snubber)
- No explosive failures
   (fault current limitation by circuit)



#### **Principle of IGCT Operation**



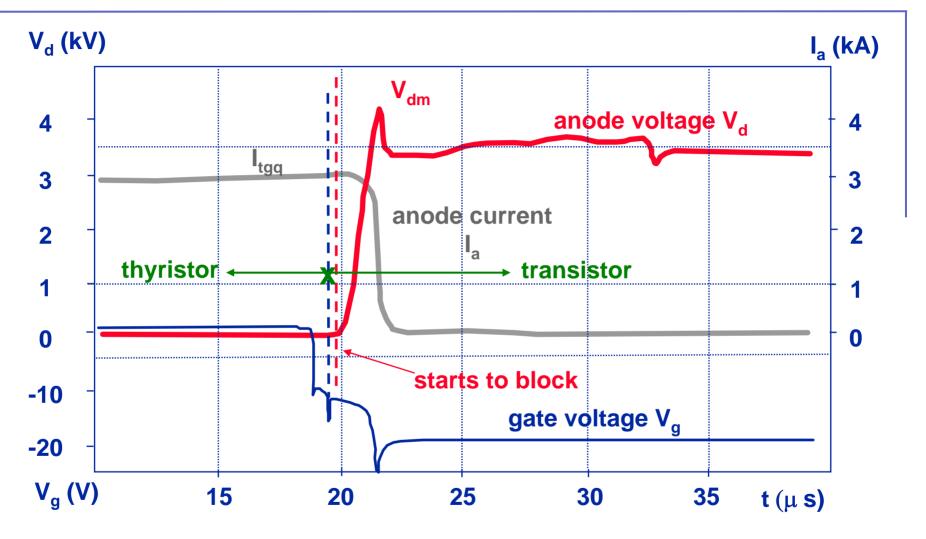




**Blocking Transistor** 



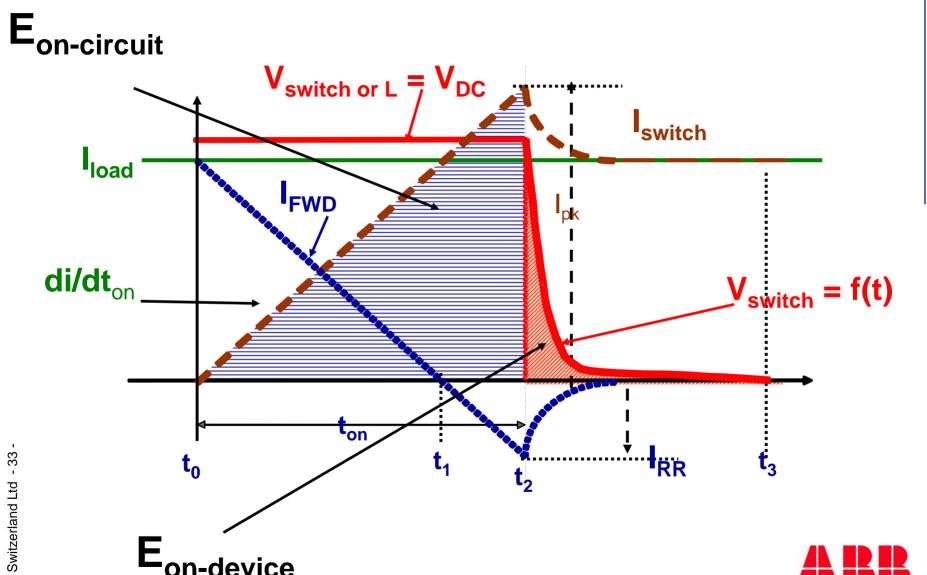
#### **IGCT turn-off**





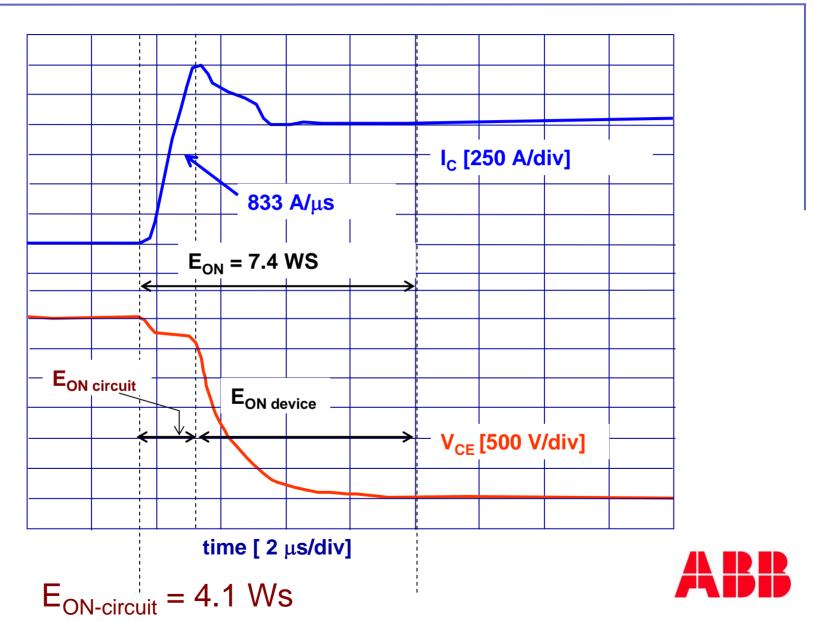
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#### General turn-on waveforms for IGCTs and IGBTs



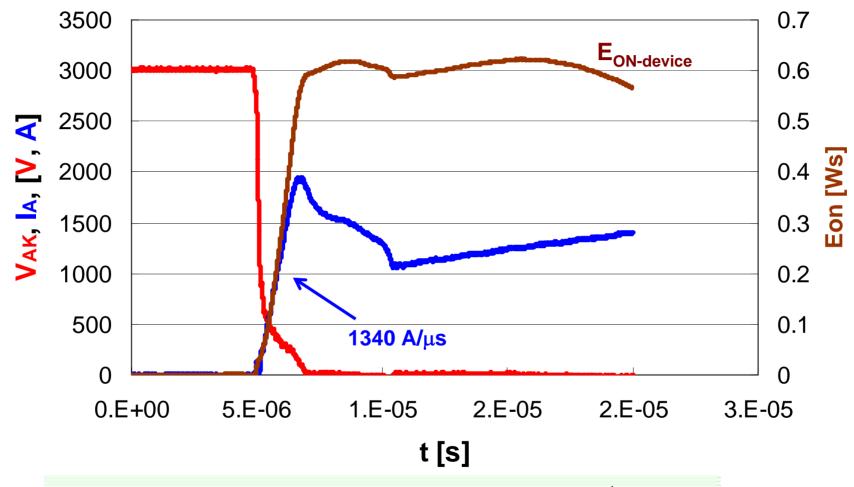
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#### 1500 A IGBT turning on 1000 A from 3000 V



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#### 4000 A IGCT turning on 1000 A from 3000 V

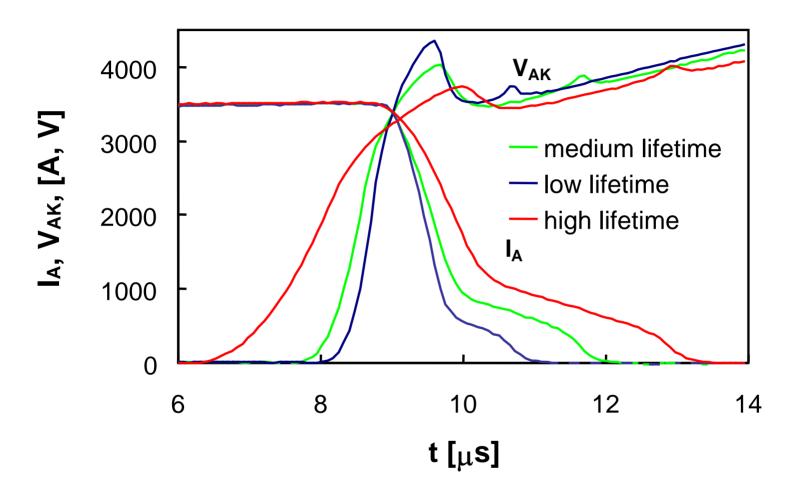


$$E_{on-circuit} = (t_2 - t_0) \bullet V_{dc} \bullet (I_{load} + I_{rr})/2....(1)$$



=1.5  $\mu s \cdot 3000 V \cdot 1900 A / 2 = 4.3 Ws$ 

#### Adjustment of dv/dt by lifetime control

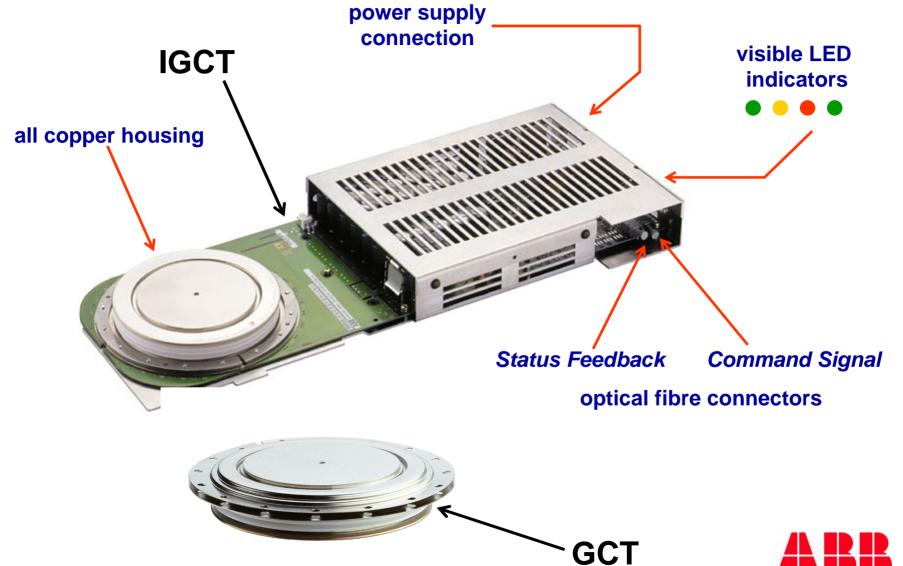




# Low inductance housing



#### 4 kA/4.5 kV IGCTs



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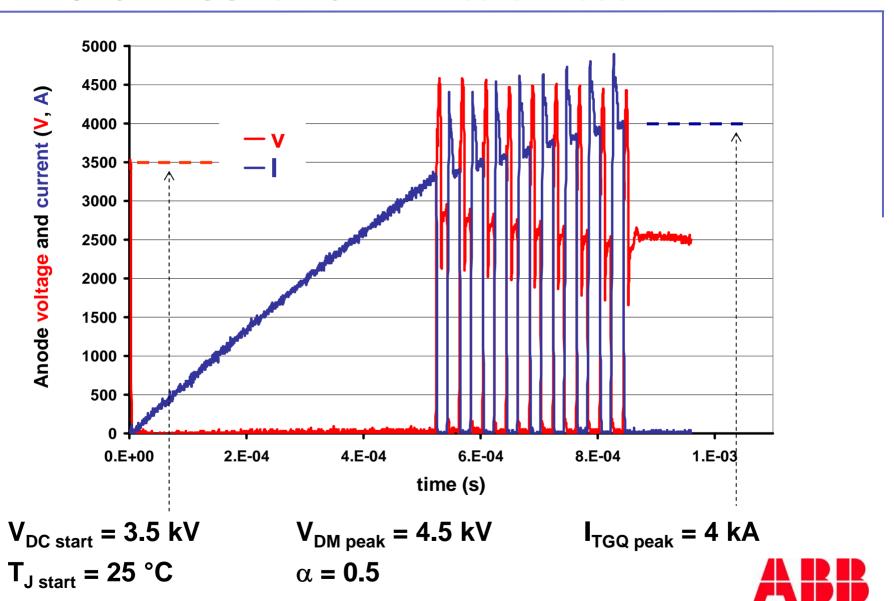
### **30 MW IGCT Power Management**



15 + 15 MW 3-Level Back-to-Back Converter for three-phase to single-phase conversion *Converter efficiency* = 99.2%



#### 4 kA/4.5 kV IGCT at 25 kHz in burst mode



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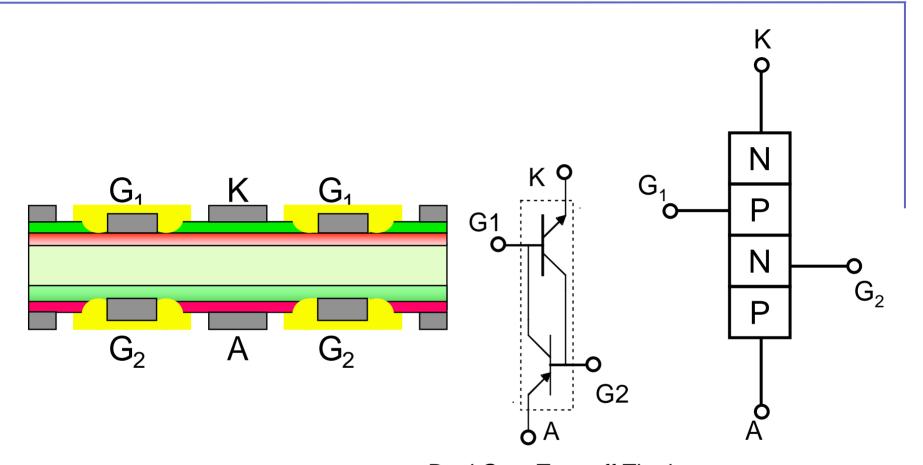
# **IGCT Outlook**



# **IGDT**



#### Structure of IGDT – Integrated Gate Dual Transistor

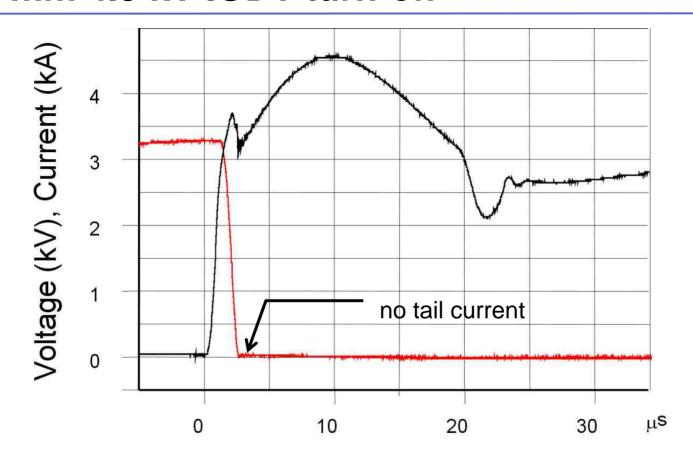


**Dual Gate Turn-off Thyristor** 



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#### 91 mm 4.5 kV IGDT turn-off



#### Dual-gate IGCT @ 85°C - gates triggered simultaneously

$$V_{DC} = 2.8 \text{ kV}$$

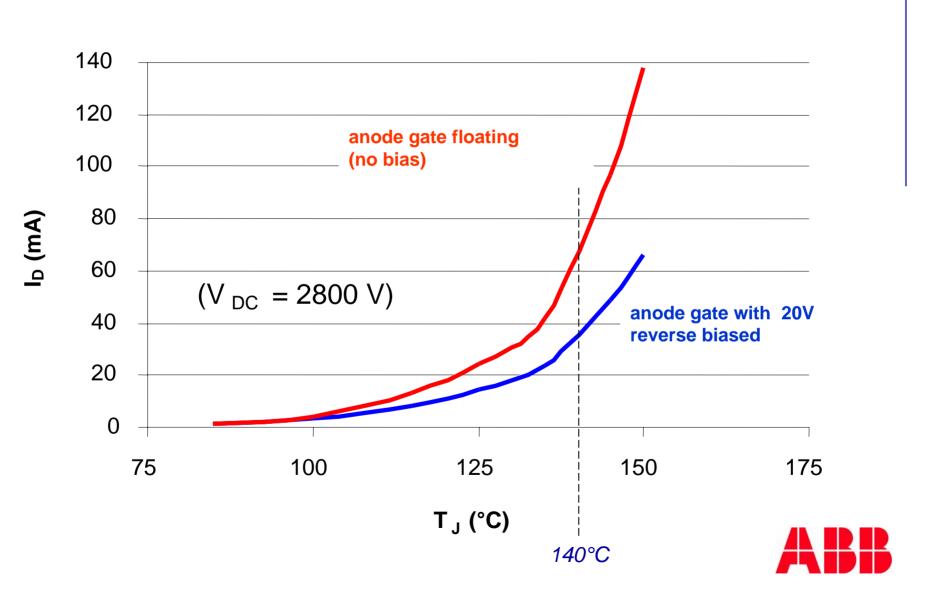
$$I_{TGQ} = 3.3 \text{ kA}$$

$$V_{DRM} = 4.5 \text{ kV}$$

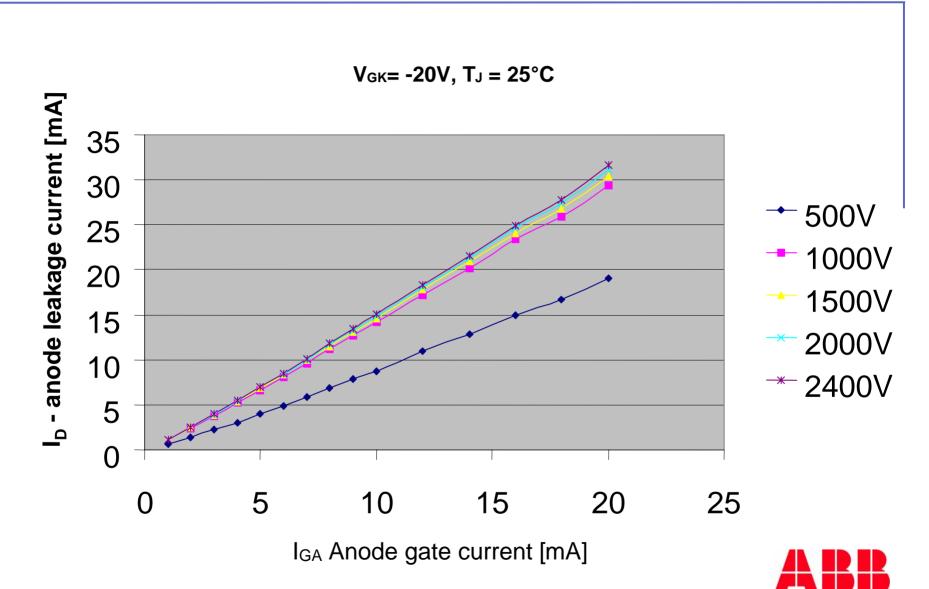
$$V_{TM} = 2.1 \text{ V } @ 4 \text{ kA}/125 ^{\circ}\text{C}$$

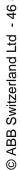


#### IGDT Series connection: leakage current reduction

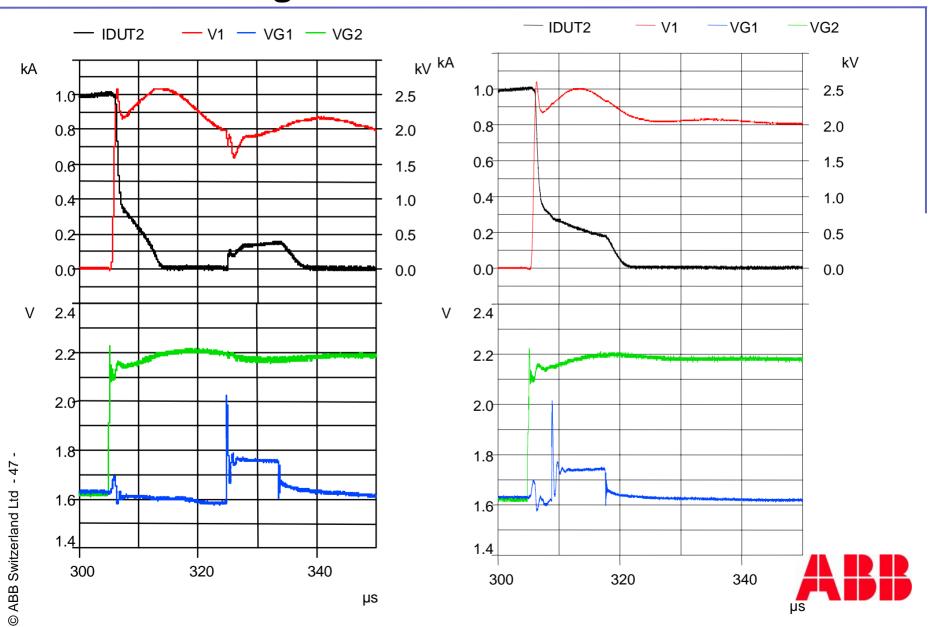


#### 91 mm 4.5 kV IGDT - Leakage current control





#### IGDT anode gate control of tail current



# **Increased SOA**



#### **IGCT SOA improvement at 4.5 kV**

#### **TODAY**

250 kW/cm<sup>2</sup>

250 kW/cm<sup>2</sup>

#### 38 mm reverse conducting



#### 91 mm asymmetric

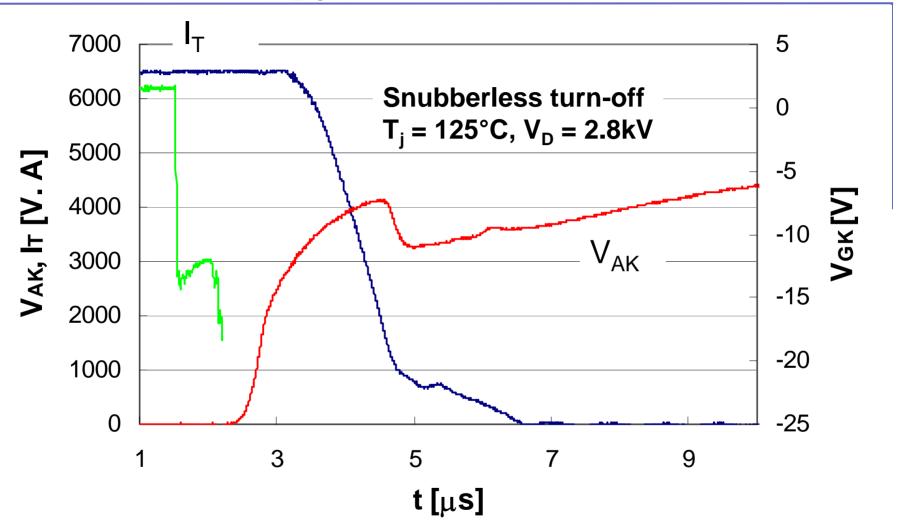
#### **TOMORROW**

1000 kW/cm<sup>2</sup>

400 kW/cm<sup>2</sup>



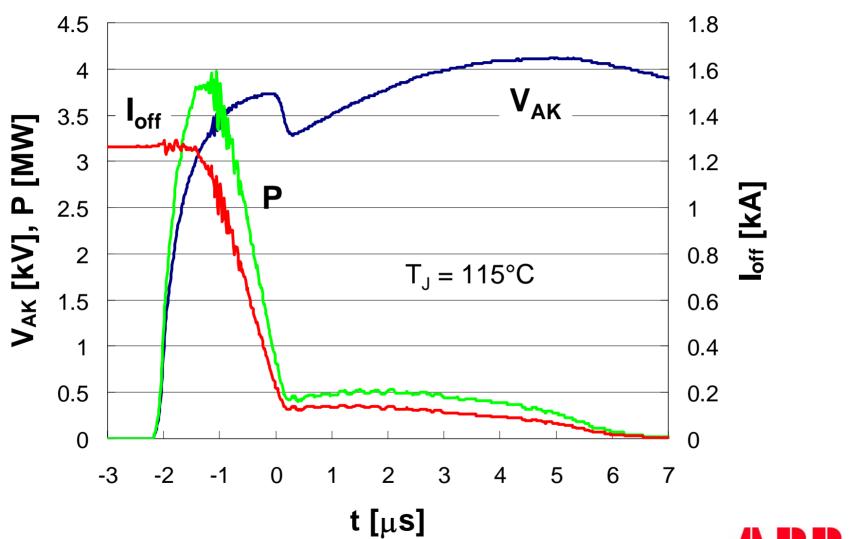
### 6.5 kA @ 2.8 kV<sub>DC</sub> on 91 mm wafer



Developmental 4" 4.5 kV IGCT with improved GU and silicon design allowing 50% SOA improvement



### 1.3 kA @ 2.8 kV<sub>DC</sub> on 38 mm RC wafer



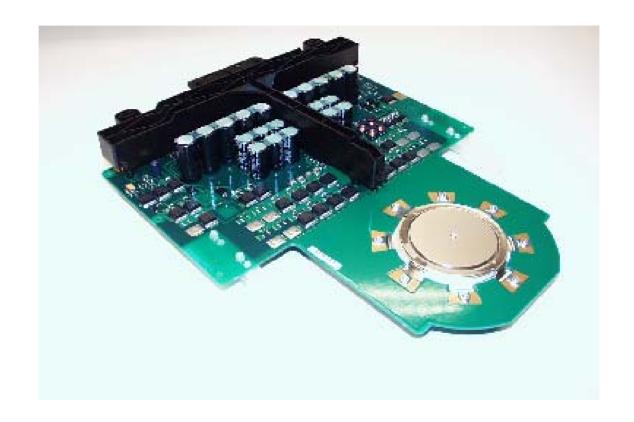


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# 10 kV IGCT

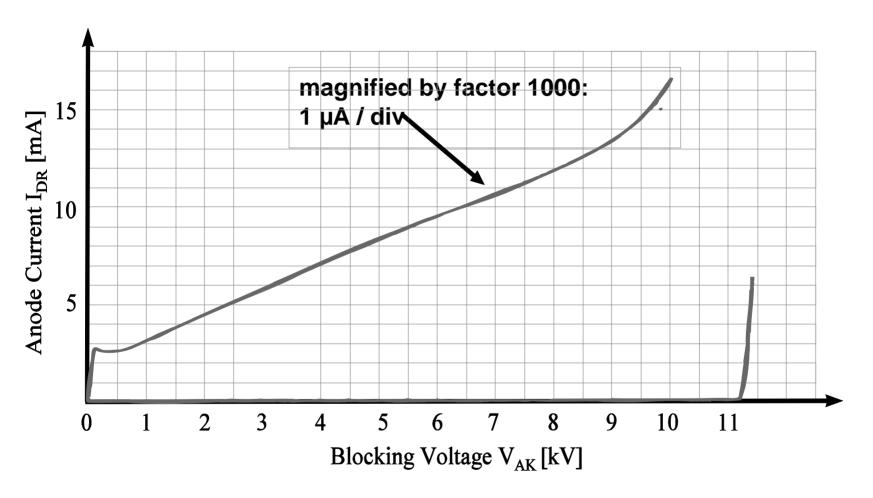


## **Engineering Sample of 68 mm 10 kV IGCT**





### Forward Blocking Characteristics at 25°C

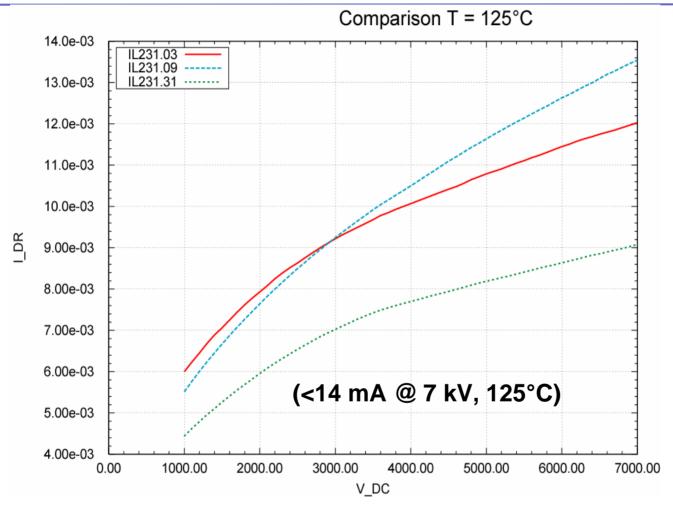


(<17 μA @ 10 kV, 25°C)



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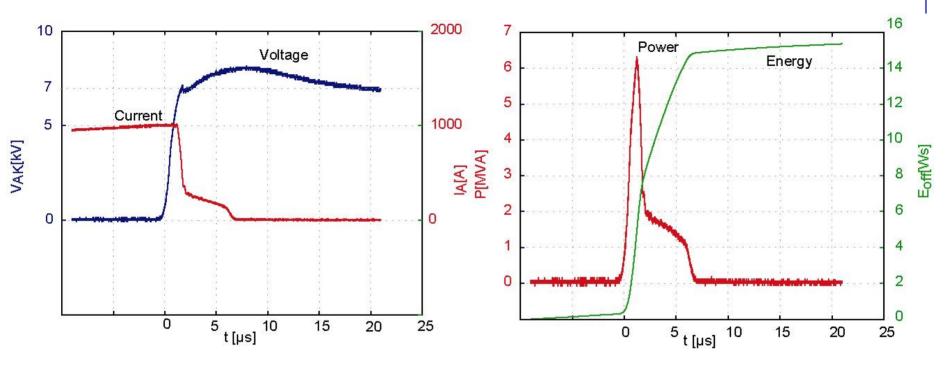
### Forward Blocking Characteristics at 125°C



(8-13 mA @ 6 kV, 125°C,  $P_L$ =50W-80W ( 5%-10% of  $P_{RP}$ )



### **Turn-off Waveforms (SOA)**



#### **Operating conditions:**

 $V_{DC} = 7kV, I_A = 1000A, T_i = 85^{\circ}C$ 

#### **Switching characteristics:**

 $E_{off} = 14.8 \text{ J}, V_{AK,max} = 8 \text{ kV}, t_{off} = 8\mu\text{s}, t_{f} = 1\mu\text{s}, t_{tail} = 5\mu\text{s}, 250 \text{ kW/cm}^{2}$ 

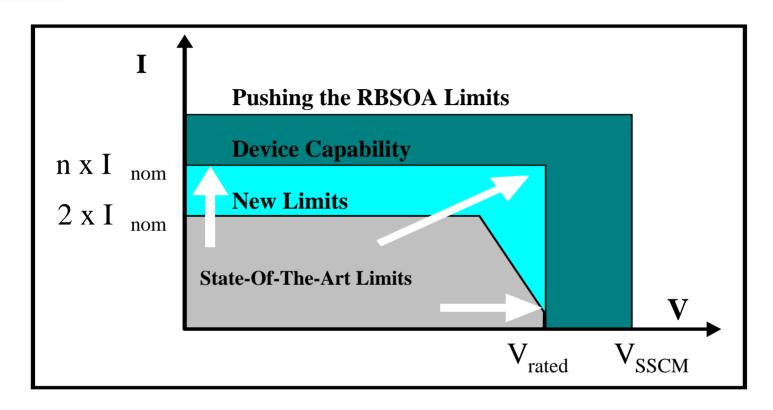


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# **Conclusions**



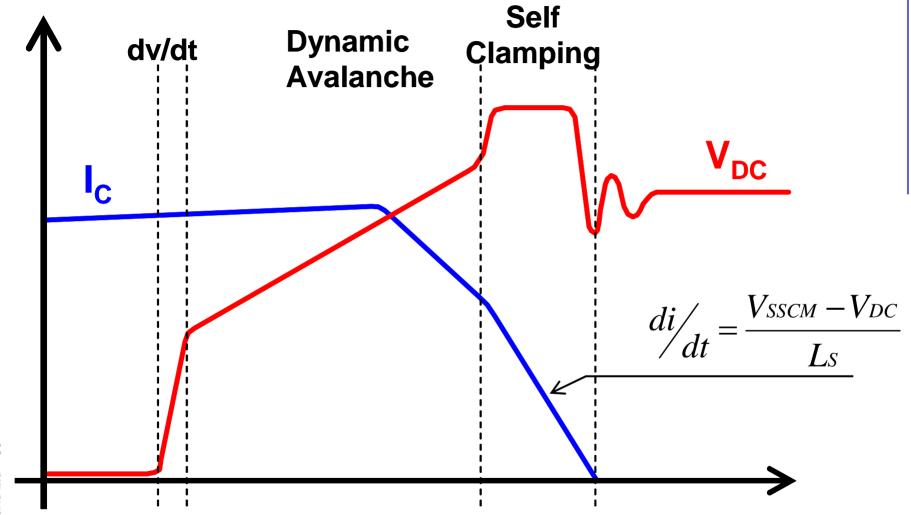
#### **SOA Limits of HV Devices are increasing**



- Under RBSOA operational conditions
  - Devices withstands dynamic avalanche mode
  - IGBTs withstands "SSCM" mode
  - Devices achieve the ultimate square SOA behaviour



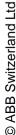
#### Switching-Self-Clamping-Mode "SSCM"



IGBT SOA turn-off waveforms including SSCM

devices start to limit voltage during turn-off

over-voltage safely reaches the static breakdown after turn-off



- For high power conversion, only two devices possible today:
  - IGBT
  - IGCT
- Safe Operating Area is increasing from 250 kW/cm<sup>2</sup> to 1 MW/cm<sup>2</sup>
- IGDT offers possibility of high voltage devices with low losses (future?)



# Challenges



#### **Challenges for HV Power ToDs**

- High voltage devices present following challenges:
  - Dynamic Avalanche ruggedness (for reliable operation)
  - Short Circuit Failure Modes (IGBT) and fault interruption (IGCT)
  - Design Trade-off between Losses and SOA
  - Critical Punch-Through voltages (for controllable voltage, low EMI)
  - High DC link voltage (leakage stability, cosmic ray withstand)
  - Large inductance and overshoot voltages in HV power systems
  - High frequency (limited by losses, T<sub>J</sub>)



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#### Challenges for this decade

- 10 kV switches with 1 kHz snubberless operation (for the 6.9 kV<sub>RMS</sub> MV line for drives and power conditioners)
- Snubberless series operation (static and dynamic for MV lines > 6.9 kV<sub>RMS</sub>)
- Power supply free operation (autogenous power supply for series connection)
- System cost-reduction (e.g. pay-back times ≈ 1 year for MV Drives)
- Reduced thermal resistance and increased T<sub>1</sub>
- Reduced losses?

#