

Field Solvers



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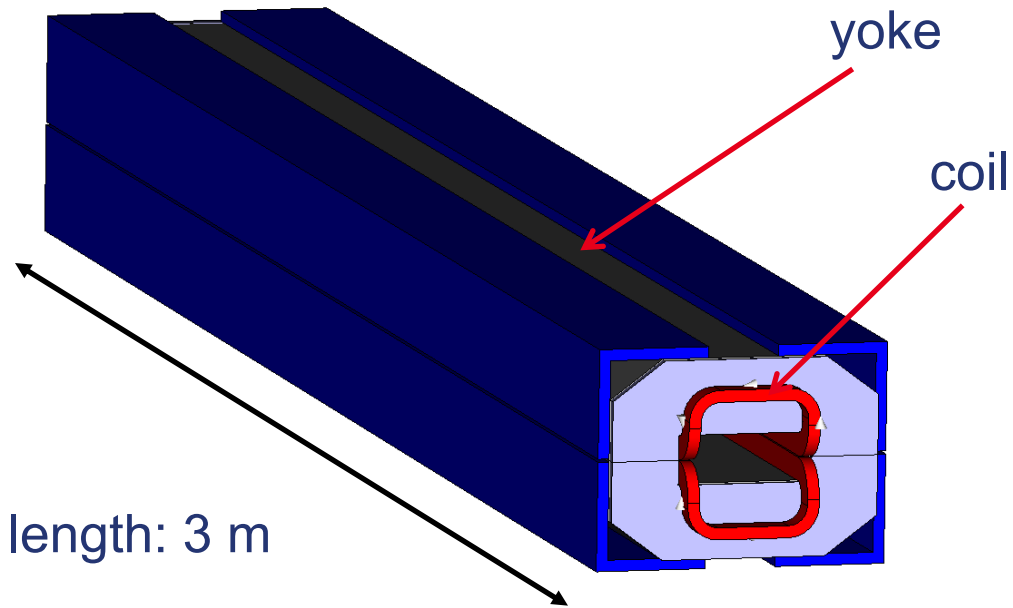
Prof. Dr.-Ing. Herbert De Gersem

CERN Accelerator School 2018

Thessaloniki, Greece, 11-23 November 2018

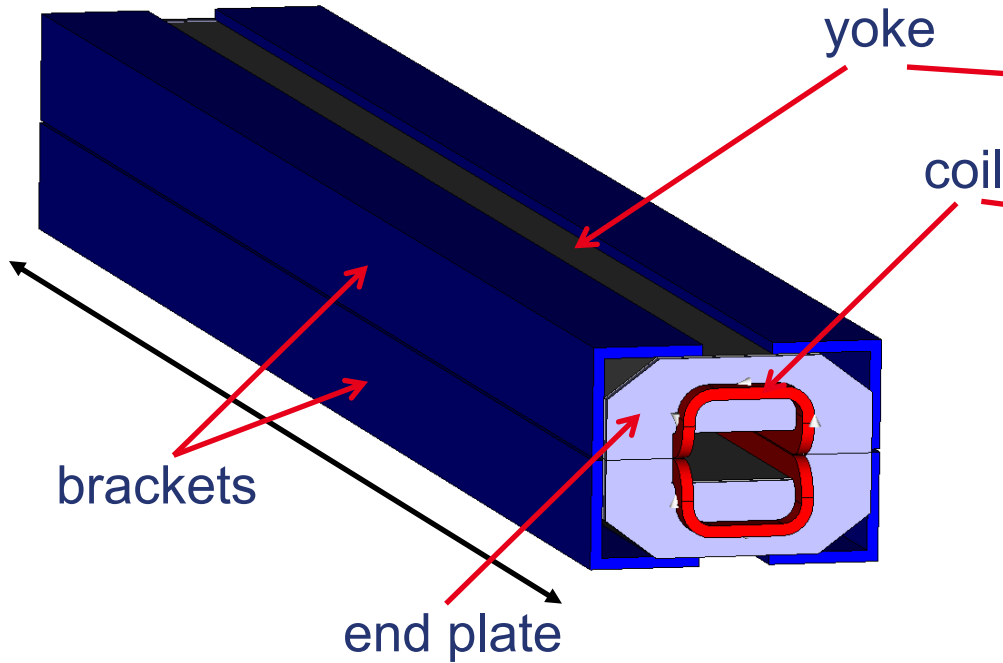
Lecture 1 : Electromagnetic Field Simulation for Accelerators: Overview

Example: accelerator magnet



comparably simple ?

Example: GSI-SIS-100 magnet



length: 3 m

SIS100 dipole (prototype)

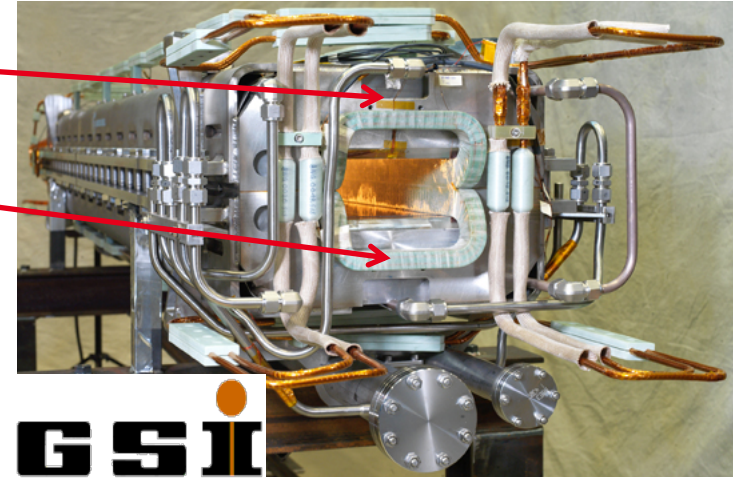
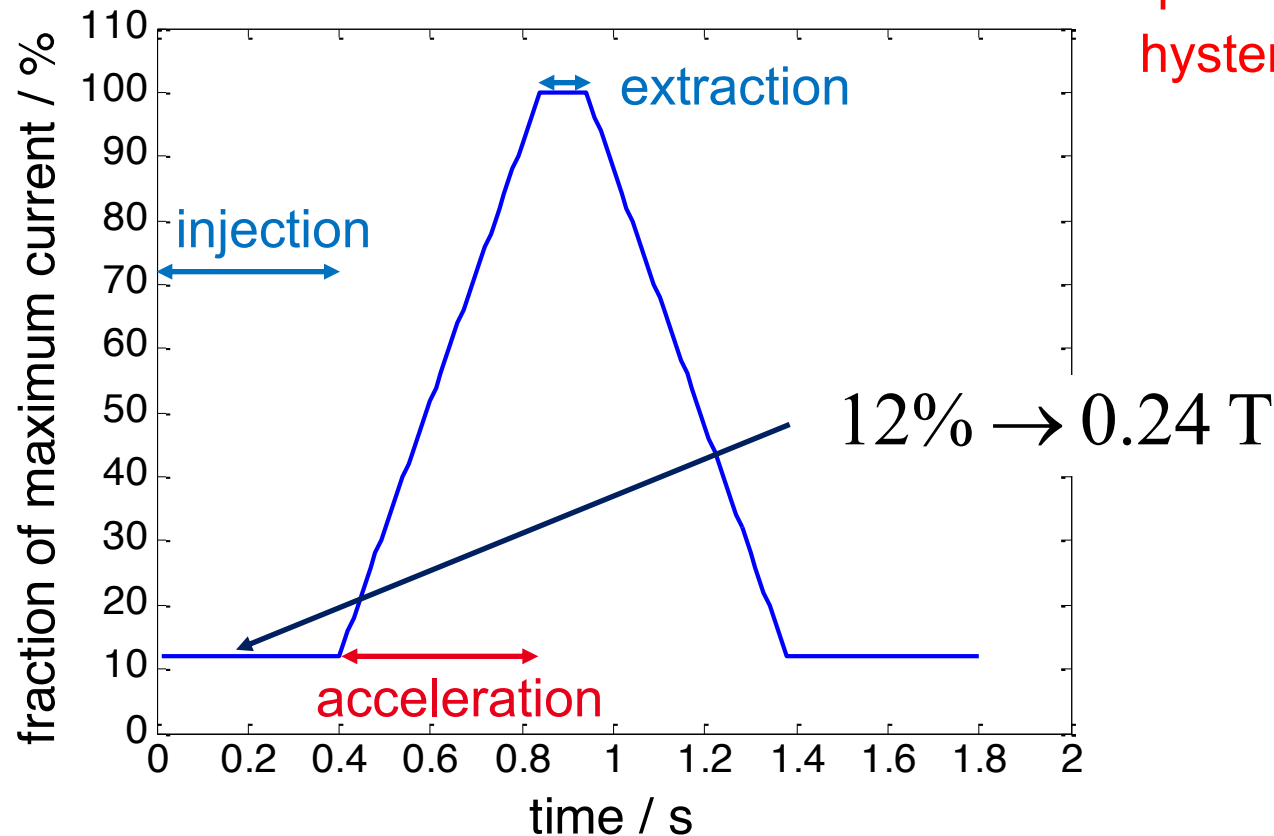


photo: J. Guse, GSI (www.gsi.de)

- many geometric details
- superconductive coils
- helium cooling
- mechanical deformation
- radioactive hazards

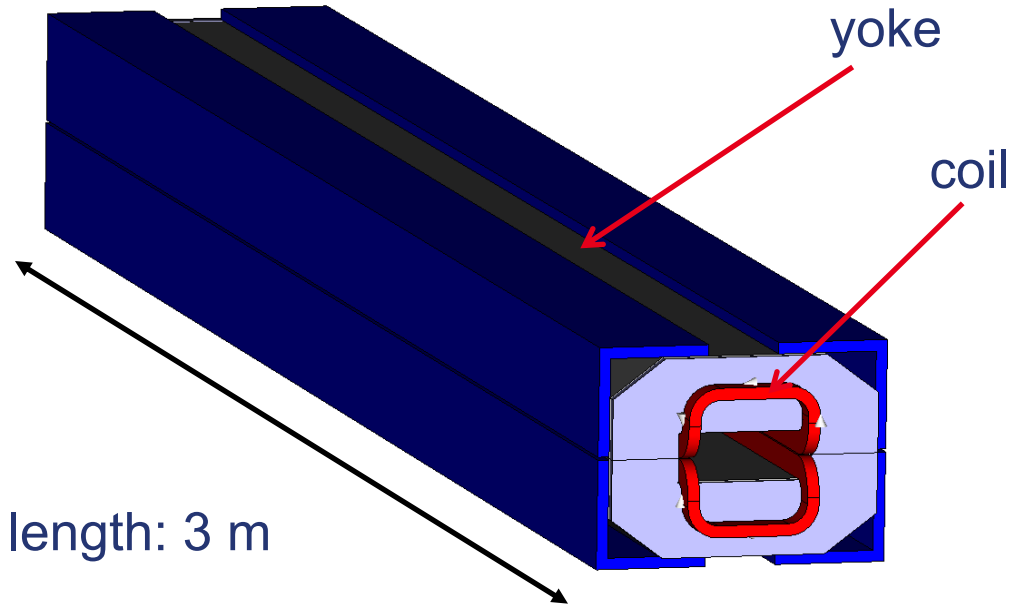
Example: GSI-SIS-100 magnet

excitation profile



eddy currents
quench of superconductors
hysteresis

Example: accelerator magnet



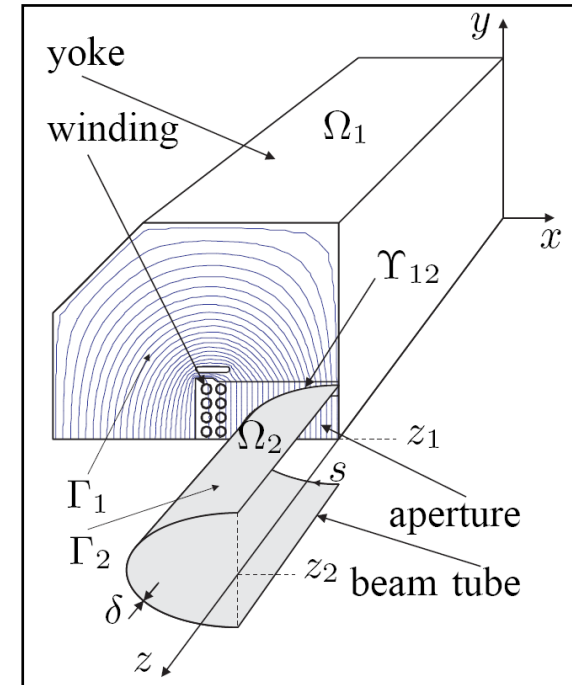
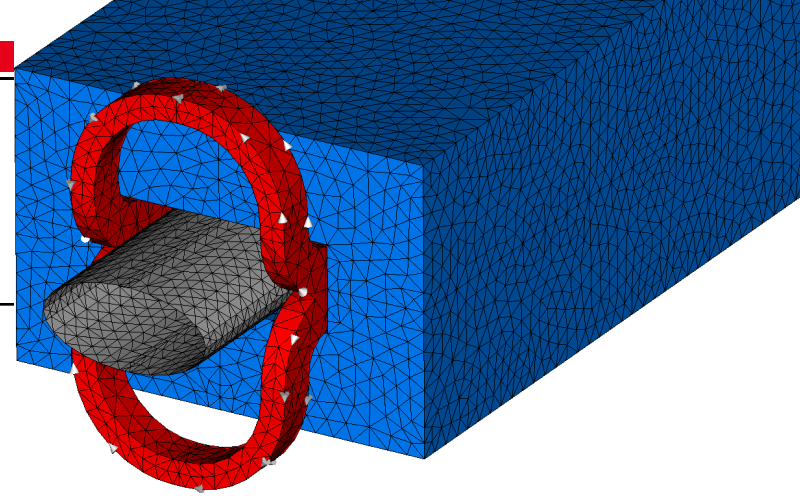
~~comparably simple ?~~



unexpected complexity !

Overview

- magnet simulation (standard 3D FE solver)
- challenges
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- magnet simulation (dedicated 3D FE solver)
- hybrid models
- stochastic models
- conclusions



Magnetoquasistatic formulation



differential equation:

$$\nabla \times (\nu \nabla \times \vec{A}) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$$

reluctivity
magnetic vector potential
conductivity
applied current density

Discretisation in space



differential equation:
$$\nabla \times (\nu \nabla \times \vec{A}) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$$

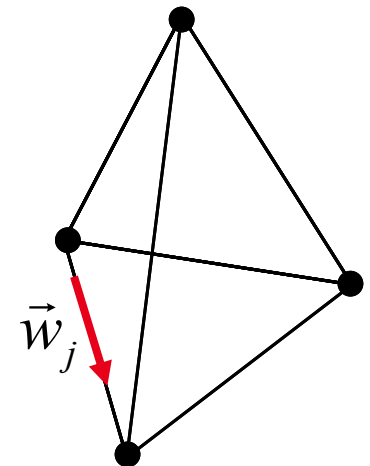
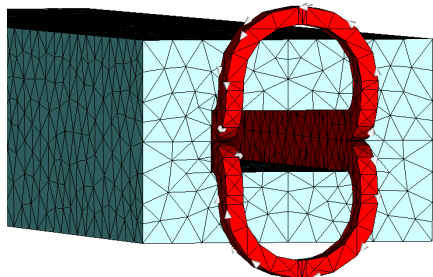
spatial discretisation



$$\vec{A} \approx \vec{A}_{\text{FE}} = \sum_j \hat{a}_j \vec{w}_j$$

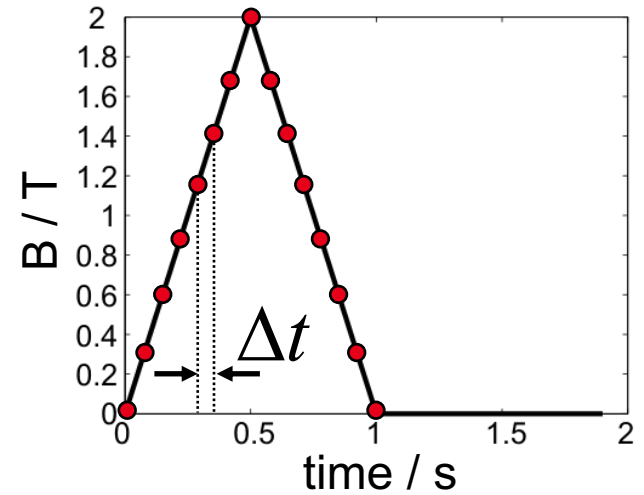
semi-discrete system:
$$\mathbf{K}_\nu \hat{\mathbf{a}} + \mathbf{M}_\sigma \frac{d\hat{\mathbf{a}}}{dt} = \hat{\mathbf{j}}_s$$

shape functions:
edge finite elements
(curl-conforming)



Discretisation in time

differential equation



spatial discretisation



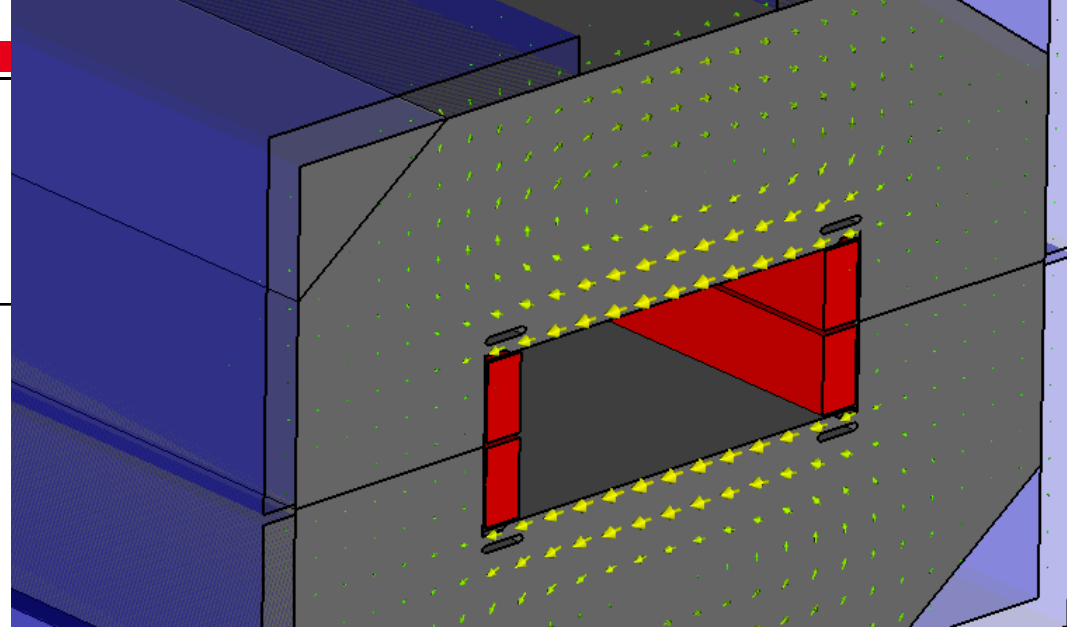
semi-discrete system: $\mathbf{K}_v \hat{\mathbf{a}} + \mathbf{M}_\sigma \frac{d\hat{\mathbf{a}}}{dt} = \hat{\mathbf{j}}_s$

temporal discretisation

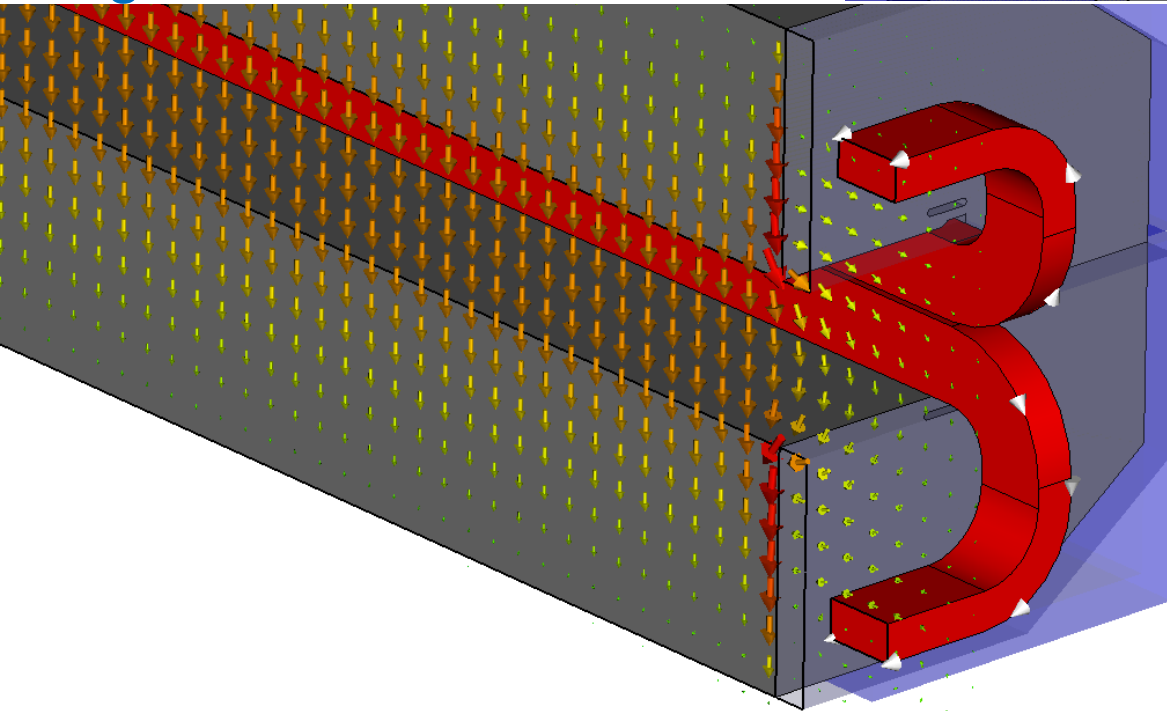


discrete system: $(\mathbf{K}_v + \alpha \mathbf{M}_\sigma) \hat{\mathbf{a}}_{k+1} = \text{RHS}$

Results



magnetic field



eddy currents
in the end plane

simulation by
CST EMStudio®

Electromagnetic field solvers



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- commercial
or academic
or freeware
- low-frequency
and/or high-frequency
- circuit
and/or 2D fields
and/or 3D fields
- problem specific
or multi-purpose
- electromagnetic fields
and/or multi-physics
- cheap or expensive



Electromagnetic field solvers



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or **multi-purpose**
- **electromagnetic fields**
and/or **multi-physics**
- **cheap** or **expensive**

non-exhaustive list !!

The image displays a collection of logos for various electromagnetic field solvers. The logos are arranged in a grid-like fashion. The CST logo is enclosed in a red rectangular border, indicating it is the focus of the slide. The other logos include CEDRAT, infolytica corporation, opera simulation software, FEMM, JMAG, ANSYS, FEKO, and COMSOL MULTIPHYSICS.

Electromagnetic field solvers



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Electromagnetic field solvers



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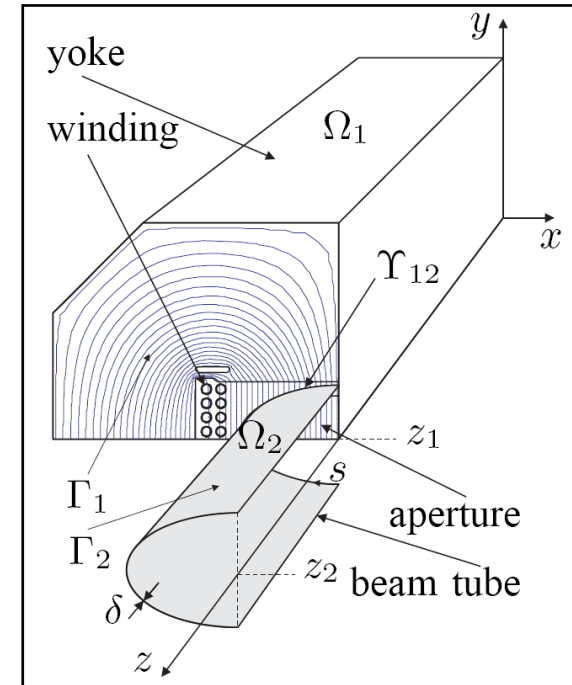
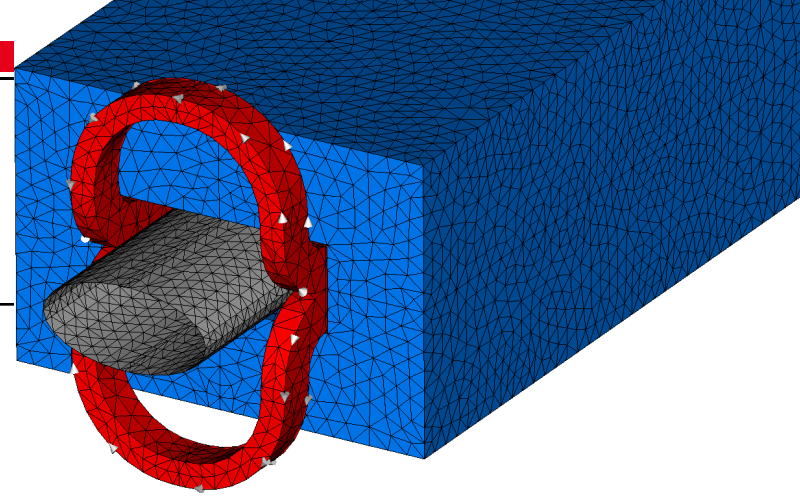
- commercial
or academic
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and/or 2D fields
and/or 3D fields
- problem specific
or multi-purpose
- electromagnetic fields
and/or multi-physics
- cheap or expensive

non-exhaustive list !!

The image displays a collection of logos for various electromagnetic field solvers. The logos are arranged in a grid-like fashion. At the top, the text 'non-exhaustive list !!' is written in red. The logos include: CEDRAT (top left), CST (top right), infolytica corporation (middle left), JMAG (middle center), ANSYS (middle right), opera simulation software (bottom left), FEMM (bottom left, below opera), FEKO (bottom right), and COMSOL MULTIPHYSICS (bottom center, highlighted with a red border). The COMSOL logo features a 3D cube with a blue and yellow gradient.

Overview

- magnet simulation (standard 3D FE solver)
- **challenges**
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- magnet simulation (dedicated 3D FE solver)
- hybrid models
- stochastic models
- conclusions



Challenge 1: Detailed geometry



yoke

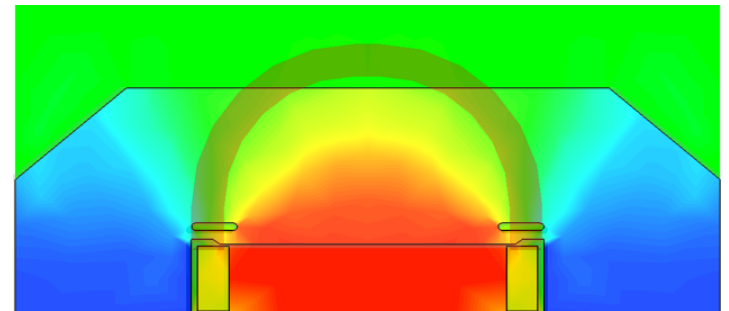
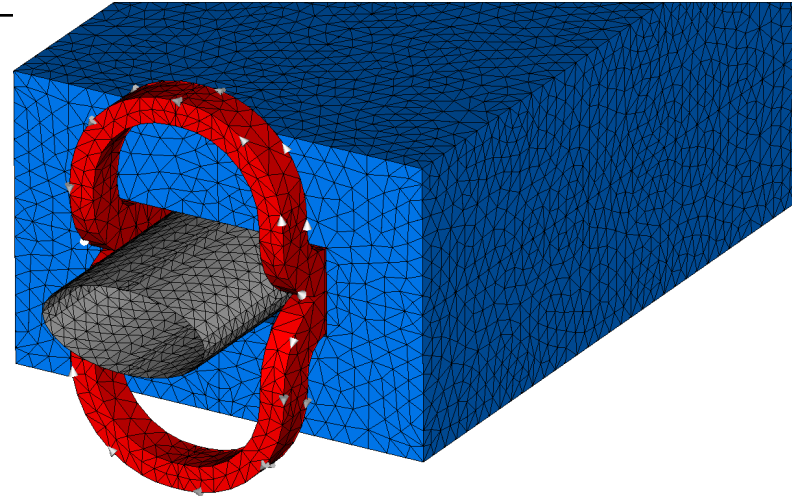
- length (meter)
vs. lamination thickness (mm)
- shimming, holes

beam tube

- < 1mm thick

end-winding parts

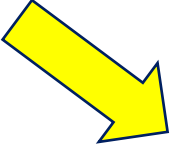
- determine the eddy currents
in the end plates



Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)


$$\bar{\bar{\nu}}(\vec{B}) = R^T \begin{bmatrix} \nu_{\text{rol}} & & \\ & \nu_{\text{trans}} & \\ & & \nu_{\text{trans}} \end{bmatrix} R$$

ν_{rol} reluctivity in the rolling direction

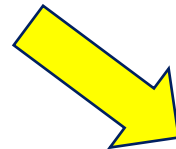
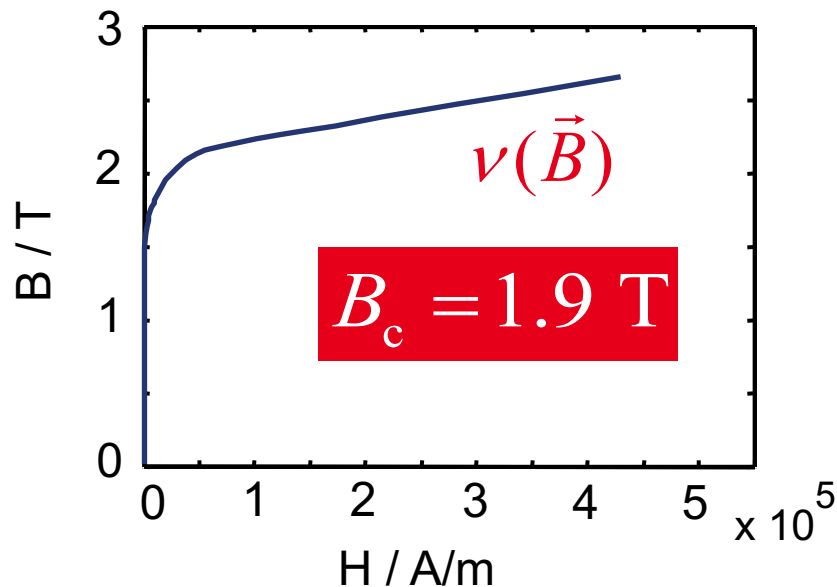
ν_{trans} reluctivity in the transversal direction

R local rotation matrix

Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)



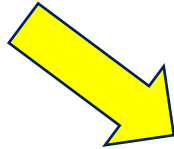
Newton method

Challenge 2: Materials



yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)



Jiles-Atherton model

Preisach model

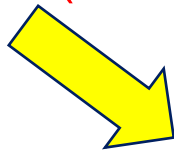
estimation of losses by Steinmetz-Bertotti

Challenge 2: Materials



yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- **composite (lamination)**

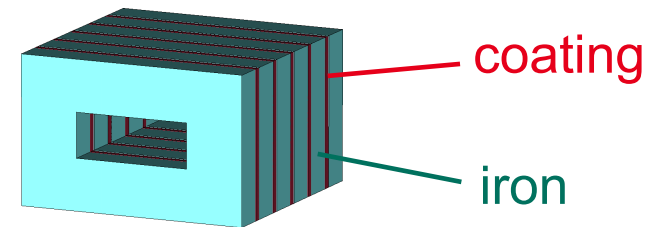


(simple) homogenisation
along lamination direction

perpendicular to laminates

stacking factor

$$\gamma_{st} \approx 0.95 \leq \sim 1$$



$$\frac{1}{\nu_{xy}} = \frac{\gamma_{st}}{\nu_{Fe}} + \frac{1 - \gamma_{st}}{\nu_0}$$

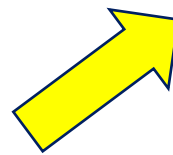
$$\nu_z = \gamma_{st} \nu_{Fe} + (1 - \gamma_{st}) \nu_0$$

Challenge 2: Materials



yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- **composite (lamination)**

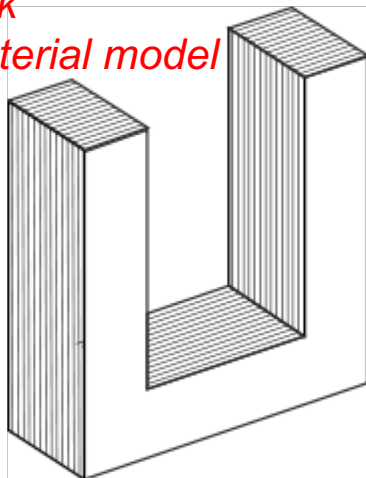


multiscale simulation

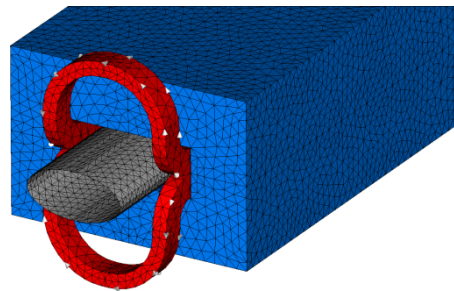
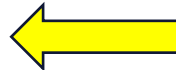
*laminated
material model*

bulk

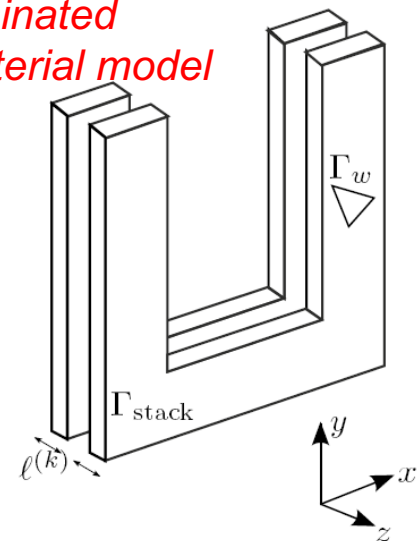
material model



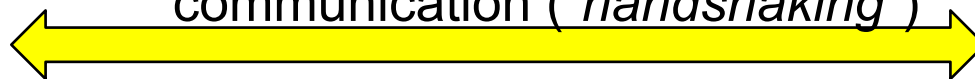
magnetic
field



eddy
currents



communication (“handshaking”)

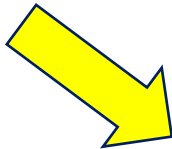


Challenge 2: Materials



yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- composite (lamination)
- **variability**



stochastics, sensitivity

Challenge 2: Materials

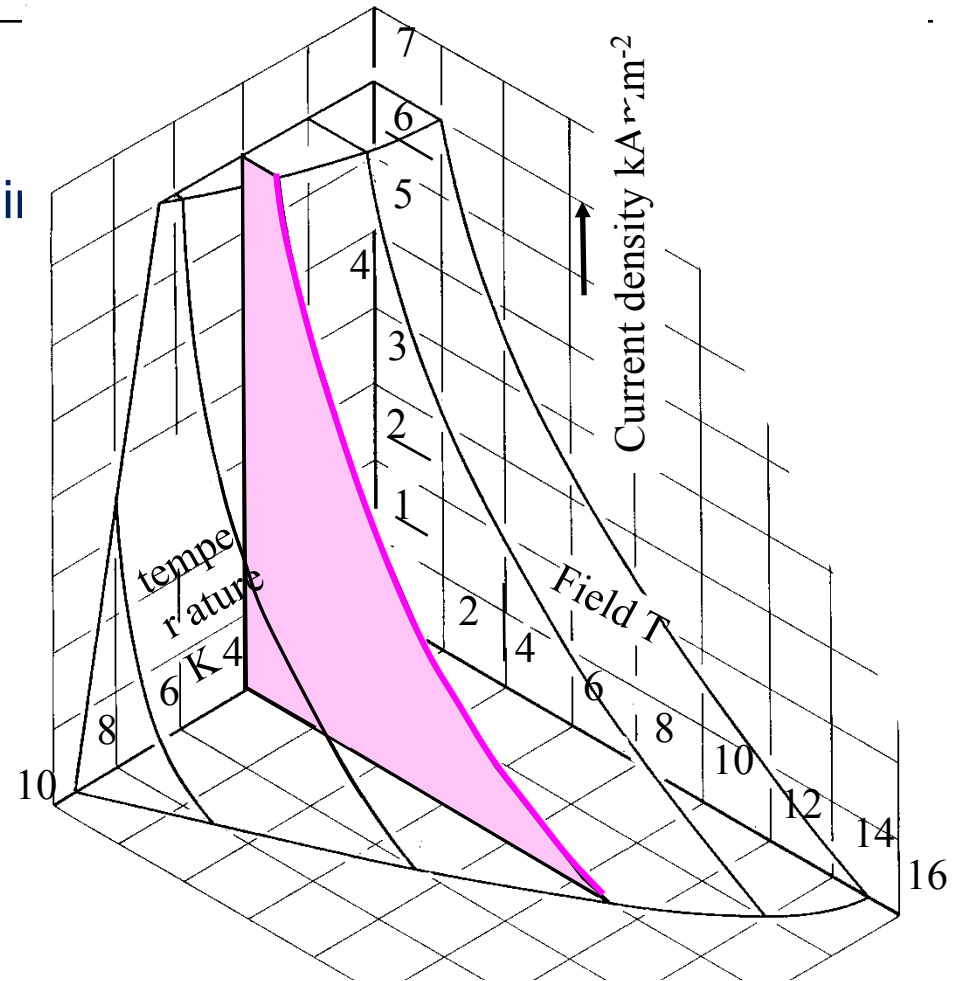


yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- composite (lamination)
- variability

superconductor:

- critical current
- temperature
- magnetic field

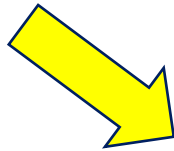


Challenge 3: Transient phenomena



lamination

- hysteresis + remanence



Jiles-Atherton model

Preisach model

estimation of the remanence

(based on data from material vendor)

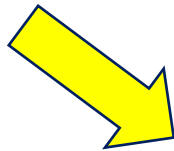
Challenge 3: Transient phenomena



lamination

- hysteresis + remanence
- eddy currents

$$\nabla \times \left(\nu \nabla \times \vec{A} \right) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$$

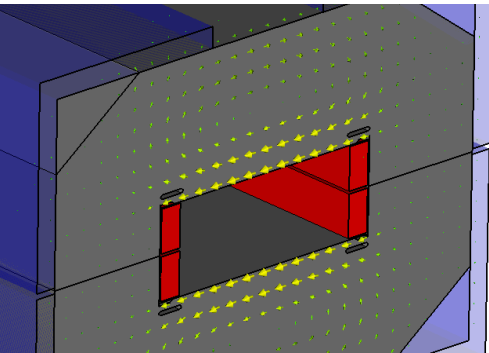


eddy current term

+ (simple) homogenisation $\sigma_{xy} = \gamma_{st} \sigma_{Fe}$

$$\sigma_z = 0$$

or + multi-scale model (hand-shaking)



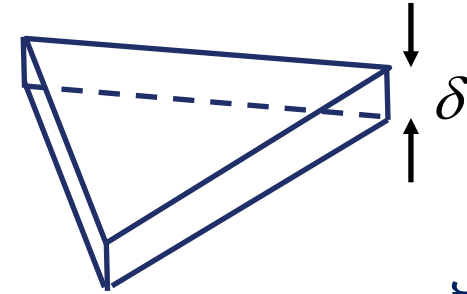
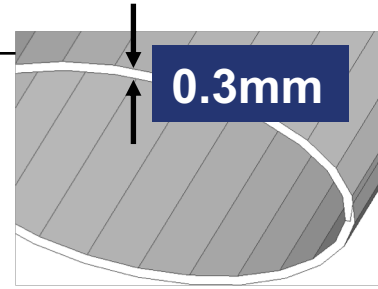
Challenge 3: Transient phenomena



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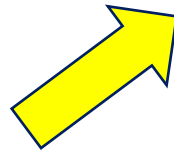
lamination

- hysteresis + remanence
- eddy currents



beam tube

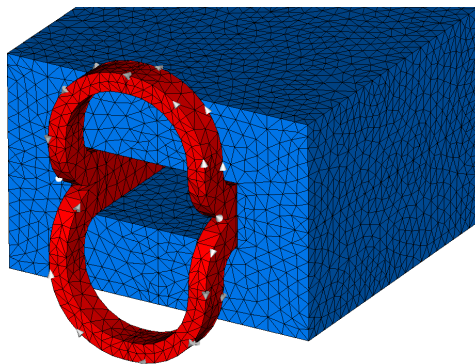
- eddy currents



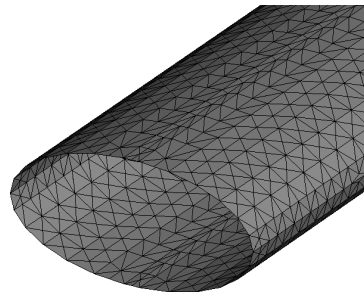
shell elements

additional matrix contributions \mathbf{K}_δ and \mathbf{M}_δ
assembling into system matrix by \mathbf{Q}

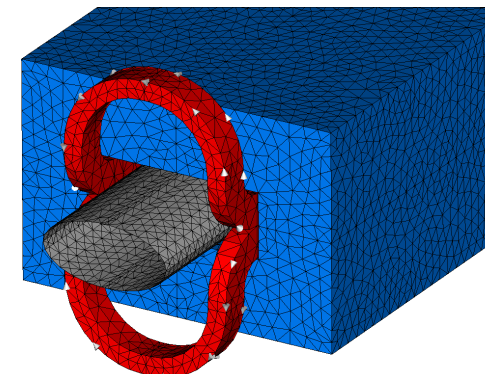
$$\mathbf{K}_V + \sigma \mathbf{M}_\sigma + \mathbf{Q}^T (\mathbf{K}_\delta + \alpha \mathbf{M}_\delta) \mathbf{Q} = \mathbf{K}_{\text{full}} + \alpha \mathbf{M}_{\text{full}}$$



+



=



Challenge 3: Transient phenomena

lamination

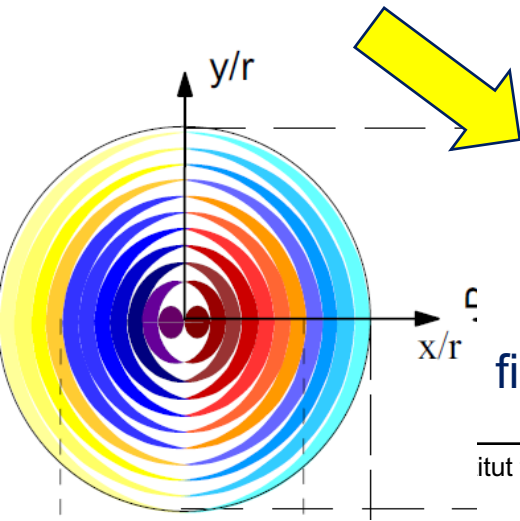
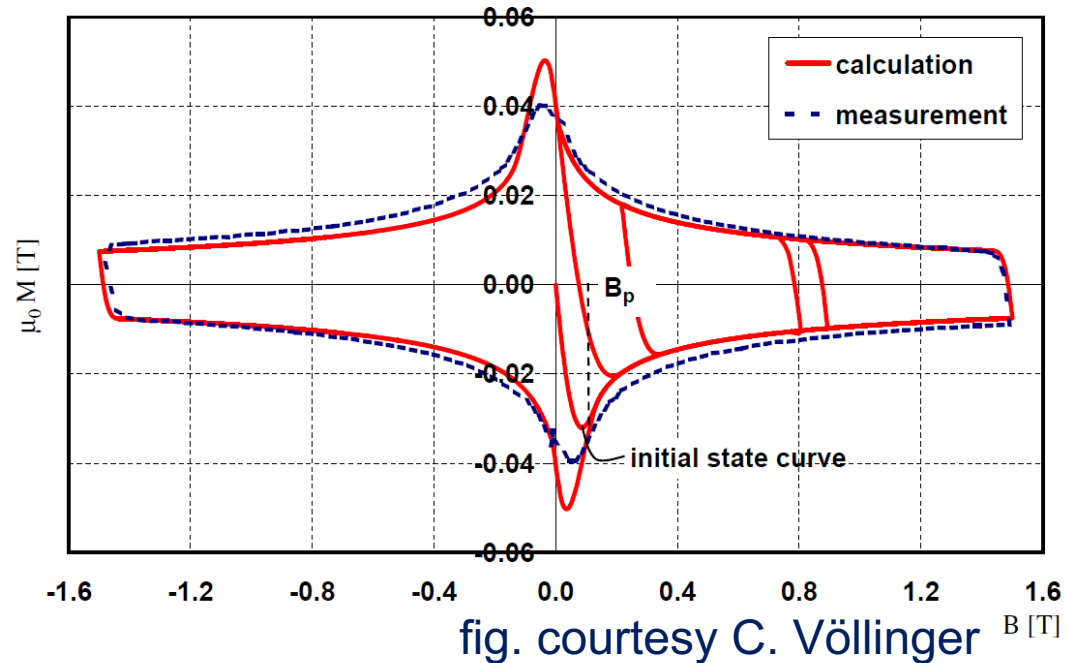
- hysteresis + remanence
- eddy currents

beam tube

- eddy currents

superconductor

- persistent currents



Bean model \rightarrow magnetisation (Christine Völlinger)
implemented in ROXIE

fig. courtesy C. Völlinger

Challenge 3: Transient phenomena



lamination

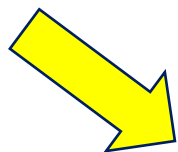
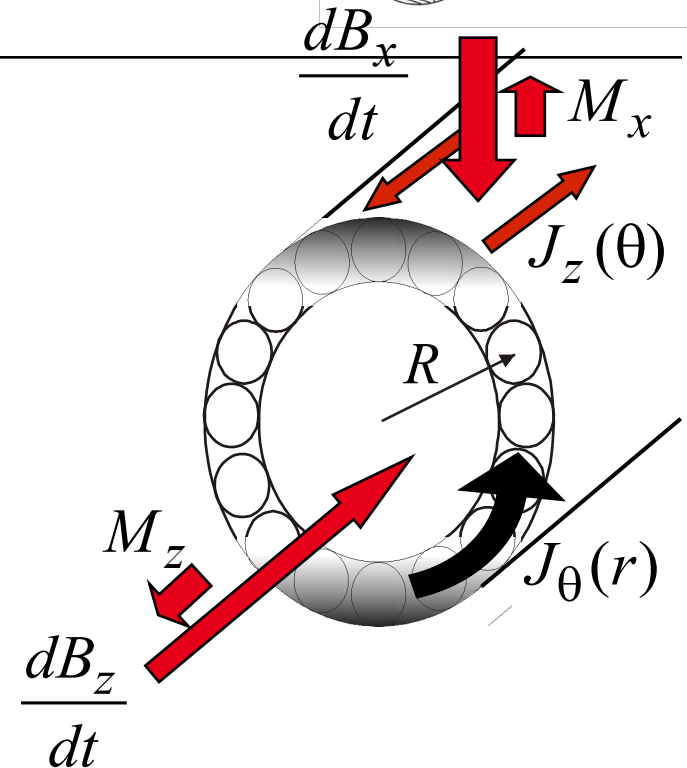
- hysteresis + remanence
- eddy currents

beam tube

- eddy currents

superconductor

- persistent currents
- coupling currents
- cable eddy currents



$$\nabla \times (\nu \nabla \times \vec{A}) + \sigma \frac{\partial \vec{A}}{\partial t} + \nabla \times \left(\nu_0 \bar{\tau}_{cb} \nabla \times \frac{\partial \vec{A}}{\partial t} \right) = \vec{J}_s$$

additional magnetisation

Challenge 4: High accuracy requirements

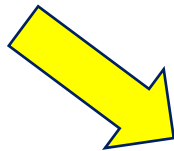


losses

- dimensioning of the cooling system
- hot spots
- quench

aperture field

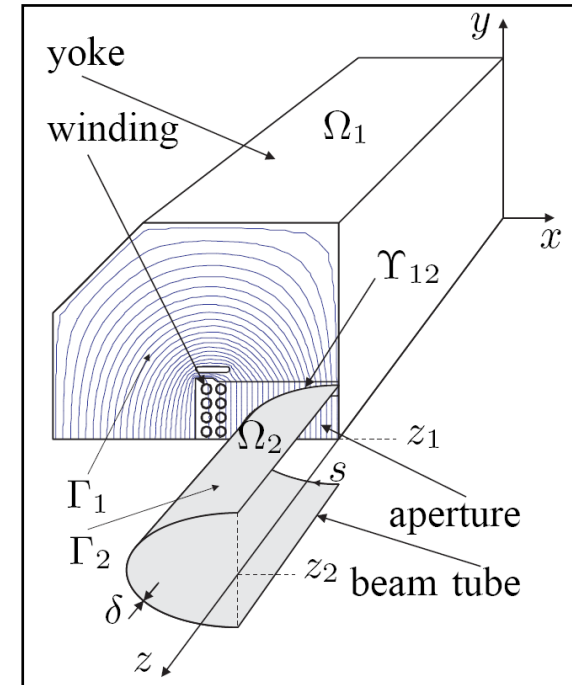
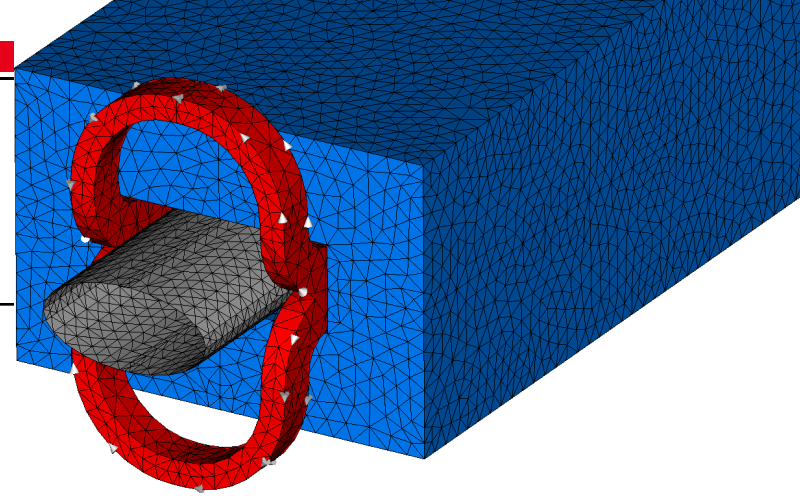
- multipoles during injection, ramping and extraction
- + influence of eddy currents



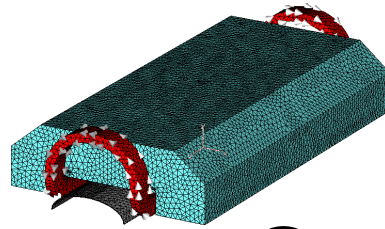
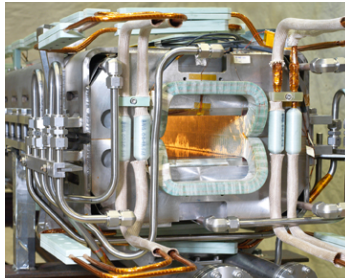
huge models
parallelisation, multi-core computers

Overview

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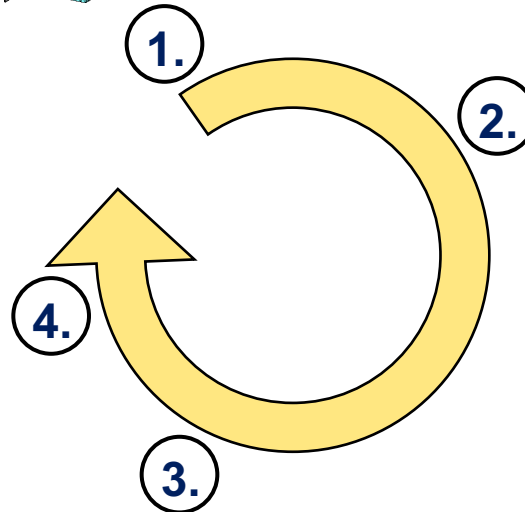
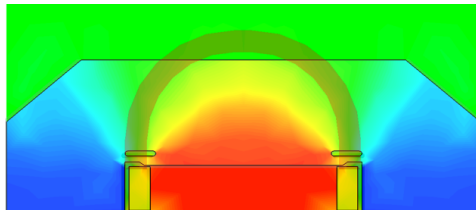


Dedicated Simulation Tool



CST Studio Suite®

- CAD modelling
- meshing
- visualisation



Matlab

- postprocessing
- visualisation

FEMSTER,
LLNL

TRILINOS,
Sandia Labs

own software

- FE assembly
(higher order FEs)
- transient solver
- nonlinear materials
- system solver

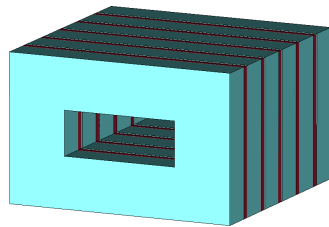
parallelisation

+ Stephan Koch, Jens Trommler

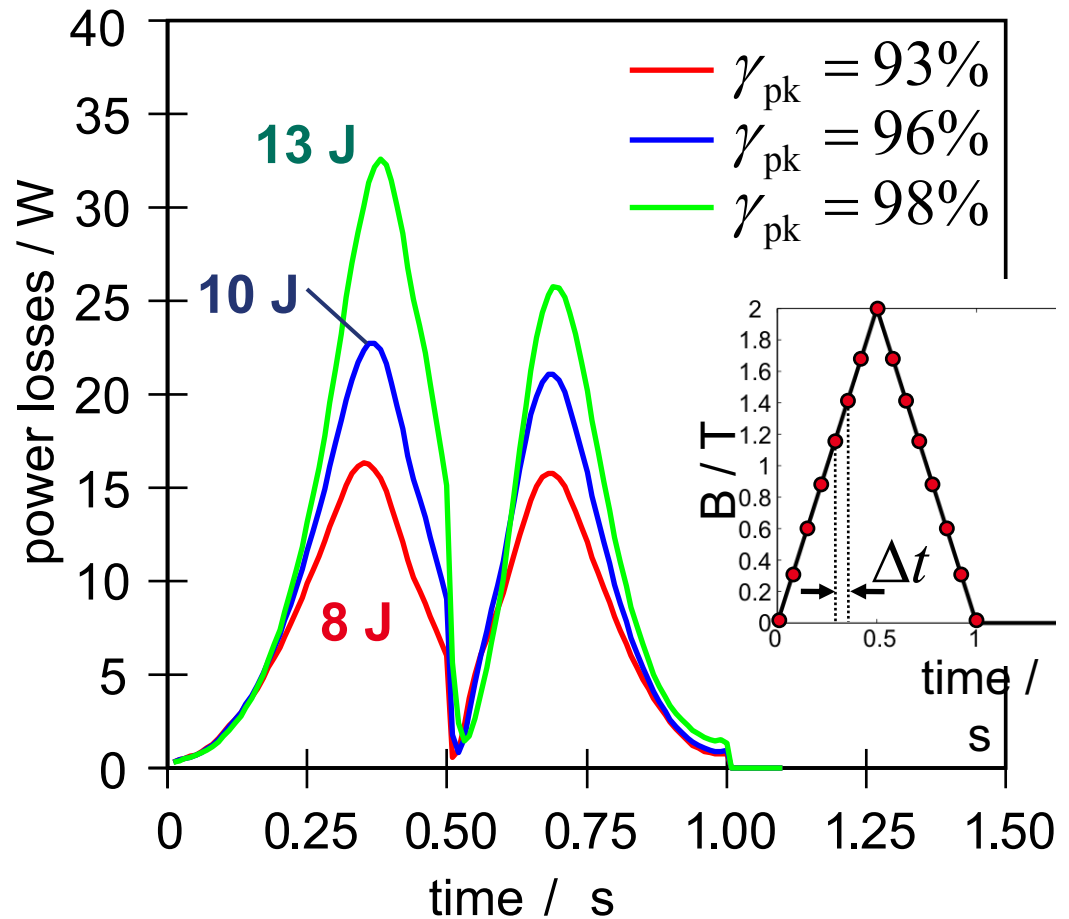
Results: Eddy-Current Losses

eddy-current losses
over one cycle

for different
stacking factors γ_{pk}



loss energy: $W = \int_0^T P dt$



+ Stephan Koch, Jens Trommler

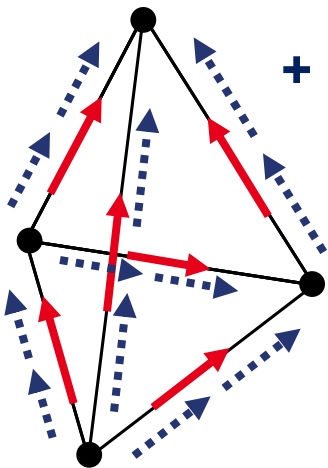
Results: Loss Energy

- discretization:
 - increase number of elements
 - increase order of approximation

$$\vec{A} \approx \vec{A}_{\text{FE}} = \sum_j a_j \vec{w}_j^{\text{tv}}$$

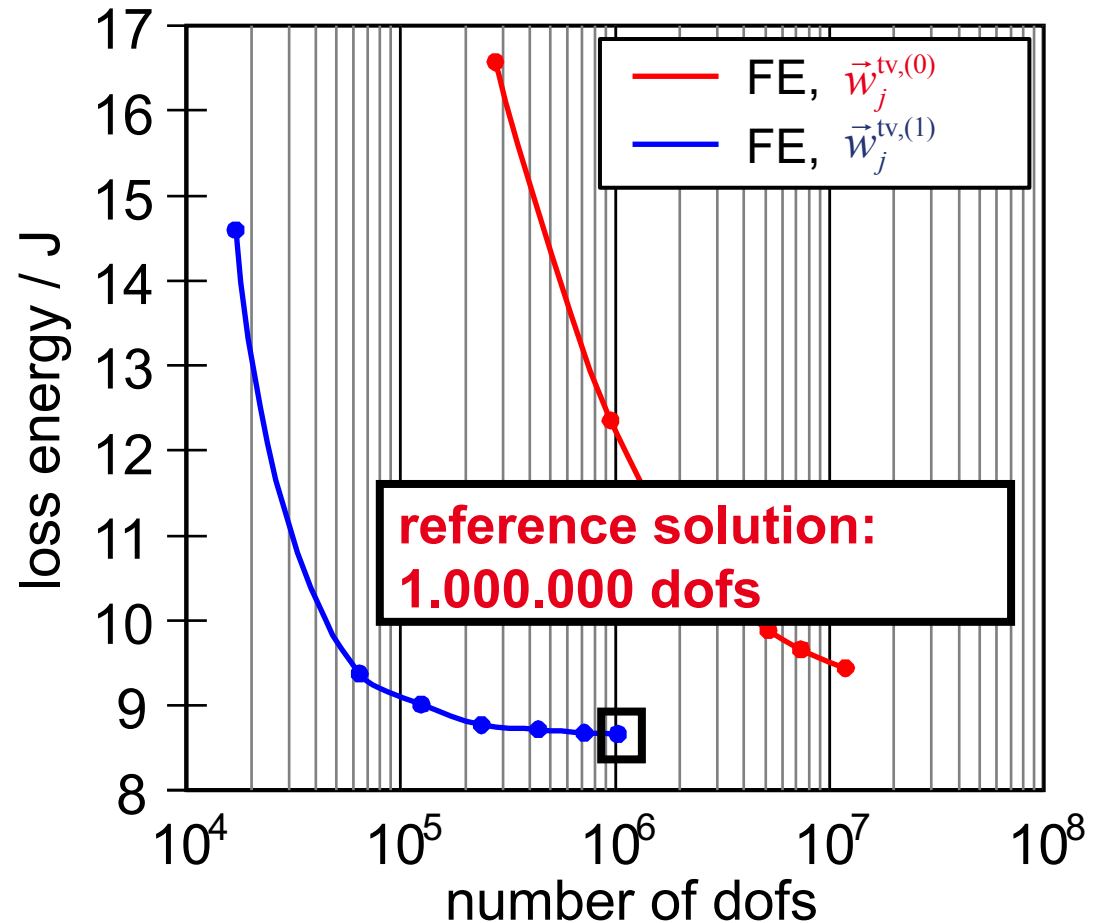
degrees of freedom:

+ 2 per face



$$\vec{w}_j^{\text{tv},(0)} \quad n_{\text{dof}} = 6$$

$$\vec{w}_j^{\text{tv},(1)} \quad n_{\text{dof}} = 20$$

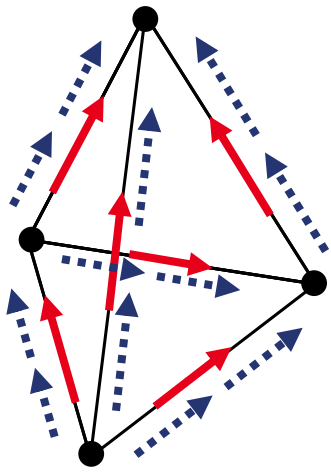


+ S. Koch, J. Trommler

Convergence: Loss Energy

- relative error with respect to reference solution

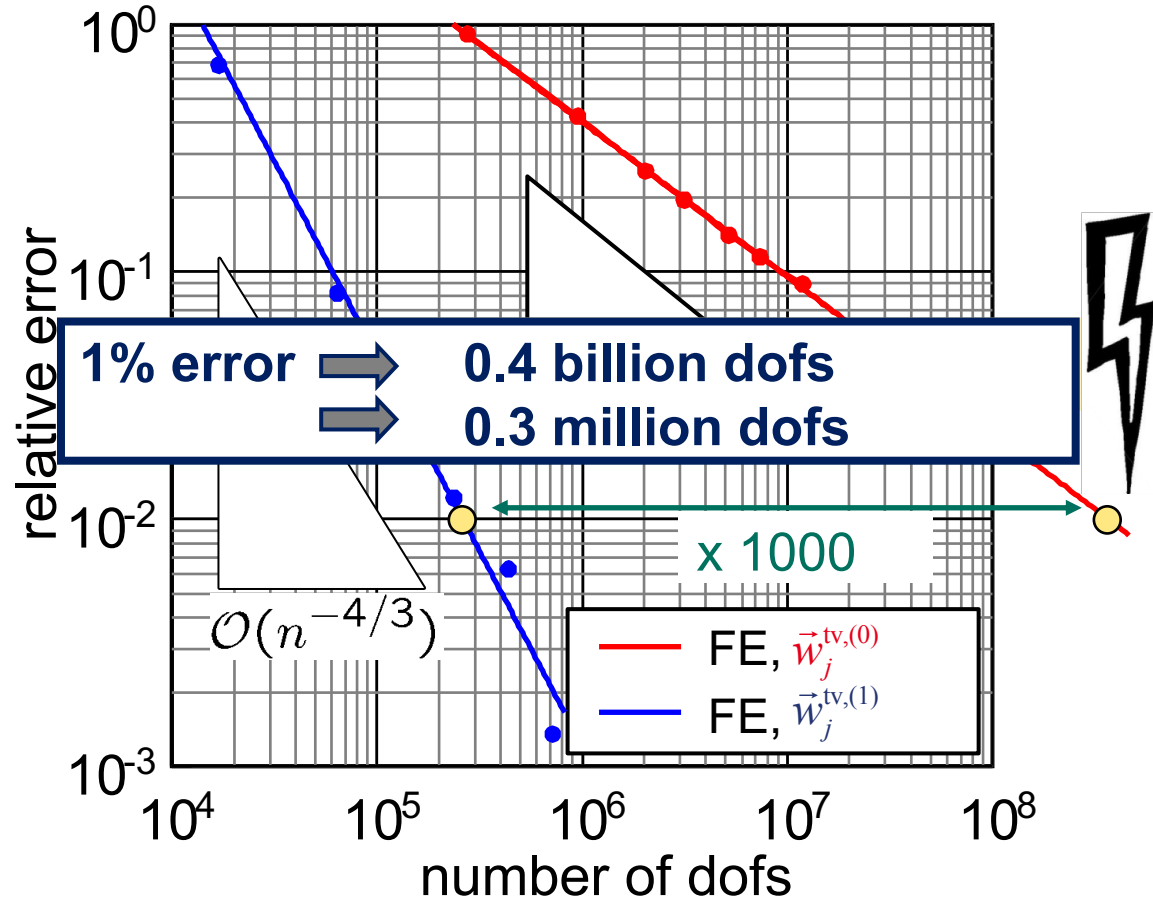
degrees of freedom:



+ 2 per face

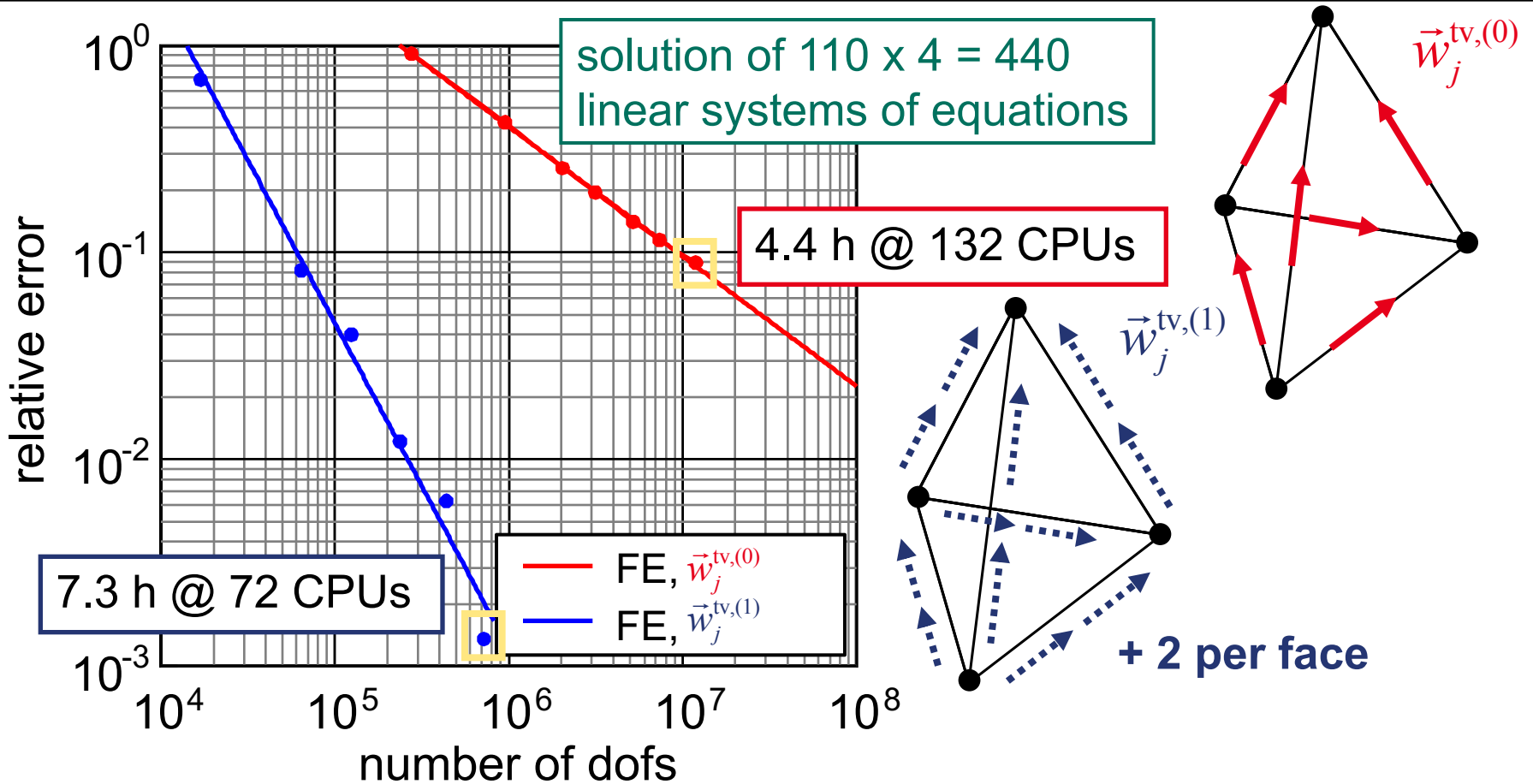
$$\vec{w}_j^{tv,(0)}$$

$$\vec{w}_j^{tv,(1)}$$



+ S. Koch, J. Trommler

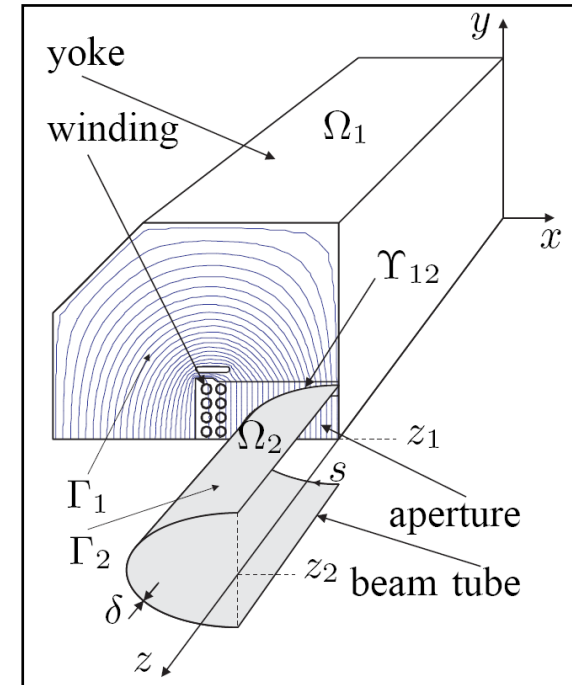
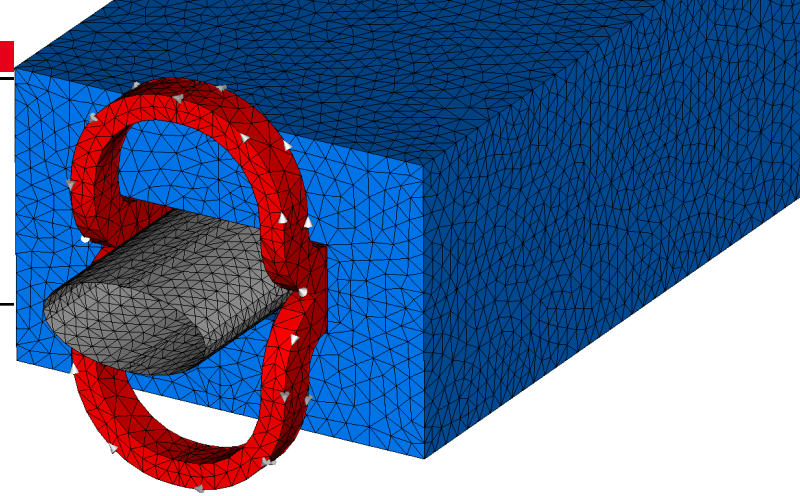
Comparison: Shape Functions



+ S. Koch, J. Trommler

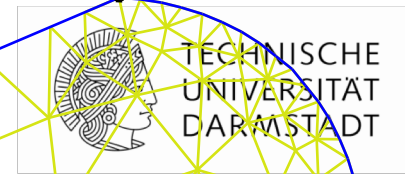
Overview

- magnet simulation (standard 3D FE solver)
- challenges
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- magnet simulation (dedicated 3D FE solver)
- **hybrid models**
- **stochastic models**
- **conclusions**

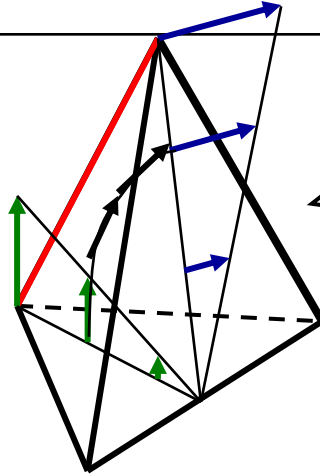


Hybrid discretisation

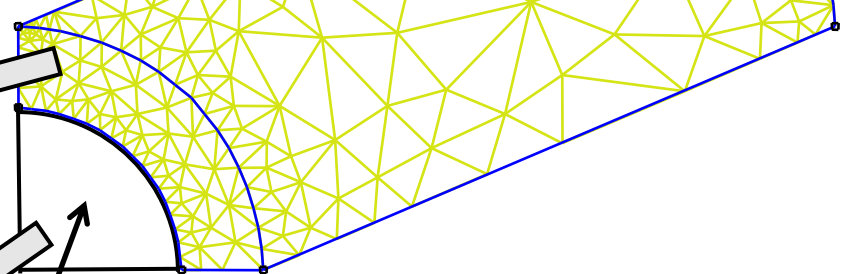
domain Ω_1



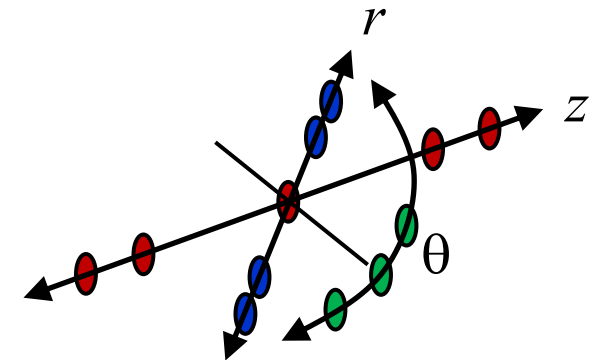
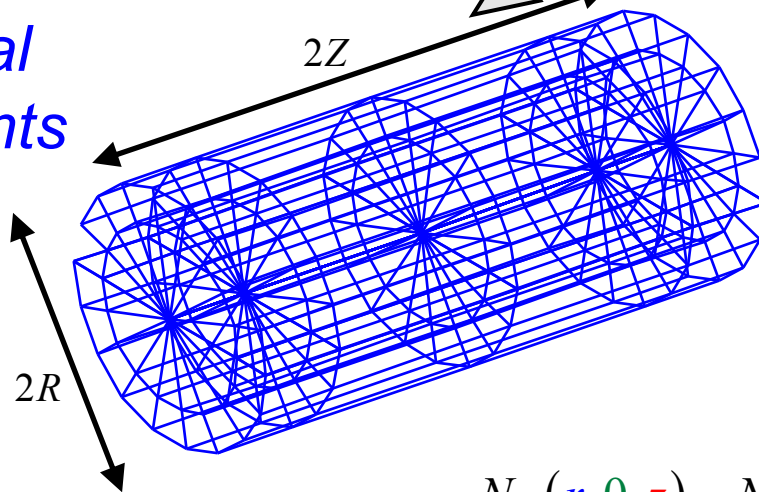
(edge)
finite
elements



domain Ω_2



spectral
elements

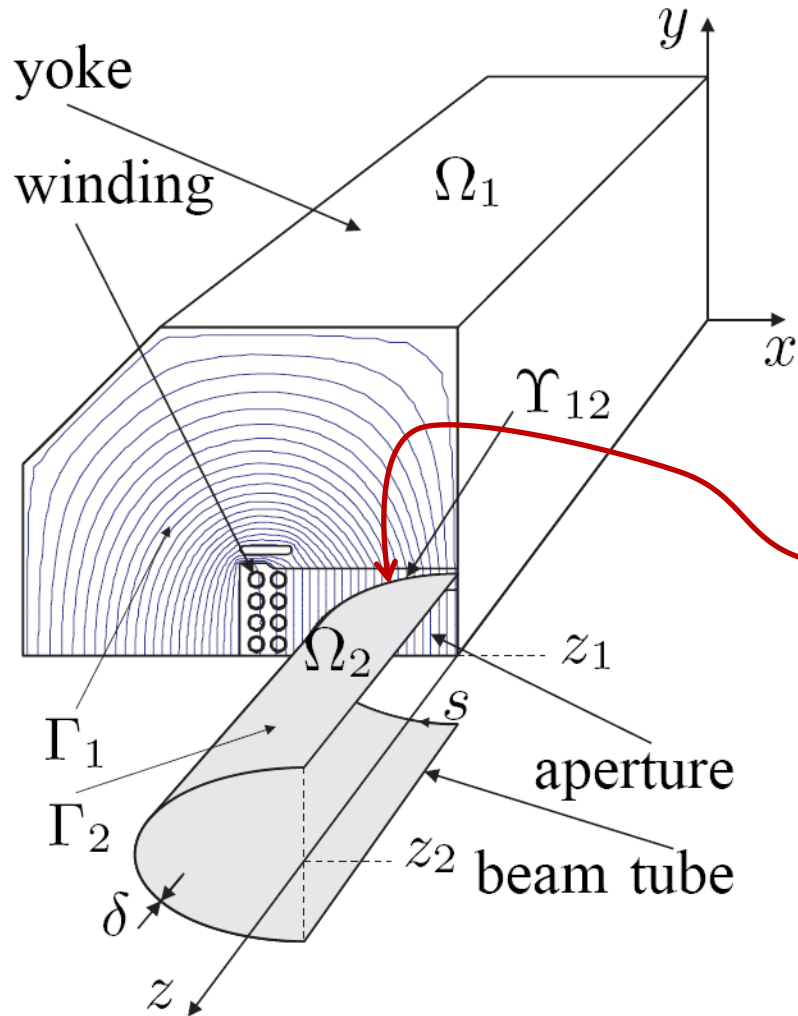


Legendre distribution in r
equidistant distribution in θ
Legendre distribution in z

$$N_q(r, \theta, z) = N_{q_1, q_2, \lambda}(r, \theta, z) = P_{q_1}\left(\frac{r}{R}\right) e^{-j\lambda_q \theta} P_{q_2}\left(\frac{z}{Z}\right)$$

+ Markus Clemens

Beam-tube end model



standard 2D model

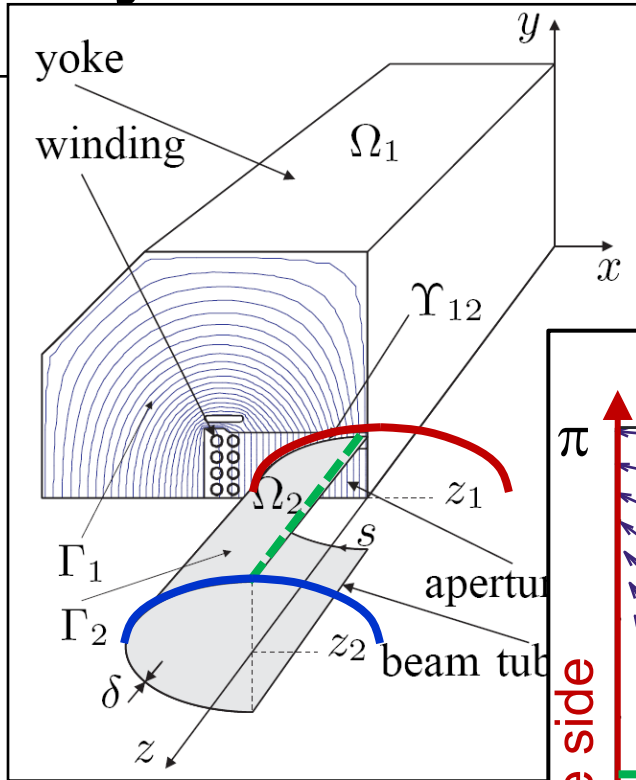
cross-section Γ_1
of volume Ω_1

common interface Y_{12}

*additional 2D model
for the beam-tube end*

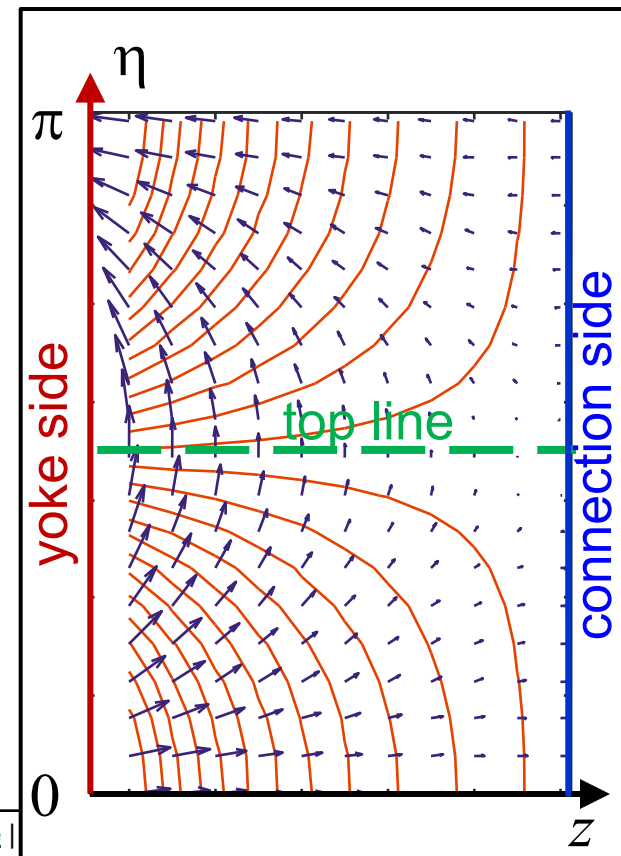
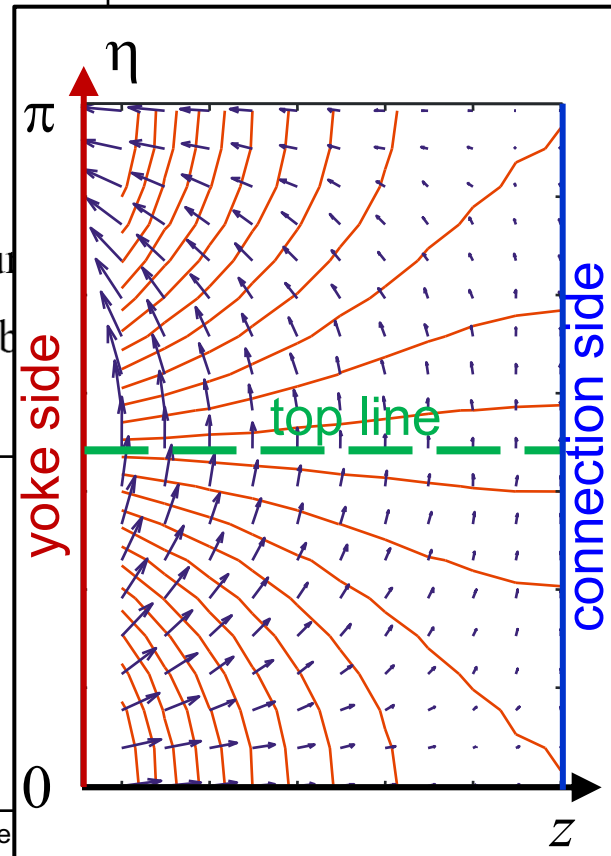
cross-section Γ_2
of volume Ω_2

Eddy-current closing paths



connected
beam tube

disconnected
beam tube



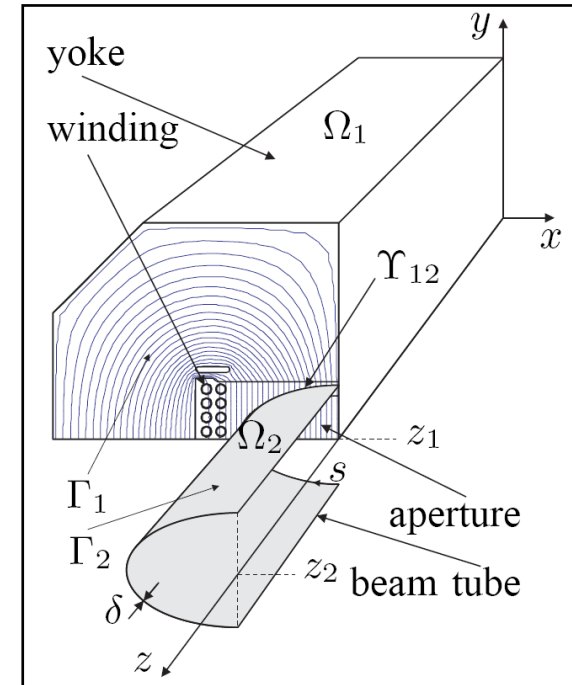
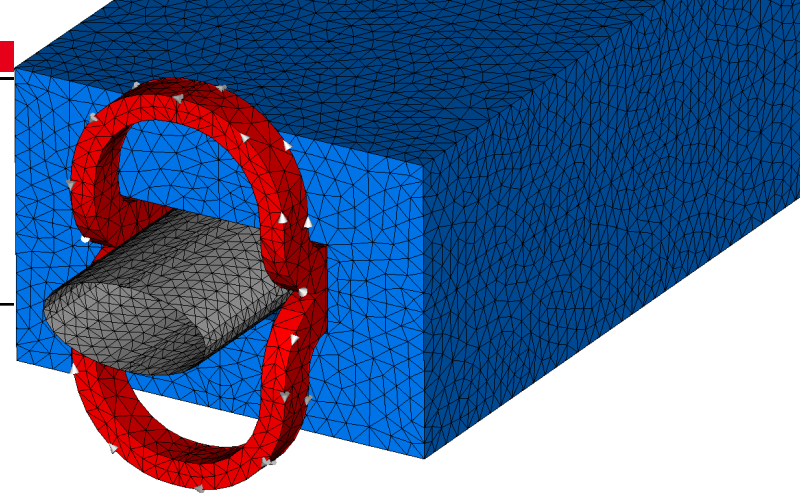
yoke side

top line

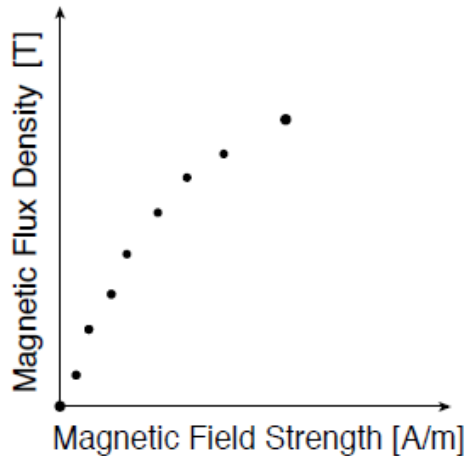
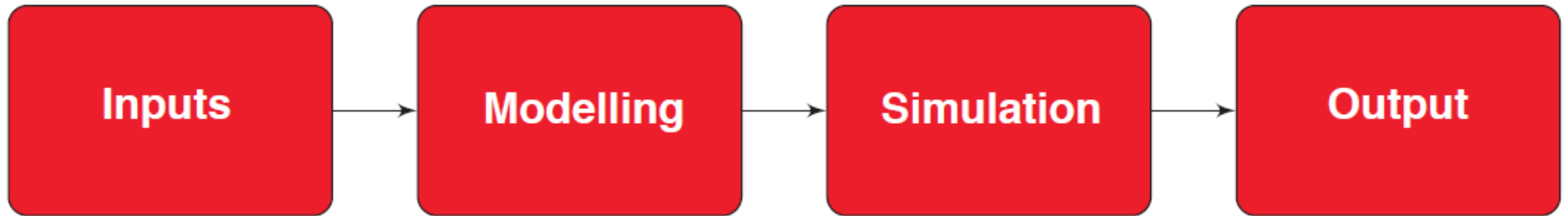
connection side

Overview

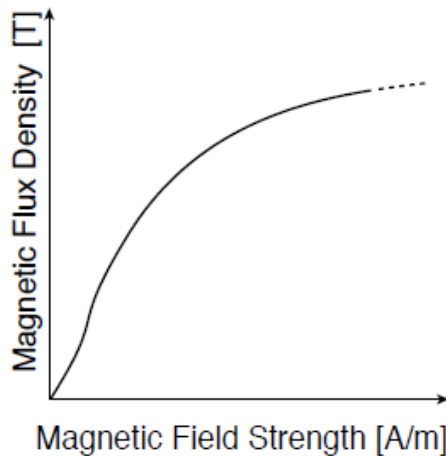
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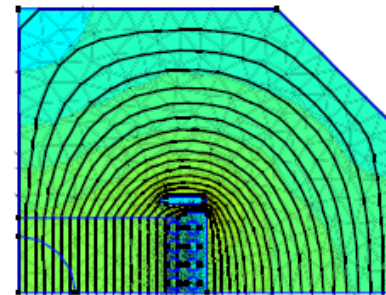
Uncertainty quantification



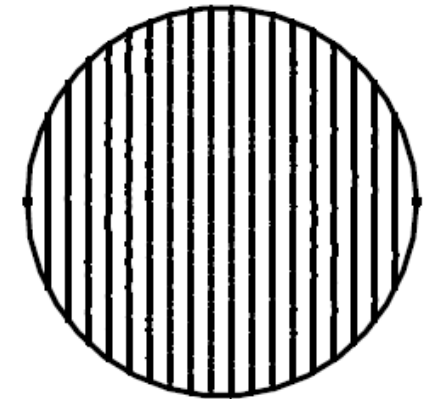
Measurement



Model of saturation



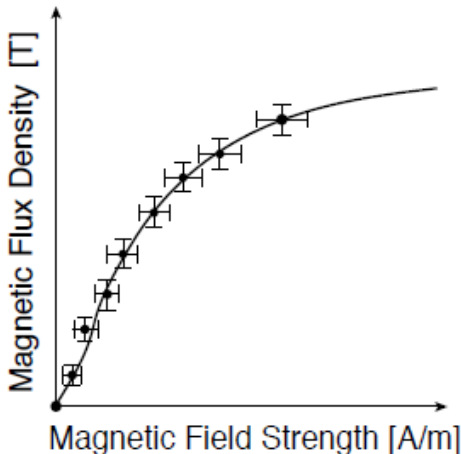
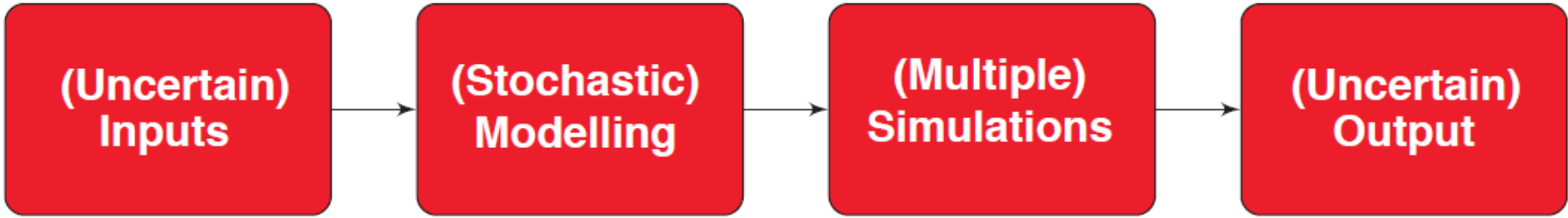
Accelerator Magnet



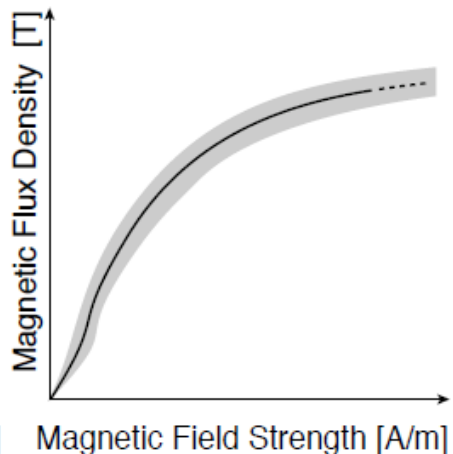
Multipoles b_j

+ Ulrich Römer, Sebastian Schöps

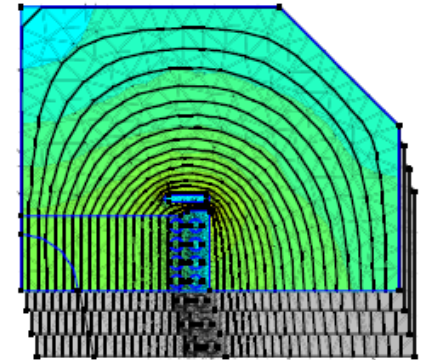
Overview



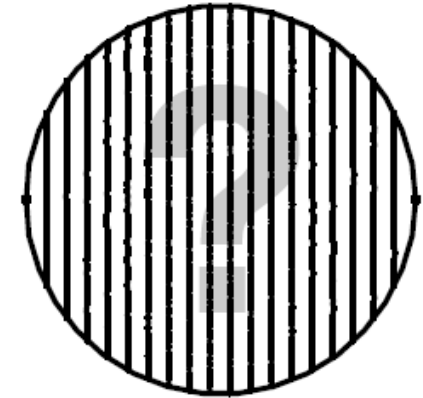
Measurement



Model of saturation



Accelerator Magnet

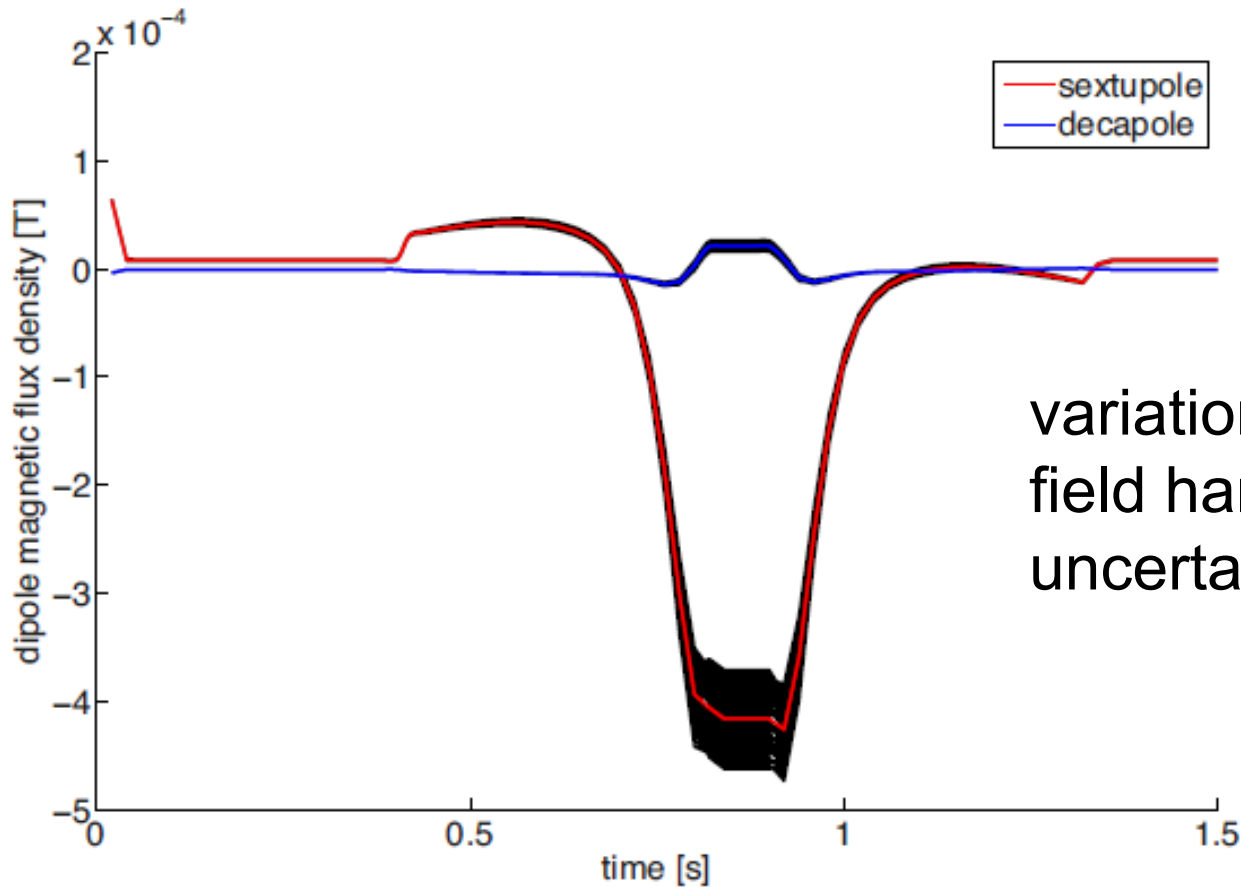


Multipoles b_i

+ Ulrich Römer, Sebastian Schöps



Uncertainty quantification



variation on the
field harmonics due to
uncertain BH-characteristic

+ Ulrich Römer, Sebastian Schöps

Conclusions

- nonlinear 3D transient magnetic simulation feasible with off-the-shell software
- challenges remain and are problem specific
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- dedicated methods and software

