

Lectures on Partial Differential Equations

Stephan Russenschuck, CAS Thessaloniki



Foundations of Vector Analysis



Directional Derivative and the Total Differential

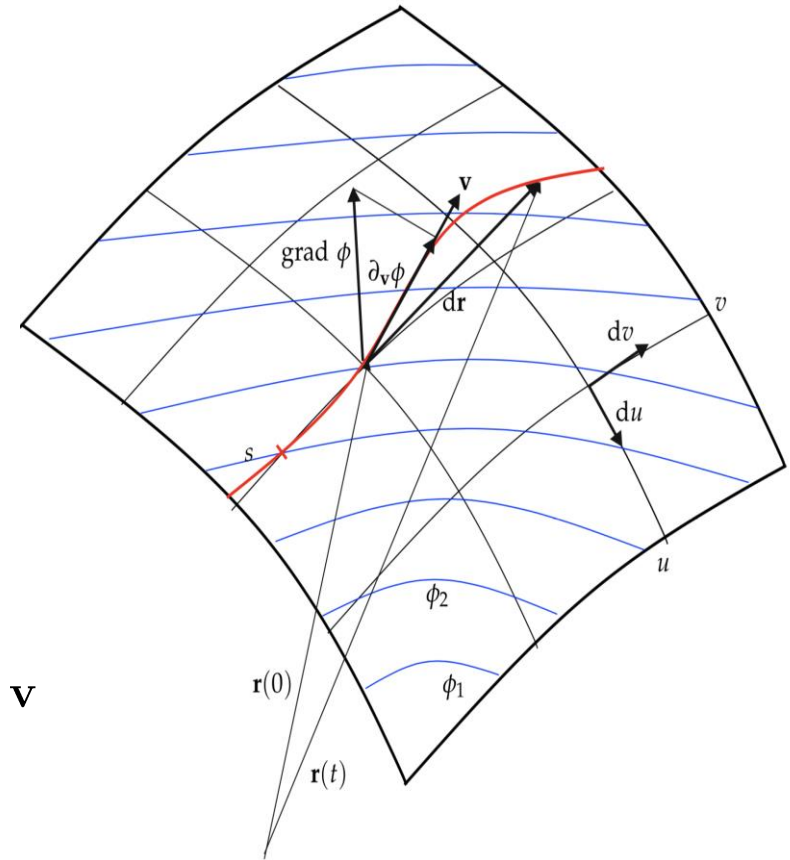
Space curve with $\mathbf{r}(t) = (x(t), y(t), z(t))$
 parametrized such that $\mathbf{r}(0) = P$.

1-smooth scalar field $\phi : E_3 \rightarrow R : \mathbf{r} \mapsto \phi(\mathbf{r})$
 expressed as $\phi(x, y, z)$, then $\phi(\mathbf{r}(t))$ at
 parameter (time) t .

$$\partial_{\mathbf{v}}\phi = \frac{\partial\phi}{\partial v} = \frac{d}{dt}[\phi(\mathbf{r} + t\mathbf{v})]_{t=0} = \lim_{t \rightarrow 0} \frac{\phi(\mathbf{r} + t\mathbf{v}) - \phi(\mathbf{r})}{t}$$

$$\partial_{\mathbf{v}}\phi = \frac{d}{dt}\phi(\mathbf{r}(t)) = \frac{\partial\phi}{\partial x} \frac{dx}{dt} + \frac{\partial\phi}{\partial y} \frac{dy}{dt} + \frac{\partial\phi}{\partial z} \frac{dz}{dt} = \text{grad } \phi \cdot \mathbf{v}$$

$$\text{grad } \phi = \frac{\partial\phi}{\partial x} \mathbf{e}_x + \frac{\partial\phi}{\partial y} \mathbf{e}_y + \frac{\partial\phi}{\partial z} \mathbf{e}_z$$



Best linear approximation of ϕ over displacement distance $d\mathbf{r}$

$$d\mathbf{r} = \mathbf{v} dt = \frac{\mathbf{v}}{v} v dt = \mathbf{T} ds \quad d\mathbf{a} = \mathbf{n} da = \left(\frac{\partial\mathbf{r}}{\partial u} \times \frac{\partial\mathbf{r}}{\partial v} \right) du dv \quad d\mathbf{f} = \frac{\partial\mathbf{f}}{\partial x} dx + \frac{\partial\mathbf{f}}{\partial y} dy + \frac{\partial\mathbf{f}}{\partial z} dz$$

Ideal Pole Shape of Conventional Magnets

Remember the Cauchy Schwarz inequality

$$| \langle \mathbf{a}, \mathbf{b} \rangle | \leq \| \mathbf{a} \| \| \mathbf{b} \|,$$

Thus for the directional derivative

$$| \partial_{\mathbf{v}} \phi | \leq | \text{grad } \phi | | \mathbf{v} |.$$

This implies that the directional derivative takes its maximum when \mathbf{v} points in the direction of the gradient. Therefore gradient points in the direction of the steepest ascent of ϕ and is thus normal to the surface of equipotential.

The flux density \mathbf{B} exits a highly permeable surface in normal direction. Therefore the pole shape of normal conducting magnets can be seen as an equipotential of the magnetic scalar potential.

$$\text{grad } \phi := \frac{\partial \phi}{\partial x} \mathbf{e}_x + \frac{\partial \phi}{\partial y} \mathbf{e}_y + \frac{\partial \phi}{\partial z} \mathbf{e}_z$$

$$\text{curl } \mathbf{g} = \left(\frac{\partial g_z}{\partial y} - \frac{\partial g_y}{\partial z} \right) \mathbf{e}_x + \left(\frac{\partial g_x}{\partial z} - \frac{\partial g_z}{\partial x} \right) \mathbf{e}_y + \left(\frac{\partial g_y}{\partial x} - \frac{\partial g_x}{\partial y} \right) \mathbf{e}_z.$$

$$\text{div } \mathbf{g} = \frac{\partial g_x}{\partial x} + \frac{\partial g_y}{\partial y} + \frac{\partial g_z}{\partial z}.$$

$$\begin{aligned}\text{curl grad } \phi &= \text{curl} \left[\frac{1}{h_1} \frac{\partial \phi}{\partial u^1} \mathbf{e}_{u^1} + \frac{1}{h_2} \frac{\partial \phi}{\partial u^2} \mathbf{e}_{u^2} + \frac{1}{h_3} \frac{\partial \phi}{\partial u^3} \mathbf{e}_{u^3} \right] \\ &= \frac{1}{h_2 h_3} \left(\frac{\partial^2 \phi}{\partial u^2 \partial u^3} - \frac{\partial^2 \phi}{\partial u^3 \partial u^2} \right) \mathbf{e}_{u^1} \\ &\quad + \frac{1}{h_3 h_1} \left(\frac{\partial^2 \phi}{\partial u^3 \partial u^1} - \frac{\partial^2 \phi}{\partial u^1 \partial u^3} \right) \mathbf{e}_{u^2} \\ &\quad + \frac{1}{h_1 h_2} \left(\frac{\partial^2 \phi}{\partial u^1 \partial u^2} - \frac{\partial^2 \phi}{\partial u^2 \partial u^1} \right) \mathbf{e}_{u^3} = 0,\end{aligned}$$

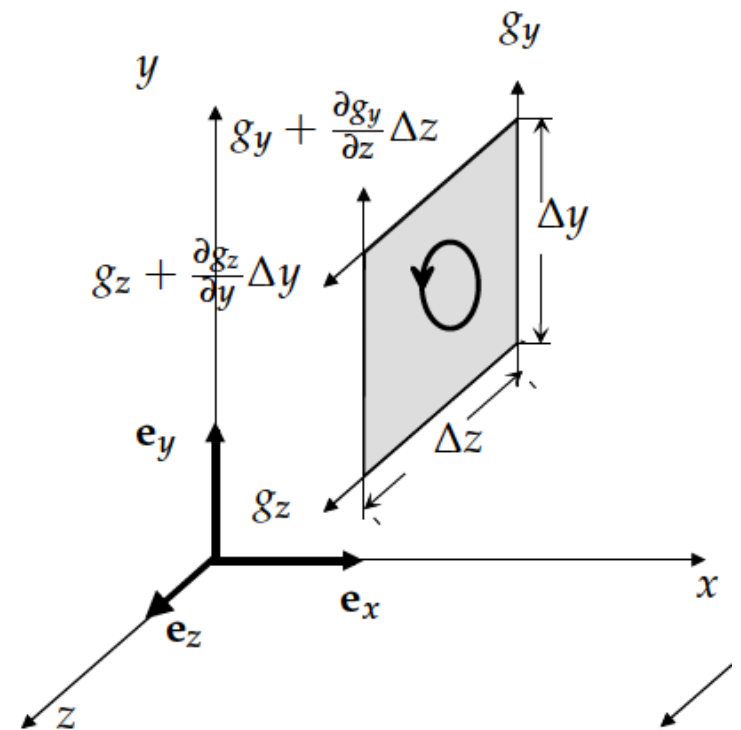
Ugly and not even a universal proof (orthogonality assumed)

Coordinate Free Definition of Grad, Curl, and Div

$$\int_{\mathcal{P}_1}^{\mathcal{P}_2} \mathbf{a} \cdot d\mathbf{r} = \int_{\mathcal{P}_1}^{\mathcal{P}_2} \text{grad } \phi \cdot d\mathbf{r} = \int_{\mathcal{P}_1}^{\mathcal{P}_2} d\phi = \phi(\mathcal{P}_2) - \phi(\mathcal{P}_1),$$

$$\mathbf{n} \cdot \text{curl } \mathbf{g} = \lim_{a \rightarrow 0} \frac{\int_{\partial \mathcal{A}} \mathbf{g} \cdot d\mathbf{r}}{a},$$

$$\text{div } \mathbf{g} = \lim_{V \rightarrow 0} \frac{\int_{\partial \mathcal{V}} \mathbf{g} \cdot d\mathbf{a}}{V},$$



$$\partial(\partial\mathcal{V}) = \emptyset, \quad \partial(\partial\mathcal{A}) = \emptyset,$$

$$\int_{\mathcal{V}} \operatorname{div} \operatorname{curl} \mathbf{g} dV = \int_{\partial\mathcal{V}} \operatorname{curl} \mathbf{g} \cdot d\mathbf{a} = \int_{\partial(\partial\mathcal{V})} \mathbf{g} \cdot d\mathbf{r} = 0,$$

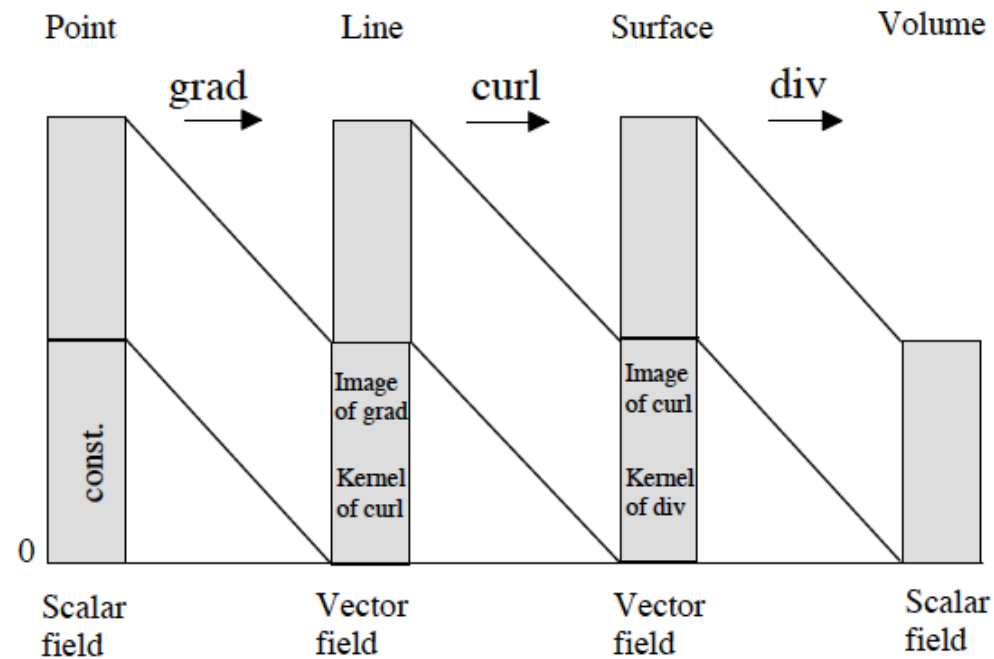
$$\int_{\mathcal{A}} \operatorname{curl} \operatorname{grad} \phi \cdot d\mathbf{a} = \int_{\partial\mathcal{A}} \operatorname{grad} \phi \cdot d\mathbf{r} = \phi|_{\partial(\partial\mathcal{A})} = 0,$$

Reversal of arguments yields two important statements (next slides):
Much nicer than writing it in coordinates

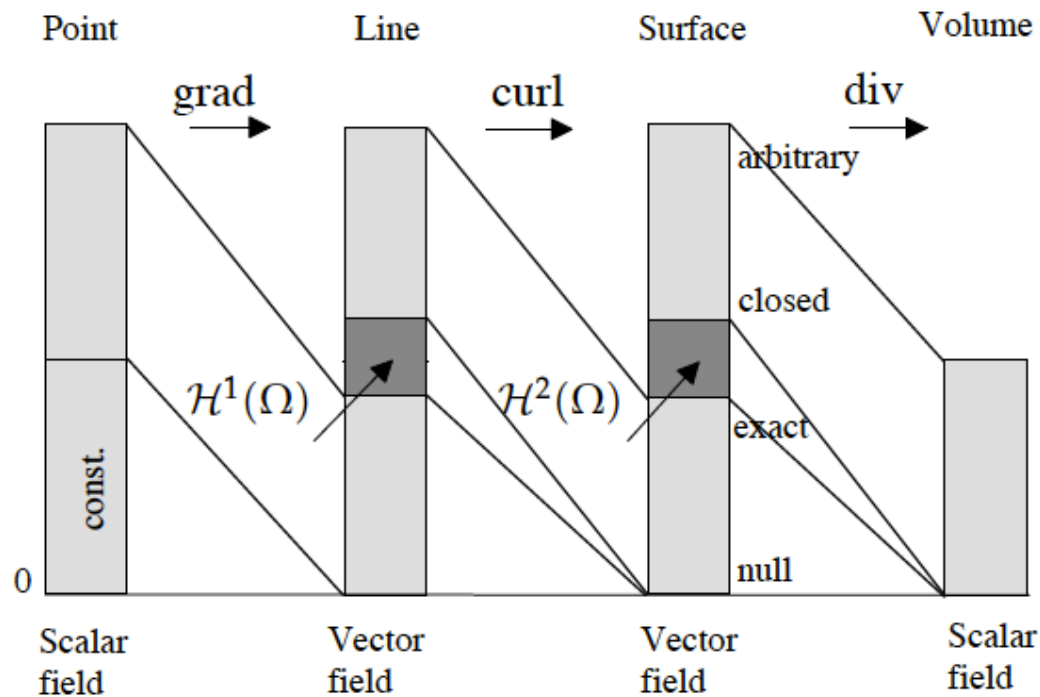
The second Lemma of Poincare (Contractible Domains)

$$\operatorname{div} \mathbf{b} = 0 \quad \rightarrow \quad \mathbf{b} = \operatorname{curl} \mathbf{a}.$$

$$\operatorname{curl} \mathbf{h} = 0 \quad \rightarrow \quad \mathbf{h} = \operatorname{grad} \phi.$$



Lemmata of Poincare (Non-Contractible Domains)



$$\mathcal{H}^1(\Omega) := \frac{\ker(\text{curl})}{\text{im}(\text{grad})}$$

$$\mathcal{H}^2(\Omega) := \frac{\ker(\text{div})}{\text{im}(\text{curl})}$$

Toroidal domain Ω in a cylindrical coordinate system (r, φ, z) :

$$H_\varphi = \frac{I}{2\pi r}$$

$$\text{curl } \mathbf{H} = \frac{1}{r} \frac{\partial}{\partial r}(r H_\varphi) = 0$$

But $\oint_C \mathbf{H} \cdot d\mathbf{s} = I$ and Ω , with $\oint_C \text{grad } \phi \cdot d\mathbf{s} = 0$

Domain Ω between two nested spheres centered at the origin.

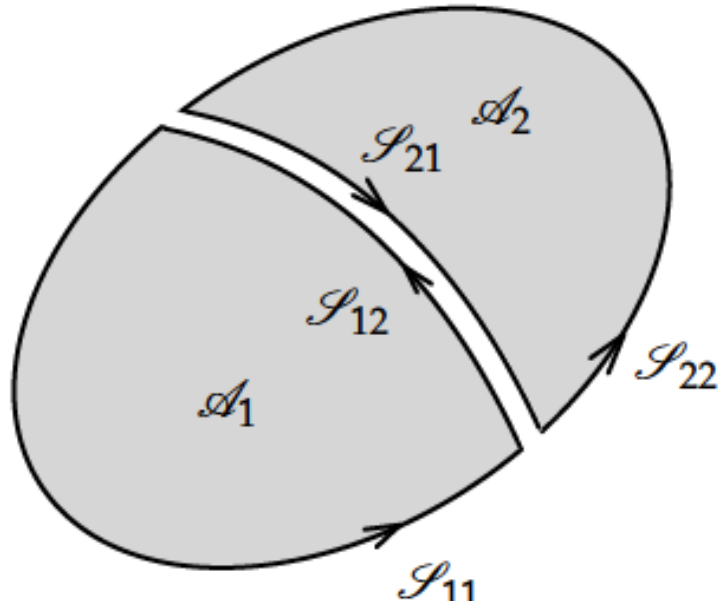
$$D_R = \frac{Q}{4\pi R^2} \mathbf{e}_R$$

$$\text{div } \mathbf{D} = \frac{1}{r^2} \frac{\partial}{\partial R}(R^2 D_R) = 0$$

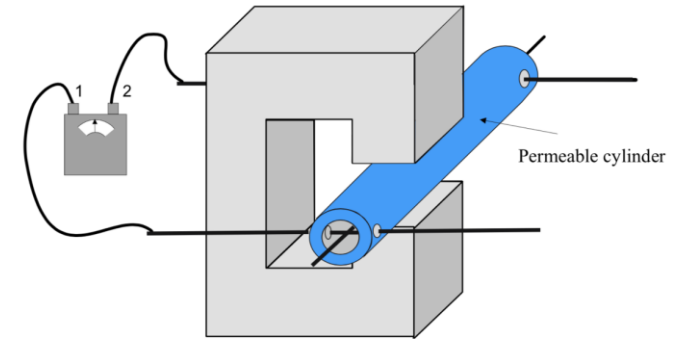
But $\oint_a \mathbf{D} \cdot d\mathbf{a} = Q$ and $\oint_a \text{curl } \mathbf{A} \cdot d\mathbf{a} = 0$

Kelvin-Stokes Theorem

Smooth vector fields, smooth surfaces with simply connected, closed, piecewise-smooth and consistently oriented boundaries, and volumes with piecewise-smooth, closed and consistently oriented surfaces.



No jump discontinuities (for example, co-moving shielding devices)

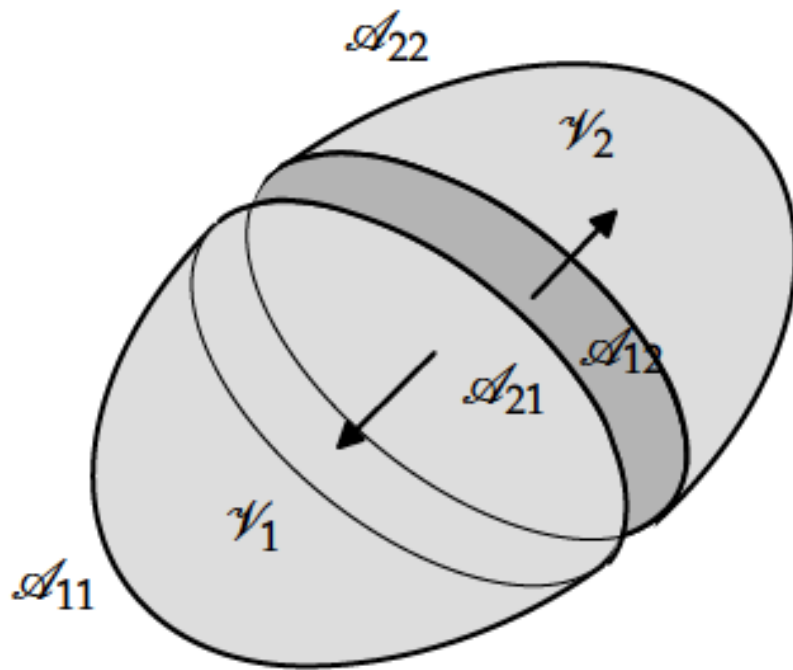


$$\int_{\partial \mathcal{A}} \mathbf{g} \cdot d\mathbf{r} = \int_{\mathcal{S}_1} \mathbf{g} \cdot d\mathbf{r} + \int_{\mathcal{S}_2} \mathbf{g} \cdot d\mathbf{r} = \int_{\mathcal{S}_{11}} \mathbf{g} \cdot d\mathbf{r} + \int_{\mathcal{S}_{22}} \mathbf{g} \cdot d\mathbf{r},$$

$$\begin{aligned} \int_{\partial \mathcal{A}} \mathbf{g} \cdot d\mathbf{r} &= \lim_{I \rightarrow \infty} \sum_{i=1}^I \int_{\partial \mathcal{A}_i} \mathbf{g} \cdot d\mathbf{r} = \lim_{I \rightarrow \infty} \sum_{i=1}^I \Delta a_i \frac{1}{\Delta a_i} \int_{\partial \mathcal{A}_i} \mathbf{g} \cdot d\mathbf{r} \\ &= \lim_{I \rightarrow \infty} \sum_{i=1}^I (\text{curl } \mathbf{g})_i \cdot \mathbf{n} \Delta a_i = \int_{\mathcal{A}} \text{curl } \mathbf{g} \cdot d\mathbf{a}. \end{aligned}$$

Gauss' Theorem

Smooth vector fields, smooth surfaces with simply connected, closed, piecewise-smooth and consistently oriented boundaries, and volumes with piecewise-smooth, closed and consistently oriented surfaces.



$$\begin{aligned}\int_{\partial\mathcal{V}} \mathbf{g} \cdot d\mathbf{a} &= \lim_{I \rightarrow \infty} \sum_{i=1}^I \int_{\partial\mathcal{V}_i} \mathbf{g} \cdot d\mathbf{a} = \lim_{I \rightarrow \infty} \sum_{i=1}^I \Delta V_i \frac{1}{\Delta V_i} \int_{\partial\mathcal{V}_i} \mathbf{g} \cdot d\mathbf{a} \\ &= \lim_{I \rightarrow \infty} \sum_{i=1}^I (\operatorname{div} \mathbf{g})_i \Delta V_i = \int_{\mathcal{V}} \operatorname{div} \mathbf{g} dV.\end{aligned}$$

$$\int_a^b f(x)g'(x) dx = [g(x)f(x)]_a^b - \int_a^b g(x)f'(x) dx$$

Green's First
$$\int_{\mathcal{V}} (\text{grad } \phi \cdot \text{grad } \psi + \phi \nabla^2 \psi) dV = \int_{\partial \mathcal{V}} \phi \partial_{\mathbf{n}} \psi da$$

Green's Second
$$\int_{\Omega} (\phi \nabla^2 \psi - \psi \nabla^2 \phi) dV = \int_{\Gamma} (\phi \partial_{\mathbf{n}} \psi - \psi \partial_{\mathbf{n}} \phi) da$$

Vector Form of Green's Second

$$\int_{\mathcal{V}} \mathbf{a} \cdot \text{curl } \mathbf{b} dV = \int_{\mathcal{V}} \mathbf{b} \cdot \text{curl } \mathbf{a} dV - \int_{\partial \mathcal{V}} \mathbf{a} \cdot (\mathbf{b} \times \mathbf{n}) da$$

Generalization of the Integration by Parts Rule

$$- \int_{\mathcal{V}} \mathbf{a} \cdot \text{grad } \phi dV = \int_{\mathcal{V}} \phi \text{div } \mathbf{a} dV - \int_{\partial \mathcal{V}} \phi (\mathbf{a} \cdot \mathbf{n}) da$$

Stratton #1 and #2

$$\int_{\mathcal{V}} \text{div}(\mathbf{a} \times \text{curl } \mathbf{b}) dV = \int_{\partial \mathcal{V}} (\mathbf{a} \times \text{curl } \mathbf{b}) \cdot \mathbf{n} da$$

$$\int_{\mathcal{V}} (\mathbf{a} \text{curl curl } \mathbf{b} - \mathbf{b} \text{curl curl } \mathbf{a}) dV = \int_{\partial \mathcal{V}} (\mathbf{b} \times \text{curl } \mathbf{a} - \mathbf{a} \times \text{curl } \mathbf{b}) \cdot \mathbf{n} da$$

Maxwell's Equations in Different Avatars



Maxwell's Equations in Different Avatars

Maxwell Equations

Integral Form

Local Form

Global Form

Laplace's Equation

Curl-Curl Equation

Harmonic Fields

Green's Functions

Weak-Forms

Kirchhoff's Theorem

Lumped circuit
calc. of NC
magnets

Field quality in
Accelerator magnets

The field of
line-currents
Coil-dominated
magnets

FEM

BEM

DEM



Maxwell Equations I: Global Form

Ampere +
Maxwell extension

$$V_m(\partial\mathcal{A}) = I(\mathcal{A}) + \frac{d}{dt}\Psi(\mathcal{A}),$$

Faraday

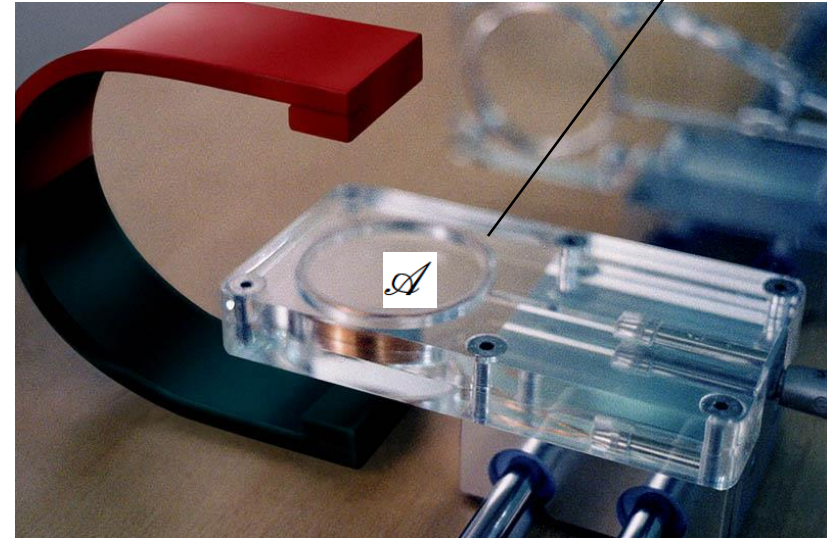
$$U(\partial\mathcal{A}) = -\frac{d}{dt}\Phi(\mathcal{A}),$$

Flux conservation

$$\Phi(\partial\mathcal{V}) = 0,$$

Gauss

$$\Psi(\partial\mathcal{V}) = Q(\mathcal{V}).$$



Required: Orientable manifolds

No switches, no Moebius strips

Maxwell Equations II: Integral Form

Global quantity	SI unit	Relation	SI unit	Field
MMF	1 A	$V_m(\mathcal{S}) = \int_{\mathcal{S}} \mathbf{H} \cdot d\mathbf{r}$	1 A m^{-1}	Magnetic field
Electric voltage	1 V	$U(\mathcal{S}) = \int_{\mathcal{S}} \mathbf{E} \cdot d\mathbf{r}$	1 V m^{-1}	Electric field
Magnetic flux	1 V s	$\Phi(\mathcal{A}) = \int_{\mathcal{A}} \mathbf{B} \cdot d\mathbf{a}$	1 V s m^{-2}	Magnetic flux density
Electric flux	1 A s	$\Psi(\mathcal{A}) = \int_{\mathcal{A}} \mathbf{D} \cdot d\mathbf{a}$	1 A s m^{-2}	Electric flux density
Electric current	1 A	$I(\mathcal{A}) = \int_{\mathcal{A}} \mathbf{J} \cdot d\mathbf{a}$	1 A m^{-2}	Electric current density
Electric charge	1 A s	$Q(\mathcal{V}) = \int_{\mathcal{V}} \rho \cdot dV$	1 A s m^{-3}	Electric charge density

$$\int_{\partial\mathcal{A}} \mathbf{H} \cdot d\mathbf{r} = \int_{\mathcal{A}} \mathbf{J} \cdot d\mathbf{a} + \frac{d}{dt} \int_{\mathcal{A}} \mathbf{D} \cdot d\mathbf{a},$$

$$\int_{\partial\mathcal{A}} \mathbf{E} \cdot d\mathbf{r} = -\frac{d}{dt} \int_{\mathcal{A}} \mathbf{B} \cdot d\mathbf{a},$$

$$\int_{\partial\mathcal{V}} \mathbf{B} \cdot d\mathbf{a} = 0,$$

$$\int_{\partial\mathcal{V}} \mathbf{D} \cdot d\mathbf{a} = \int_{\mathcal{V}} \rho dV.$$

Required: Orientable manifolds,
orientation, frame, metric, continuity

No switches, no Moebius strips

Maxwell's Equations in Local Form

$$\int_{\mathcal{A}} \text{curl } \mathbf{g} \cdot d\mathbf{a} = \int_{\partial\mathcal{A}} \mathbf{g} \cdot d\mathbf{r},$$

$$\int_{\mathcal{V}} \text{div } \mathbf{g} dV = \int_{\partial\mathcal{V}} \mathbf{g} \cdot d\mathbf{a},$$

$$\int_{\partial\mathcal{A}} \mathbf{H} \cdot d\mathbf{r} = \int_{\mathcal{A}} \mathbf{J} \cdot d\mathbf{a} + \frac{d}{dt} \int_{\mathcal{A}} \mathbf{D} \cdot d\mathbf{a},$$

$$\int_{\partial\mathcal{A}} \mathbf{E} \cdot d\mathbf{r} = -\frac{d}{dt} \int_{\mathcal{A}} \mathbf{B} \cdot d\mathbf{a},$$

$$\int_{\partial\mathcal{V}} \mathbf{B} \cdot d\mathbf{a} = 0,$$

$$\int_{\partial\mathcal{V}} \mathbf{D} \cdot d\mathbf{a} = \int_{\mathcal{V}} \rho dV.$$

$$\int_{\mathcal{A}} \text{curl } \mathbf{H} \cdot d\mathbf{a} = \int_{\mathcal{A}} \left(\mathbf{J} + \frac{\partial}{\partial t} \mathbf{D} \right) \cdot d\mathbf{a},$$

$$\int_{\mathcal{A}} \text{curl } \mathbf{E} \cdot d\mathbf{a} = -\int_{\mathcal{A}} \frac{\partial}{\partial t} \mathbf{B} \cdot d\mathbf{a},$$

$$\int_{\mathcal{V}} \text{div } \mathbf{B} dV = 0,$$

$$\int_{\mathcal{V}} \text{div } \mathbf{D} dV = \int_{\mathcal{V}} \rho dV.$$

$$\text{curl } \mathbf{H} = \mathbf{J} + \frac{\partial}{\partial t} \mathbf{D},$$

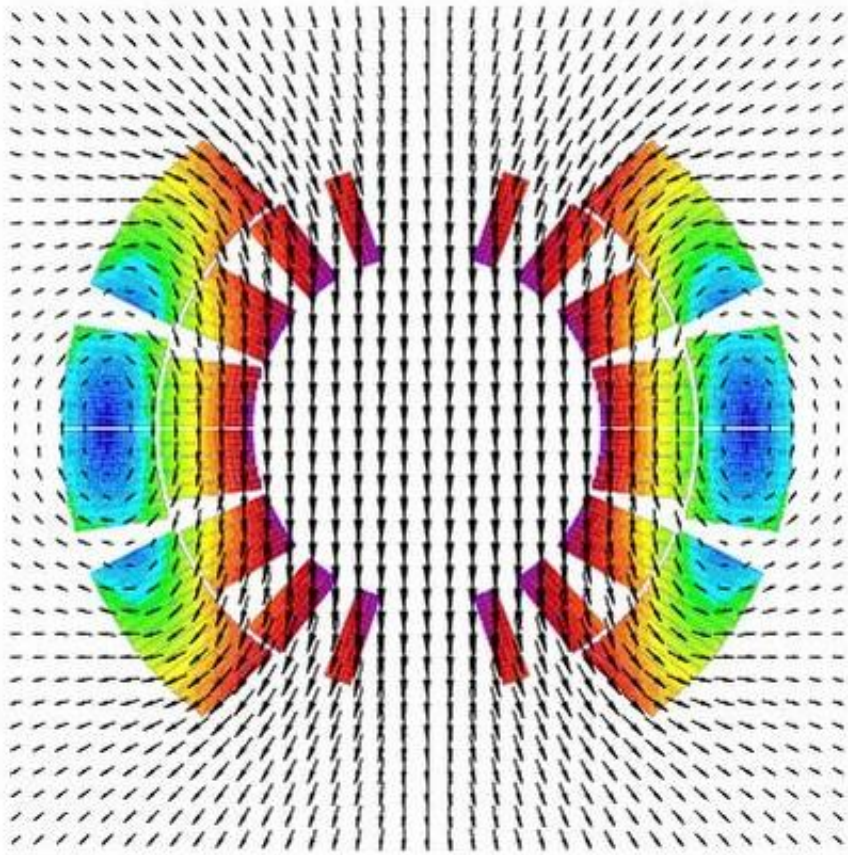
$$\text{curl } \mathbf{E} = -\frac{\partial}{\partial t} \mathbf{B},$$

$$\text{div } \mathbf{B} = 0,$$

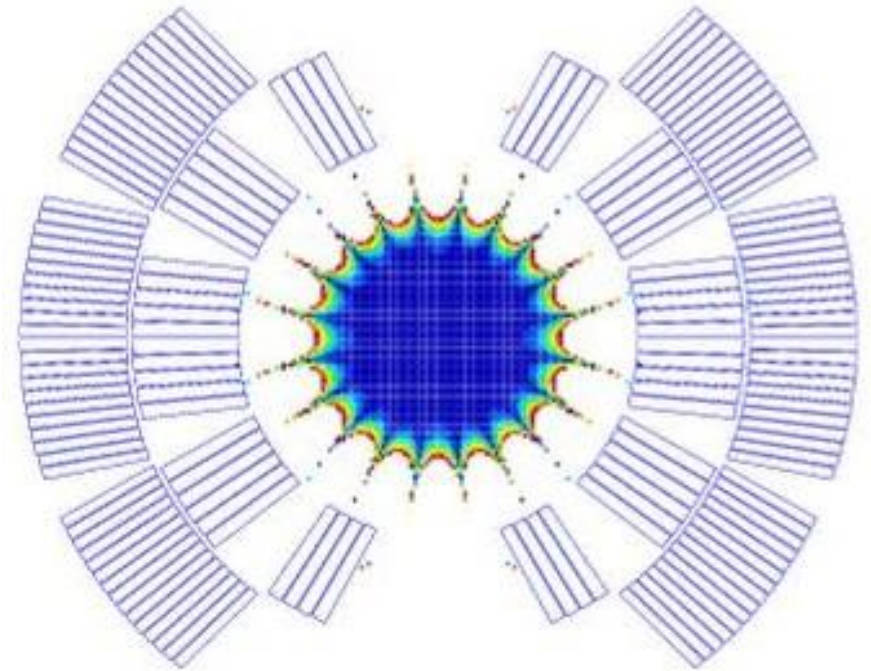
$$\text{div } \mathbf{D} = \rho.$$

Harmonic Fields





Field map



Good field region

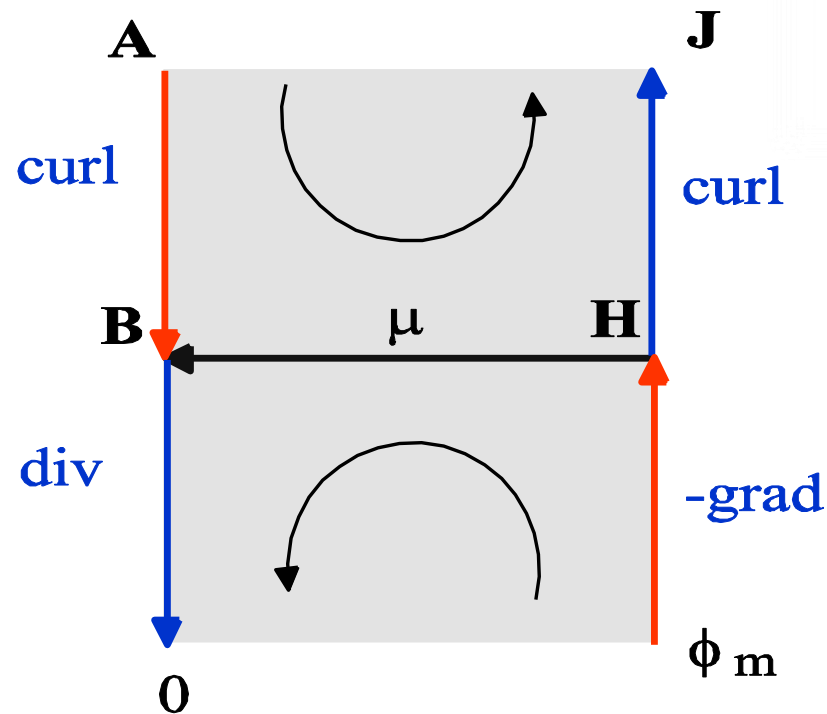
Maxwell's Facade

$$\text{curl} \frac{1}{\mu} \text{curl} \mathbf{A} = \mathbf{J}$$

$$\frac{1}{\mu_0} \text{curl} \text{curl} \mathbf{A} = \mathbf{J}$$

$$\nabla^2 \mathbf{A} - \text{grad} \text{div} \mathbf{A} = 0$$

$$\nabla^2 A_z = 0$$



$$\text{div} \mu \text{grad} \phi_m = 0$$

$$\mu_0 \text{div} \text{grad} \phi_m = 0$$

$$\nabla^2 \phi_m = 0$$

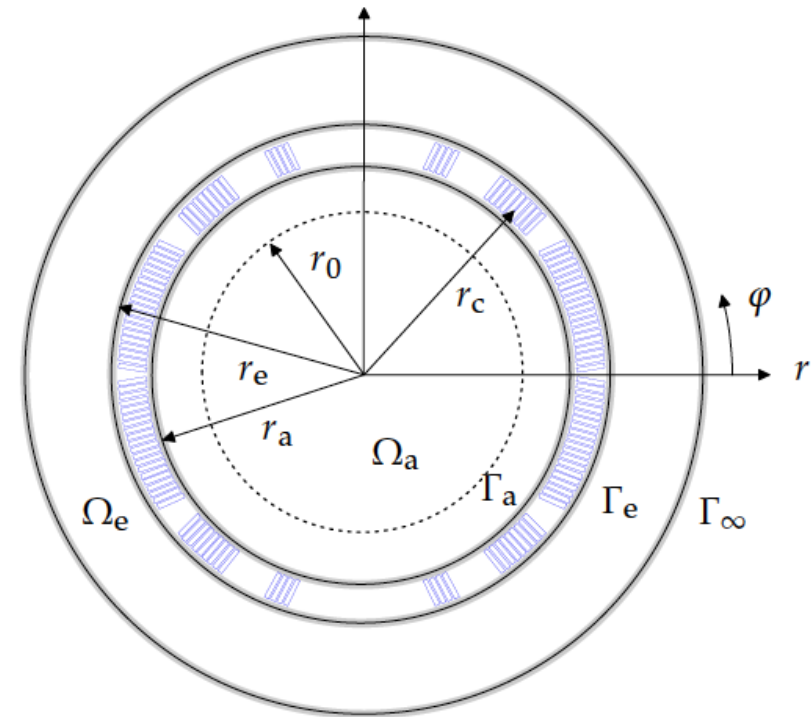
Solving of Boundary Value Problems

1. Governing equation in the air domain

$$\nabla^2 A_z = 0,$$

2. Chose a suitable coordinate system

$$r^2 \frac{\partial^2 A_z}{\partial r^2} + r \frac{\partial A_z}{\partial r} + \frac{\partial^2 A_z}{\partial \varphi^2} = 0,$$



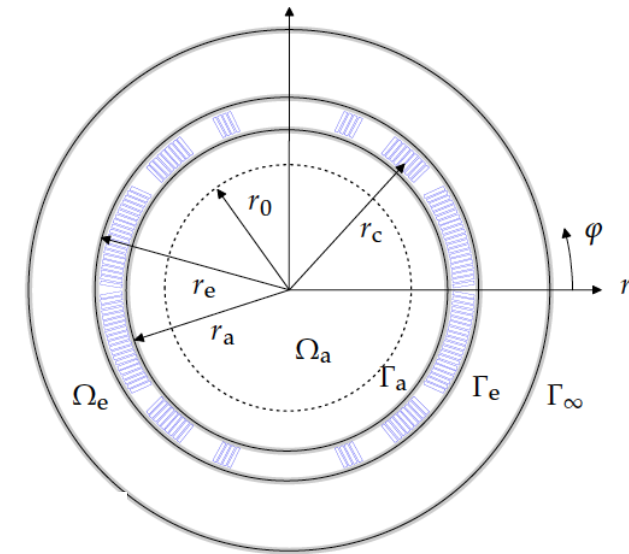
3. Find eigenfunctions. Coefficients are not know yet

$$A_z(r, \varphi) = \sum_{n=1}^{\infty} (\mathcal{E}_n r^n + \mathcal{F}_n r^{-n}) (\mathcal{G}_n \sin n\varphi + \mathcal{H}_n \cos n\varphi).$$

Solving of Boundary Value Problems

4. Incorporate a bit of knowledge and rename

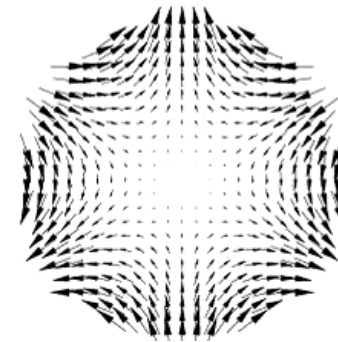
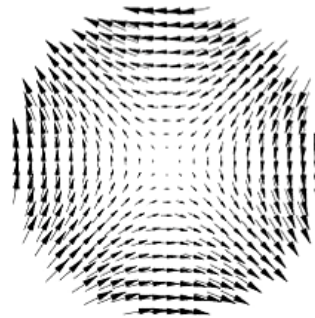
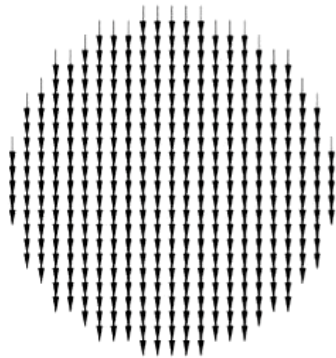
$$A_z(r, \varphi) = \sum_{n=1}^{\infty} r^n (\mathcal{A}_n \sin n\varphi + \mathcal{B}_n \cos n\varphi).$$



5. Calculate a field component

$$B_r(r, \varphi) = \frac{1}{r} \frac{\partial A_z}{\partial \varphi} = \sum_{n=1}^{\infty} n r^{n-1} (\mathcal{A}_n \cos n\varphi - \mathcal{B}_n \sin n\varphi),$$

$$B_\varphi(r, \varphi) = -\frac{\partial A_z}{\partial r} = -\sum_{n=1}^{\infty} n r^{n-1} (\mathcal{A}_n \sin n\varphi + \mathcal{B}_n \cos n\varphi),$$

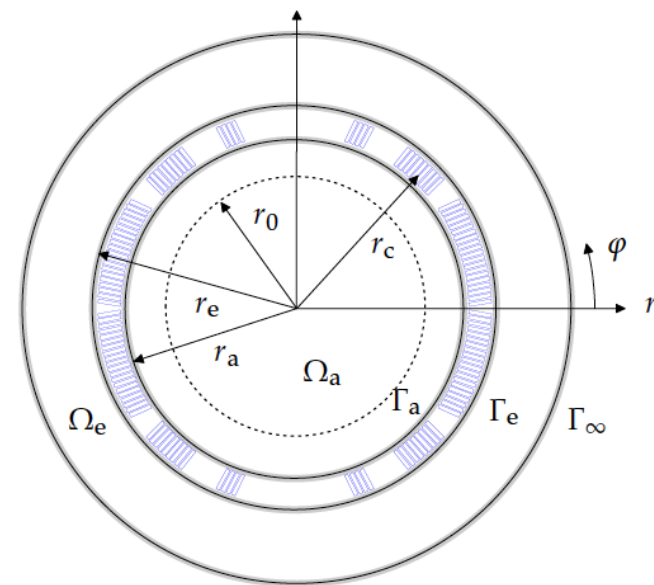


Solving of Boundary Value Problems

$$B_r(r, \varphi) = \frac{1}{r} \frac{\partial A_z}{\partial \varphi} = \sum_{n=1}^{\infty} n r^{n-1} (\mathcal{A}_n \cos n\varphi - \mathcal{B}_n \sin n\varphi),$$

6. Measure or calculate the field on a reference radius and perform Fourier analysis (develop into the eigenfunctions). **Coefficients known here.**

$$B_r(r_0, \varphi) = \sum_{n=1}^{\infty} (B_n(r_0) \sin n\varphi + A_n(r_0) \cos n\varphi),$$



Solving the Boundary Value Problem

7: Compare the known and unknown coefficients

$$B_r(r, \varphi) = \frac{1}{r} \frac{\partial A_z}{\partial \varphi} = \sum_{n=1}^{\infty} n r^{n-1} (\mathcal{A}_n \cos n\varphi - \mathcal{B}_n \sin n\varphi),$$

$$B_r(r_0, \varphi) = \sum_{n=1}^{\infty} (B_n(r_0) \sin n\varphi + A_n(r_0) \cos n\varphi),$$

$$\mathcal{A}_n = \frac{1}{n r_0^{n-1}} A_n(r_0), \quad \mathcal{B}_n = \frac{-1}{n r_0^{n-1}} B_n(r_0).$$

8. Put this into the original solution for the entire air domain

$$A_z(r, \varphi) = - \sum_{n=1}^{\infty} \frac{r_0}{n} \left(\frac{r}{r_0} \right)^n (B_n(r_0) \cos n\varphi - A_n(r_0) \sin n\varphi).$$

Solving the Boundary Value Problem

9: Calculate fields and potential in the entire air domain

$$A_z(r, \varphi) = - \sum_{n=1}^{\infty} \frac{r_0}{n} \left(\frac{r}{r_0} \right)^n (B_n(r_0) \cos n\varphi - A_n(r_0) \sin n\varphi).$$

$$B_r(r, \varphi) = \sum_{n=1}^{\infty} \left(\frac{r}{r_0} \right)^{n-1} (B_n(r_0) \sin n\varphi + A_n(r_0) \cos n\varphi)$$

$$B_\varphi(r, \varphi) = \sum_{n=1}^{\infty} \left(\frac{r}{r_0} \right)^{n-1} (B_n(r_0) \cos n\varphi - A_n(r_0) \sin n\varphi)$$

$$B_x(r, \varphi) = \sum_{n=1}^{\infty} \left(\frac{r}{r_0} \right)^{n-1} (B_n(r_0) \sin(n-1)\varphi + A_n(r_0) \cos(n-1)\varphi)$$

$$B_y(r, \varphi) = \sum_{n=1}^{\infty} \left(\frac{r}{r_0} \right)^{n-1} (B_n(r_0) \cos(n-1)\varphi - A_n(r_0) \sin(n-1)\varphi)$$

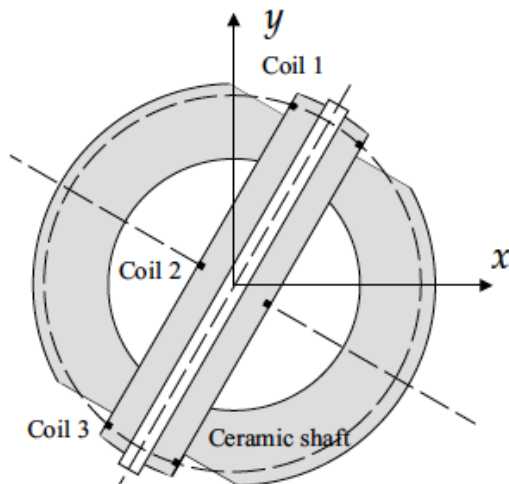
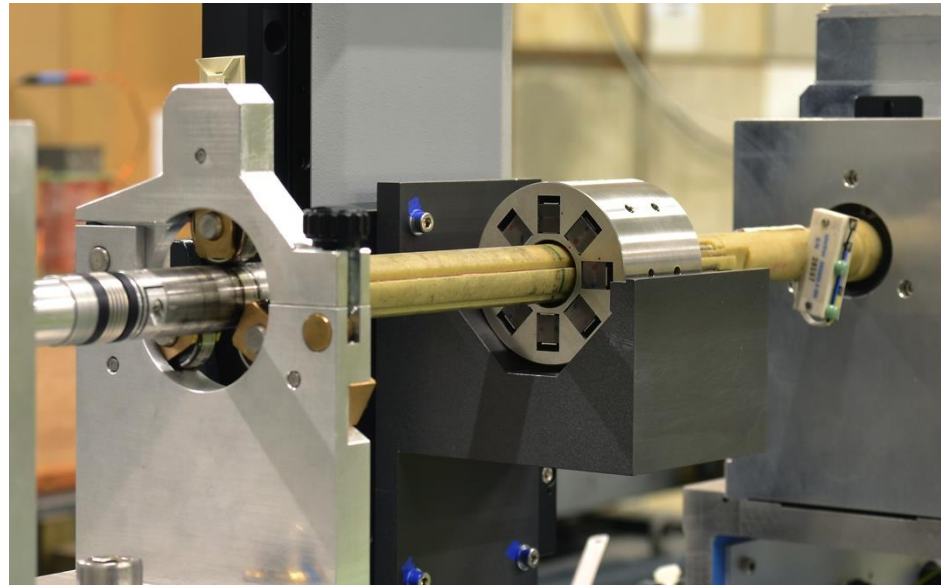
$$B_r(r, \varphi) = \sum_{n=1}^{\infty} \left(\frac{r}{r_0}\right)^{n-1} (B_n(r_0) \sin n\varphi + A_n(r_0) \cos n\varphi)$$

$$B_r(r, \varphi) = B_N \sum_{n=1}^{\infty} \left(\frac{r}{r_0}\right)^{n-N} (b_n(r_0) \sin n\varphi + a_n(r_0) \cos n\varphi).$$

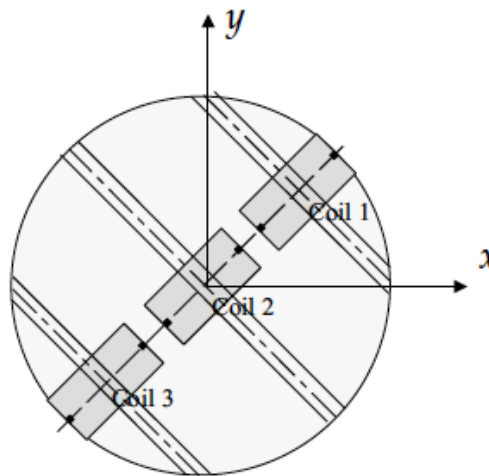
$$A_n(r_1) = \left(\frac{r_1}{r_0}\right)^{n-1} A_n(r_0), \quad B_n(r_1) = \left(\frac{r_1}{r_0}\right)^{n-1} B_n(r_0),$$

$$b_n(r_1) = \frac{B_n(r_1)}{B_N(r_1)} = \frac{\left(\frac{r_1}{r_0}\right)^{n-1} B_n(r_0)}{\left(\frac{r_1}{r_0}\right)^{N-1} B_N(r_0)} = \left(\frac{r_1}{r_0}\right)^{n-N} b_n(r_0),$$

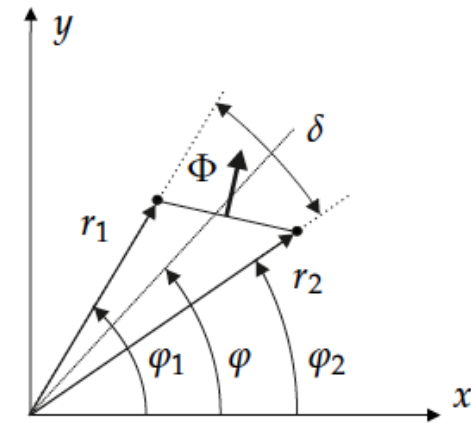
Rotating Coil Measurements



Tangential coil
Radial flux



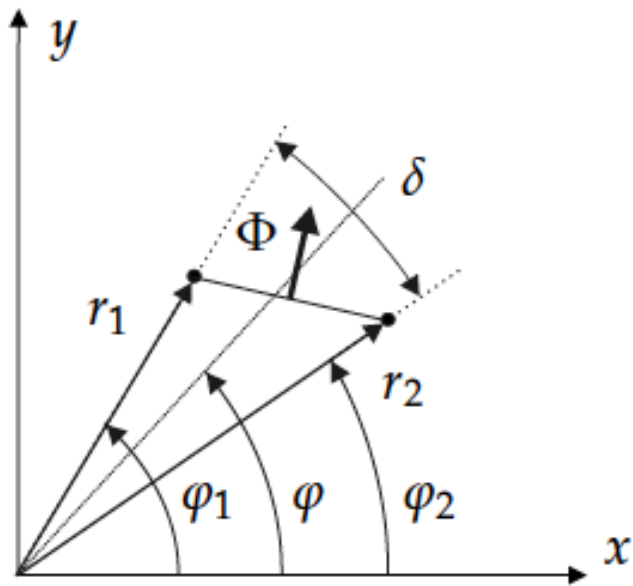
Radial coil
Tangential flux



Rotating Coil Measurements

$$\begin{aligned}\Phi(\varphi) &= N \int_{\mathcal{A}} \mathbf{B} \cdot d\mathbf{a} = N \int_{\mathcal{A}} \text{curl } \mathbf{A} \cdot d\mathbf{a} = N \int_{\partial\mathcal{A}} \mathbf{A} \cdot d\mathbf{r} \\ &= N\ell [A_z(\mathcal{P}_1) - A_z(\mathcal{P}_2)],\end{aligned}$$

$$\begin{aligned}\Phi(\varphi) &= N\ell \left[\sum_{n=1}^{\infty} \frac{r_0}{n} \left(\frac{r_2}{r_0}\right)^n (B_n(r_0) \cos n\varphi_2 - A_n(r_0) \sin n\varphi_2) \right. \\ &\quad \left. - \sum_{n=1}^{\infty} \frac{r_0}{n} \left(\frac{r_1}{r_0}\right)^n (B_n(r_0) \cos n\varphi_1 - A_n(r_0) \sin n\varphi_1) \right],\end{aligned}$$



$$\begin{aligned}\Phi(\varphi) &= \sum_{n=1}^{\infty} S_n^{\text{rad}} (B_n(r_0) \cos n\varphi - A_n(r_0) \sin n\varphi) \\ &\quad + S_n^{\text{tan}} (B_n(r_0) \sin n\varphi + A_n(r_0) \cos n\varphi)\end{aligned}$$

$$S_n^{\text{rad}} = \frac{N\ell}{nr_0^{n-1}} \left[r_2^n \cos n(\varphi_2 - \varphi) - r_1^n \cos n(\varphi_1 - \varphi) \right],$$

$$S_n^{\text{tan}} = -\frac{N\ell}{nr_0^{n-1}} \left[r_2^n \sin n(\varphi_2 - \varphi) - r_1^n \sin n(\varphi_1 - \varphi) \right],$$

Cartesian Coordinates (Eigensolutions for the Ideal Dipole)

$$\phi_m = X(x)Y(y)$$

$$\underbrace{\frac{1}{X(x)} \frac{d^2 X(x)}{dx^2}}_{p^2} + \underbrace{\frac{1}{Y(y)} \frac{d^2 Y(y)}{dy^2}}_{-p^2} = 0$$

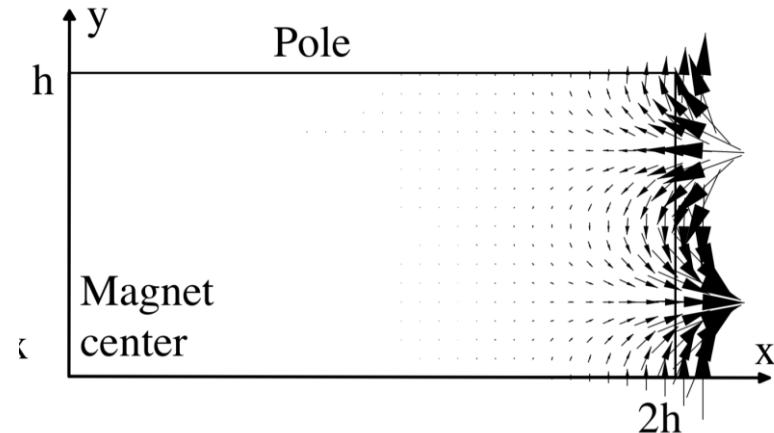
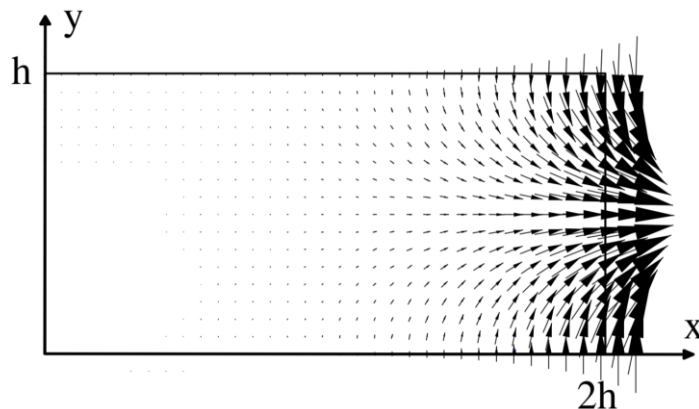
$$X_p(x) = C_p \cos px + D_p \sin px,$$

$$p = n \frac{2\pi}{\lambda} =: nk_0.$$

$$Y_p(y) = \mathcal{E}_p \cosh py + \mathcal{F}_p \sinh py,$$

$$B_x(x, y) = \mu_0 \sum_{n=1}^{\infty} \mathcal{A}_n \sinh\left(\frac{n\pi}{h}x\right) \sin\left(\frac{n\pi}{h}y\right),$$

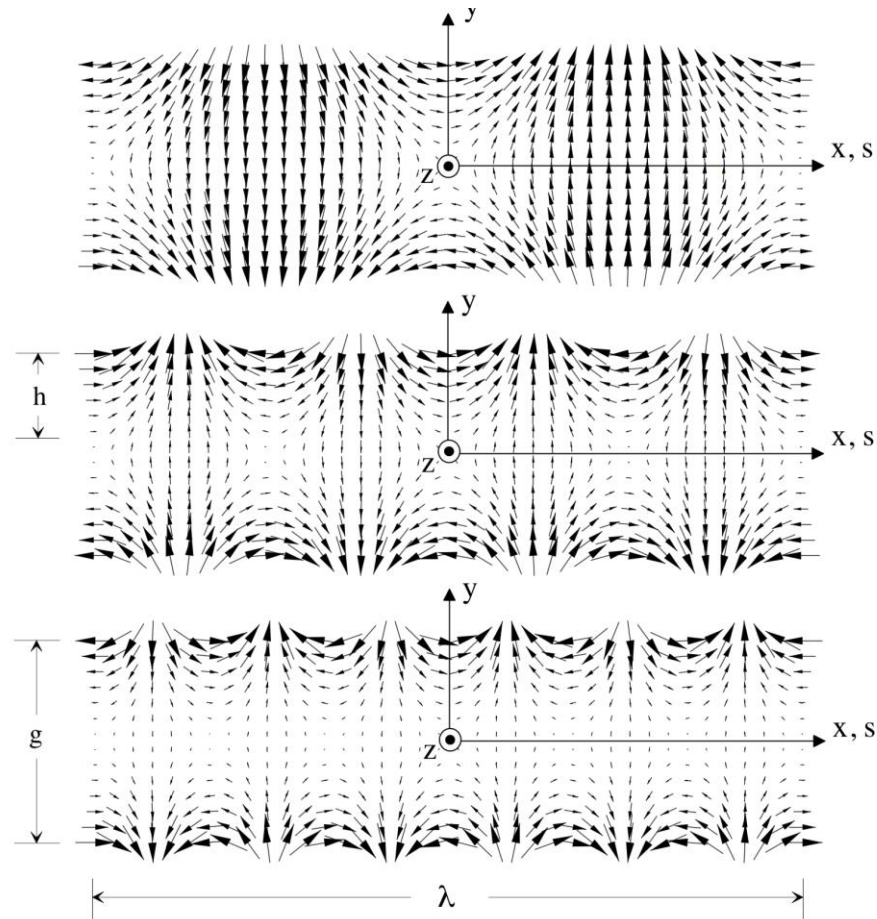
$$B_y(x, y) = B_0 + \mu_0 \sum_{n=1}^{\infty} \mathcal{A}_n \cosh\left(\frac{n\pi}{h}x\right) \cos\left(\frac{n\pi}{h}y\right).$$



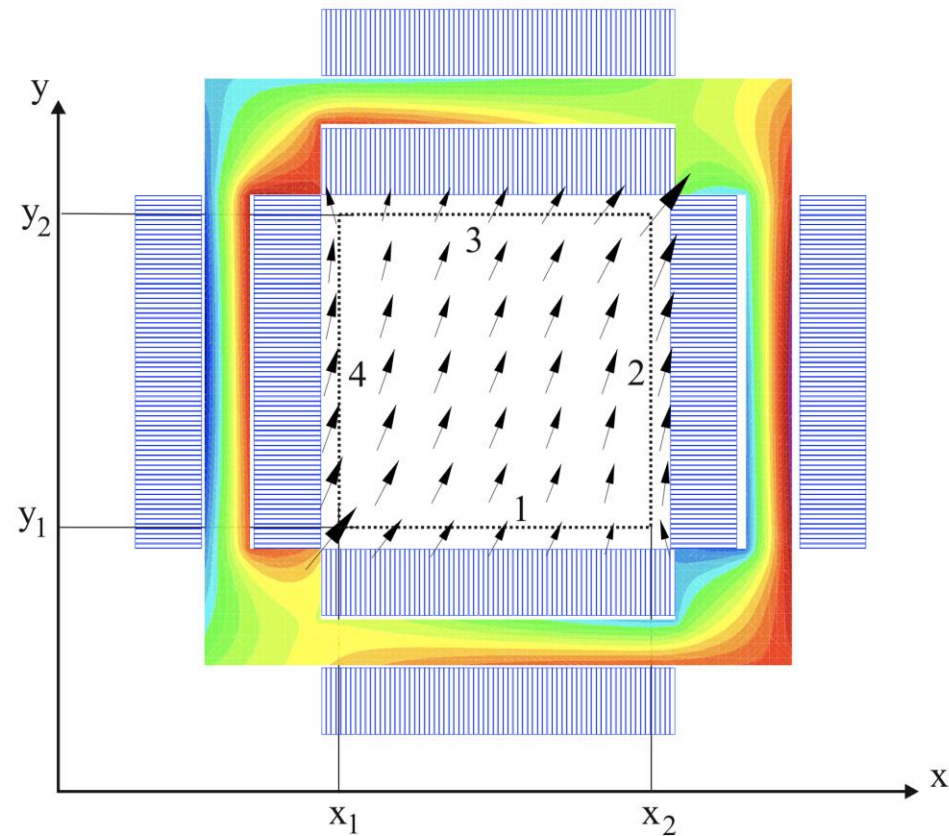
Cartesian Coordinates (Eigensolutions for the Wiggler)

$$B_x(x, y) = \mu_0 \sum_{n=1}^{\infty} (-\mathcal{A}_n \sin(nk_0x) + \mathcal{B}_n \cos(nk_0x)) \sinh(nk_0y) ,$$

$$B_y(x, y) = \mu_0 \sum_{n=1}^{\infty} (\mathcal{A}_n \cos(nk_0x) + \mathcal{B}_n \sin(nk_0x)) \cosh(nk_0y) .$$

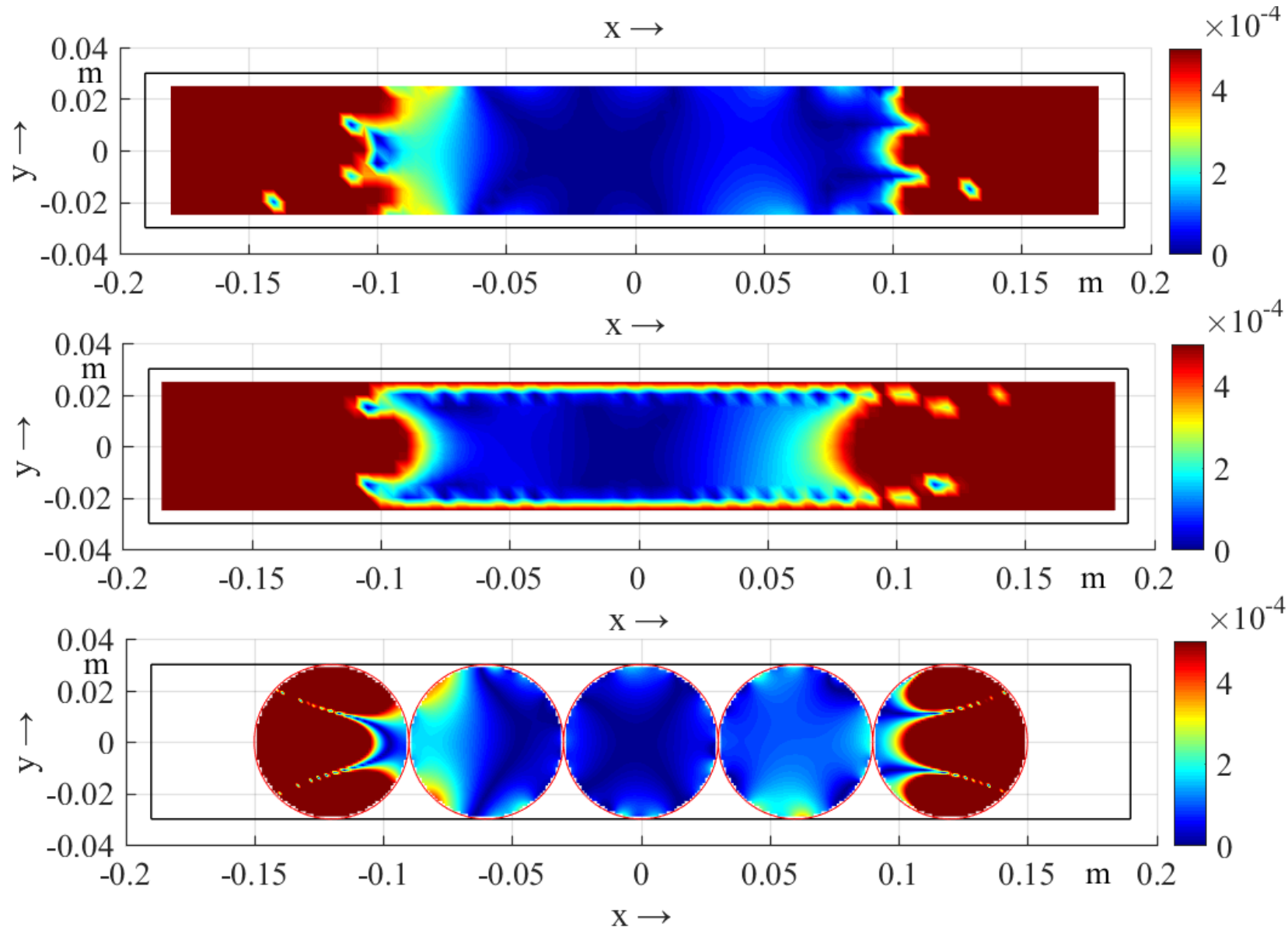


Determining the Coefficients



$$A_z^{(1)}(x, y) = \sum_n A_n^{(1)} \frac{\sinh\left(n\pi \frac{y_2 - y}{x_2 - x_1}\right)}{\sinh\left(n\pi \frac{y_2 - y_1}{x_2 - x_1}\right)} \sin\left(n\pi \frac{x_2 - x}{x_2 - x_1}\right)$$

Field Reconstruction from Boundary Data



Theorems on Harmonic Fields

Theorem 5.1 *If ϕ is harmonic in the closed contractible volume $\mathcal{V} \subset \Omega$ bounded by the surface $\partial\mathcal{V}$, the surface integral of the normal derivative of ϕ vanishes.*

Flux in = flux out

Theorem 5.2 *If ϕ is harmonic in the closed, contractible volume $\mathcal{V} \subset \Omega$, bounded by the surface $\partial\mathcal{V}$, with the same magnitude at all points on that surface, then ϕ is constant throughout \mathcal{V} and equal to its value ϕ_0 on the boundary.*

Faraday cage

Theorem 5.3 *If ϕ is harmonic in the closed contractible volume $\mathcal{V} \subset \Omega$ bounded by $\partial\mathcal{V}$ and its value is specified at each point of that boundary, then ϕ is uniquely determined at all points inside the volume.*

Determine fields by Fourier analysis on boundary

Theorem 5.5 (Liouville) *If ϕ is a harmonic scalar field in E_n with an upper (or lower) bound, ϕ is constant.*

Watch out for singularities (sources of the field), maximum field at the boundary

$$\mathbf{H} = -\text{grad } \phi = -\frac{\partial \phi}{\partial x} \mathbf{e}_x - \frac{\partial \phi}{\partial y} \mathbf{e}_y,$$

$$\mathbf{B} = \text{curl}(\mathbf{e}_z A_z) = \frac{\partial A_z}{\partial y} \mathbf{e}_x - \frac{\partial A_z}{\partial x} \mathbf{e}_y.$$

This implies

$$\frac{\partial A_z}{\partial y} = -\mu_0 \frac{\partial \phi}{\partial x} \quad \text{and} \quad \frac{\partial A_z}{\partial x} = \mu_0 \frac{\partial \phi}{\partial y},$$

Which are the Cauchy Riemann equations of

$$w(z) := u(x, y) + iv(x, y) = A_z(x, y) + i\mu_0 \phi(x, y).$$

$$-\frac{dw}{dz} = -\frac{\partial A_z}{\partial x} - i\mu_0 \frac{\partial \phi}{\partial x} = i\frac{\partial A_z}{\partial y} - \mu_0 \frac{\partial \phi}{\partial y} = B_y(x, y) + iB_x(x, y) =: B(z).$$

Theorem 9.2 *Real and imaginary parts of a holomorphic function are harmonic functions.*

Proof. If $f(z) = f(x, y) = u(x, y) + iv(x, y)$ is holomorphic, the Cauchy-Riemann equations yield

$$\nabla^2 u = \frac{\partial}{\partial x} \left(\frac{\partial u}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{\partial u}{\partial y} \right) = \frac{\partial}{\partial x} \left(\frac{\partial v}{\partial y} \right) + \frac{\partial}{\partial y} \left(-\frac{\partial v}{\partial x} \right) = 0,$$

$$\nabla^2 v = \frac{\partial}{\partial x} \left(\frac{\partial v}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{\partial v}{\partial y} \right) = \frac{\partial}{\partial x} \left(-\frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial y} \left(\frac{\partial u}{\partial x} \right) = 0.$$

Complex Representation of the Field in Accelerator Magnets

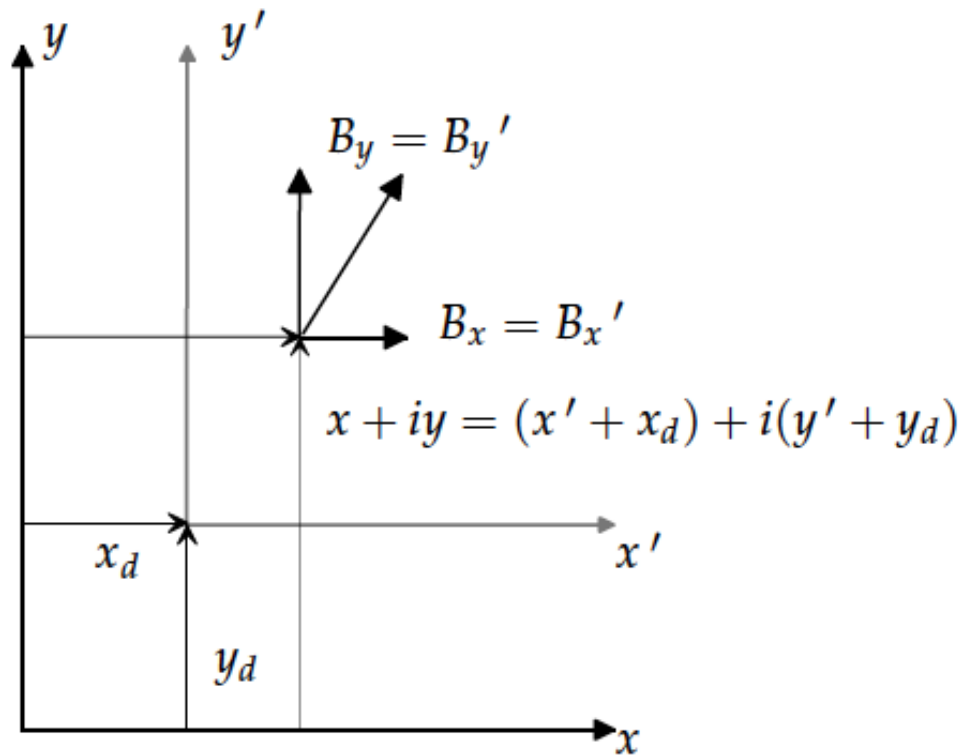
$$B_x = B_r \cos \varphi - B_\varphi \sin \varphi, \quad B_y = B_r \sin \varphi + B_\varphi \cos \varphi,$$

$$B_y + iB_x = (B_\varphi + iB_r)e^{-i\varphi}.$$

$$\begin{aligned} B_y + iB_x &= \sum_{n=1}^{\infty} (B_n(r_0) + iA_n(r_0)) \left(\frac{r}{r_0}\right)^{n-1} e^{i(n-1)\varphi} \\ &= \sum_{n=1}^{\infty} (B_n(r_0) + iA_n(r_0)) \left(\frac{z}{r_0}\right)^{n-1} \\ &= B_N \sum_{n=1}^{\infty} (b_n(r_0) + i a_n(r_0)) \left(\frac{z}{r_0}\right)^{n-1}, \end{aligned}$$

$$b_n = \frac{r^{n-1}}{B_N} \frac{1}{(n-1)!} \left. \frac{d^{n-1} B_y}{dx^{n-1}} \right|_{x=y=0}$$

Feed-down (Holomorphic Continuation)



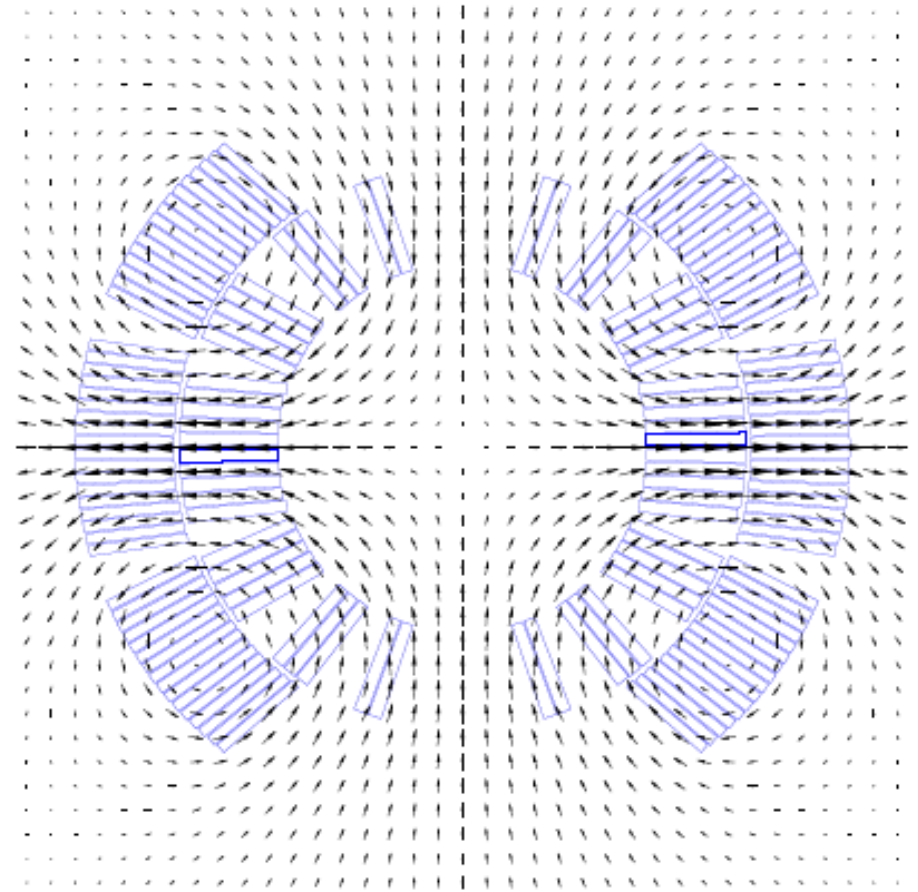
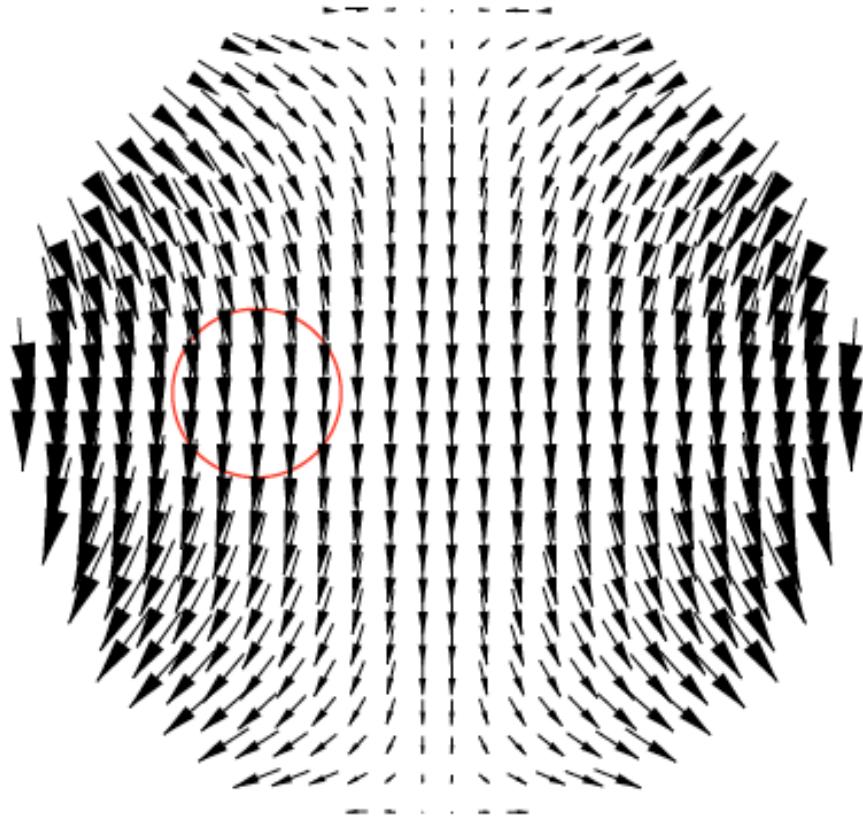
$$\sum_{n=1}^{\infty} C_n \left(\frac{z}{r_0} \right)^{n-1} \stackrel{!}{=} \sum_{n=1}^{\infty} C'_n \left(\frac{z'}{r_0} \right)^{n-1},$$

$$\binom{n}{p} = \frac{n!}{p!(n-p)!} \text{ for } 0 \leq p \leq n$$

$$C'_n = \sum_{k=n}^{\infty} C_k \binom{k-1}{n-1} \left(\frac{z_d}{r_0} \right)^{k-n}.$$

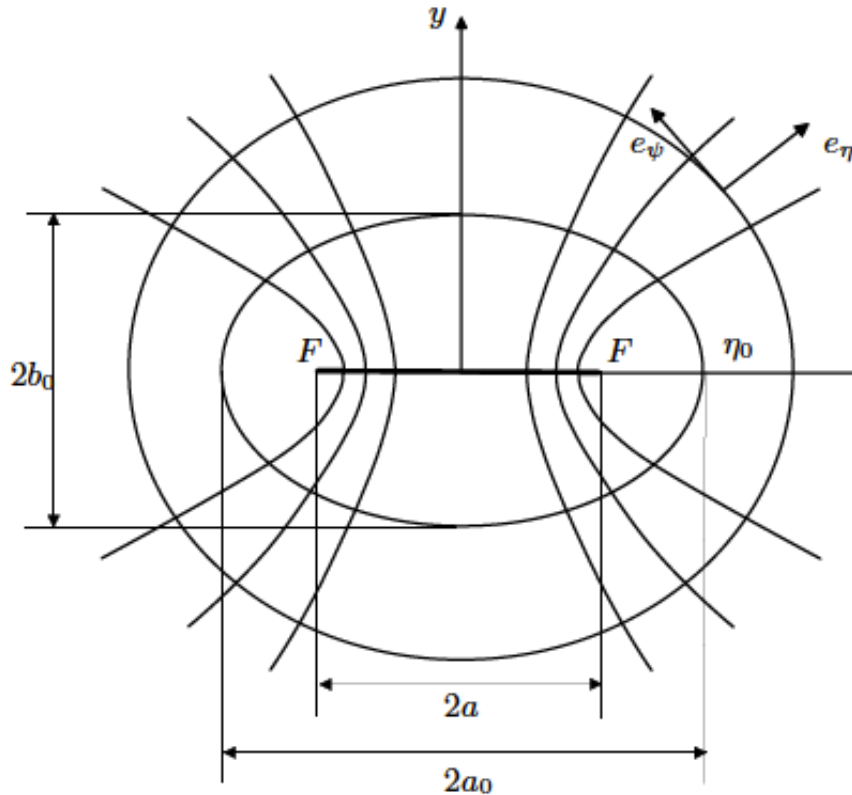
$$C'_2 = C_2 + 2 C_3 \left(\frac{z_d}{r_0} \right) + 3 C_4 \left(\frac{z_d}{r_0} \right)^2 + \dots,$$

Feed-down: Enemy and Friend



Elliptical Harmonics

$$B_\eta(\eta, \psi) = \frac{1}{h_2} \sum_{n=1}^{\infty} (n \mathcal{A}_n \sinh n\eta \cos n\psi - n \mathcal{B}_n \cosh n\eta \sin n\psi) .$$



$$B_\eta = \frac{1}{h_1} (a \sinh \eta \cos \psi B_x + a \cosh \eta \sin \psi B_y) .$$

$$B_\eta(\eta_0, \psi) = \sum_{n=1}^{\infty} (B_n(\eta_0) \sin n\psi + A_n(\eta_0) \cos n\psi),$$

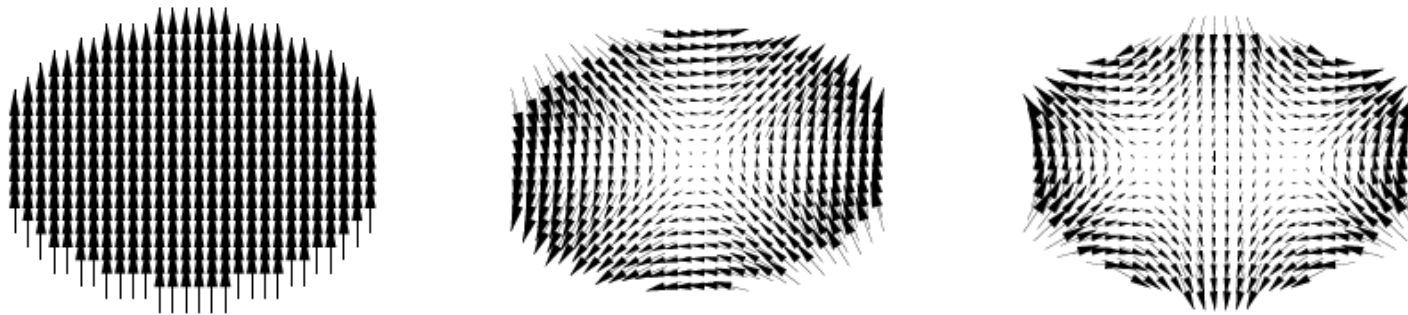
$$h_1 = h_2 = a \sqrt{\cosh^2 \eta - \cos^2 \psi} .$$

Solution: Use covariant derivative, i.e, differential forms (Auchmann, Kurz, Petrone, Russenschuck 2015)

Metric-Free Elliptic Multipoles

$$\tilde{B}_\eta = \frac{\partial A_z}{\partial \psi} \quad \tilde{B}_\psi = \frac{\partial A_z}{\partial \eta} .$$

$$\tilde{B}_\eta(\eta, \psi) = \sum_{n=1}^{\infty} (n\mathcal{A}_n \sinh n\eta \cos n\psi - n\mathcal{B}_n \cosh n\eta \sin n\psi) .$$



$$\tilde{B}_\eta(\eta_0, \psi) = \sum_{n=1}^{\infty} (\tilde{B}_n(\eta_0) \sin n\psi + \tilde{A}_n(\eta_0) \cos n\psi) ,$$

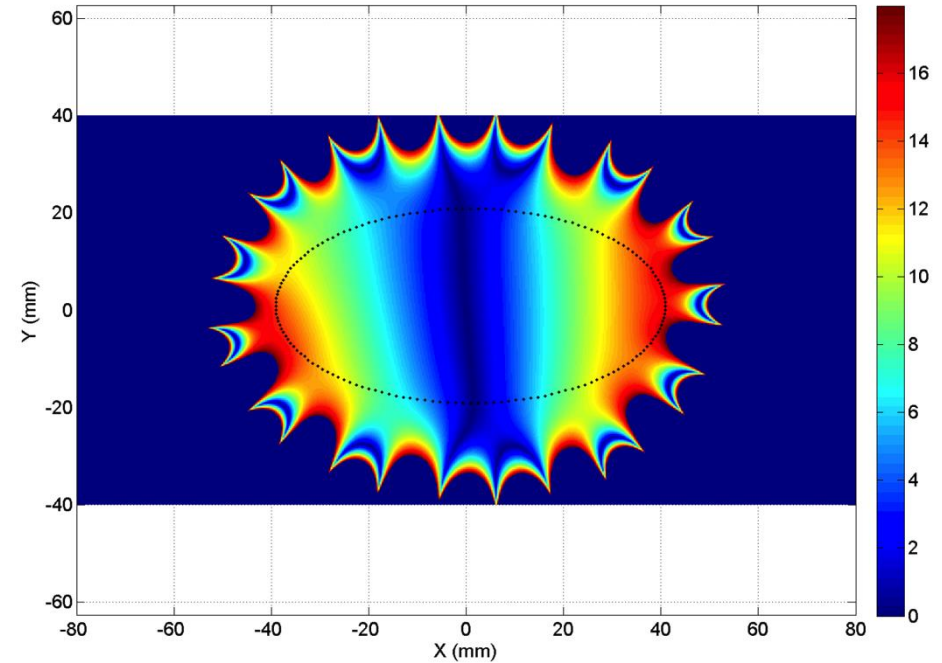
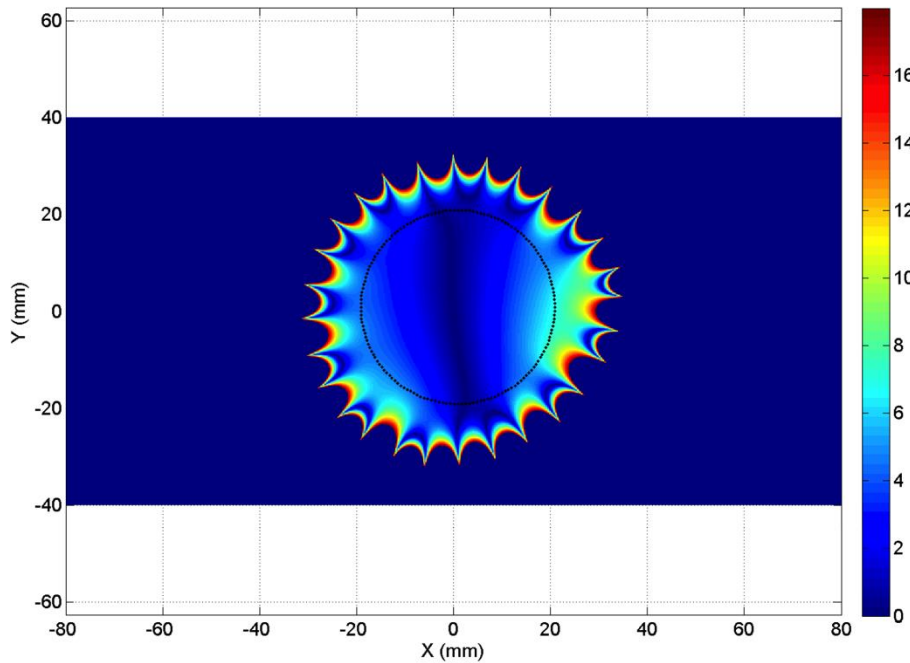
$$\mathcal{A}_n = \frac{1}{n \sinh n\eta_0} \tilde{A}_n(\eta_0), \quad \mathcal{B}_n = -\frac{1}{n \cosh n\eta_0} \tilde{B}_n(\eta_0) ,$$

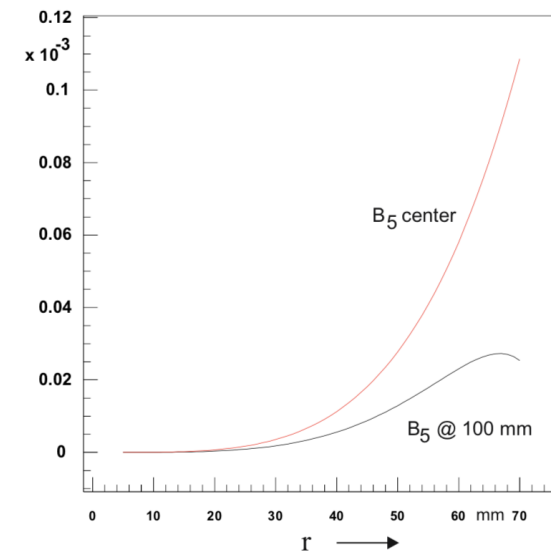
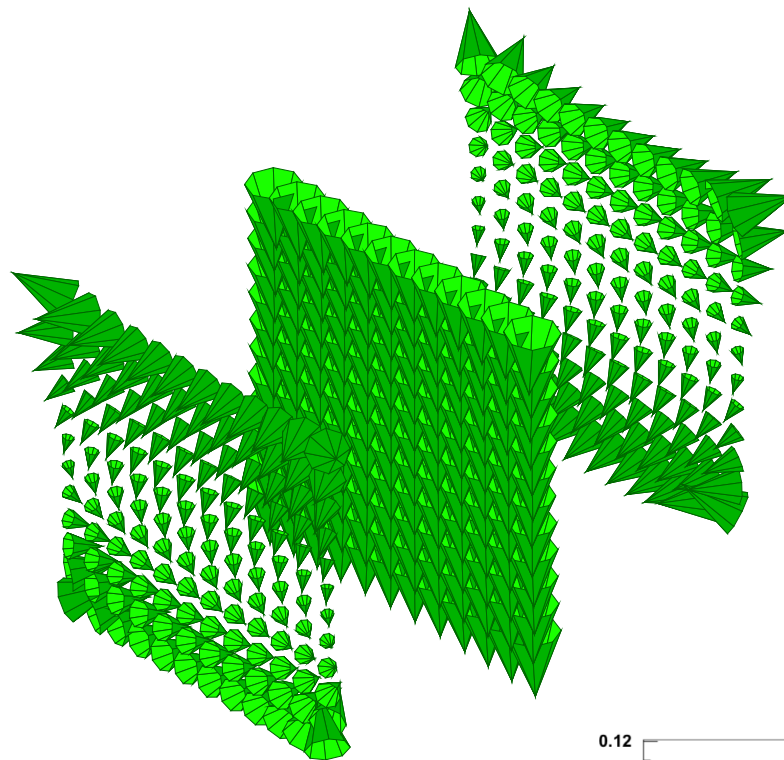
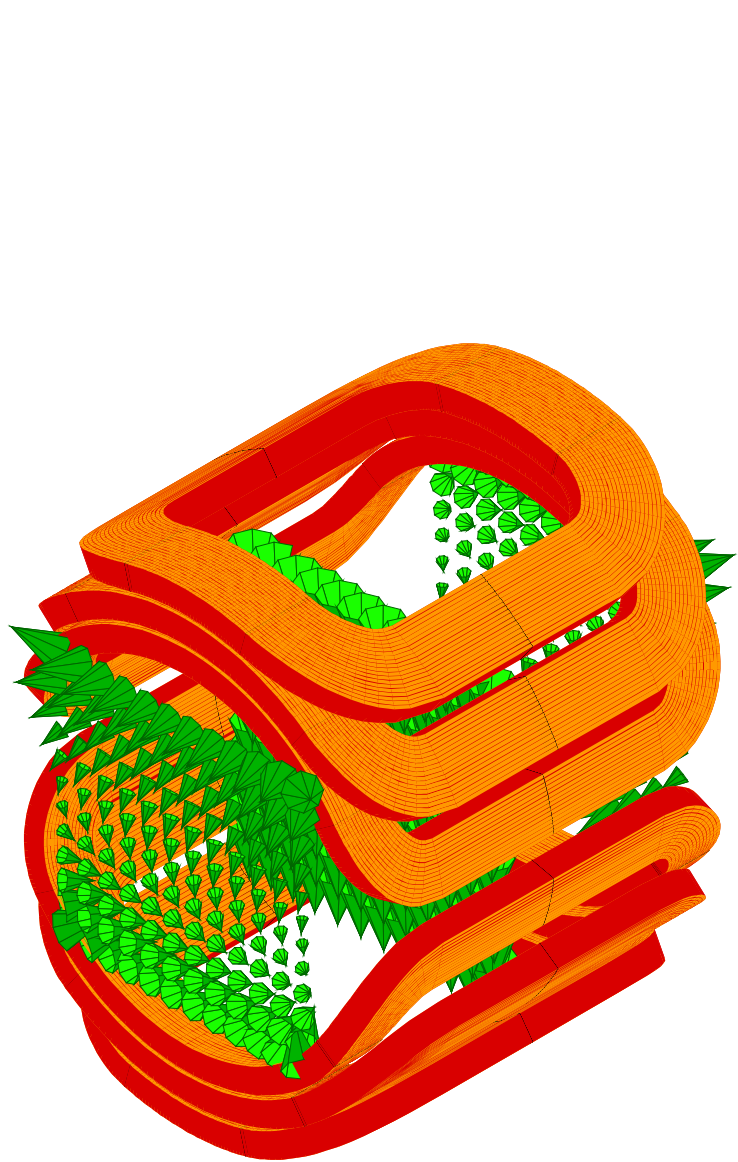
Results for the MM-Section's Calibration Magnets (ISR dipole)

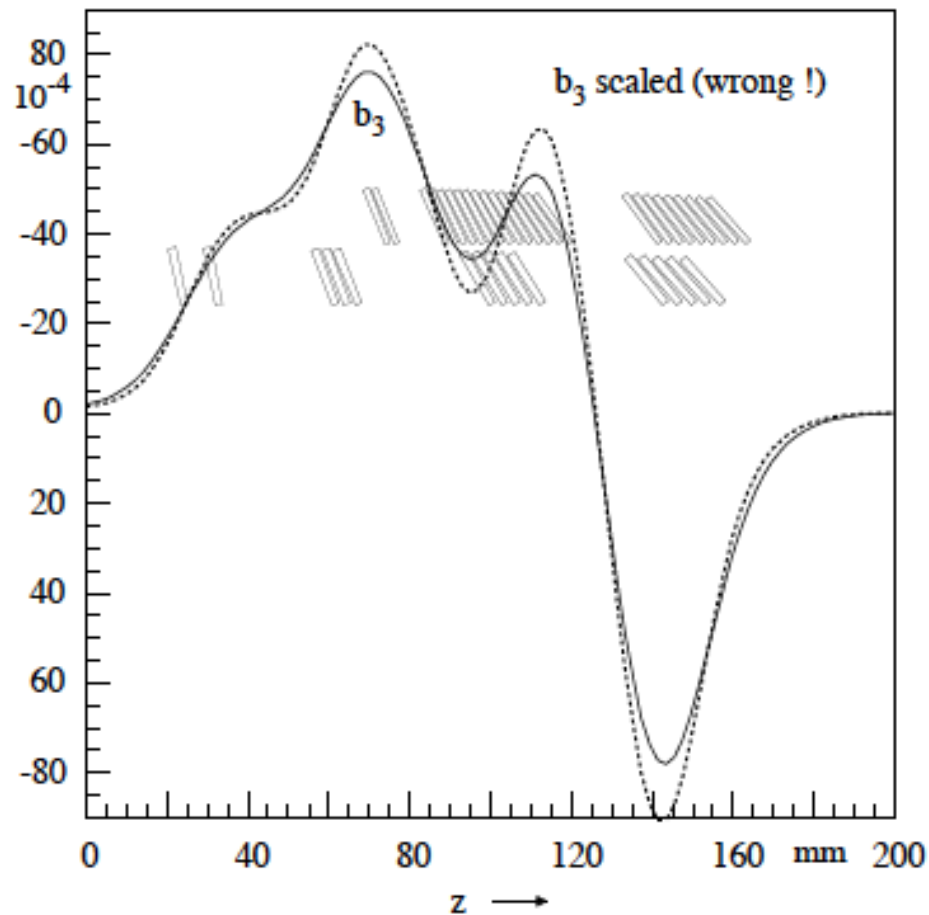


$$B_{\eta}(\eta, \psi) = \frac{1}{h_2} \sum_{n=1}^{\infty} \left(\tilde{B}_n(\eta_0) \frac{\cosh n\eta}{\cosh n\eta_0} \sin n\psi + \tilde{A}_n(\eta_0) \frac{\sinh n\eta}{\sinh n\eta_0} \cos n\psi \right),$$

$$B_{\psi}(\eta, \psi) = \frac{1}{h_1} \sum_{n=1}^{\infty} \left(\tilde{B}_n(\eta_0) \frac{\sinh n\eta}{\cosh n\eta_0} \cos n\psi - \tilde{A}_n(\eta_0) \frac{\cosh n\eta}{\sinh n\eta_0} \sin n\psi \right).$$







Local transverse harmonics calculated at different reference radii and scaled with the 2D laws

$$b_n(r_1) = \left(\frac{r_1}{r_0}\right)^{n-N} b_n(r_0),$$

wrong

$$\nabla^2 \phi_m(x, y, z) = \frac{\partial^2 \phi_m(x, y, z)}{\partial x^2} + \frac{\partial^2 \phi_m(x, y, z)}{\partial y^2} + \frac{\partial^2 \phi_m(x, y, z)}{\partial z^2} = 0.$$

$$\bar{\phi}_m(x, y) := \int_{-z_0}^{z_0} \phi_m(x, y, z) dz.$$

$$\begin{aligned} \frac{\partial^2 \bar{\phi}_m(x, y)}{\partial x^2} + \frac{\partial^2 \bar{\phi}_m(x, y)}{\partial y^2} &= \int_{-z_0}^{z_0} \left(\frac{\partial^2 \phi_m}{\partial x^2} + \frac{\partial^2 \phi_m}{\partial y^2} \right) dz \\ &= \int_{-z_0}^{z_0} \left(-\frac{\partial^2 \phi_m}{\partial z^2} \right) dz = - \left. \frac{\partial \phi_m}{\partial z} \right|_{-z_0}^{z_0} \\ &= H_z(-z_0) - H_z(z_0) \stackrel{!}{=} 0. \end{aligned}$$

The 2D scaling laws hold for the **integrated** harmonics

Pseudo-Multipoles (Fourier Bessel Series)

$$\phi_m(r, \varphi, z) = \begin{Bmatrix} \cos n\varphi \\ \sin n\varphi \end{Bmatrix} I_n(pr) \begin{Bmatrix} \cos pz \\ \sin pz \end{Bmatrix}$$

$$I_n(pr) = \sum_{k=0}^{\infty} \frac{1}{k! \Gamma(k+n+1)} \left(\frac{pr}{2}\right)^{n+2k}$$

$$\phi_m = \sum_{k=0}^{\infty} \sum_{n=1}^{\infty} r^{n+2k} (\mathcal{C}_{n+2k,n}(z) \sin n\varphi + \mathcal{D}_{n+2k,n}(z) \cos n\varphi)$$

$$\begin{aligned}
& \frac{1}{r} \frac{\partial}{\partial r} \left\{ \sum_{k=0}^{\infty} \sum_{n=1}^{\infty} (n+2k) r^{n+2k} (\mathcal{C}_{n+2k,n}(z) \sin n\varphi + \mathcal{D}_{n+2k,n}(z) \cos n\varphi) \right\} \\
& - \frac{1}{r^2} \sum_{k=0}^{\infty} \sum_{n=1}^{\infty} n^2 r^{n+2k} (\mathcal{C}_{n+2k,n}(z) \sin n\varphi + \mathcal{D}_{n+2k,n}(z) \cos n\varphi) \\
& + \sum_{k=0}^{\infty} \sum_{n=1}^{\infty} r^{n+2k} (\mathcal{C}_{n+2k,n}^{(2)}(z) \sin n\varphi + \mathcal{D}_{n+2k,n}^{(2)}(z) \cos n\varphi) \\
& = \sum_{k=0}^{\infty} \sum_{n=1}^{\infty} (n+2k)^2 r^{n+2k-2} (\mathcal{C}_{n+2k,n}(z) \sin n\varphi + \mathcal{D}_{n+2k,n}(z) \cos n\varphi) \\
& - \sum_{k=0}^{\infty} \sum_{n=1}^{\infty} n^2 r^{n+2k-2} (\mathcal{C}_{n+2k,n}(z) \sin n\varphi + \mathcal{D}_{n+2k,n}(z) \cos n\varphi) \\
& + \sum_{k=1}^{\infty} \sum_{n=1}^{\infty} r^{n+2k-2} (\mathcal{C}_{n+2k-2,n}^{(2)}(z) \sin n\varphi + \mathcal{D}_{n+2k-2,n}^{(2)}(z) \cos n\varphi) \\
& = 0, \tag{
\end{aligned}$$

$$C_{n+2k,n}(z) \left((n+2k)^2 - n^2 \right) + C_{n+2k-2,n}^{(2)}(z) = 0,$$

$$D_{n+2k,n}(z) \left((n+2k)^2 - n^2 \right) + D_{n+2k-2,n}^{(2)}(z) = 0.$$

$$C_{n+2k,n}(z) = \frac{1}{\prod_{m=1}^k (n^2 - (n+2m)^2)} C_{n,n}^{(2k)}(z),$$

$$\begin{aligned} \phi_m &= \sum_{n=1}^{\infty} \left\{ \sum_{k=0}^{\infty} \frac{1}{\prod_{m=1}^k (n^2 - (n+2m)^2)} \mathcal{C}_{n,n}^{(2k)}(z) \right\} r^n \sin n\varphi \\ &+ \sum_{n=1}^{\infty} \left\{ \sum_{k=0}^{\infty} \frac{1}{\prod_{m=1}^k (n^2 - (n+2m)^2)} \mathcal{D}_{n,n}^{(2k)}(z) \right\} r^n \cos n\varphi, \end{aligned}$$

$$\begin{aligned} \phi_m &= \sum_{n=1}^{\infty} \left\{ \mathcal{C}_{n,n}(z) - \frac{\mathcal{C}_{n,n}^{(2)}(z)}{4(n+1)} r^2 \right. \\ &\quad \left. + \frac{\mathcal{C}_{n,n}^{(4)}(z)}{32(n+1)(n+2)} r^4 - \frac{\mathcal{C}_{n,n}^{(6)}(z)}{384(n+1)(n+2)(n+3)} r^6 + \dots \right\} r^n \sin n\varphi \\ &+ \sum_{n=1}^{\infty} \left\{ \mathcal{D}_{n,n}(z) - \frac{\mathcal{D}_{n,n}^{(2)}(z)}{4(n+1)} r^2 \right. \\ &\quad \left. + \frac{\mathcal{D}_{n,n}^{(4)}(z)}{32(n+1)(n+2)} r^4 - \frac{\mathcal{D}_{n,n}^{(6)}(z)}{384(n+1)(n+2)(n+3)} r^6 + \dots \right\} r^n \cos n\varphi, \end{aligned}$$

$$\begin{aligned} \frac{-1}{\mu_0} B_y(x, y = 0, z) \approx & \\ & C_{1,1}(z) - \frac{C_{1,1}^{(2)}(z)}{8} x^2 + \frac{C_{1,1}^{(4)}(z)}{192} x^4 - \frac{C_{1,1}^{(6)}(z)}{9216} x^6 \\ & + 3 C_{3,3}(z) x^2 - \frac{3 C_{3,3}^{(2)}(z)}{16} x^4 + \frac{3 C_{3,3}^{(4)}(z)}{640} x^6 \\ & + 5 C_{5,5}(z) x^4 - \frac{5 C_{5,5}^{(2)}(z)}{24} x^6 \\ & + 7 C_{7,7}(z) x^6 \end{aligned}$$

Field Components from Pseudo-Multipoles

$$\phi_m(r, \varphi) = \sum_{n=1}^{\infty} r^n (\tilde{\mathcal{C}}_n(r, z) \sin n\varphi + \tilde{\mathcal{D}}_n(z) \cos n\varphi).$$

$$B_r(r, \varphi, z) = -\mu_0 \sum_{n=1}^{\infty} r^{n-1} (\bar{\mathcal{C}}_n(r, z) \sin n\varphi + \bar{\mathcal{D}}_n(r, z) \cos n\varphi),$$

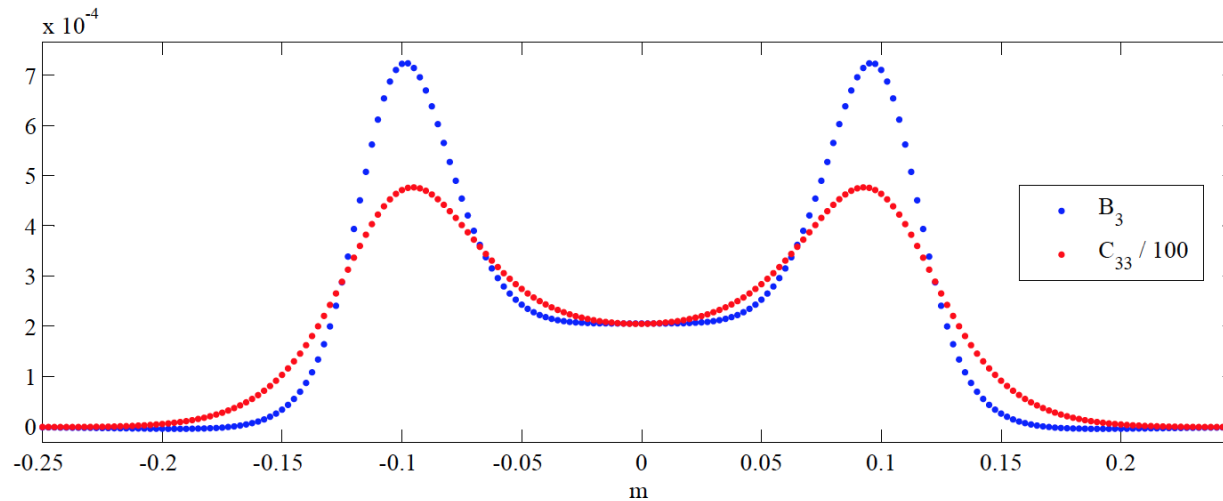
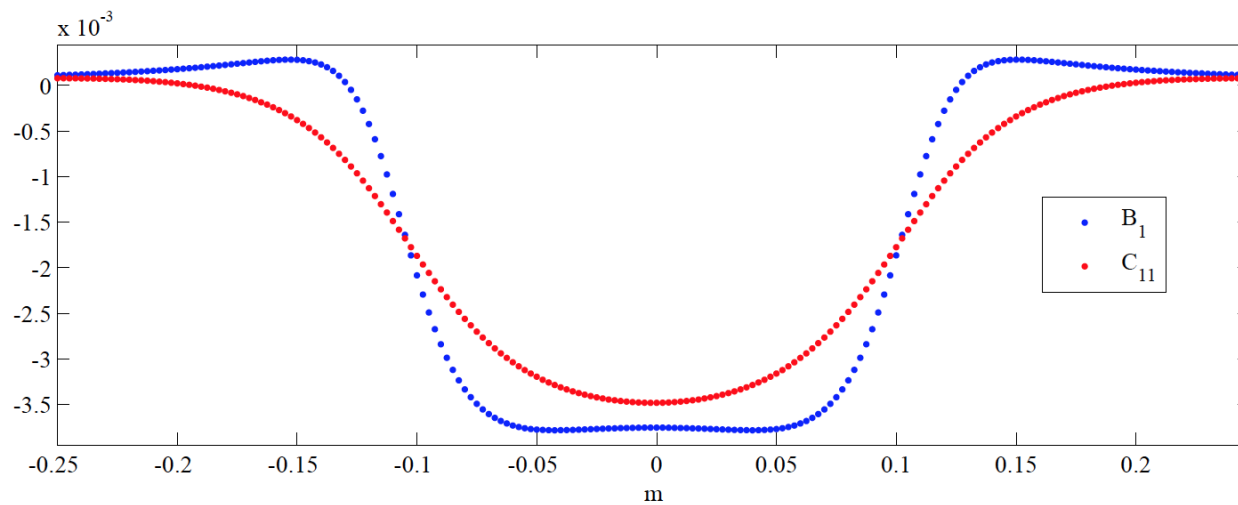
$$B_\varphi(r, \varphi, z) = -\mu_0 \sum_{n=1}^{\infty} n r^{n-1} (\tilde{\mathcal{C}}_n(r, z) \cos n\varphi - \tilde{\mathcal{D}}_n(r, z) \sin n\varphi),$$

$$B_z(r, \varphi, z) = -\mu_0 \sum_{n=1}^{\infty} r^n \left(\frac{\partial \tilde{\mathcal{C}}_n(r, z)}{\partial z} \sin n\varphi + \frac{\partial \tilde{\mathcal{D}}_n(r, z)}{\partial z} \cos n\varphi \right),$$

$$\bar{\mathcal{C}}_n(r, z) = n \mathcal{C}_{n,n}(z) - \frac{(n+2)\mathcal{C}_{n,n}^{(2)}(z)}{4(n+1)} r^2 + \frac{(n+4)\mathcal{C}_{n,n}^{(4)}(z)}{32(n+1)(n+2)} r^4 - \dots$$

$$\tilde{\mathcal{C}}_n(r, z) := \mathcal{C}_{n,n}(z) - \frac{\mathcal{C}_{n,n}^{(2)}(z)}{4(n+1)} r^2 + \frac{\mathcal{C}_{n,n}^{(4)}(z)}{32(n+1)(n+2)} r^4 - \dots,$$

The Leading Term is NOT the Measured One



Fourier Transform for the Extractions of $C_{n,n}$

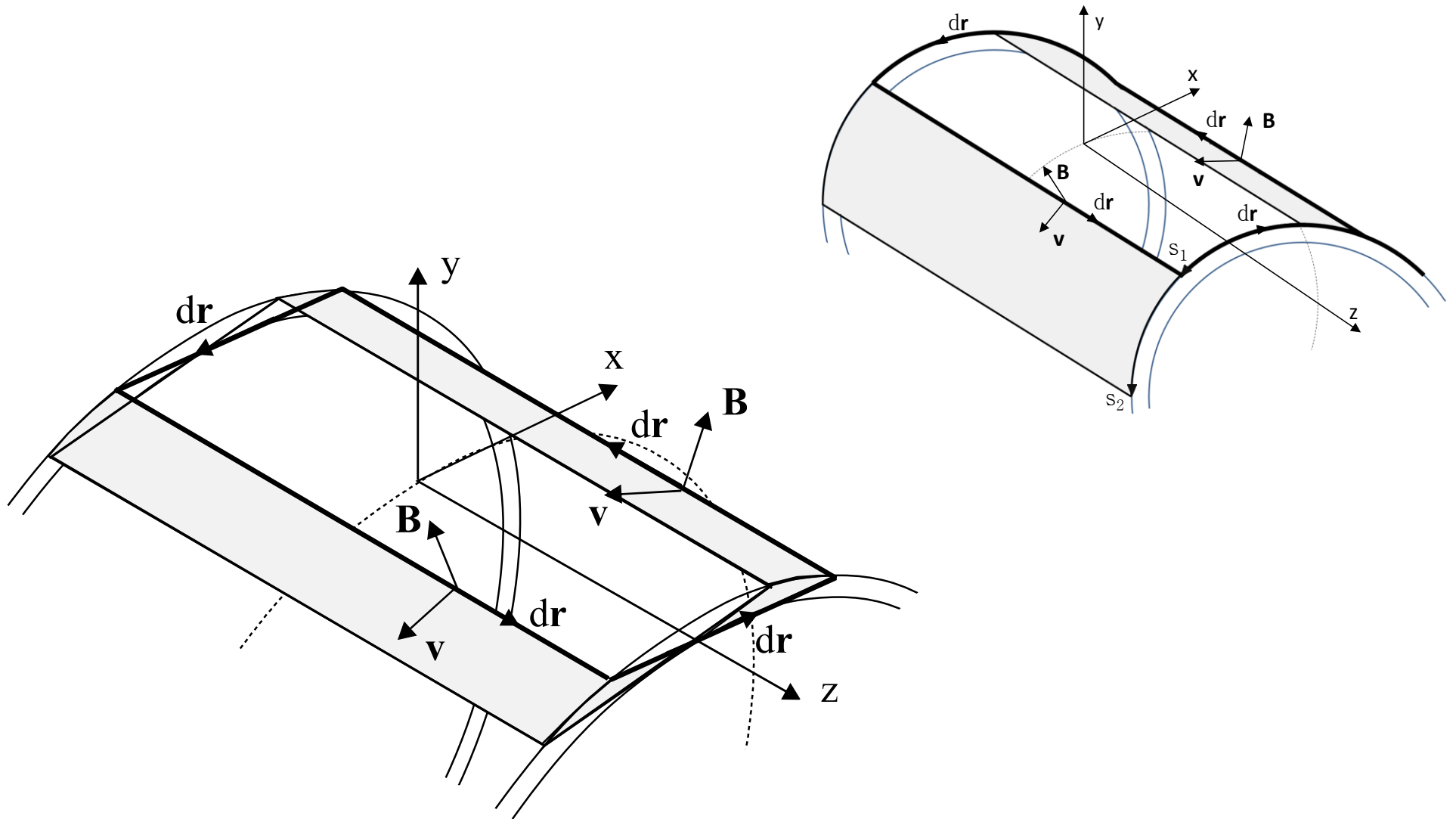
$$B_n(r_0, z) = -\mu_0 r_0^{n-1} \bar{C}_n(r_0, z) =$$

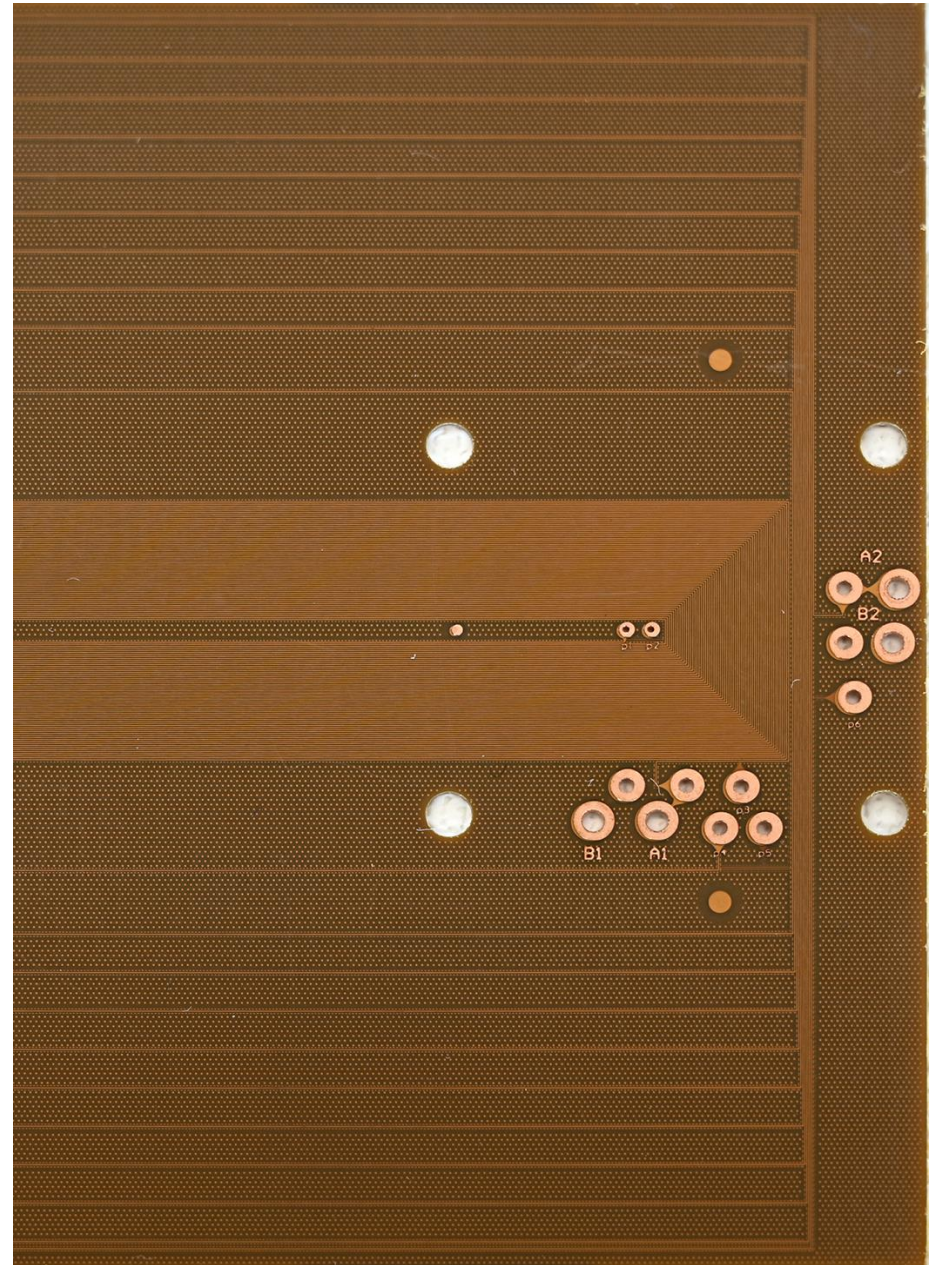
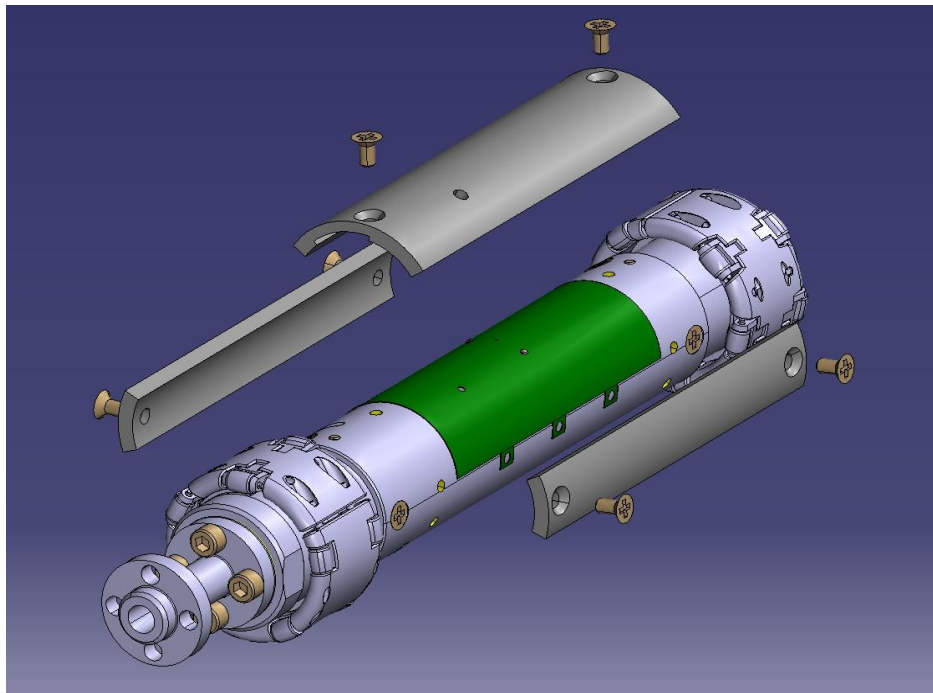
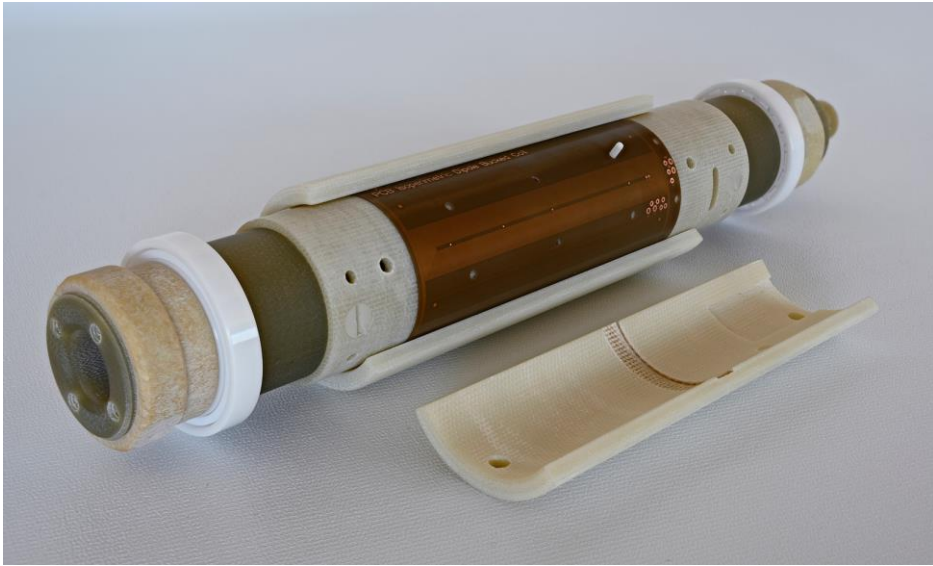
$$-\mu_0 r_0^{n-1} \left(n C_{n,n}(z) - \frac{(n+2)C_{n,n}^{(2)}(z)}{4(n+1)} r_0^2 + \frac{(n+4)C_{n,n}^{(4)}(z)}{32(n+1)(n+2)} r_0^4 - \dots \right).$$

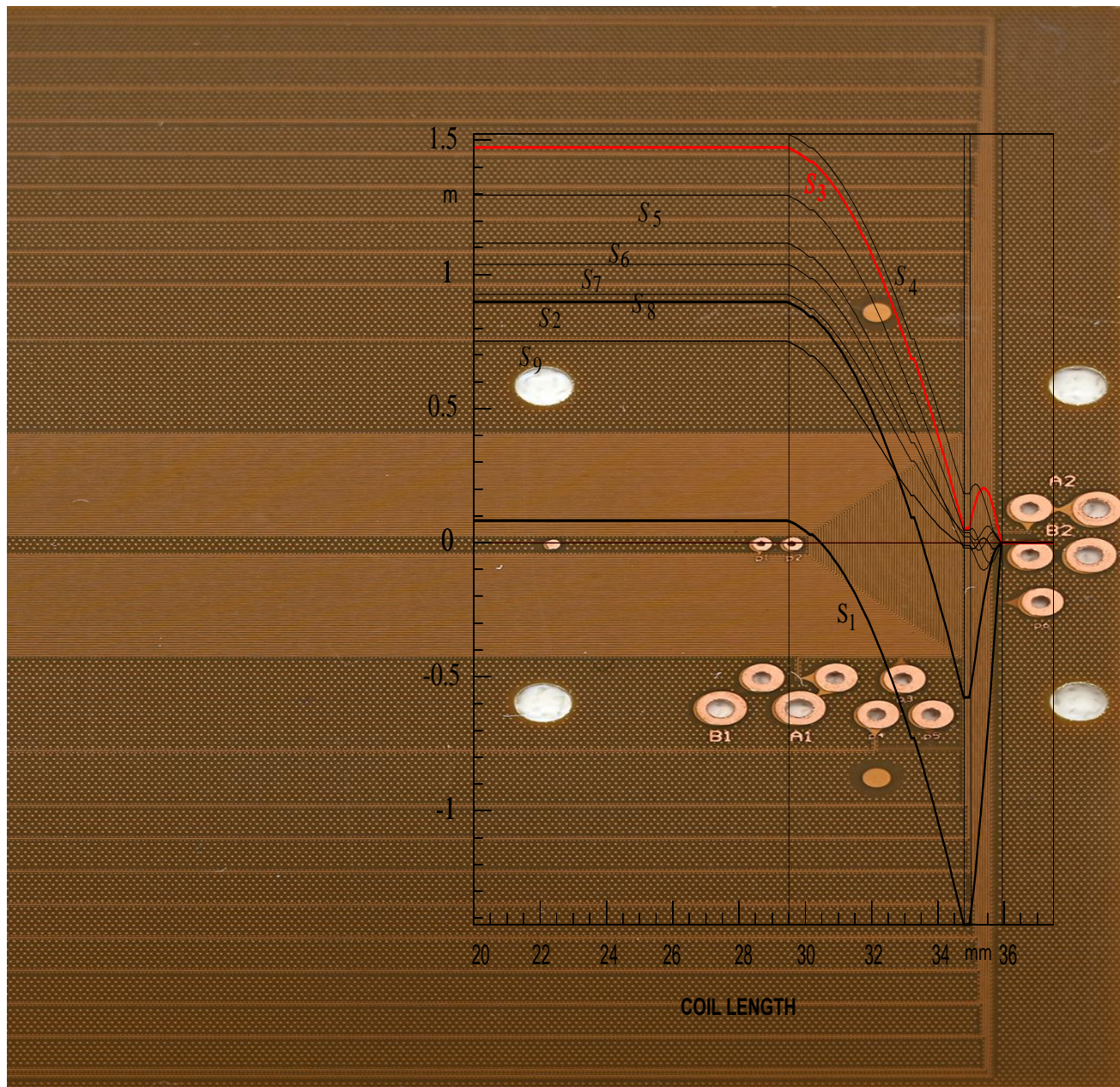
$$\mathcal{F}\{C_{n,n}(z)\} = \frac{-\mathcal{F}\{B_n(r_0, z)\}}{\mu_0 r_0^{n-1} \left(n - \frac{(n+2)(i\omega)^2}{4(n+1)} r_0^2 + \frac{(n+4)(i\omega)^4}{32(n+1)(n+2)} r_0^4 - \dots \right)}$$

$$\mathcal{F}\{C_{n,n}(z)\} = \frac{\mathcal{F}\{\tilde{B}_n(r_0, z)\}}{\mathcal{F}\{K_n(r_0, z)\}} \frac{-1}{\mu_0 r_0^{n-1} \left(n - \frac{(n+2)(i\omega)^2}{4(n+1)} r_0^2 + \frac{(n+4)(i\omega)^4}{32(n+1)(n+2)} r_0^4 - \dots \right)}$$

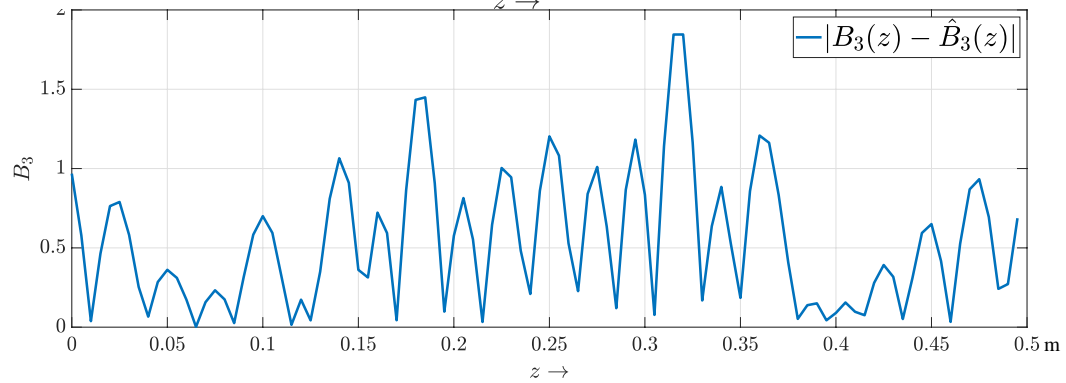
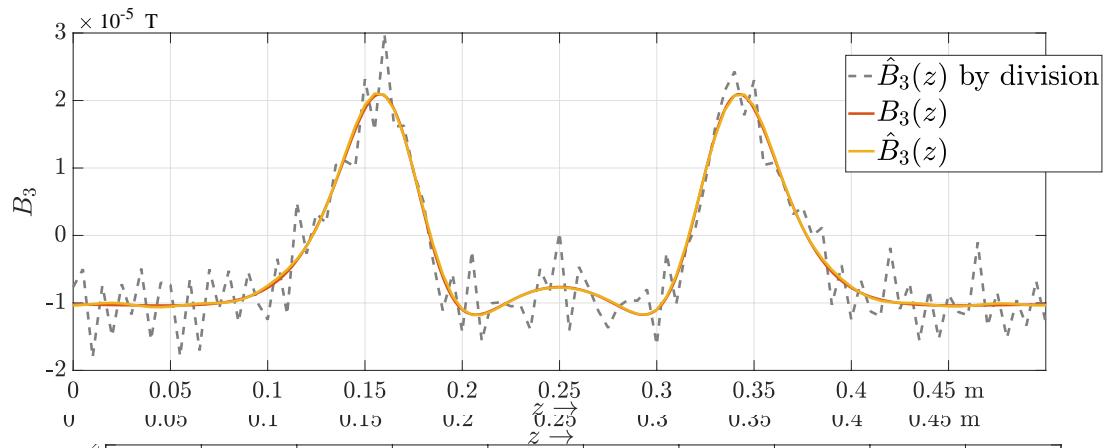
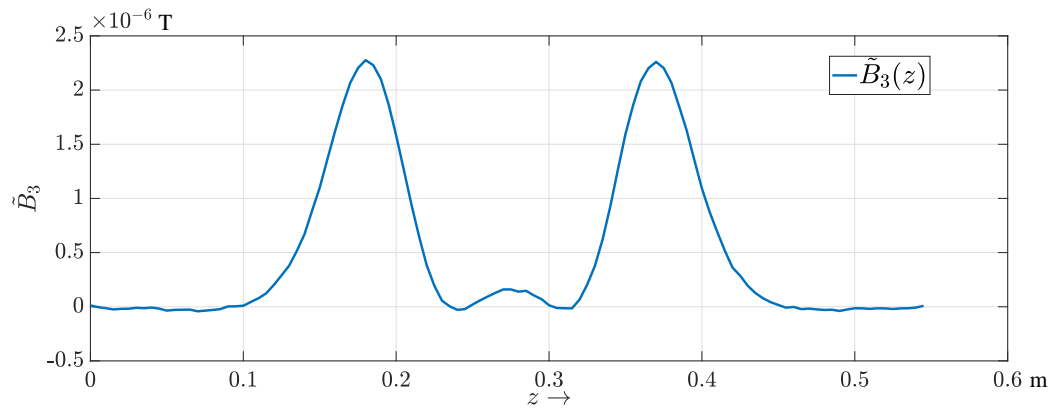
Classical Induction Coils Intercept the B_z Component

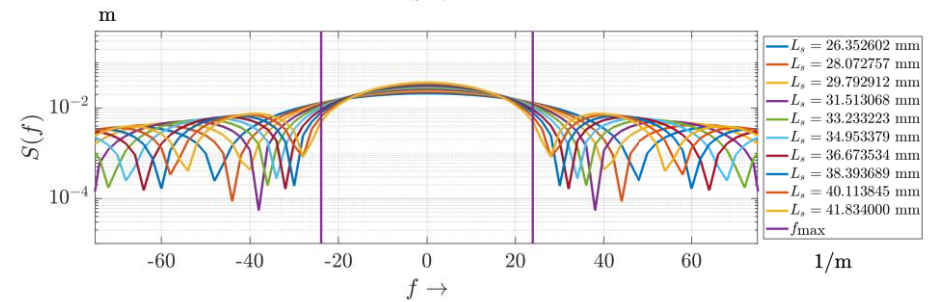
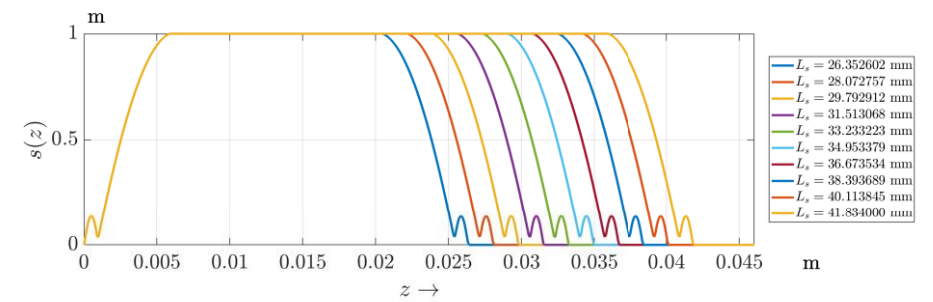
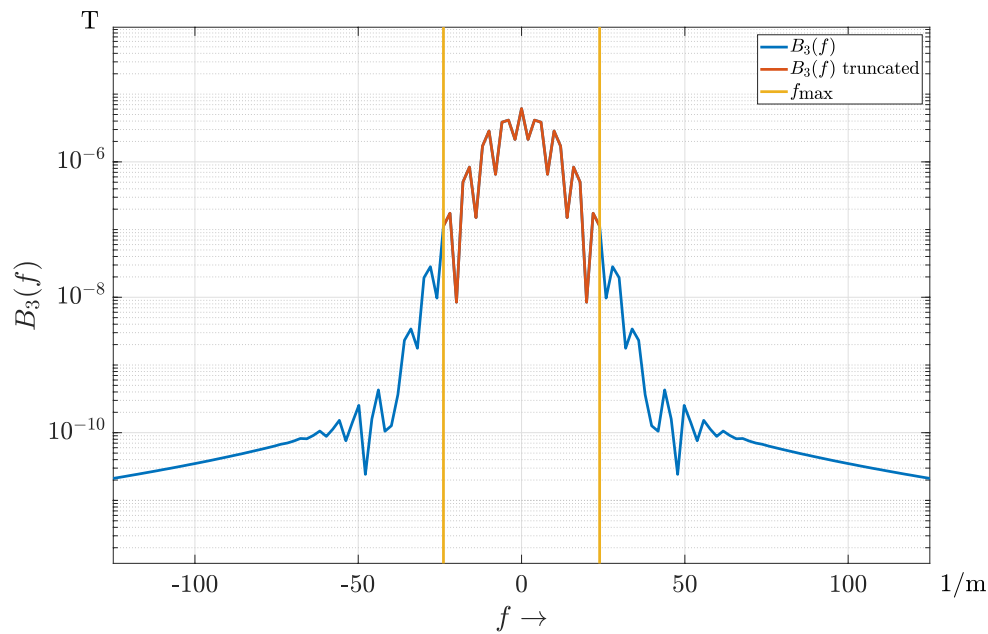
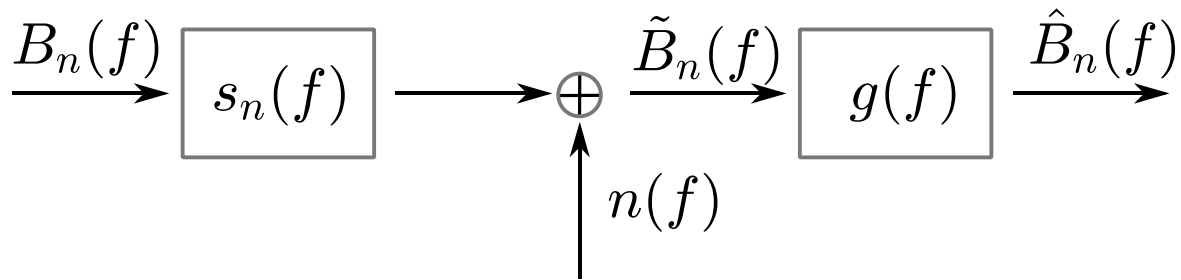






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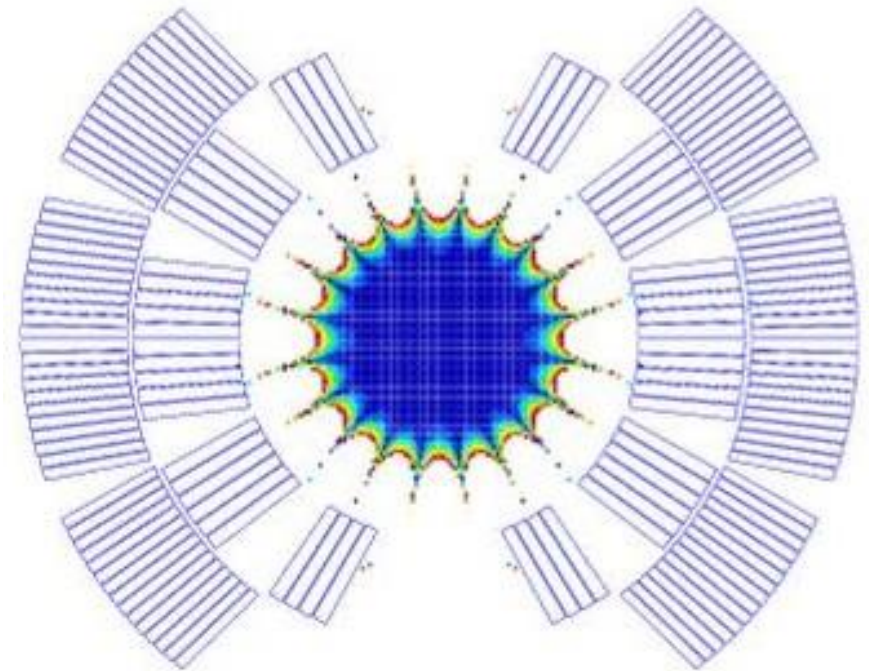
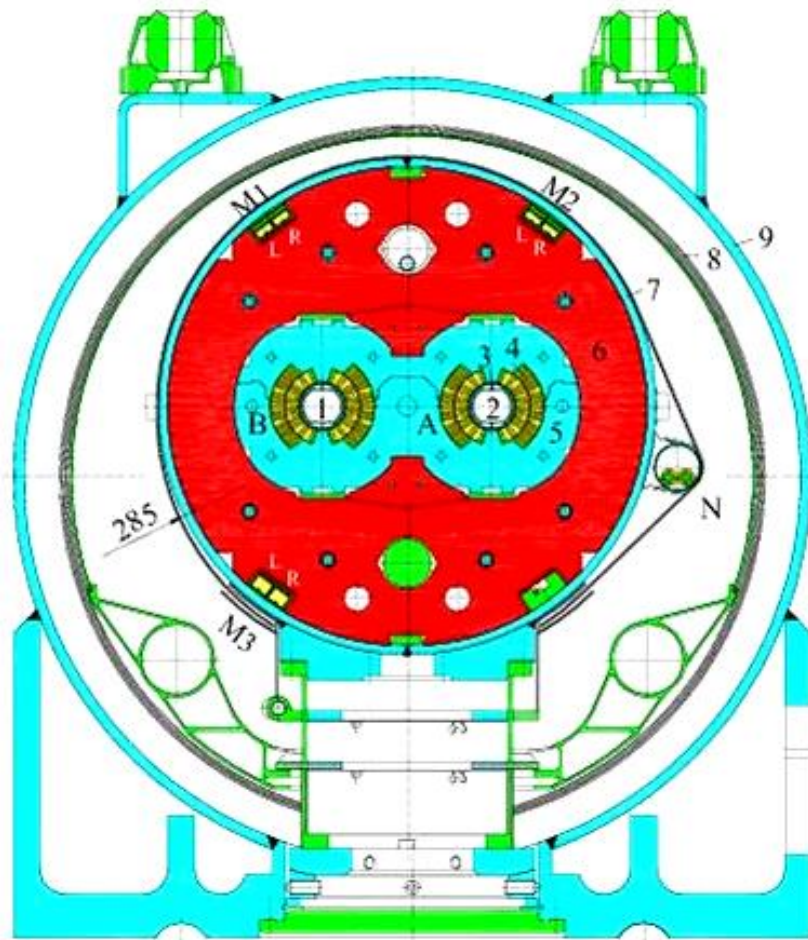




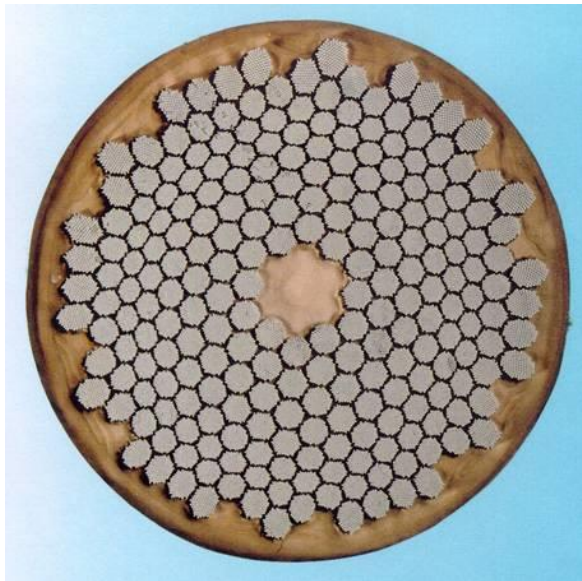
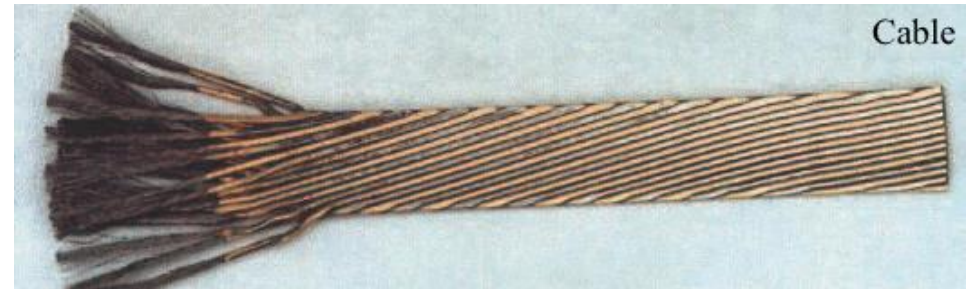
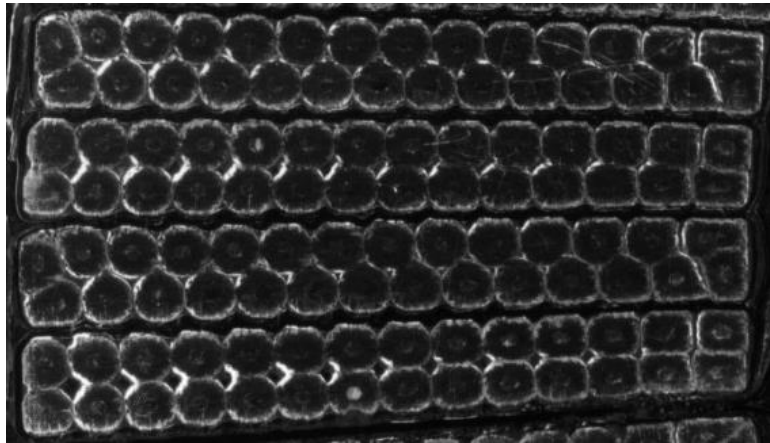
Field Singularities - The Green's Functions



Cross-section of Cryodipole



Rutherford (Roebel) Kabel, Strand, Nb-Ti Filament



200 nm 

The Field of Line Currents

$$\mathbf{r} \mapsto \vec{\phi}(|\mathbf{r} - \mathbf{r}'|)$$

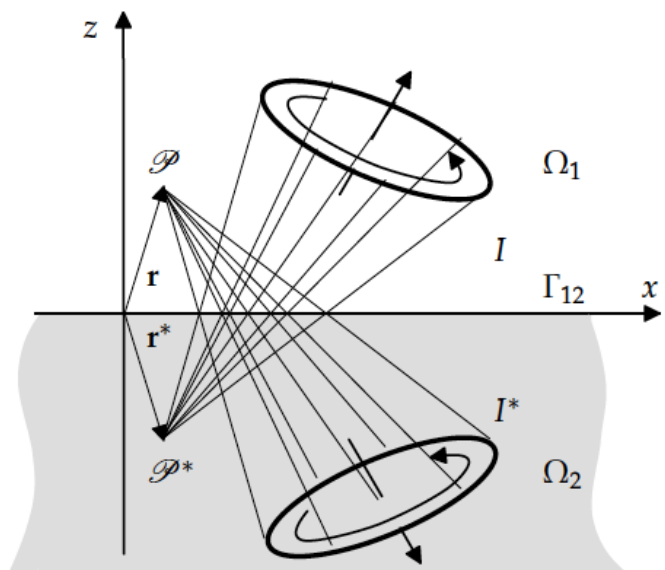
$$\mathbf{r}' \mapsto \vec{\phi}(|\mathbf{r} - \mathbf{r}'|)$$

$$\text{grad } \phi(|\mathbf{r} - \mathbf{r}'|) = -\text{grad}_{\mathbf{r}'} \phi(|\mathbf{r} - \mathbf{r}'|),$$

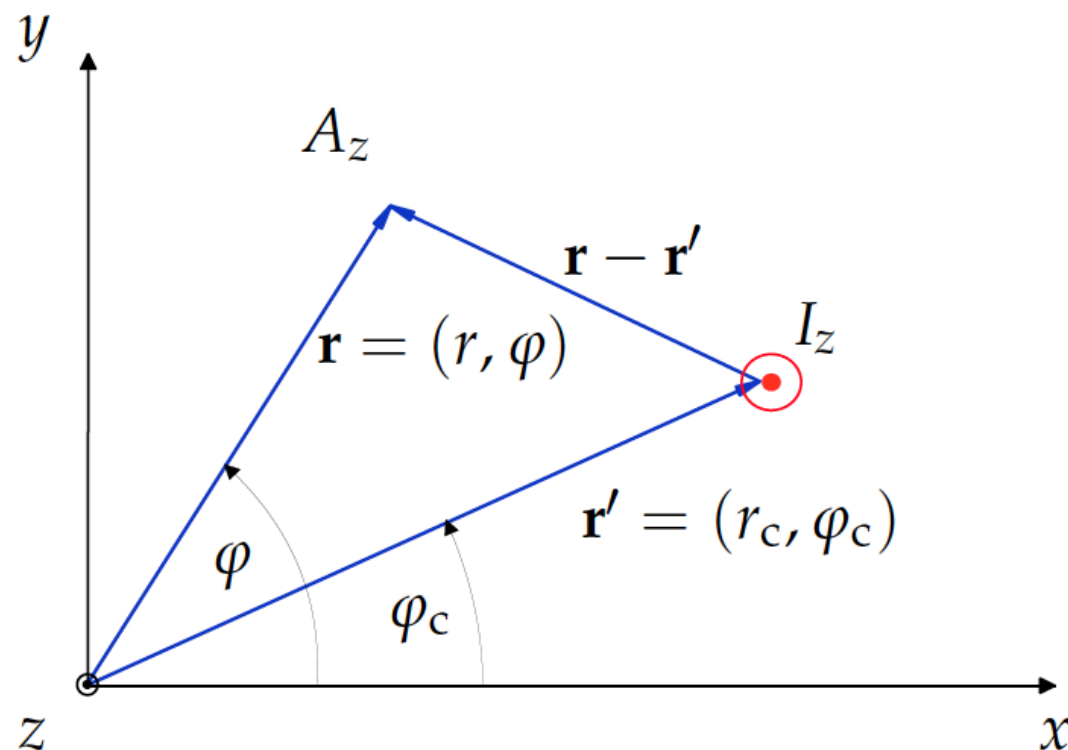
$$\text{div } \mathbf{a}(|\mathbf{r} - \mathbf{r}'|) = -\text{div}_{\mathbf{r}'} \mathbf{a}(|\mathbf{r} - \mathbf{r}'|),$$

$$\text{curl } \mathbf{a}(|\mathbf{r} - \mathbf{r}'|) = -\text{curl}_{\mathbf{r}'} \mathbf{a}(|\mathbf{r} - \mathbf{r}'|),$$

$$\nabla^2 \phi(|\mathbf{r} - \mathbf{r}'|) = \nabla_{\mathbf{r}'}^2 \phi(|\mathbf{r} - \mathbf{r}'|).$$



Why bother? Reciprocity; except for sign it does not matter if we exchange the source and field points



$$\mathcal{L}_{\mathbf{r}'}\phi(\mathbf{r}') = -f(\mathbf{r}')$$

$$\mathcal{L}_{\mathbf{r}'}G(\mathbf{r}, \mathbf{r}') = -\delta(\mathbf{r} - \mathbf{r}'),$$



$$\int_{\mathcal{V}} \mathcal{L}_{\mathbf{r}'}G(\mathbf{r}, \mathbf{r}') f(\mathbf{r})dV = - \int_{\mathcal{V}} \delta(\mathbf{r} - \mathbf{r}')f(\mathbf{r})dV = -f(\mathbf{r}').$$

$$\mathcal{L}_{\mathbf{r}'}\phi(\mathbf{r}') = \int_{\mathcal{V}} \mathcal{L}_{\mathbf{r}'}G(\mathbf{r}, \mathbf{r}')f(\mathbf{r})dV = \mathcal{L}_{\mathbf{r}'} \int_{\mathcal{V}} G(\mathbf{r}, \mathbf{r}')f(\mathbf{r})dV,$$

$$\phi(\mathbf{r}') = \int_{\mathcal{V}} G(\mathbf{r}, \mathbf{r}')f(\mathbf{r})dV.$$

$$G_2(\mathbf{r}, \mathbf{r}') = \frac{1}{2\pi} \ln \left(\frac{|\mathbf{r} - \mathbf{r}'|}{r_{\text{ref}}} \right),$$

$$G_3(\mathbf{r}, \mathbf{r}') = \frac{1}{4\pi|\mathbf{r} - \mathbf{r}'|}$$

Green's Functions of Free Space

$$\phi(\mathbf{r}') = \int_{\mathcal{V}} G(\mathbf{r}, \mathbf{r}') f(\mathbf{r}) dV.$$

$$\phi(\mathbf{r}) = \int_{\mathcal{V}} G(\mathbf{r}, \mathbf{r}') f(\mathbf{r}') dV'.$$

But what if boundaries are present?

Use Green's second identity (integration by parts)

$$\int_{\Omega} (\phi \nabla^2 \psi - \psi \nabla^2 \phi) dV = \int_{\Gamma} (\phi \partial_{\mathbf{n}} \psi - \psi \partial_{\mathbf{n}} \phi) da$$

$$\phi(\mathbf{r}) = \int_{\mathcal{V}} G(\mathbf{r}, \mathbf{r}') f(\mathbf{r}') dV'$$

$$+ \int_{\partial \mathcal{V}} \left(-\phi(\mathbf{r}') \partial_{\mathbf{n}'} G(\mathbf{r}, \mathbf{r}') + G(\mathbf{r}, \mathbf{r}') \partial_{\mathbf{n}'} \phi(\mathbf{r}') \right) da'.$$

Surface current

Surface density of dipole moments

$$\nabla^2 \mathbf{A} = -\mu_0 \mathbf{J}, \quad G_3(\mathbf{r}, \mathbf{r}') = \frac{1}{4\pi |\mathbf{r} - \mathbf{r}'|}$$

$$A_i(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_{\mathcal{V}} \frac{J_i(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV',$$

$$\mathbf{A}(\mathbf{r}) = A_x \mathbf{e}_x + A_y \mathbf{e}_y + A_z \mathbf{e}_z = \frac{\mu_0}{4\pi} \int_{\mathcal{V}} \frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV'.$$

This works only in Cartesian Coordinates

$$\mathbf{B}(\mathbf{r}) = \text{curl } \mathbf{A}(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_{\mathcal{V}} \text{curl} \left(\frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} \right) dV'$$

$$A_i(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_{\mathcal{V}} \frac{1}{|\mathbf{r} - \mathbf{r}'|} \sum_{k=1}^3 J_k(\mathbf{r}') (\mathbf{e}_i(\mathbf{r}) \cdot \mathbf{e}_k(\mathbf{r}')) dV'. \quad dV'$$

$$= \frac{\mu_0}{4\pi} \int_{\mathcal{V}} \frac{\mathbf{J}(\mathbf{r}') \wedge (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3} dV'.$$

But wait a minute: Are we finished? Are we sure that the divergence of the vector potential is zero as it was required for the Laplace equation?

$$\begin{aligned}\operatorname{div} \mathbf{A}(\mathbf{r}) &= \frac{\mu_0}{4\pi} \int_{\mathcal{V}'} \operatorname{div} \left(\frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} \right) dV' \\ &= \frac{\mu_0}{4\pi} \int_{\mathcal{V}'} \left(\mathbf{J}(\mathbf{r}') \cdot \operatorname{grad} \left(\frac{1}{|\mathbf{r} - \mathbf{r}'|} \right) + \frac{1}{|\mathbf{r} - \mathbf{r}'|} \operatorname{div} \mathbf{J}(\mathbf{r}') \right) dV' \\ &= \frac{\mu_0}{4\pi} \int_{\mathcal{V}'} \mathbf{J}(\mathbf{r}') \cdot \operatorname{grad} \left(\frac{1}{|\mathbf{r} - \mathbf{r}'|} \right) dV' \\ &= -\frac{\mu_0}{4\pi} \int_{\mathcal{V}'} \mathbf{J}(\mathbf{r}') \cdot \operatorname{grad}_{\mathbf{r}'} \left(\frac{1}{|\mathbf{r} - \mathbf{r}'|} \right) dV' \\ &= -\frac{\mu_0}{4\pi} \int_{\mathcal{V}'} \left(\operatorname{div}_{\mathbf{r}'} \left(\frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} \right) - \frac{1}{|\mathbf{r} - \mathbf{r}'|} \operatorname{div}_{\mathbf{r}'} \mathbf{J}(\mathbf{r}') \right) dV' \\ &= -\frac{\mu_0}{4\pi} \int_{\mathcal{V}'} \operatorname{div}_{\mathbf{r}'} \left(\frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} \right) dV' = -\frac{\mu_0}{4\pi} \int_{\partial \mathcal{V}'} \frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} \cdot d\mathbf{a}' .\end{aligned}$$

Current loops must always be closed and must not leave the problem domain

Biot-Savart's Law for Line Currents

$$\mathbf{A}(\mathbf{r}) = A_x \mathbf{e}_x + A_y \mathbf{e}_y + A_z \mathbf{e}_z = \frac{\mu_0}{4\pi} \int_{\mathcal{V}} \frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV'.$$

$$\mathbf{A}(\mathbf{r}) = \frac{\mu_0 I}{4\pi} \int_{\mathcal{C}} \frac{d\mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|}$$

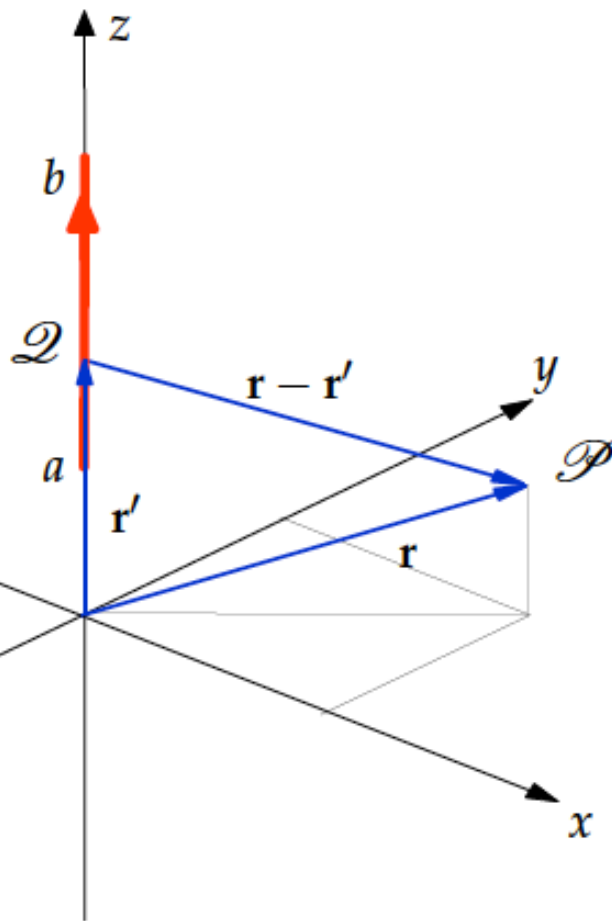
$$\mathbf{B}(\mathbf{r}) = \frac{\mu_0 I}{4\pi} \int_{\mathcal{C}} \frac{d\mathbf{r}' \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3},$$

Vector Potential of a Line Current

$$A_z(x, y, z) = \frac{\mu_0 I}{4\pi} \int_a^b \frac{dz_c}{|\mathbf{r} - \mathbf{r}'|} = \frac{\mu_0 I}{4\pi} \int_a^b \frac{dz_c}{\sqrt{x^2 + y^2 + (z - z_c)^2}}$$

$$= \frac{-\mu_0 I}{4\pi} \ln \left((z - z_c) + \sqrt{x^2 + y^2 + (z - z_c)^2} \right) \Big|_a^b$$

$$= \frac{\mu_0 I}{4\pi} \ln \frac{z - a + \sqrt{x^2 + y^2 + (z - a)^2}}{z - b + \sqrt{x^2 + y^2 + (z - b)^2}}.$$



Field of a Line Current (Infinitely Long)

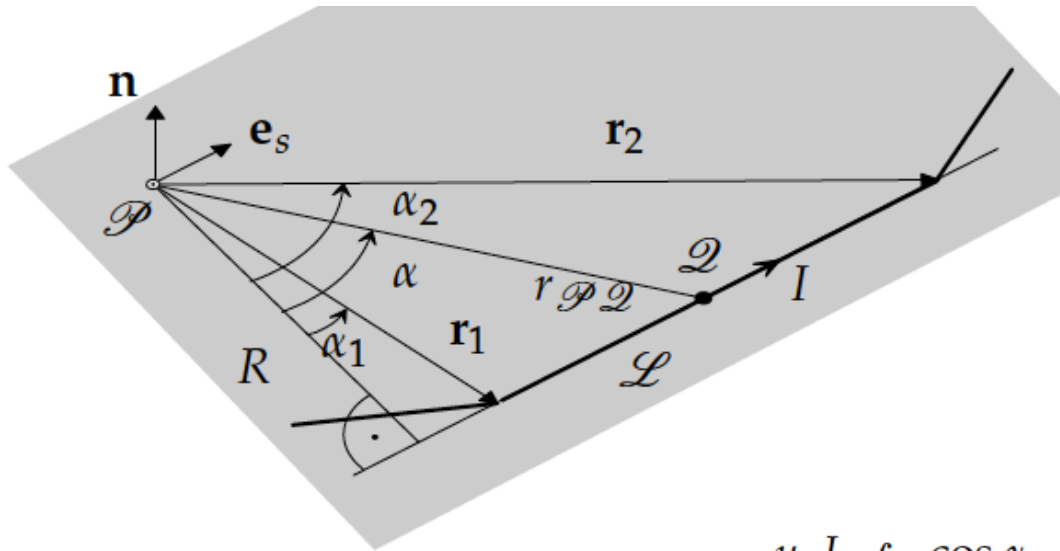
$$\begin{aligned}
 \lim_{a,b \rightarrow \pm\infty} \ln \frac{z - a + \sqrt{x^2 + y^2 + (z - a)^2}}{z - b + \sqrt{x^2 + y^2 + (z - b)^2}} &= \lim_{a,b \rightarrow \pm\infty} \ln \frac{-a + |a| \sqrt{1 + \frac{x^2 + y^2}{a^2}}}{-b + |b| \sqrt{1 + \frac{x^2 + y^2}{b^2}}} \\
 &= \lim_{a,b \rightarrow \pm\infty} \ln \frac{-a - a(1 + \frac{x^2 + y^2}{2a^2} + \dots)}{-b + b(1 + \frac{x^2 + y^2}{2b^2} + \dots)} = \lim_{a,b \rightarrow \pm\infty} \ln \frac{-2a}{-b + b + \frac{x^2 + y^2}{2b}} \\
 &= \lim_{a,b \rightarrow \pm\infty} \ln \frac{-4ab}{x^2 + y^2}.
 \end{aligned}$$

$$A_z(x, y) = \lim_{a,b \rightarrow \pm\infty} \frac{\mu_0 I}{4\pi} \ln \left(\frac{-4ab}{x_0^2 + y_0^2} \right) - \frac{\mu_0 I}{4\pi} \ln \left(\frac{x^2 + y^2}{x_0^2 + y_0^2} \right).$$

Arbitrarily large but constant

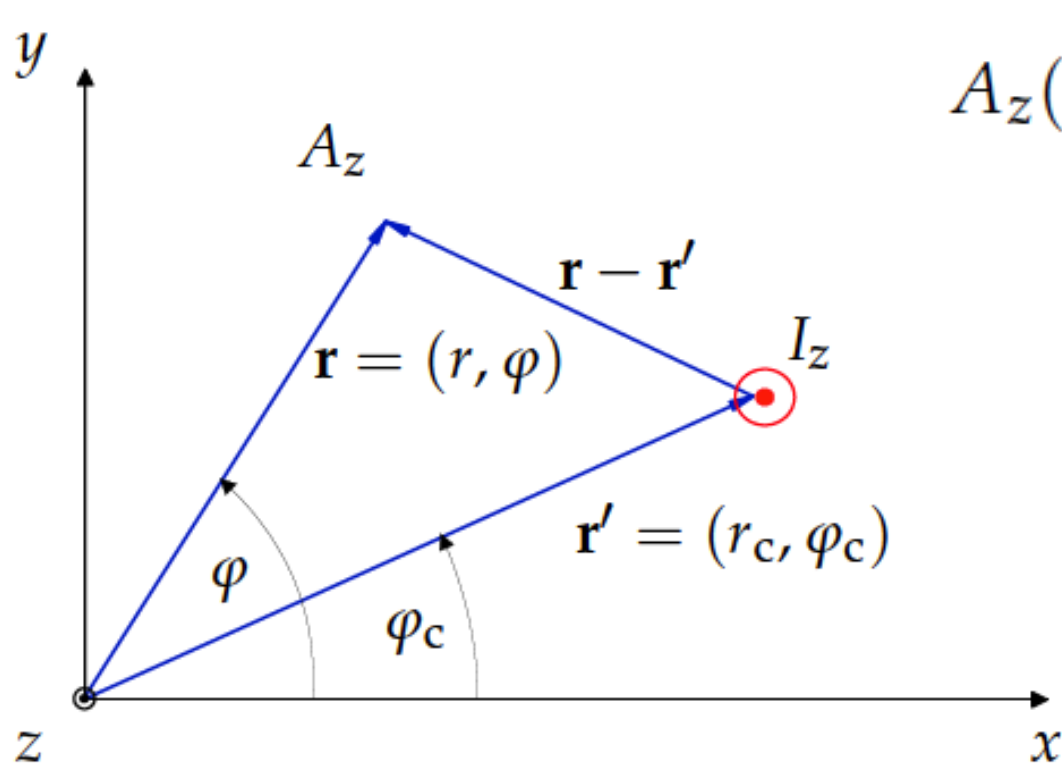
$$\mathbf{A}(x, y) = -\frac{\mu_0 I}{4\pi} \ln \left(\frac{x^2 + y^2}{x_0^2 + y_0^2} \right) \mathbf{e}_z = -\frac{\mu_0 I}{2\pi} \ln \left(\frac{r}{r_{\text{ref}}} \right) \mathbf{e}_z,$$

Field of a Line Current Segment



$$\begin{aligned}
 \mathbf{B}(\mathcal{P}) &= \frac{\mu_0 I}{4\pi} \int_{\mathcal{L}} \frac{\cos \alpha}{r_{\mathcal{P}\mathcal{Q}}^2} d\mathbf{r}' = \frac{\mu_0 I}{4\pi R} \mathbf{n} \int_{\alpha_1}^{\alpha_2} \cos \alpha d\alpha = \frac{\mu_0 I}{4\pi R} (\sin \alpha_2 - \sin \alpha_1) \mathbf{n} \\
 &= \frac{\mu_0 I}{4\pi} \frac{\cos \alpha_2 + \cos \alpha_1}{R} \frac{\sin \alpha_2 - \sin \alpha_1}{\cos \alpha_2 + \cos \alpha_1} \mathbf{n} \\
 &= \frac{\mu_0 I}{4\pi} \left(\frac{1}{|\mathbf{r}_1|} + \frac{1}{|\mathbf{r}_2|} \right) \frac{\sin(\alpha_2 - \alpha_1)}{1 + \cos(\alpha_2 - \alpha_1)} \mathbf{n} \\
 &= \frac{\mu_0 I}{4\pi} \left(\frac{1}{|\mathbf{r}_1|} + \frac{1}{|\mathbf{r}_2|} \right) \frac{\sin(\alpha_2 - \alpha_1)}{1 + \frac{\mathbf{r}_1 \cdot \mathbf{r}_2}{|\mathbf{r}_1| |\mathbf{r}_2|}} \frac{\mathbf{r}_1 \times \mathbf{r}_2}{|\mathbf{r}_1| |\mathbf{r}_2| \sin(\alpha_2 - \alpha_1)} \\
 &= \frac{\mu_0 I}{4\pi} \frac{|\mathbf{r}_1| + |\mathbf{r}_2|}{|\mathbf{r}_1| |\mathbf{r}_2| + \mathbf{r}_1 \cdot \mathbf{r}_2} \frac{\mathbf{r}_1 \times \mathbf{r}_2}{|\mathbf{r}_1| |\mathbf{r}_2|}
 \end{aligned}$$

Expanding the Green's Function



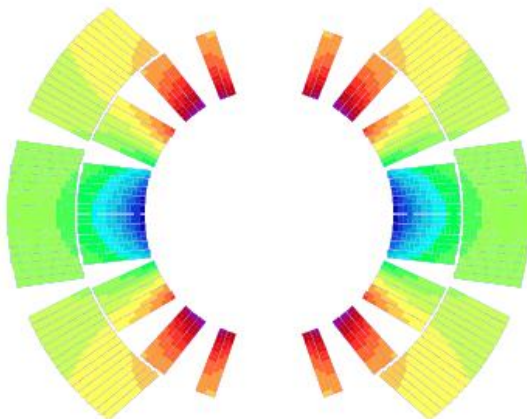
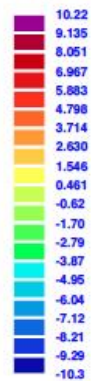
$$A_z(\mathbf{r}) = -\frac{\mu_0 I}{2\pi} \ln \left(\frac{|\mathbf{r} - \mathbf{r}'|}{r_{\text{ref}}} \right)$$

$$A_z(r, \varphi) = -\frac{\mu_0 I}{2\pi} \ln \left(\frac{r_c}{r_{\text{ref}}} \right) + \frac{\mu_0 I}{2\pi} \sum_{n=1}^{\infty} \frac{1}{n} \left(\frac{r}{r_c} \right)^n \cos n(\varphi - \varphi_c)$$

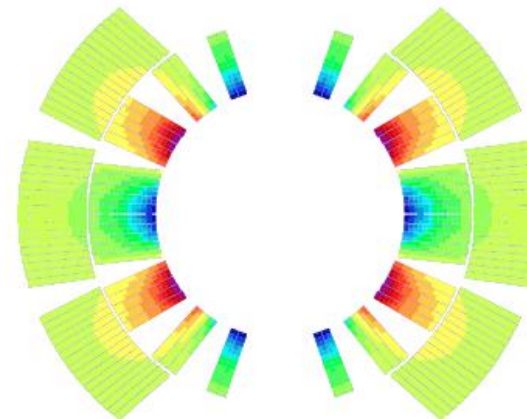
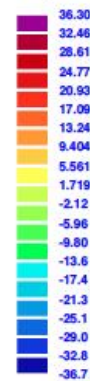
$$B_n(r_0) = -\frac{\mu_0 I}{2\pi r_c} \left(\frac{r_0}{r_c} \right)^{n-1} \cos n\varphi_c, \quad A_n(r_0) = \frac{\mu_0 I}{2\pi r_c} \left(\frac{r_0}{r_c} \right)^{n-1} \sin n\varphi_c.$$

Expanding the Green's Function II

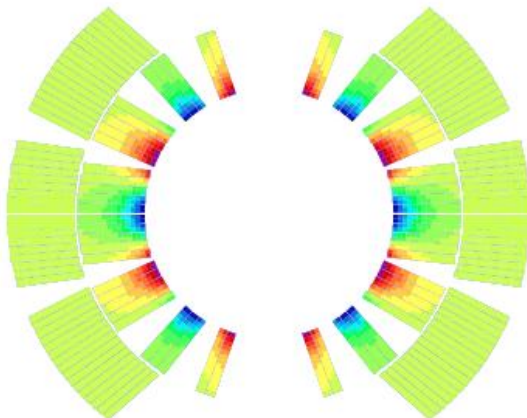
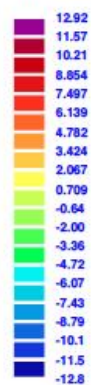
B3 (10E-4 T)



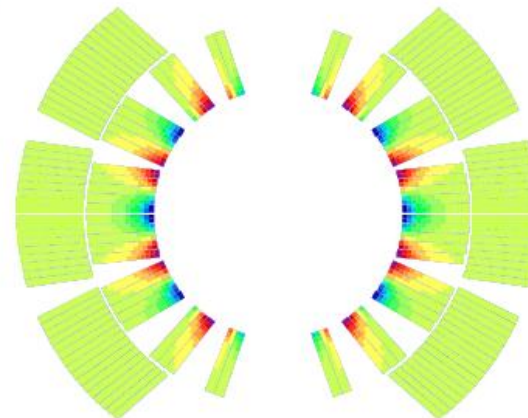
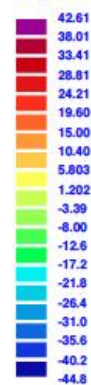
B5 (10E-5 T)



B7 (10E-5 T)



B9 (10E-6 T)

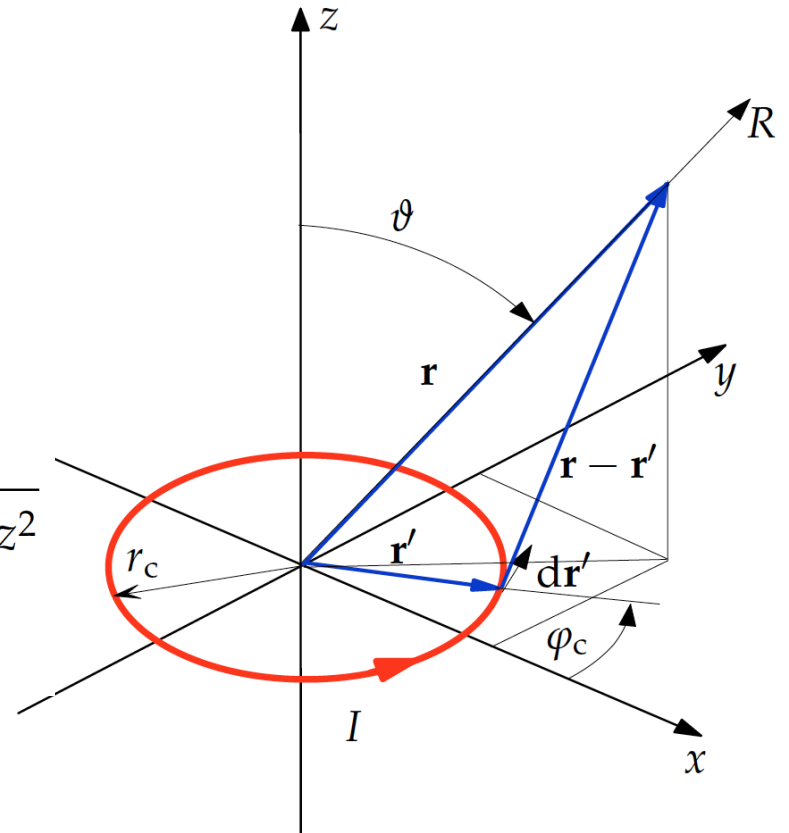


Field of a Ring Current

$$\mathbf{r}' = \cos \varphi_c r_c \mathbf{e}_x + \sin \varphi_c r_c \mathbf{e}_y$$

$$d\mathbf{r}' = -\sin \varphi_c r_c d\varphi_c \mathbf{e}_x + \cos \varphi_c r_c d\varphi_c \mathbf{e}_y$$

$$\begin{aligned} |\mathbf{r} - \mathbf{r}'| &= \sqrt{(x - x_c)^2 + (y - y_c)^2 + z^2} \\ &= \sqrt{(r \cos \varphi - r_c \cos \varphi_c)^2 + (r \sin \varphi - r_c \sin \varphi_c)^2 + z^2} \\ &= \sqrt{r^2 + r_c^2 + z^2 - 2rr_c \cos \varphi_c}, \end{aligned}$$



Field of a Ring Current

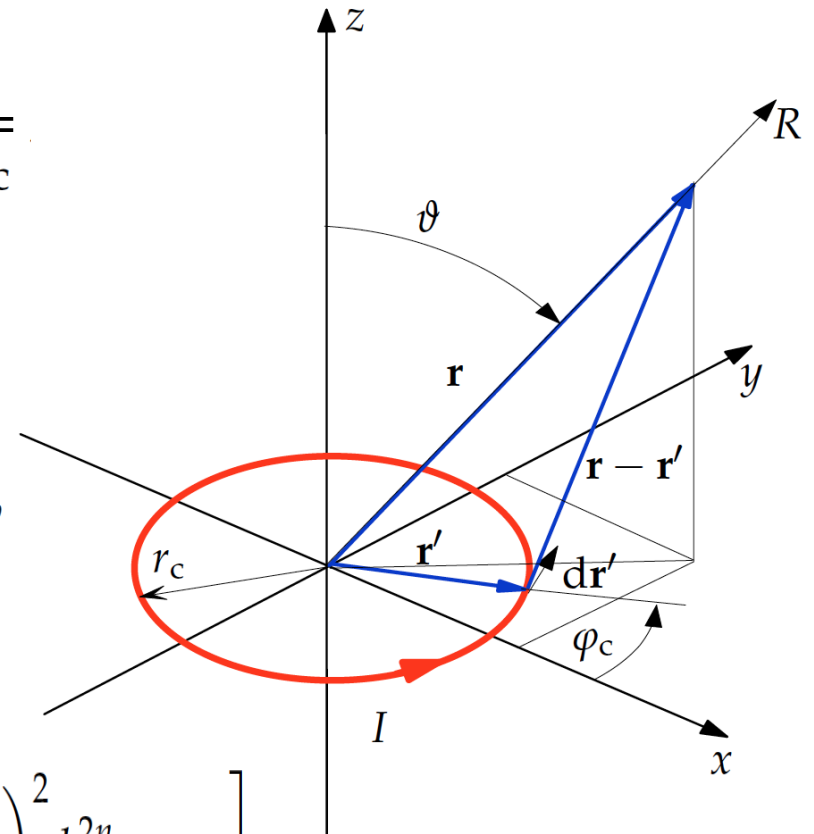
$$A_y(r, z) = \frac{\mu_0 I r_c}{2\pi} \int_0^\pi \frac{\cos \varphi_c d\varphi_c}{\sqrt{r^2 + r_c^2 + z^2 - 2rr_c \cos \varphi_c}}$$

$$\psi := (\pi + \varphi_c)/2, \quad k^2 := \frac{4rr_c}{(r + r_c)^2 + z^2}$$

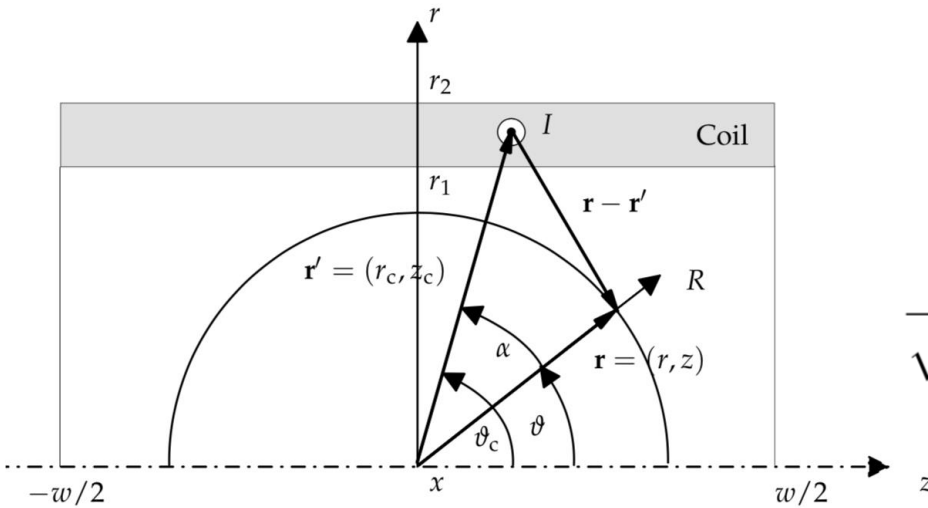
$$A_\varphi(r, z) = \frac{\mu_0 I r_c}{\pi \sqrt{(r + r_c)^2 + z^2}} \int_0^{\pi/2} \frac{2 \sin^2 \psi - 1}{\sqrt{1 - k^2 \sin^2 \psi}} d\psi$$

$$K\left(\frac{\pi}{2}, k\right) = \frac{\pi}{2} \left[1 + \left(\frac{1}{2}\right)^2 k^2 + \left(\frac{1 \cdot 3}{2 \cdot 4}\right)^2 k^4 + \dots + \left(\frac{(2n)!}{2^{2n}(n!)^2}\right)^2 k^{2n} + \dots \right]$$

$$A_\varphi(r, z) = \frac{\mu_0 I}{2\pi r} \sqrt{(r + r_c)^2 + z^2} \left[\left(1 - \frac{k^2}{2}\right) K\left(\frac{\pi}{2}, k\right) - E\left(\frac{\pi}{2}, k\right) \right]$$



Expanding the Green's Function



$$A_\varphi(R, \vartheta) = \sum_{n=1}^{\infty} \mu_0 \mathcal{A}_n R^n P_n^1(\cos \vartheta),$$

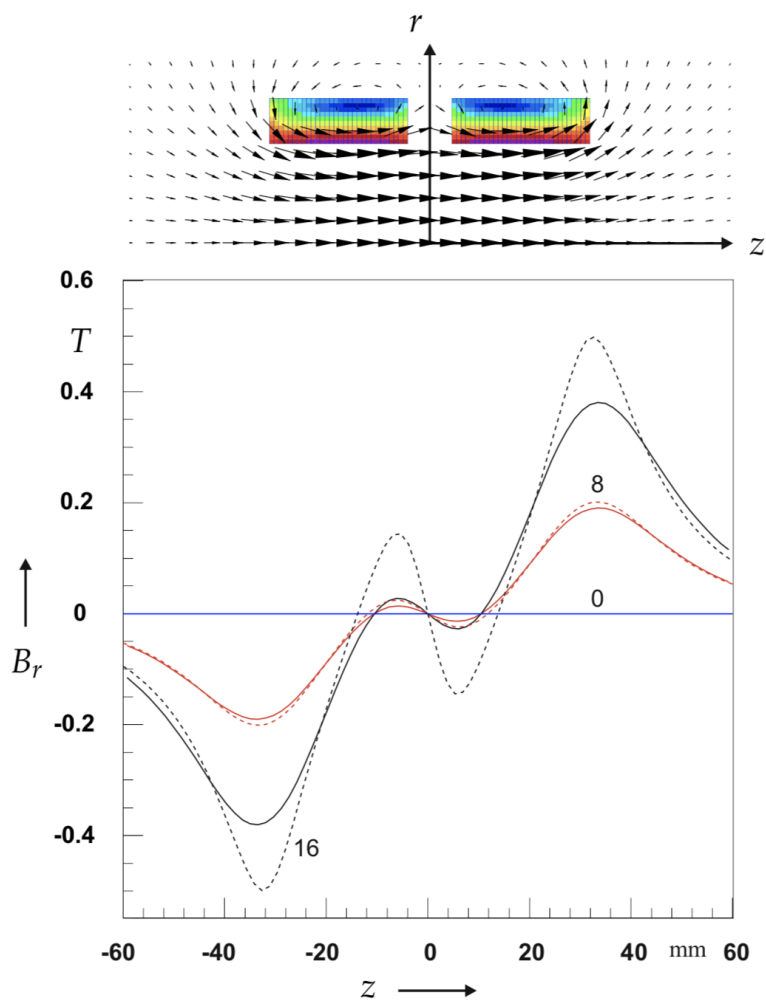
$$\frac{1}{\sqrt{|\mathbf{r}|^2 + |\mathbf{r}'|^2 - 2|\mathbf{r}||\mathbf{r}'| \cos \alpha}} = \frac{1}{|\mathbf{r}'|} \sum_{n=0}^{\infty} \left(\frac{|\mathbf{r}|}{|\mathbf{r}'|} \right)^n P_n(\cos \alpha)$$

$$\begin{aligned} A_\varphi &= \frac{\mu_0 I r_c}{2\pi} \int_0^\pi \frac{\cos \varphi_c d\varphi_c}{\sqrt{r^2 + r_c^2 + (z - z_c)^2 - 2r r_c \cos \varphi_c}} \\ &= \frac{\mu_0 I r_c}{2\pi} \int_0^\pi \frac{\cos \varphi_c d\varphi_c}{\sqrt{|\mathbf{r}|^2 + |\mathbf{r}'|^2 - 2|\mathbf{r}||\mathbf{r}'|(\cos \vartheta \cos \vartheta_c + \sin \vartheta \sin \vartheta_c \cos \varphi_c)}} \\ &= \frac{\mu_0 I r_c}{2} \frac{1}{|\mathbf{r}'|} \sum_{n=1}^{\infty} \left(\frac{|\mathbf{r}|}{|\mathbf{r}'|} \right)^n \frac{(n-1)!}{(n+1)!} P_n^1(\cos \vartheta) P_n^1(\cos \vartheta_c). \end{aligned}$$

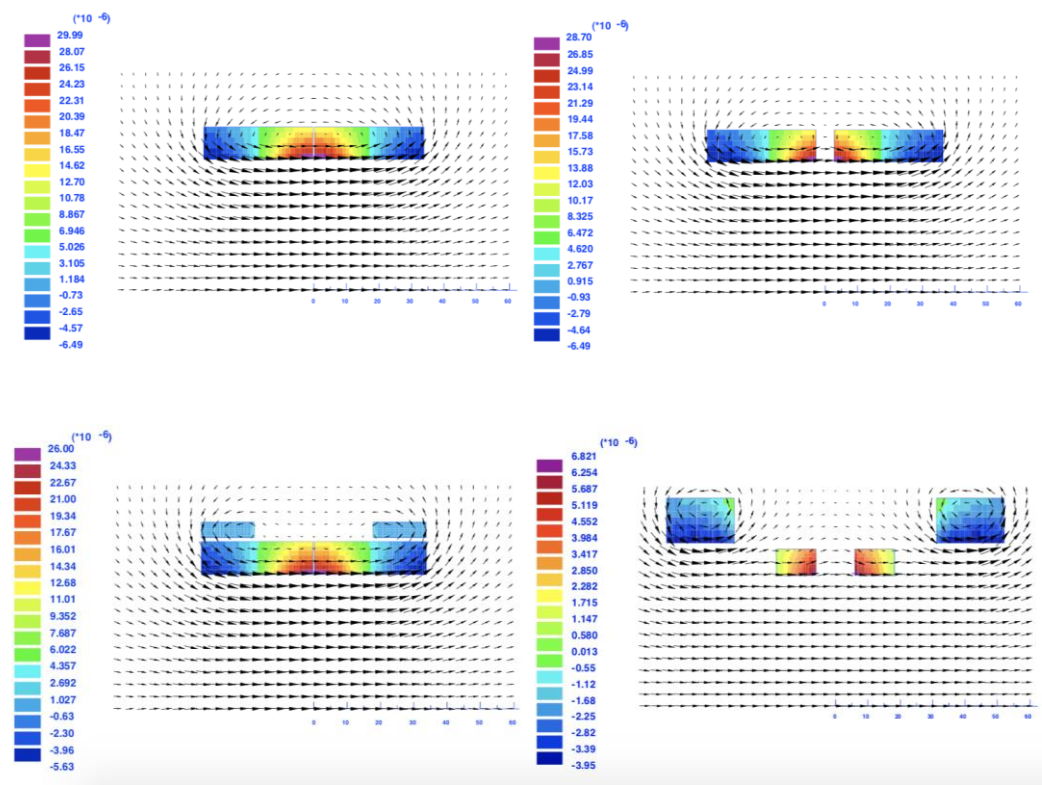
$$\mathcal{A}_n = \frac{I r_c}{2} \frac{1}{R_c^{n+1}} \frac{1}{n(n+1)} P_n^1(\cos \vartheta_c).$$

Split-Coil Solenoids

Field approximation up to first order
(at different radii)



Optimization of the field homogeneity
(suppressing the 3rd zonal harmonic)



Magnetic Dipole Moment

Far field approximation

$$A_\varphi(R, \vartheta) \approx \frac{\mu_0 I r_c^2 \pi \sin \vartheta}{4\pi R^2} = \frac{\mu_0 m \sin \vartheta}{4\pi R^2},$$

$$R = \sqrt{r^2 + z^2} \text{ and } \sin \vartheta = r/R,$$

$$[m] = 1 \text{ A m}^2. \quad \text{Definition} \quad m := I r_c^2 \pi$$
$$\mathbf{m} = I \mathbf{a},$$

$$\mathbf{m} = \frac{I}{2} \int_{\mathcal{C}} \mathbf{r} \times d\mathbf{r},$$

$$\mathbf{M}(\mathbf{r}) := \frac{d\mathbf{m}}{dV} = \frac{1}{2} \mathbf{r} \times \mathbf{J}(\mathbf{r}),$$

Solid Angle and Magnetic Scalar Potential

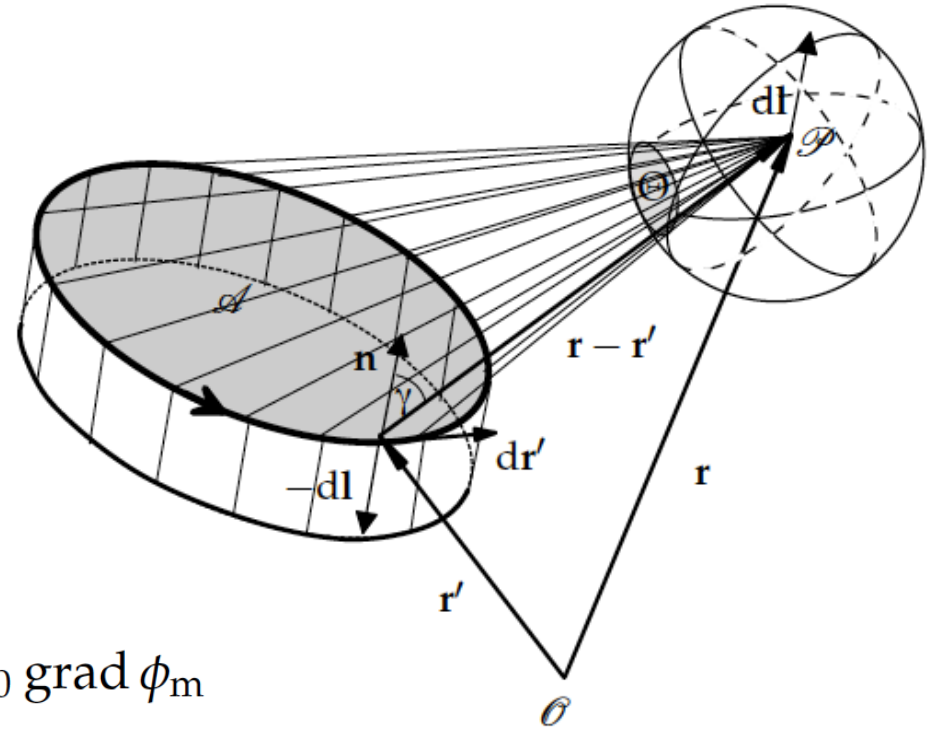
$$d\Theta = - \int_{\partial\mathcal{A}} \frac{1}{|\mathbf{r} - \mathbf{r}'|^2} (d\mathbf{l} \times d\mathbf{r}') \cdot \mathbf{e}_R = - \int_{\partial\mathcal{A}} \frac{(\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3} \cdot (d\mathbf{l} \times d\mathbf{r}') \\ = -d\mathbf{l} \int_{\partial\mathcal{A}} \frac{d\mathbf{r}' \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3}.$$

Expressing $d\Theta$ as $\text{grad } \Theta \cdot d\mathbf{l}$

$$\text{grad } \Theta = - \int_{\partial\mathcal{A}} \frac{d\mathbf{r}' \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3}$$

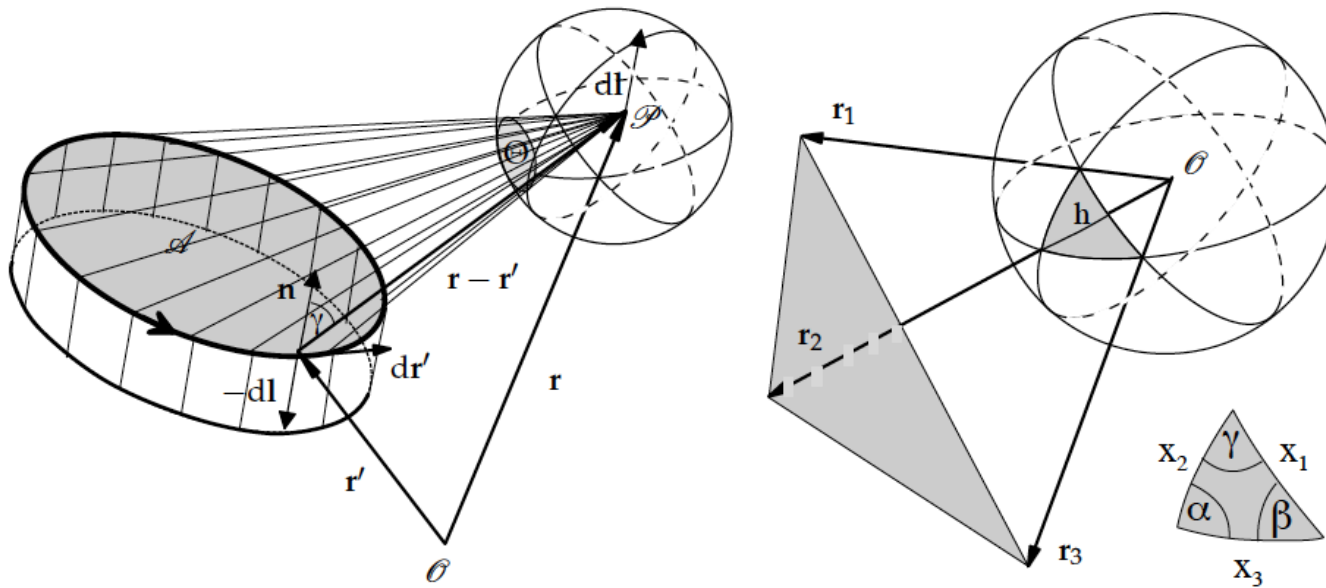
$$\mathbf{B}(\mathbf{r}) = \frac{\mu_0 I}{4\pi} \int_{\partial\mathcal{A}_c} \frac{d\mathbf{r}' \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3} = \mu_0 \mathbf{H} = -\mu_0 \text{grad } \phi_m$$

$$\phi_m(\mathbf{r}) = \frac{I}{4\pi} \Theta.$$



Solid angle (easy to compute) yields the magnetic scalar potential of a current loop

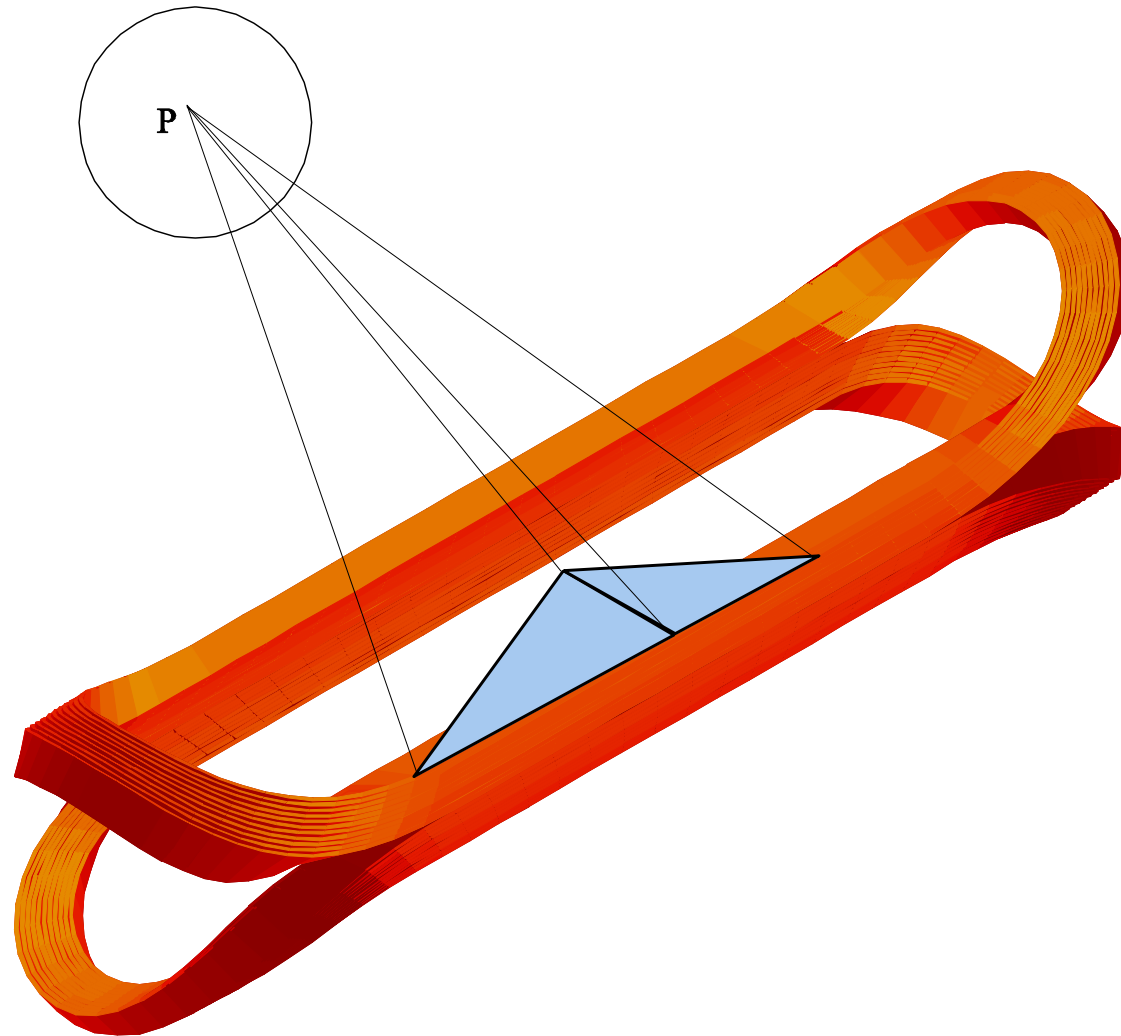
Solid Angle and Magnetic Scalar Potential



$$\Theta = \int_{\mathcal{A}} \frac{\cos \gamma}{R^2} da = \int_{\mathcal{A}} \frac{(\mathbf{r} - \mathbf{r}') \cdot \mathbf{n}}{|\mathbf{r} - \mathbf{r}'|^3} da,$$

$$\tan \left(\frac{\Theta}{2} \right) = \frac{\mathbf{r}_1 \cdot (\mathbf{r}_2 \times \mathbf{r}_3)}{r_1 r_2 r_3 + (\mathbf{r}_1 \cdot \mathbf{r}_2) r_3 + (\mathbf{r}_1 \cdot \mathbf{r}_3) r_2 + (\mathbf{r}_2 \cdot \mathbf{r}_3) r_1}.$$

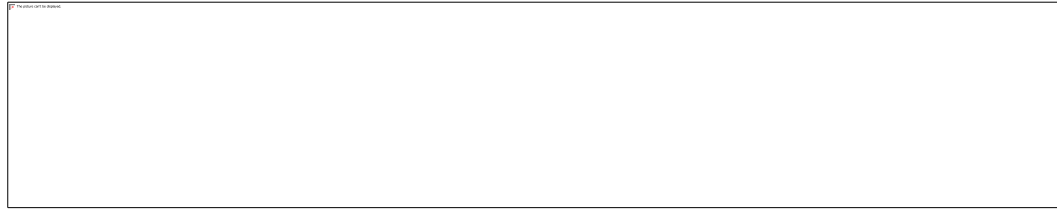
Total Magnetic Scalar Potential



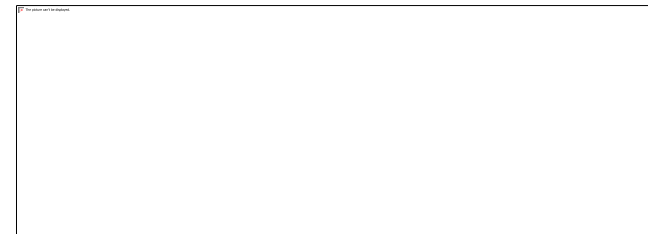
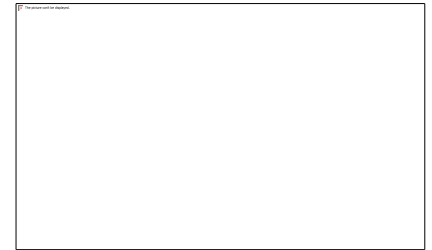
Finite-Element Shape Functions



The Model Problem (1-D)

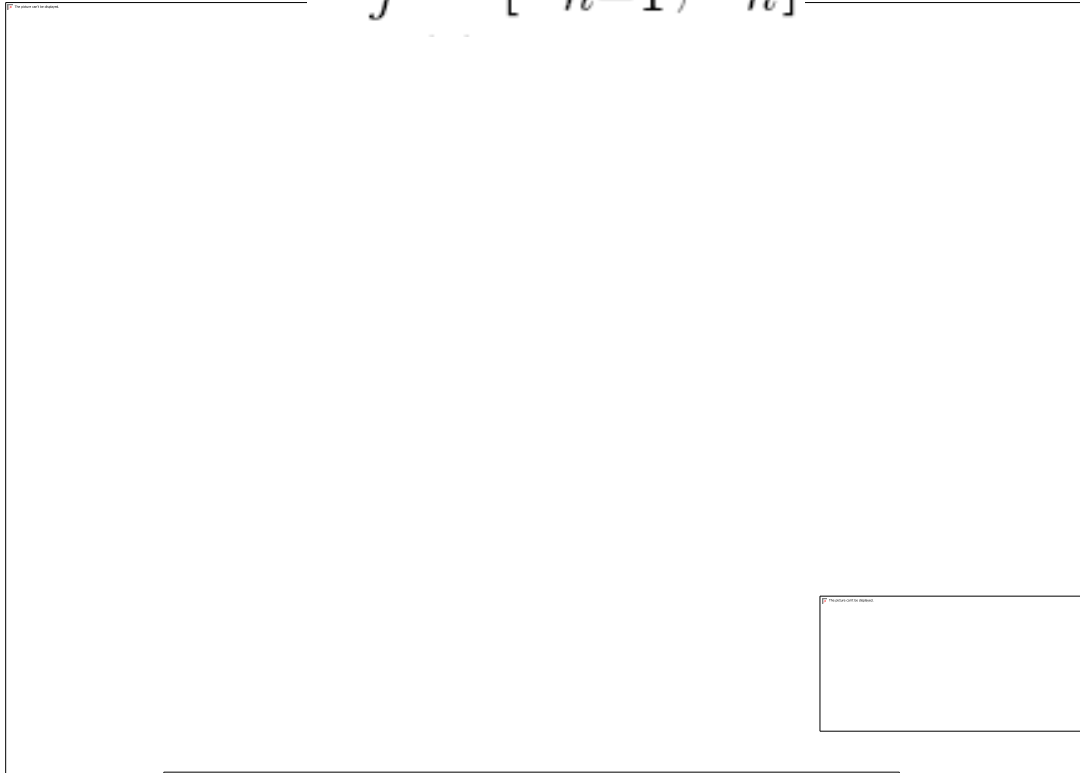


or



Shape Functions

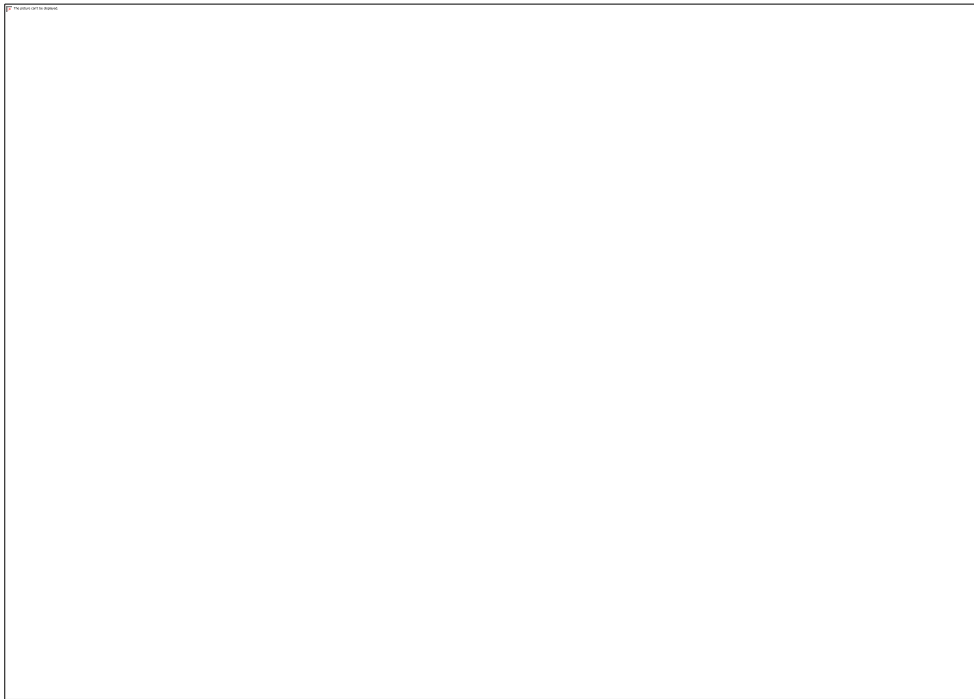
$$\Omega_j = [x_{n-1}, x_n]$$



$$\Omega = \bigcup_{j=1}^J \Omega_j$$



$$u_n = \alpha_{j1} + \alpha_{j2}x_n$$

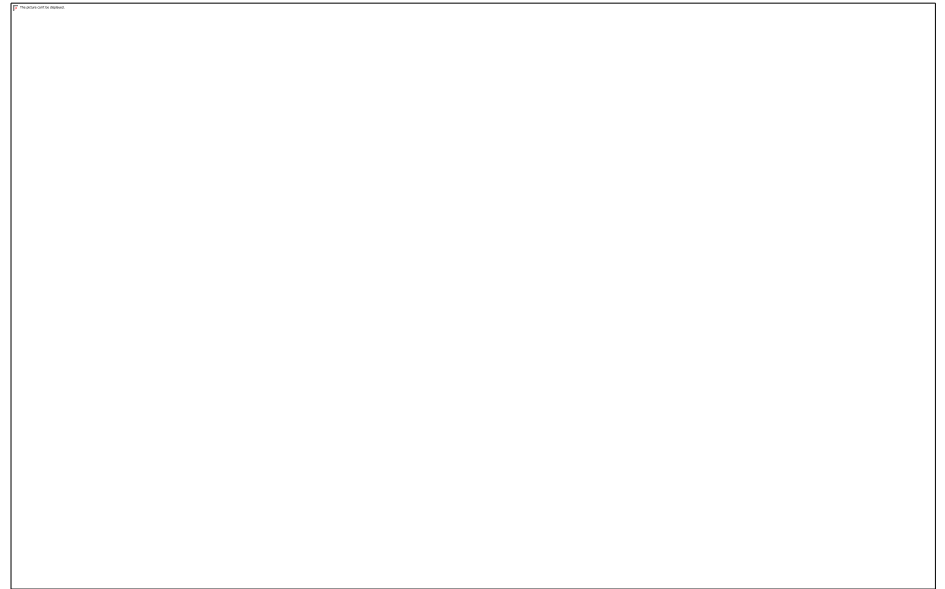
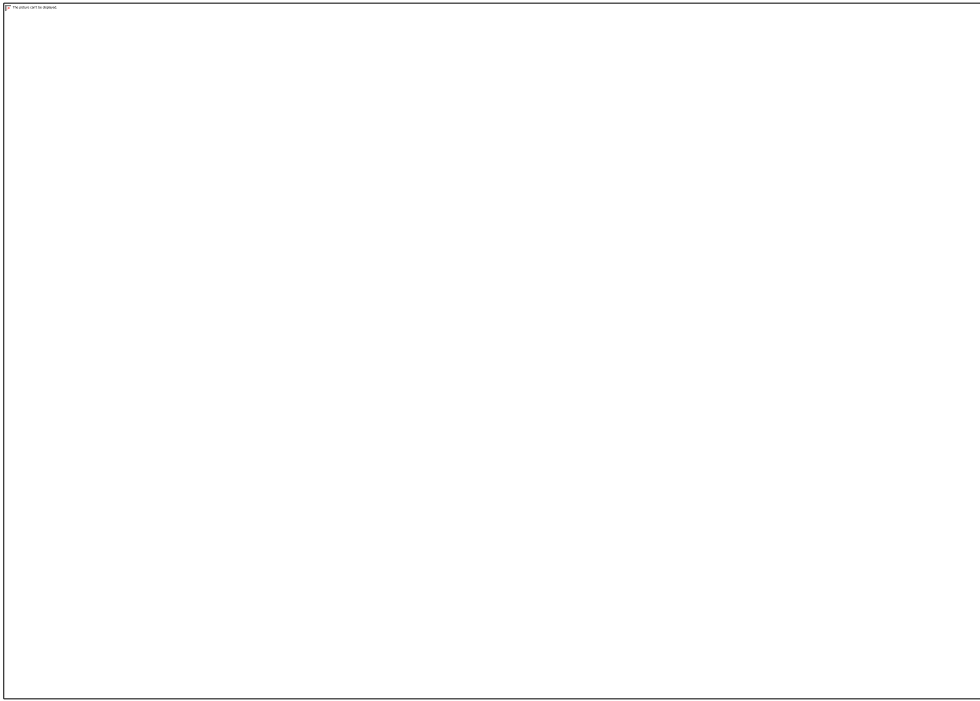


Cramer's rule



$$u_j(x) = \alpha_{j1} + \alpha_{j2}x = \frac{x_n - x}{x_n - x_{n-1}}u_{n-1} + \frac{-x_{n-1} + x}{x_n - x_{n-1}}u_n$$

Shape Functions



$$N_{j1}(x) = \frac{x_n - x}{x_n - x_{n-1}}$$



What have we won? We can express the field in the element as a function of the node potentials using known polynomials in the spatial coordinates

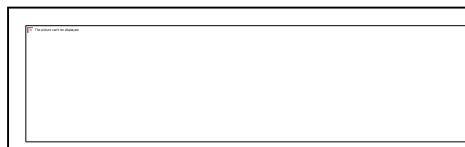
The Weighted Residual



What have we won? Removal of the second derivative, a way to incorporate Neumann boundary conditions



$$\int_{\Omega_j} \frac{dw_l(x)}{dx} \sum_{k=1,2} \frac{dN_{jk}(x)}{dx} u^{(k)} d\Omega_j = - \int_{\Omega_j} w_l(x) f(x) d\Omega_j, \quad l = 1, 2.$$

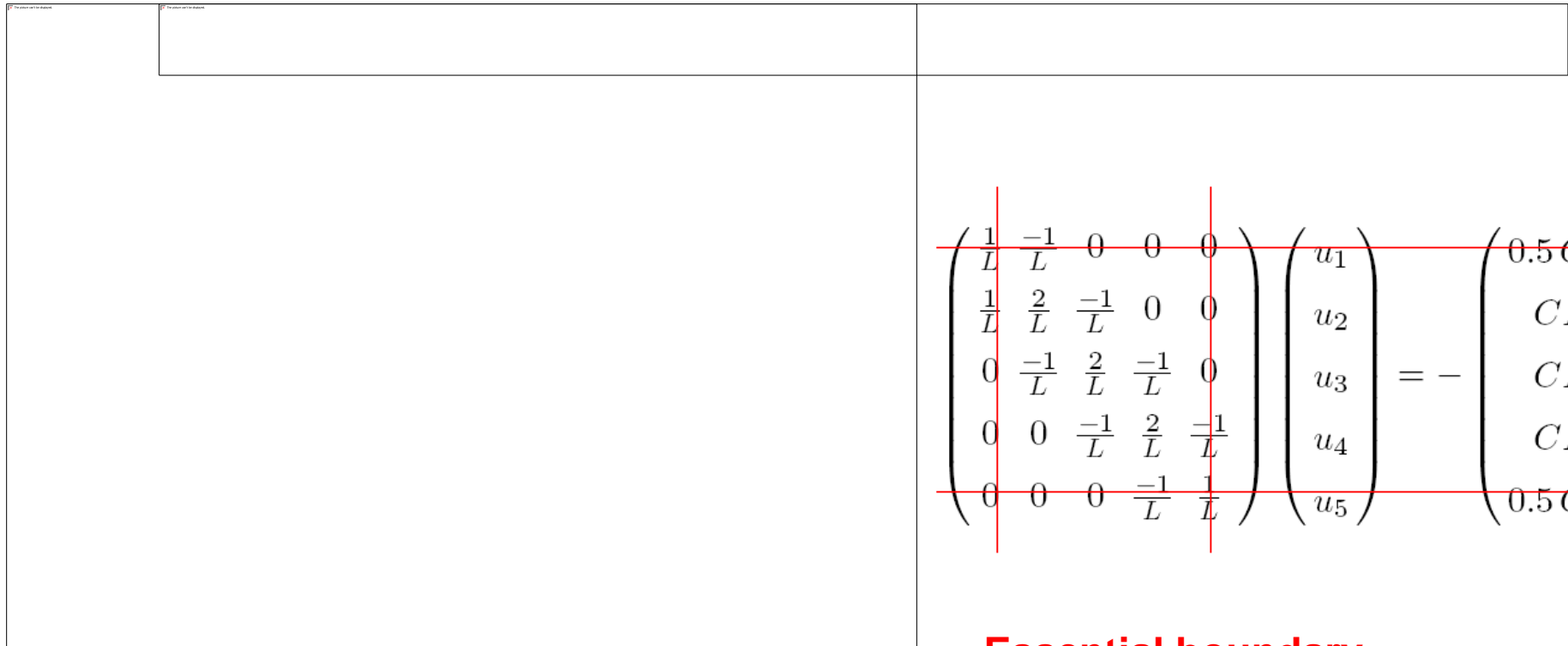


Linear equation system for the node potentials

Numerical Example

$$\{f_j\} = - \int_{x_{n-1}}^{x_n} \begin{pmatrix} N_{j1} \\ N_{j2} \end{pmatrix} C dx = -C \int_{x_{n-1}}^{x_n} \begin{pmatrix} \frac{x_n - x}{x_n - x_{n-1}} \\ \frac{-x_{n-1} + x}{x_n - x_{n-1}} \end{pmatrix} dx$$

Numerical Example



$$\begin{pmatrix} \frac{1}{L} & -\frac{1}{L} & 0 & 0 & 0 \\ \frac{1}{L} & \frac{2}{L} & -\frac{1}{L} & 0 & 0 \\ 0 & -\frac{1}{L} & \frac{2}{L} & -\frac{1}{L} & 0 \\ 0 & 0 & -\frac{1}{L} & \frac{2}{L} & -\frac{1}{L} \\ 0 & 0 & 0 & -\frac{1}{L} & \frac{1}{L} \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \end{pmatrix} = - \begin{pmatrix} 0.5CL \\ CL \\ CL \\ CL \\ 0.5CL \end{pmatrix}$$

Essential boundary conditions (Dirichlet)

$$\begin{pmatrix} u_2 \\ u_3 \\ u_4 \end{pmatrix} = - \begin{pmatrix} \frac{3L}{4} & \frac{L}{2} & \frac{L}{4} \\ \frac{L}{2} & L & \frac{L}{2} \\ \frac{L}{4} & \frac{L}{2} & \frac{2L}{4} \end{pmatrix} \begin{pmatrix} CL \\ CL \\ CL \end{pmatrix} = \begin{pmatrix} -0.375 \\ -0.5 \\ -0.375 \end{pmatrix}$$

Higher order elements

$$u^{(1)} = \alpha_{j1} + \alpha_{j2}x_1 + \alpha_{j3}x_1^2$$

$$u^{(2)} = \alpha_{j1} + \alpha_{j2}x_2 + \alpha_{j3}x_2^2$$

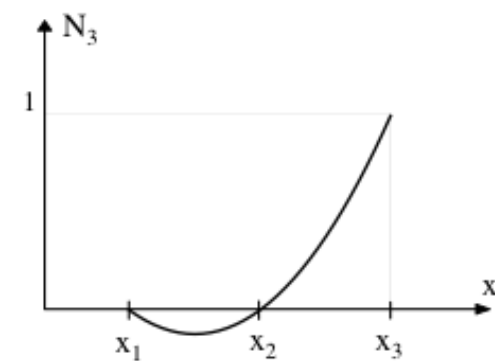
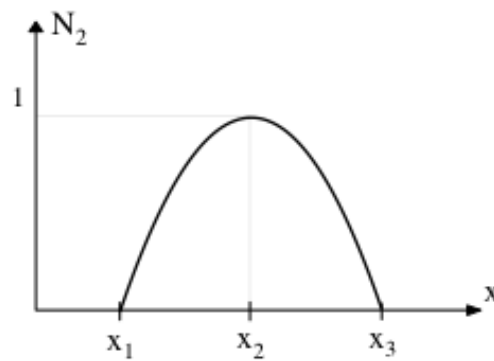
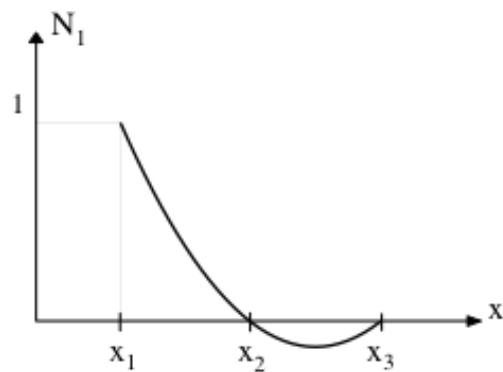
$$u^{(3)} = \alpha_{j1} + \alpha_{j2}x_3 + \alpha_{j3}x_3^2$$

$$u_j(x) = \sum_{k=1}^3 N_{jk}(x)u^{(k)}$$

$$N_{j1}(x) = \frac{(x - x_2)(x - x_3)}{(x_1 - x_2)(x_1 - x_3)},$$

$$N_{j2}(x) = \frac{(x - x_1)(x - x_3)}{(x_2 - x_1)(x_2 - x_3)}$$

$$N_{j3}(x) = \frac{(x - x_1)(x - x_2)}{(x_3 - x_1)(x_3 - x_2)}.$$



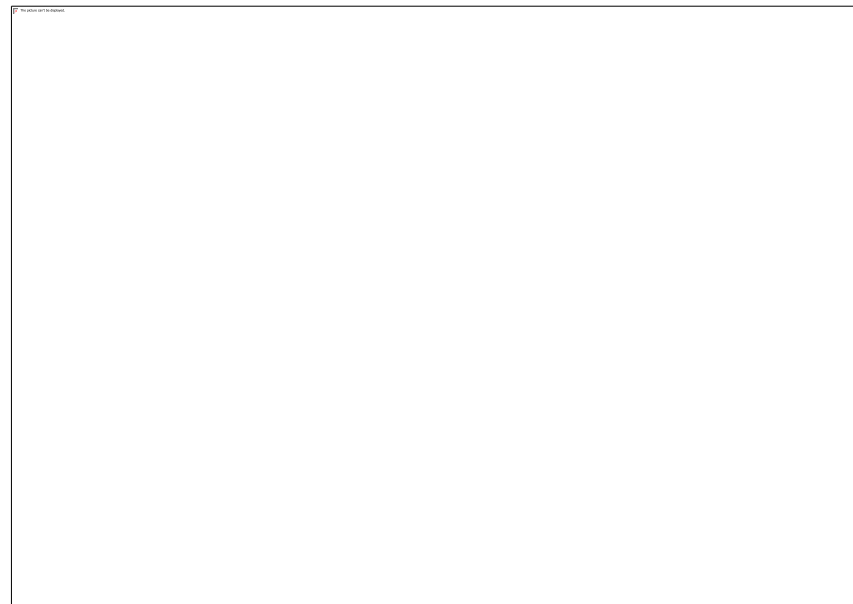
Two Quadratic Elements

$$[k_j] = \int_{x_1}^{x_3} \begin{pmatrix} \frac{dN_{j1}}{dx} \frac{dN_{j1}}{dx} & \frac{dN_{j1}}{dx} \frac{dN_{j2}}{dx} & \frac{dN_{j1}}{dx} \frac{dN_{j3}}{dx} \\ \frac{dN_{j2}}{dx} \frac{dN_{j1}}{dx} & \frac{dN_{j2}}{dx} \frac{dN_{j2}}{dx} & \frac{dN_{j2}}{dx} \frac{dN_{j3}}{dx} \\ \frac{dN_{j3}}{dx} \frac{dN_{j1}}{dx} & \frac{dN_{j3}}{dx} \frac{dN_{j2}}{dx} & \frac{dN_{j3}}{dx} \frac{dN_{j3}}{dx} \end{pmatrix} dx \quad [k_j] = \begin{pmatrix} \frac{7}{6l} & \frac{-8}{6l} & \frac{1}{6l} \\ \frac{-8}{6l} & \frac{16}{6l} & \frac{-8}{6l} \\ \frac{1}{6l} & \frac{-8}{6l} & \frac{7}{6l} \end{pmatrix}$$

$$\{f_j\} = - \int_{x_1}^{x_3} \begin{pmatrix} N_{j1} \\ N_{j2} \\ N_{j3} \end{pmatrix} f(x) dx \quad \{f_j\} = -\frac{1}{3}c \begin{pmatrix} l \\ 4l \\ l \end{pmatrix}$$

$$\begin{pmatrix} \frac{2}{l} & \frac{-1}{l} & 0 \\ \frac{-1}{l} & \frac{2}{l} & \frac{-1}{l} \\ 0 & \frac{-1}{l} & \frac{2}{l} \end{pmatrix} \begin{pmatrix} u_2 \\ u_3 \\ u_4 \end{pmatrix} = - \begin{pmatrix} cl \\ cl \\ cl \end{pmatrix}$$

$$\begin{pmatrix} u_2 \\ u_3 \\ u_4 \end{pmatrix} = - \begin{pmatrix} \frac{3l}{4} & \frac{l}{2} & \frac{l}{4} \\ \frac{l}{2} & l & \frac{l}{2} \\ \frac{l}{4} & \frac{l}{2} & \frac{3l}{4} \end{pmatrix} \begin{pmatrix} cl \\ cl \\ cl \end{pmatrix} = \begin{pmatrix} -0.375 \\ -0.5 \\ -0.375 \end{pmatrix}$$



Shape Functions

$$A_j(\mathbf{x}) = A_{z_j}(x, y)$$

$$A^{(1)} = \alpha_1 + \alpha_2 x_1 + \alpha_3 y_1$$

$$A^{(2)} = \alpha_1 + \alpha_2 x_2 + \alpha_3 y_2$$

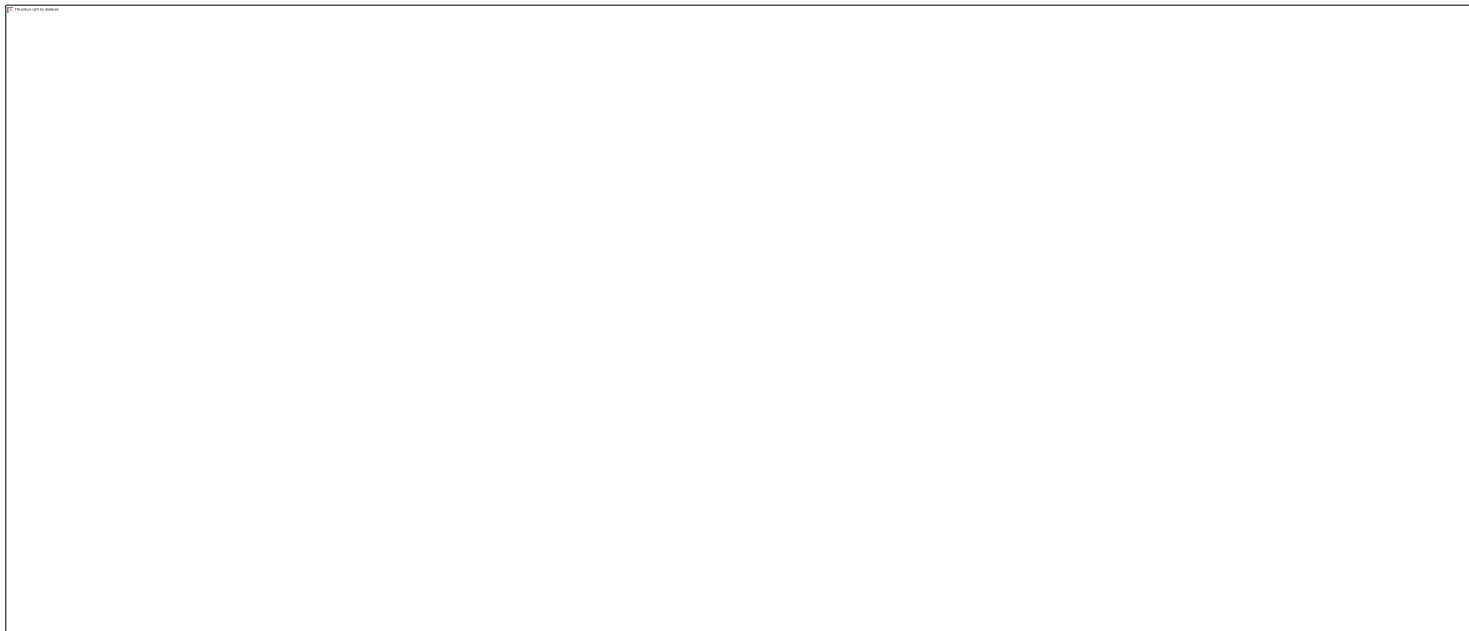
$$A^{(3)} = \alpha_1 + \alpha_2 x_3 + \alpha_3 y_3$$

Mapped Elements

$$x = x(\xi, \eta, \zeta),$$

$$y = y(\xi, \eta, \zeta),$$

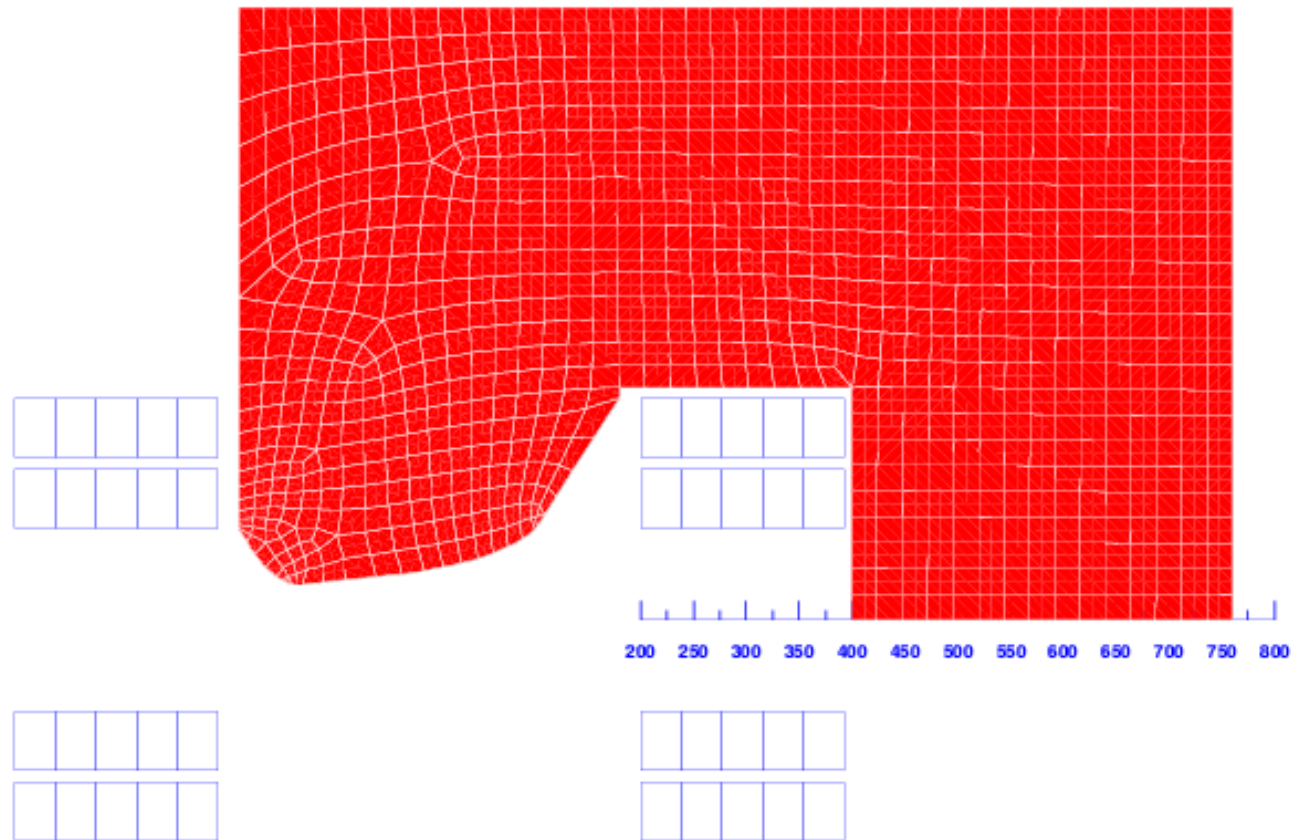
$$z = z(\xi, \eta, \zeta)$$



$$y_j(\boldsymbol{\xi}) = \sum_{k=1}^K N_k(\boldsymbol{\xi}) y^{(k)}$$

Use of the same shape functions for the transformation of the elements

Higher Order Elements



Higher accuracy of the field solution, but also better modeling of the iron contour

Mapped Elements



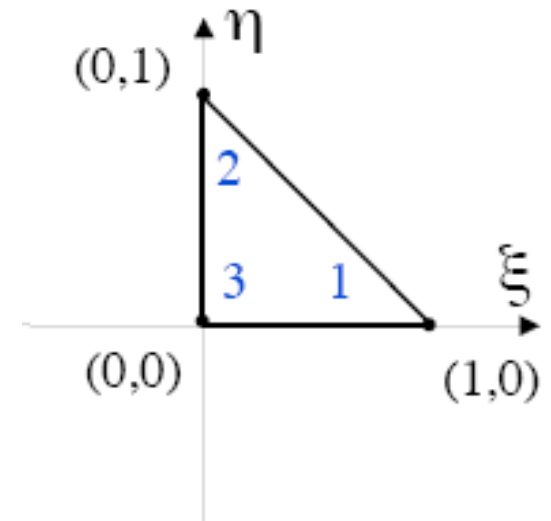
Transformation of Differential Operators



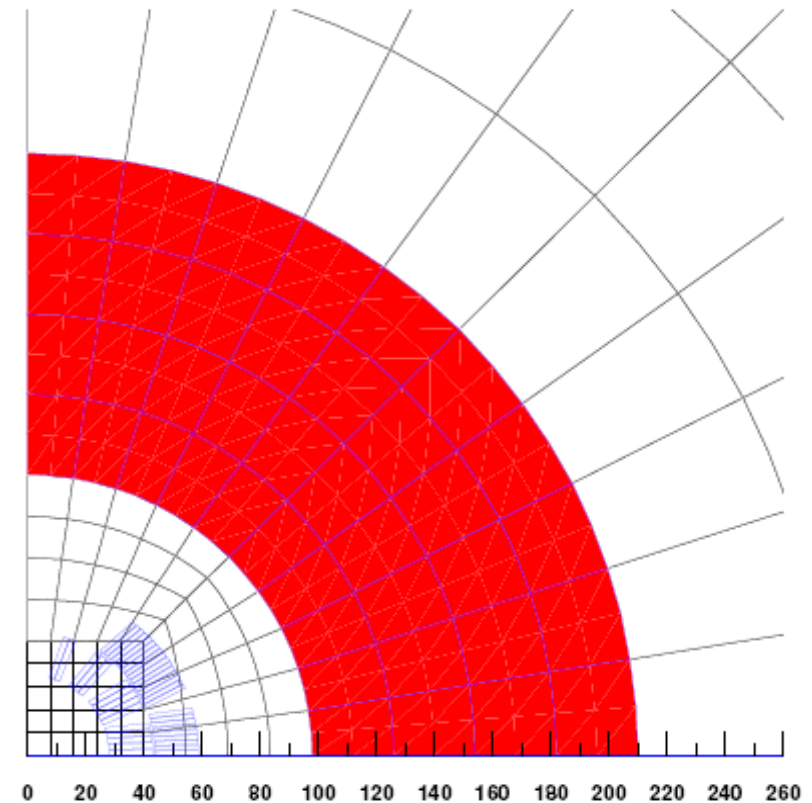
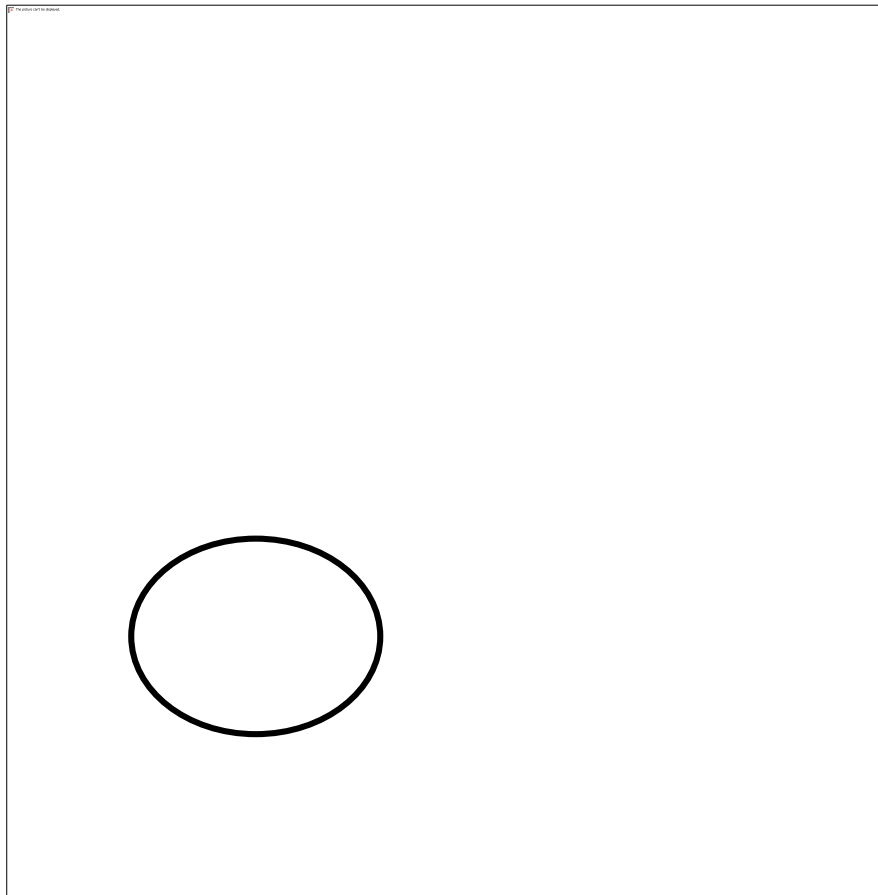
Complicated

$$\begin{pmatrix} \frac{\partial}{\partial x} \\ \frac{\partial}{\partial y} \end{pmatrix} N_k = \begin{pmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \eta}{\partial x} \\ \frac{\partial \xi}{\partial y} & \frac{\partial \eta}{\partial y} \end{pmatrix} \begin{pmatrix} \frac{\partial}{\partial \xi} \\ \frac{\partial}{\partial \eta} \end{pmatrix} N_k = [J]_{T^{-1}} \begin{pmatrix} \frac{\partial}{\partial \xi} \\ \frac{\partial}{\partial \eta} \end{pmatrix} N_k$$

Easy



Collinear Sides yield Singular Jacobi Matrices

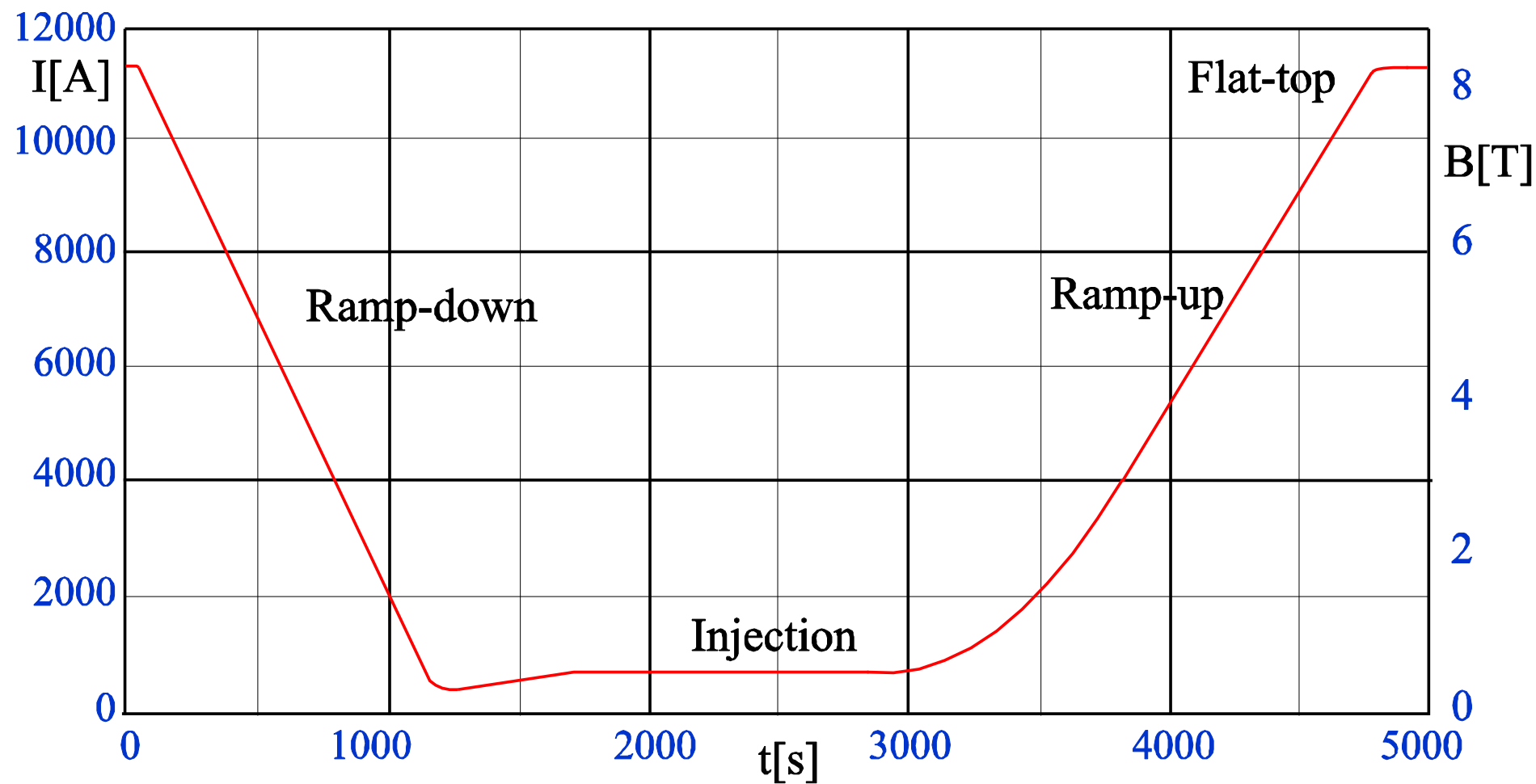


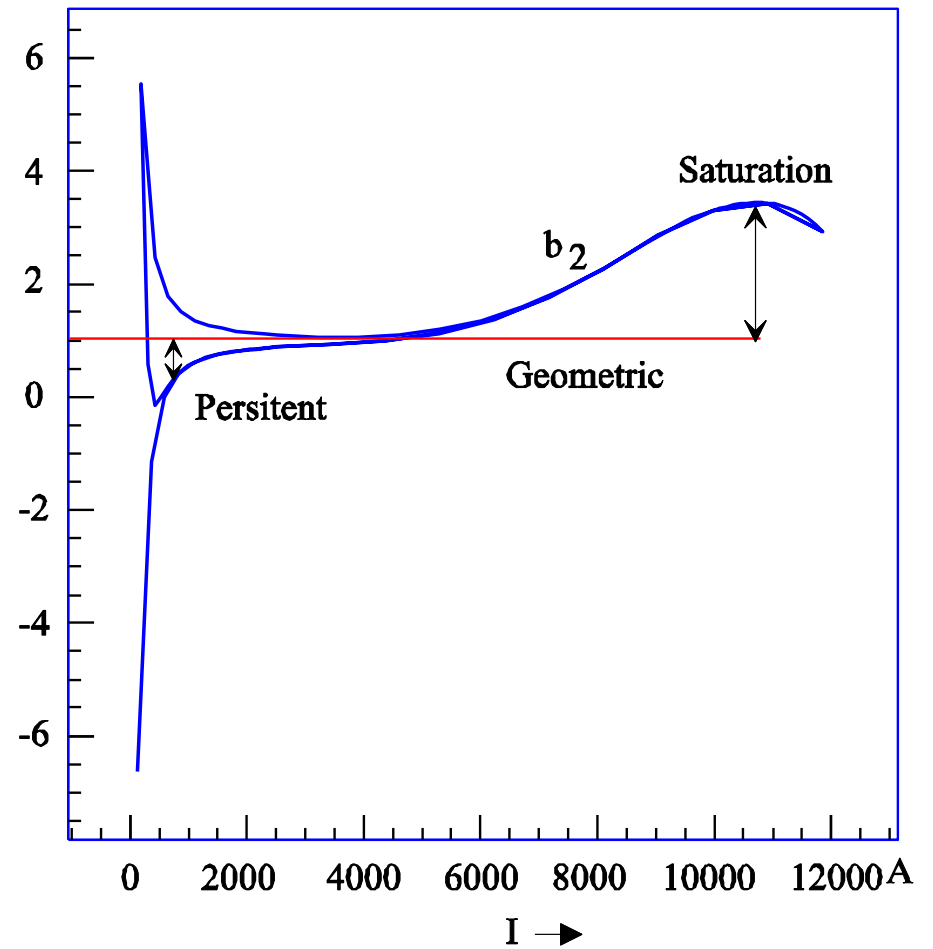
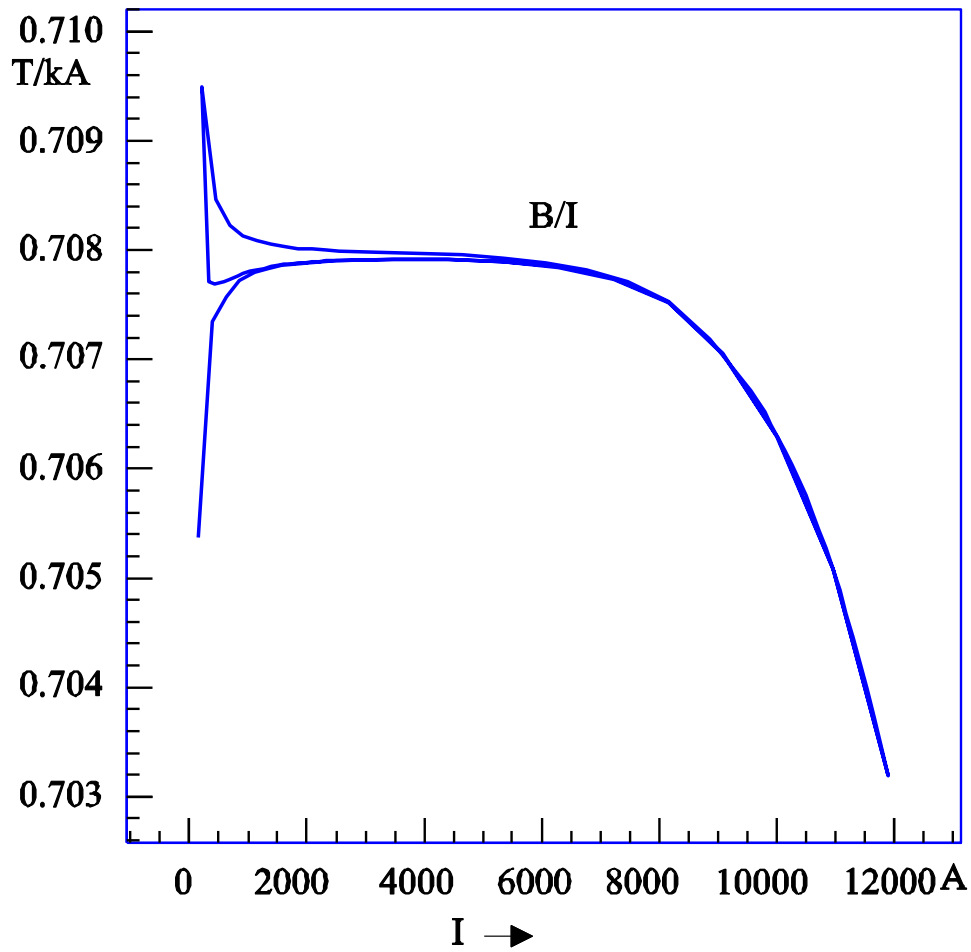
Note: Bad meshing is not a trivial offence

Numerical Methods for the Curl-Curl Equation

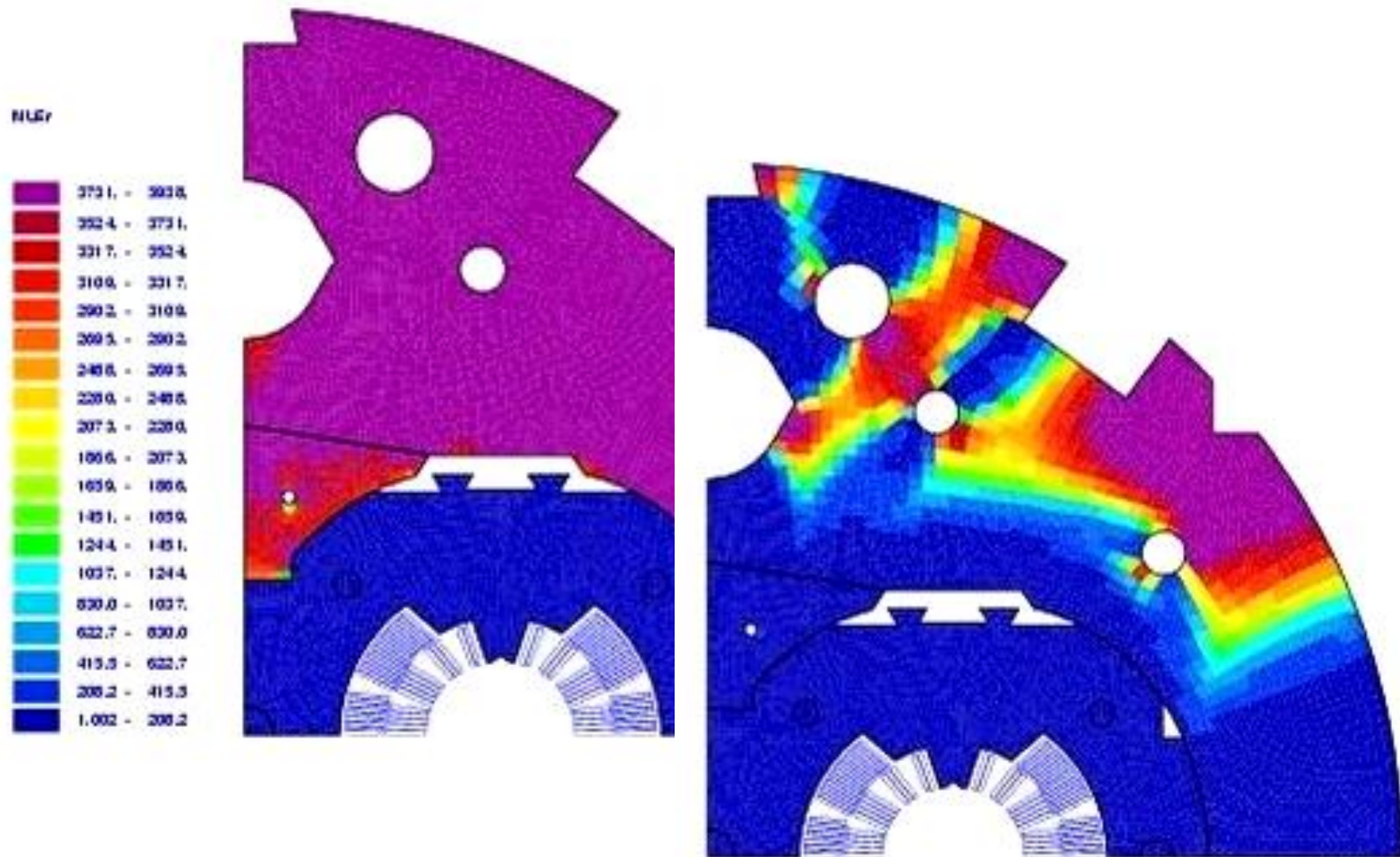


Excitation Cycle

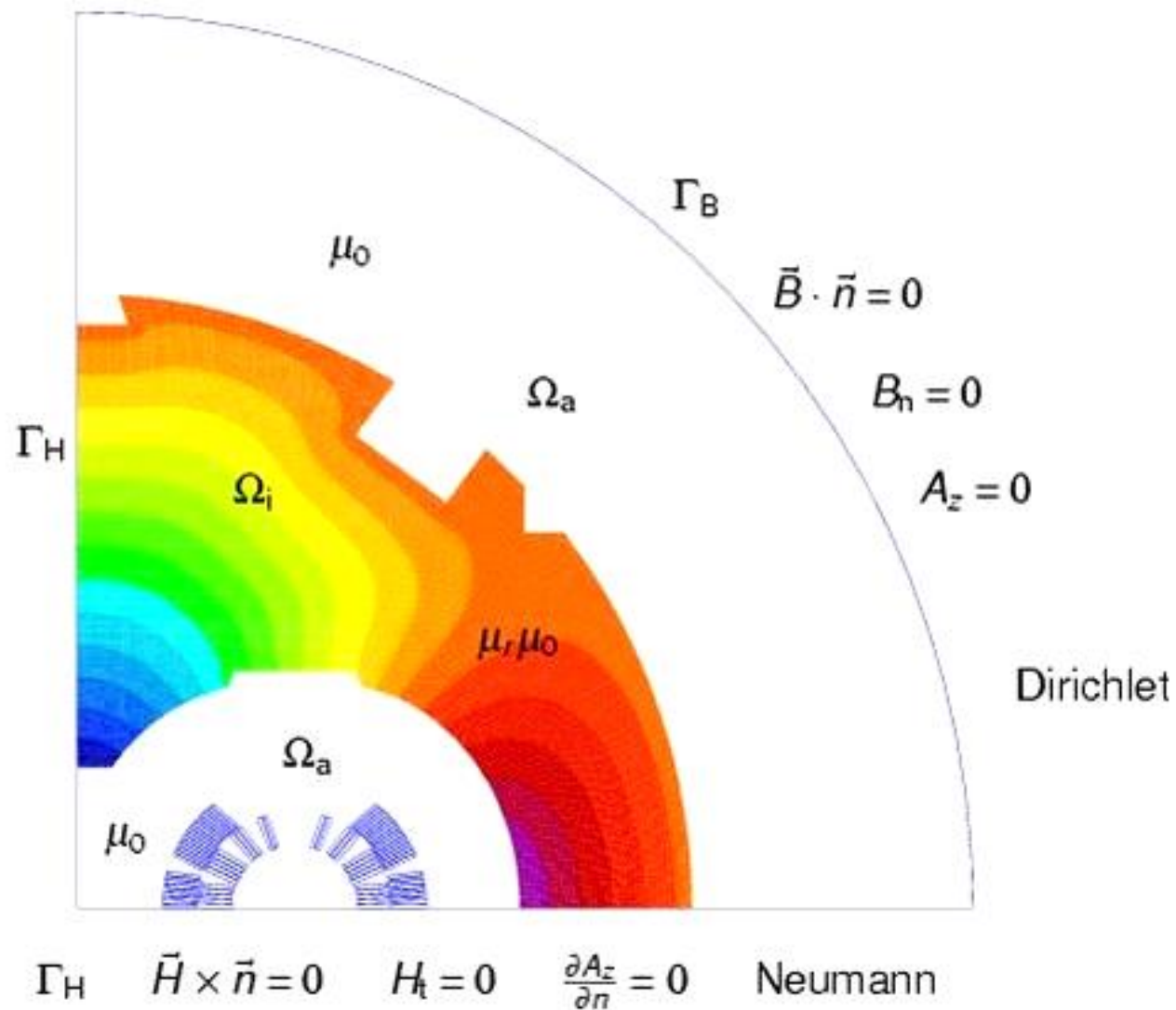




Saturation Effects in the Dipole Iron Yoke



The Problem Domain



$$\mathbf{B} = \text{curl } \mathbf{A} \quad \text{in } \Omega$$

$$\text{curl } \frac{1}{\mu} \text{curl } \mathbf{A} = \mathbf{J} \quad \text{in } \Omega$$

$$\mathbf{H}_t = \mathbf{0} \quad \rightarrow \quad \frac{1}{\mu} (\text{curl } \mathbf{A}) \times \mathbf{n} = \mathbf{0} \quad \text{on } \Gamma_H$$

$$B_n = 0 \quad \rightarrow \quad \mathbf{B} \cdot \mathbf{n} = \text{curl } \mathbf{A} \cdot \mathbf{n} = 0 \quad \text{on } \Gamma_B$$

$$\left[\frac{1}{\mu} (\text{curl } \mathbf{A}) \times \mathbf{n} \right]_{\text{ai}} = \mathbf{0} \quad \text{on } \Gamma_{\text{ai}}$$

$$[\mathbf{A}]_{\text{ai}} = \mathbf{0} \quad \text{on } \Gamma_{\text{ai}}$$

Problem in 3-D: Gauging

$$\mathbf{A} \rightarrow \mathbf{A}' : \mathbf{A}' = \mathbf{A} + \text{grad } \psi$$

$$\text{div } \mathbf{A}' = q$$

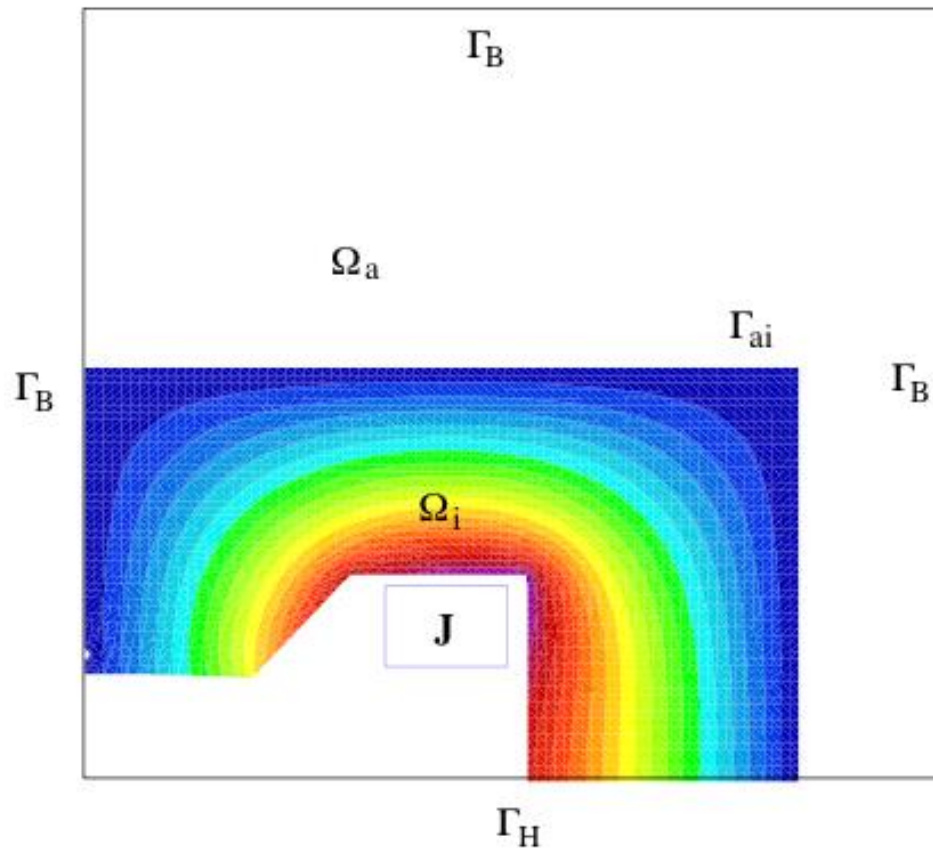
$$q = \text{div } \mathbf{A} + \nabla^2 \psi$$

$$\frac{1}{\mu} \text{div } \mathbf{A} = 0 \quad \text{in } \Omega$$

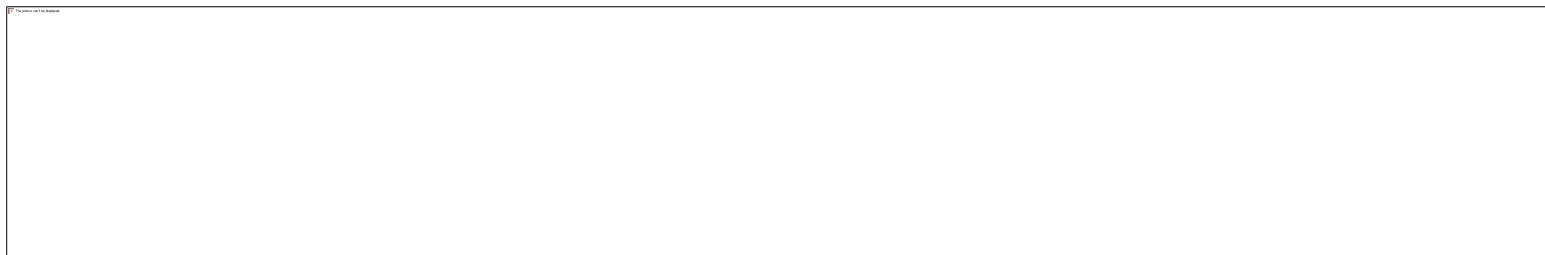
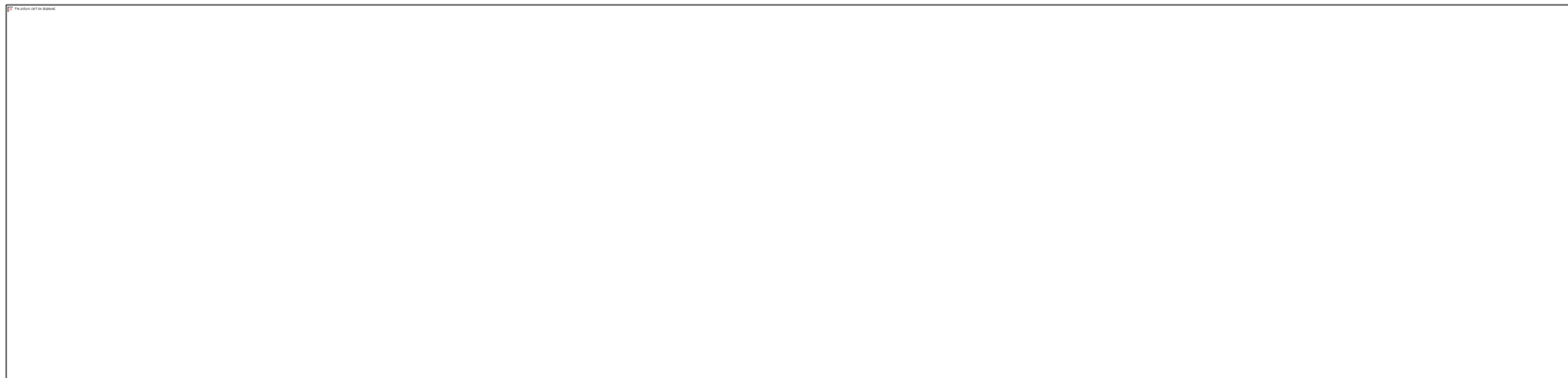
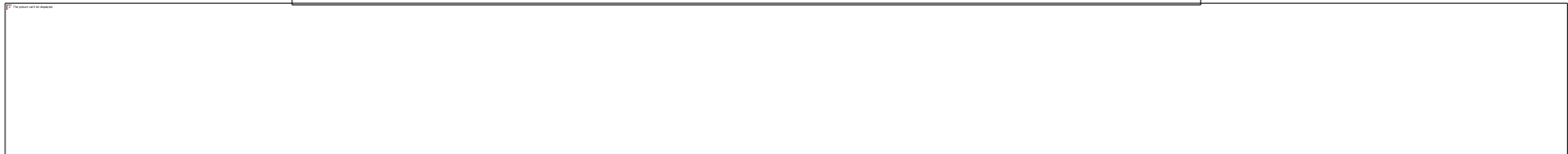
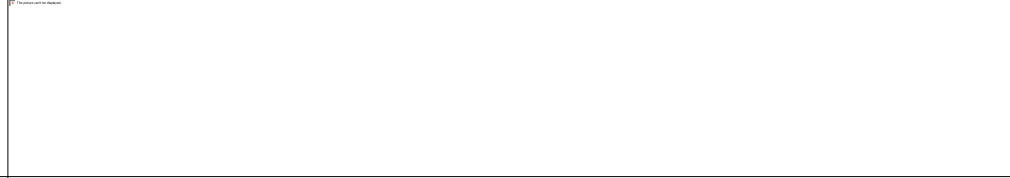
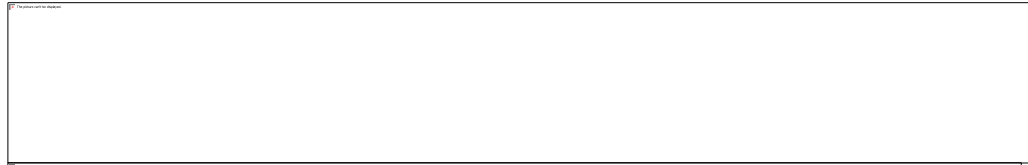
$$\mathbf{A} \cdot \mathbf{n} = 0 \quad \text{on } \Gamma_H$$

$$\text{curl } \frac{1}{\mu} \text{curl } \mathbf{A} - \text{grad } \frac{1}{\mu} \text{div } \mathbf{A} = \mathbf{J} \quad \text{in } \Omega$$

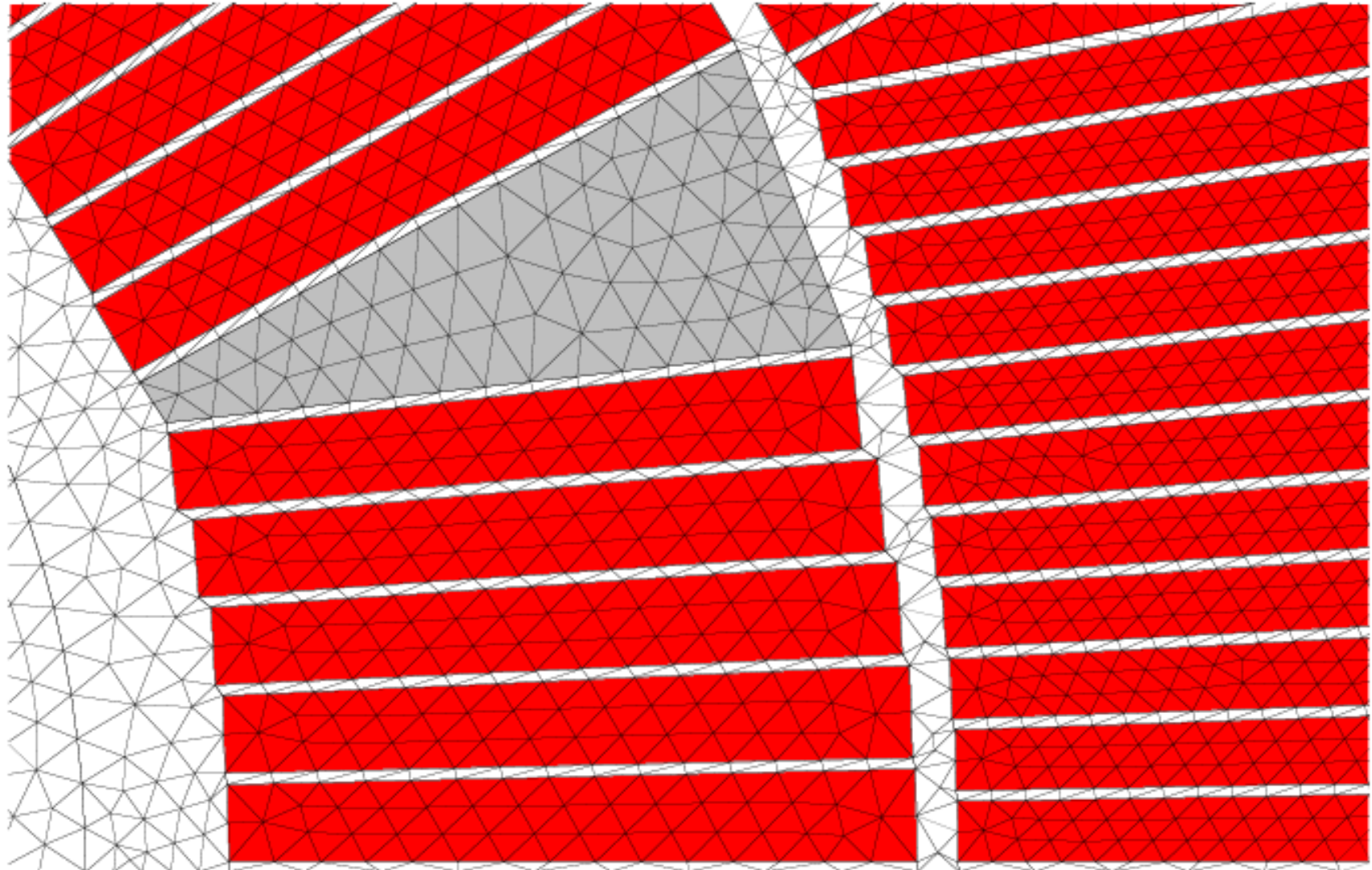
Weak Form in the FEM Problem



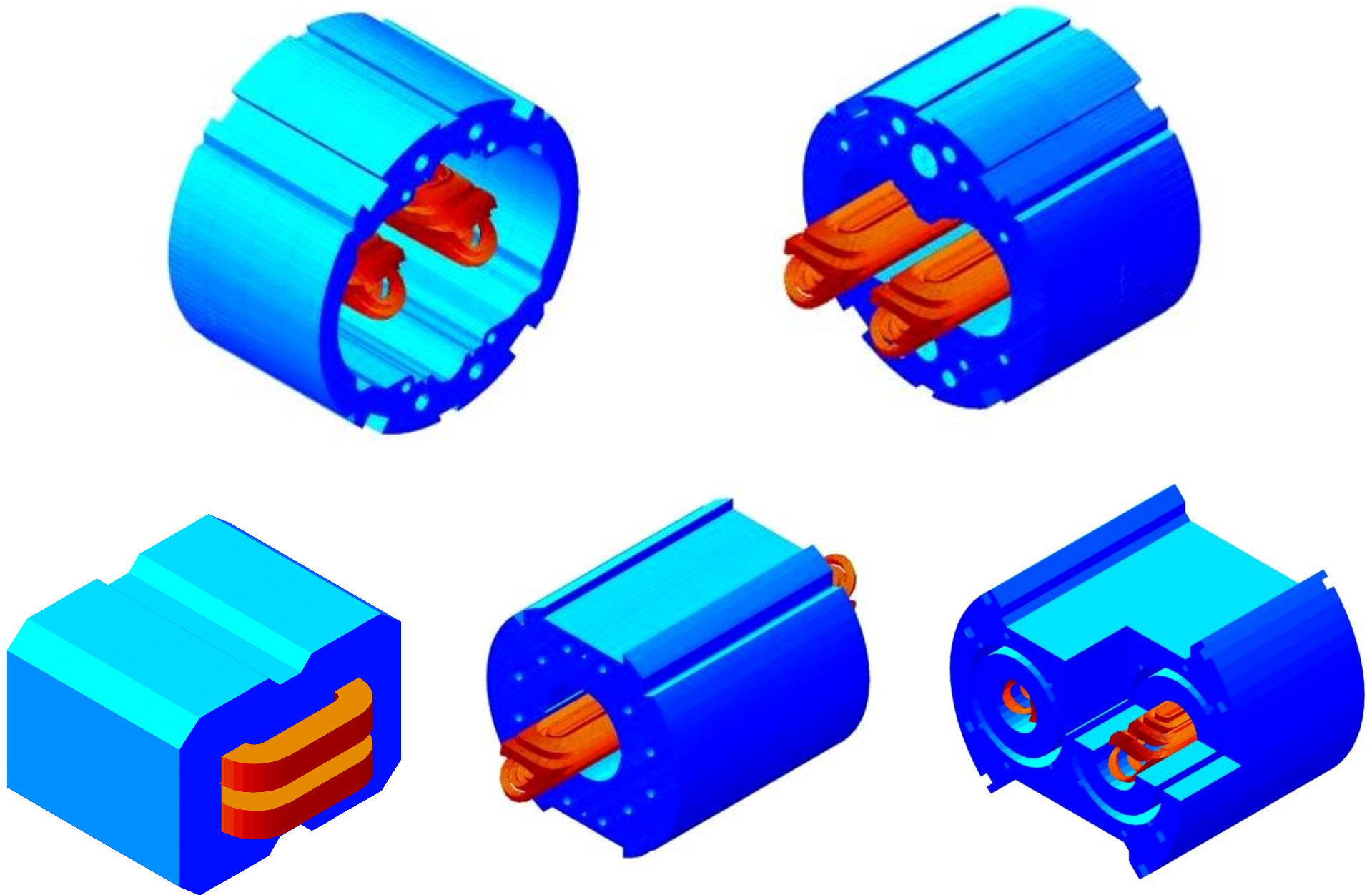
Weak Form in the FEM Problem



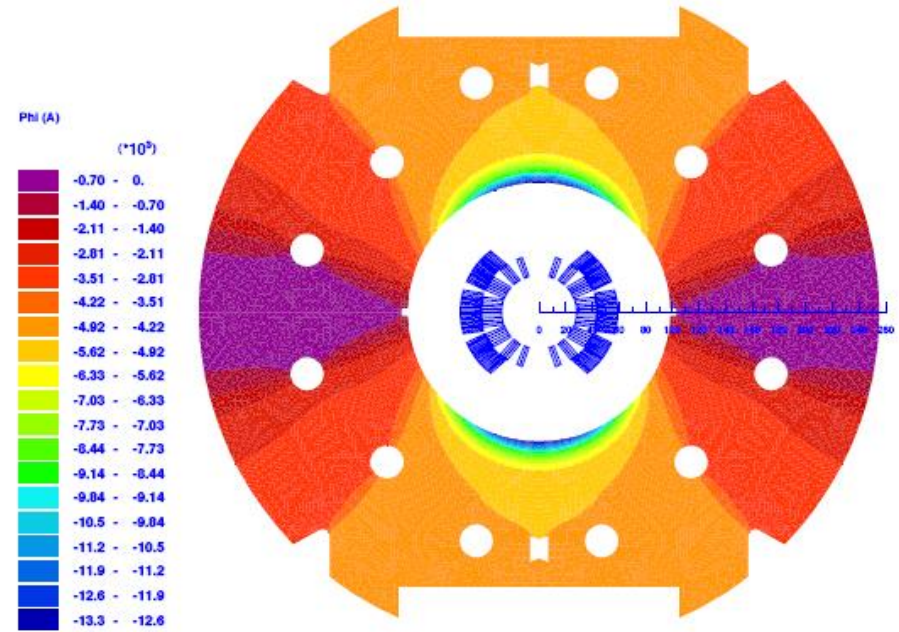
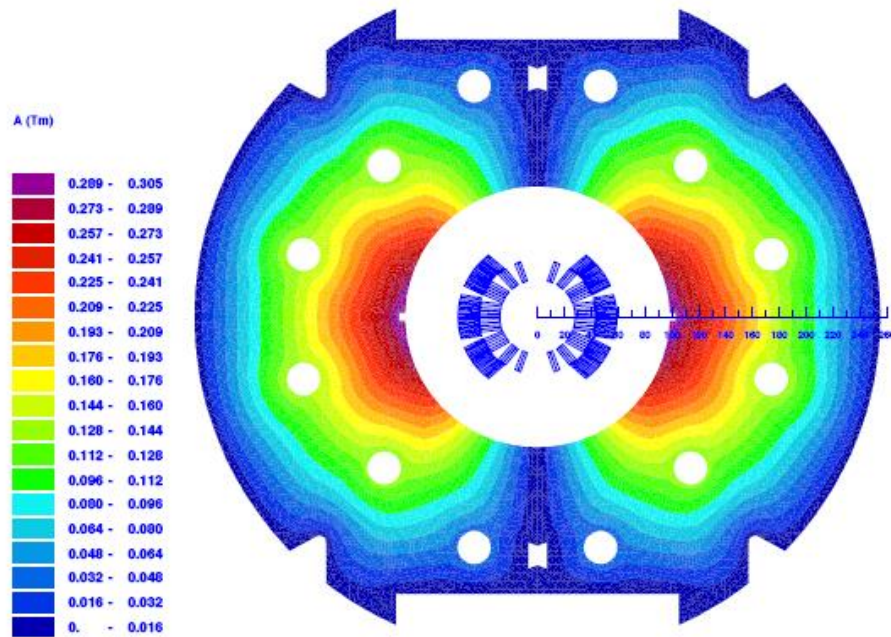
Meshing the Coil



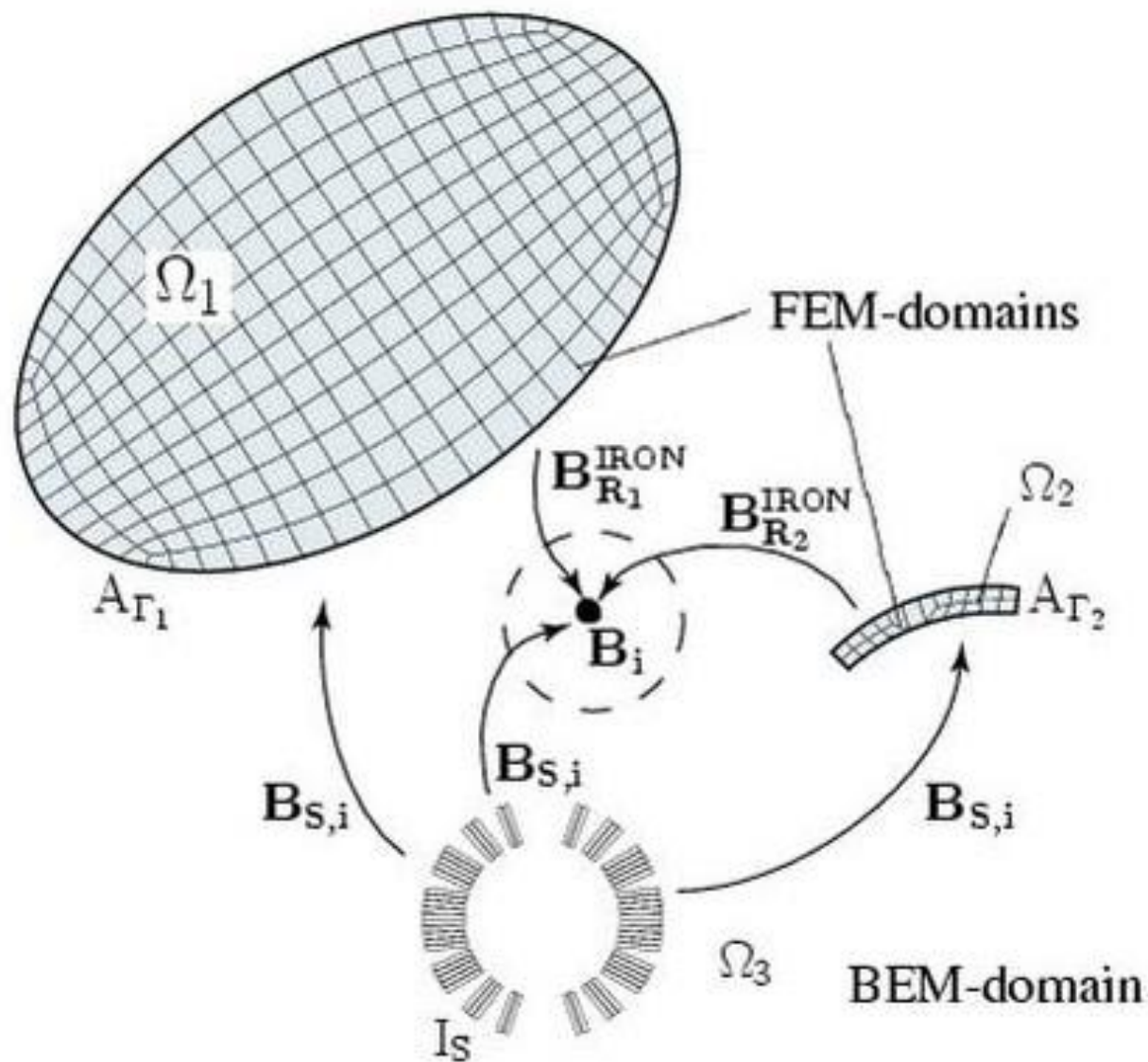
Magnet Extremities



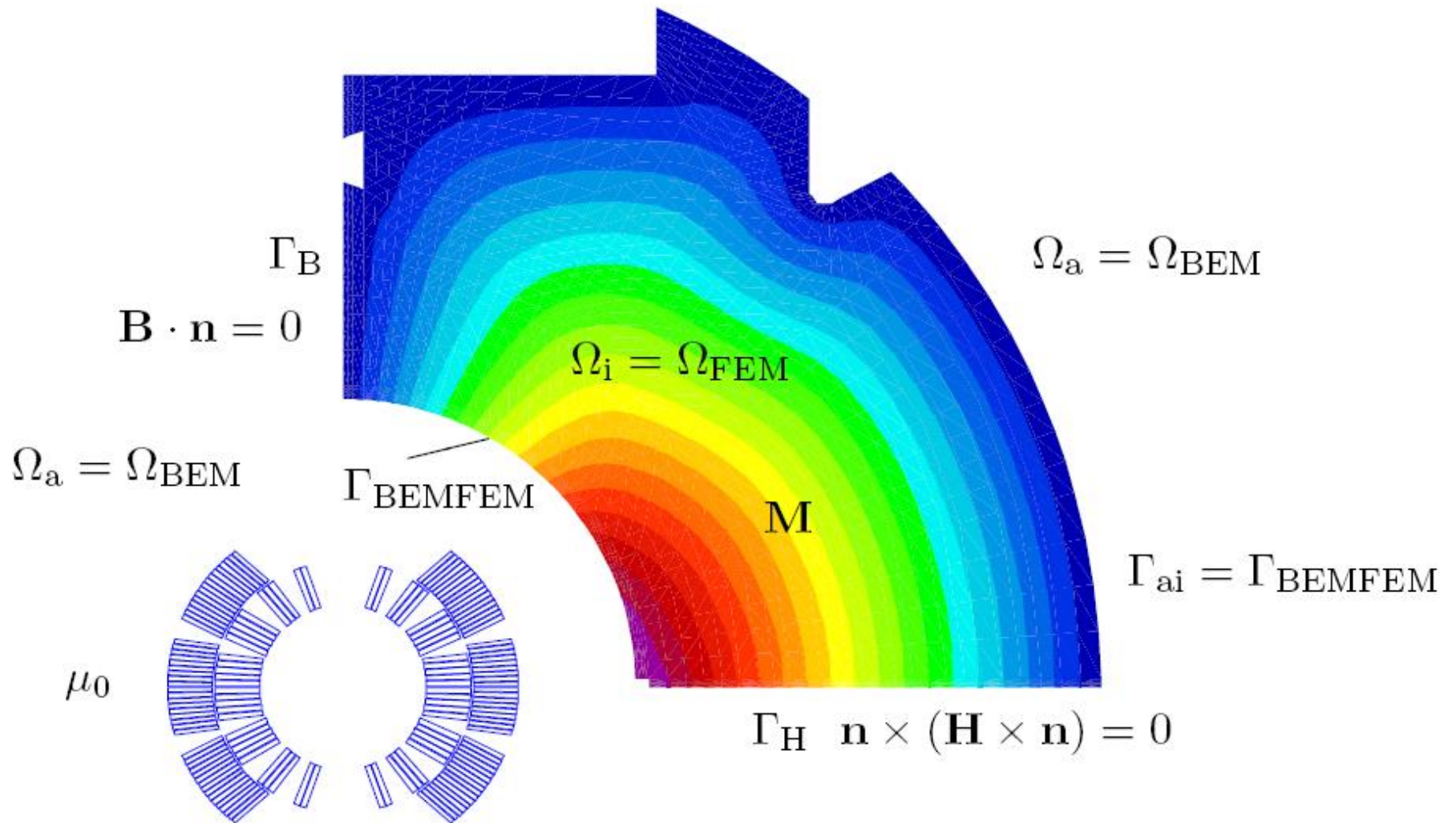
Vector Potential and Total Scalar Potential



BEM-FEM Coupling (Elementary Model Problem)

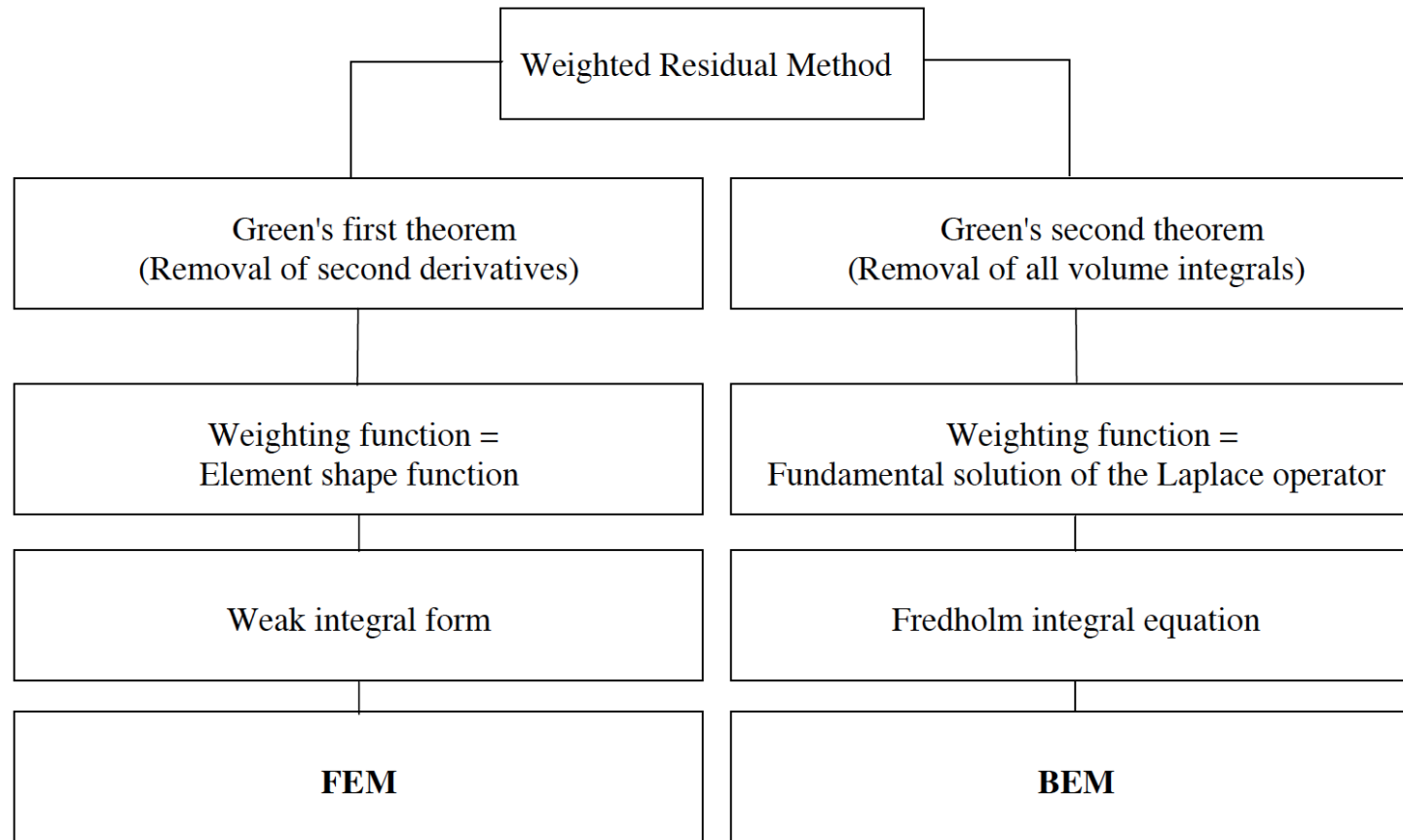


The Elementary Model Problem in Magnet Design



Green's First and Second Identities in FEM and BEM

$$\int_{\Omega} (\text{grad } \phi \cdot \text{grad } \psi + \phi \nabla^2 \psi) dV = \int_{\Gamma} \phi \text{grad } \psi \cdot \mathbf{n} da,$$



$$\int_{\Omega} (\phi \nabla^2 \psi - \psi \nabla^2 \phi) dV = \int_{\Gamma} (\phi \partial_{\mathbf{n}} \psi - \psi \partial_{\mathbf{n}} \phi) da,$$

The FEM Part (Vector Laplace Equation)

$$-\frac{1}{\mu_0} \nabla^2 \mathbf{A} = \mathbf{J} + \text{curl } \mathbf{M}$$

in Ω_i ,

$$\mathbf{A} \cdot \mathbf{n} = 0$$

on Γ_H ,

$$\frac{1}{\mu_0} \text{div } \mathbf{A} = 0$$

on Γ_B ,

$$\mathbf{n} \times (\mathbf{A} \times \mathbf{n}) = \mathbf{0}$$

on Γ_B ,

$$\frac{1}{\mu} (\text{curl } \mathbf{A}) \times \mathbf{n} = \mathbf{0}$$

on Γ_H ,

$$\left[\frac{1}{\mu_0} \text{div } \mathbf{A}_a \right]_{\text{ai}} = 0$$

on Γ_{ai} ,

$$\frac{1}{\mu_0} (\text{curl } \mathbf{A}_i - \mu_0 \mathbf{M}) \times \mathbf{n}_i + \frac{1}{\mu_0} (\text{curl } \mathbf{A}_a) \times \mathbf{n}_a = \mathbf{0}$$

on Γ_{ai} ,

$$[\mathbf{A}]_{\text{ai}} = \mathbf{0}$$

on Γ_{ai} .

$$\frac{1}{\mu_0} \int_{\Omega_i} \text{grad}(\mathbf{A} \cdot \mathbf{e}_a) \cdot \text{grad} w_a d\Omega_i - \frac{1}{\mu_0} \oint_{\Gamma_{ai}} \left(\frac{\partial \mathbf{A}}{\partial n_i} - (\mu_0 \mathbf{M} \times \mathbf{n}_i) \right) \cdot \mathbf{w}_a d\Gamma_{ai} = \int_{\Omega_i} \mathbf{M} \cdot \text{curl} \mathbf{w}_a d\Omega_i$$



$$[K] \{A\} - [T] \{Q\} = \{F(\mathbf{M})\}$$

Vector Laplace

Weighted Residual

From Green's second theorem:

$$\int_{\Omega_a} A \nabla^2 w d\Omega_a = - \int_{\Omega_a} \mu_0 J w d\Omega_a + \int_{\Gamma_{ai}} A \frac{\partial w}{\partial n_a} d\Gamma_{ai} - \int_{\Gamma_{ai}} \frac{\partial A}{\partial n_a} w d\Gamma_{ai}$$

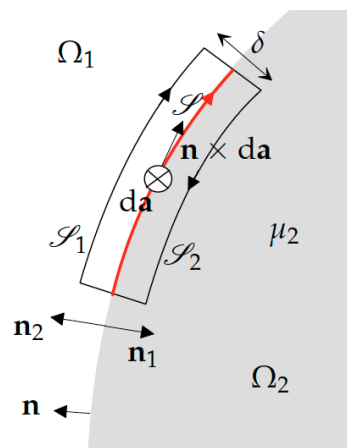
Representation Formula (Fredholm Integral Equation)

$$\frac{\ominus}{4\pi} A(\mathbf{r}) = \int_{\Gamma} \partial_{\mathbf{n}_a} A(\mathbf{r}') u^*(\mathbf{r}, \mathbf{r}') da' - \int_{\Gamma} A(\mathbf{r}') q^*(\mathbf{r}, \mathbf{r}') da'$$

Single-layer potential

$$\boldsymbol{\alpha}(\mathbf{r}') := -\frac{1}{\mu} \partial_{\mathbf{n}_a} A(\mathbf{r}')$$

$$[\boldsymbol{\alpha}] = 1 \text{ A m}^{-1}$$

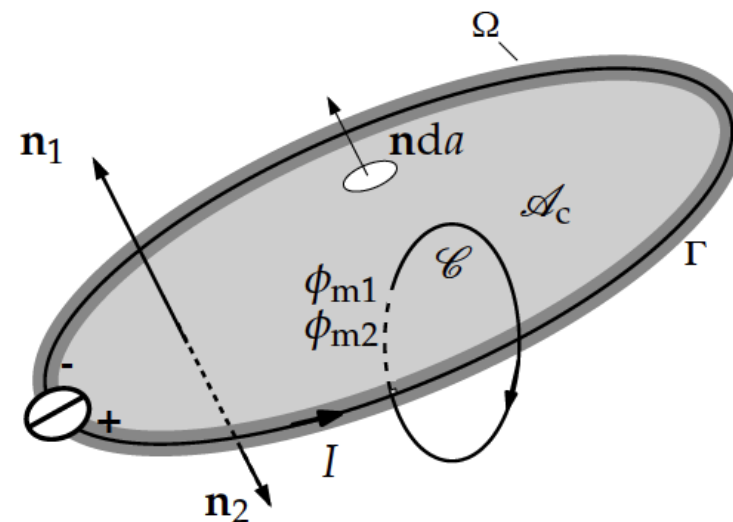


$$\boldsymbol{\alpha} = \mathbf{n} \times (\mathbf{H}_1 - \mathbf{H}_2)$$

Double-layer potential

$$\boldsymbol{\tau}(\mathbf{r}') := \frac{1}{\mu} A(\mathbf{r}')$$

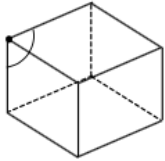


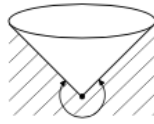
$$[\boldsymbol{\tau}] = 1 \text{ A}$$

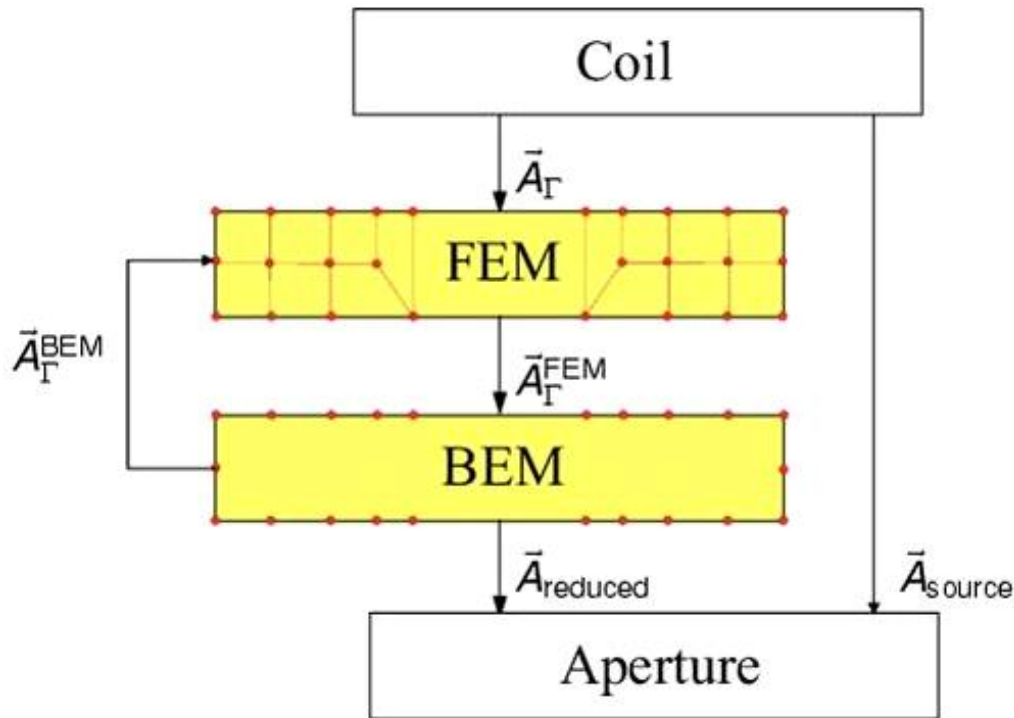


Point-Collocation (Compute One from the Other)

$$\frac{\Theta}{4\pi} A(\mathbf{r}) = \int_{\Gamma} \partial_{\mathbf{n}_a} A(\mathbf{r}') u^*(\mathbf{r}, \mathbf{r}') da' - \int_{\Gamma} A(\mathbf{r}') q^*(\mathbf{r}, \mathbf{r}') da'$$

$$C(\mathbf{r}_p) A(\mathbf{r}_p) + \sum_{e=1}^E \int_{\Gamma_e} -\partial_{\mathbf{n}_a} A(\mathbf{r}) u^*(\mathbf{r}, \mathbf{r}_p) da + \sum_{e=1}^E \int_{\Gamma_e} A(\mathbf{r}) q^*(\mathbf{r}, \mathbf{r}_p) da = 0$$

Ω_a				
	90° Corner	90° Cone inner	Half-space	90° Cone outer
Θ	$\frac{1}{2} \pi$	$(2 - \sqrt{2}) \pi$	2π	$(2 + \sqrt{2}) \pi$
$\frac{\Theta}{4\pi}$	$\frac{1}{8}$	$\frac{2 - \sqrt{2}}{4}$	$\frac{1}{2}$	$\frac{2 + \sqrt{2}}{4}$



BEM

$$\{Q\} = -[G]^{-1}[H]\{A\} + [G]^{-1}\{A_s\}$$

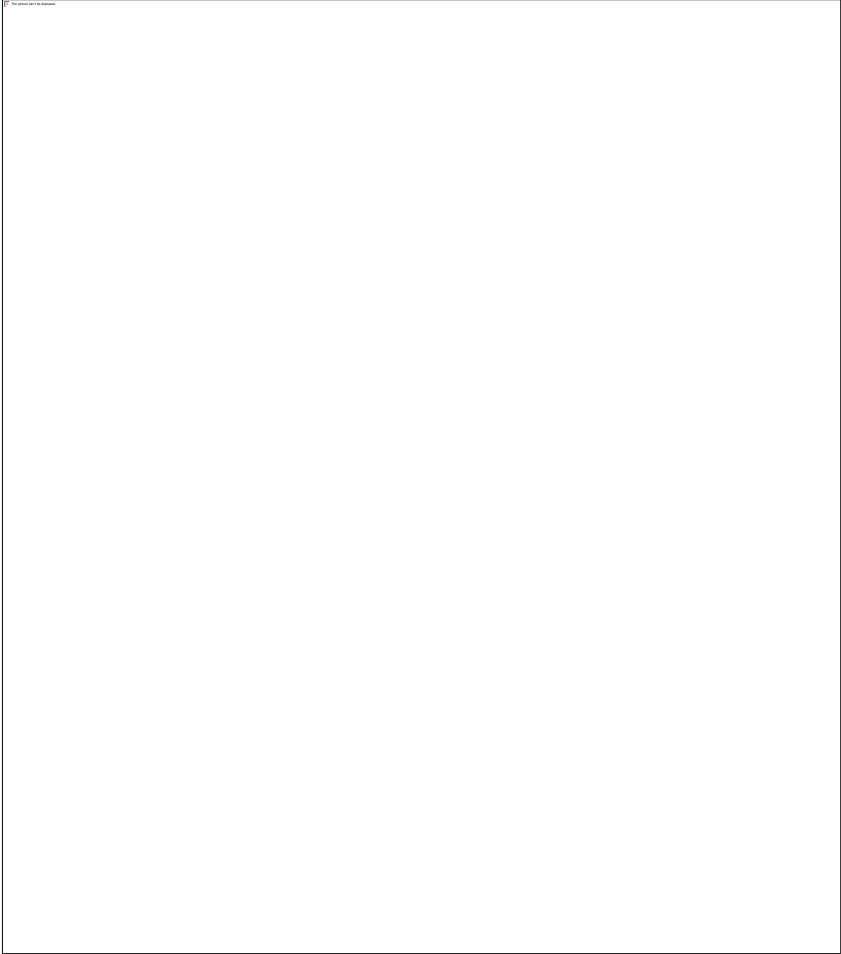
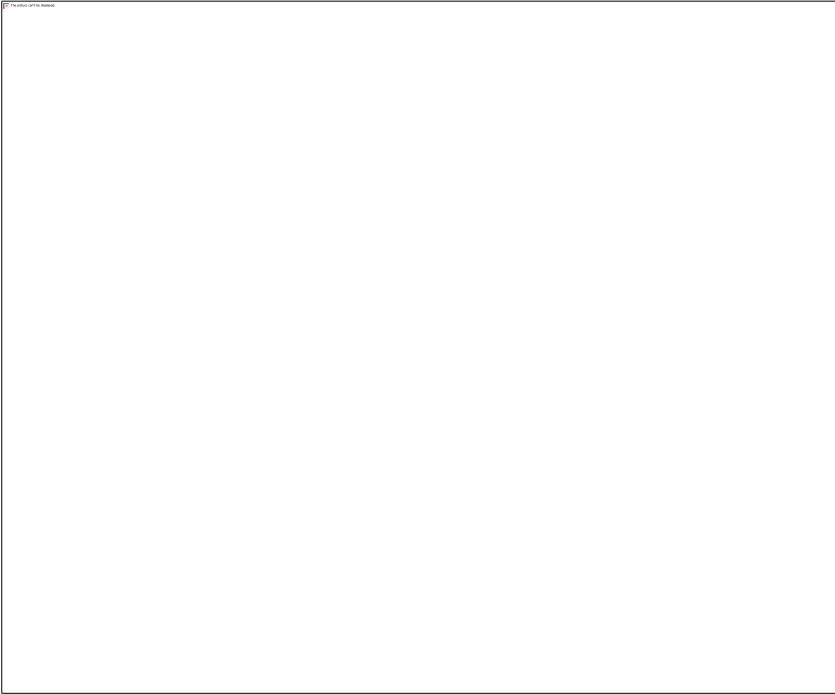
FEM

$$[K]\{A\} - [T]\{Q\} = \{F(\mathbf{M})\}$$

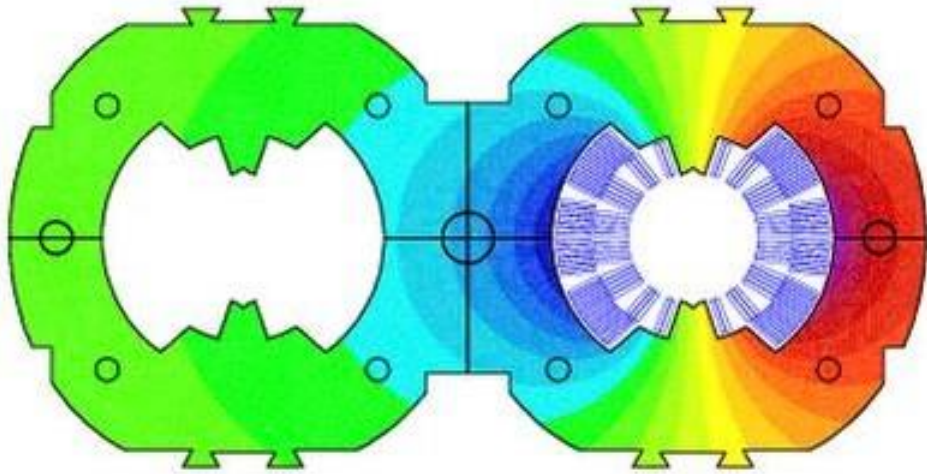
$$\left([K] + [T][G]^{-1}[H] \right) \{A\} = \{F(\mathbf{M})\} + [T][G]^{-1}\{A_s\}$$

$$[\bar{K}]\{A\} = \{\bar{F}(A_s, \mathbf{M})\}$$

LHC Beam Screen



Open Boundary Problem (2)



Collared Coil
Field Problem

Collared Coil
Measurements in
Industry



Forces (N) in the Connection Ends of the LHC Main Dipole

I	F _x	F _y	F _z
1	-39.7	-44.0	-45.4
2	-6.5	3.7	-41.7
3	-6.1	88.3	-38.2
4	1.25	3.9	-28.5
5	48.1	-46.7	-48.5
Su m	-2.95	5.2	-202.3

