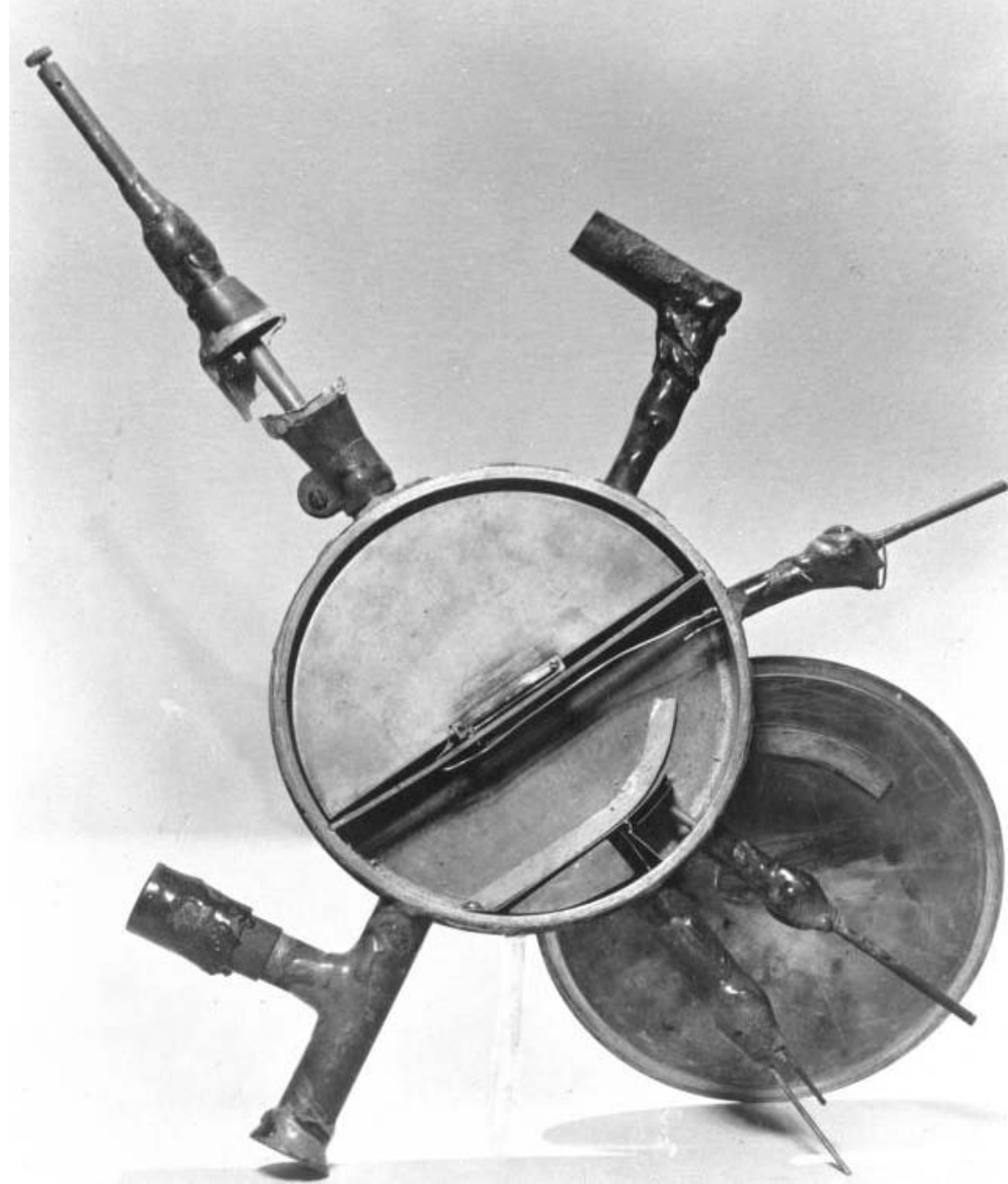


cyclotron

RF

systems



outline

- cyclotron basics
- resonator design techniques
 - transmission line
 - 3D finite element
- tuning
- power coupling
- RF control
- flat topping
- some specific examples

cyclotron basics

- original observation: homogeneous magnetic field isochronous (Lawrence & Livingston 1931)

$$\frac{mv^2}{R} = qvB \quad R = \frac{mv}{Bq} \quad v_{\text{orb}} = \frac{Bq}{2\pi m}$$

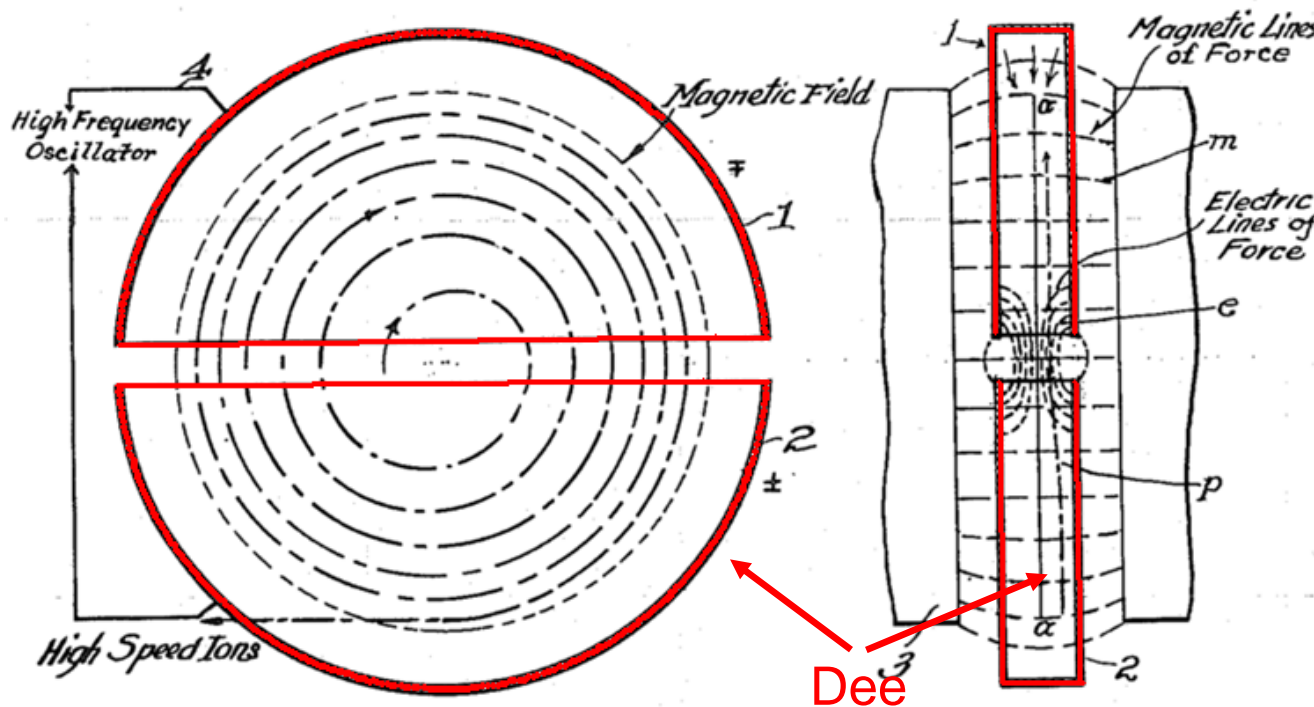
centrifugal force Lorentz force

cyclotron basics

- original observation: homogeneous magnetic field isochronous (Lawrence & Livingston 1931)

$$\frac{mv^2}{R} = qvB \quad R = \frac{mv}{Bq} \quad v_{\text{orb}} = \frac{Bq}{2\pi m}$$

- accelerate with RF electric field with $v_{\text{RF}} = h v_{\text{orb}}$ (h integer)
- drift tube linac “rolled up” in a magnetic field



U.S. Patent 1948384 -- Ernest O. Lawrence --
Method and apparatus for the acceleration of ions.

rsuniversiteit
mingen

why it should not work

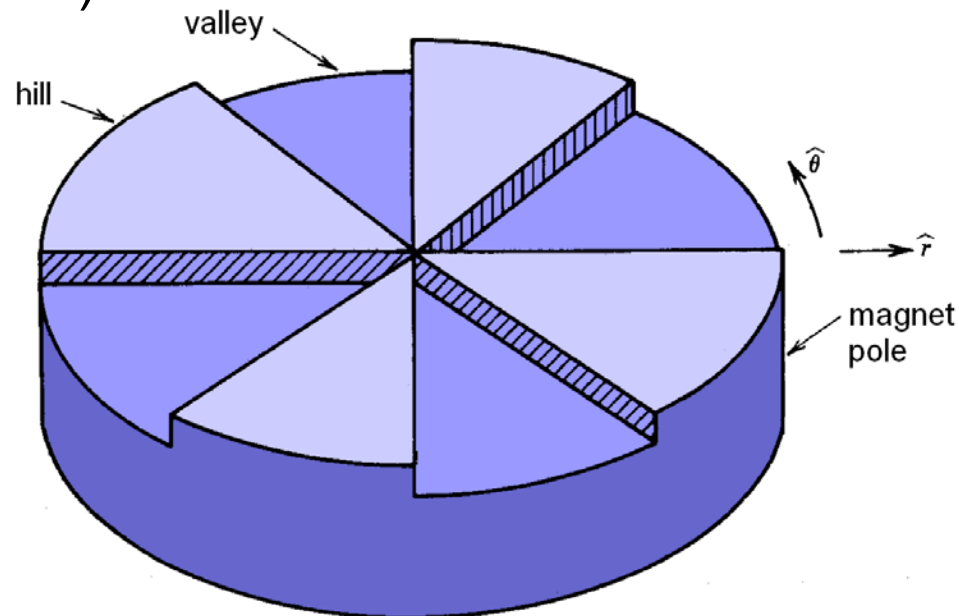
- transverse optics
 - homogeneous field: fieldindex $n = 0$
 - $Q_z, \nu_z = 0$; **no vertical stability**
è linear growth of vertical beamsize
 - $Q_r, \nu_r = 1$; **resonance**
è no stable orbit due to imperfections
- longitudinal optics
 - isochronous: no longitudinal stability
 - relativistic mass increase
è loss of synchronisation with accelerating voltage

why it works after all to some extent

- fringe field effects: fieldindex $n = \varepsilon > 0$
 - $Q_z, \nu_z > 0$; marginal vertical stability
 - è large beamsize è **bad transmission**
 - $Q_r, \nu_r < 1$; no resonance
 - “weak” focussing
- loss of synchronisation with accelerating voltage gradual
 - è acceleration possible over limited number of turns
 - maximum energy dependent on acceleration voltage
50 keV acceleration voltage: 12 MeV protons
Bethe and Rose, Phys. Rev. 52 (1937) 1254–1255

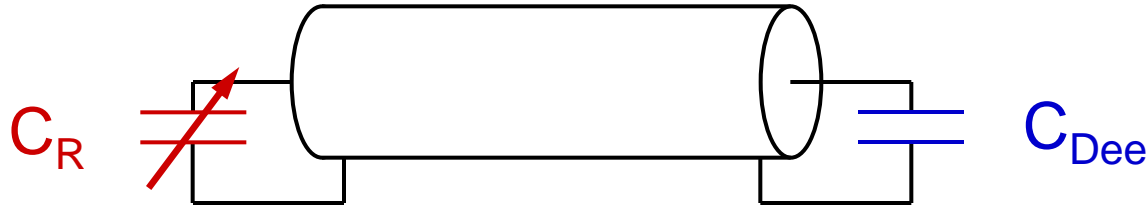
how to get it really working

- radially decreasing field + RF frequency modulation
 - è vertical and phase stability
 - E. MacMillan, Phys. Rev. 68 (1945) 144
 - V. Veksler, Phys. Rev. 69 (1946) 244
 - **synchro-cyclotron è synchrotron è storage ring**
workhorse high energy physics
- radially increasing field + azimuthal field modulation
 - vertical stability and isochronism
 - Thomas, Phys. Rev. 54 (1938) 580 and 588
 - **isochronous cyclotron**
workhorse nuclear physics

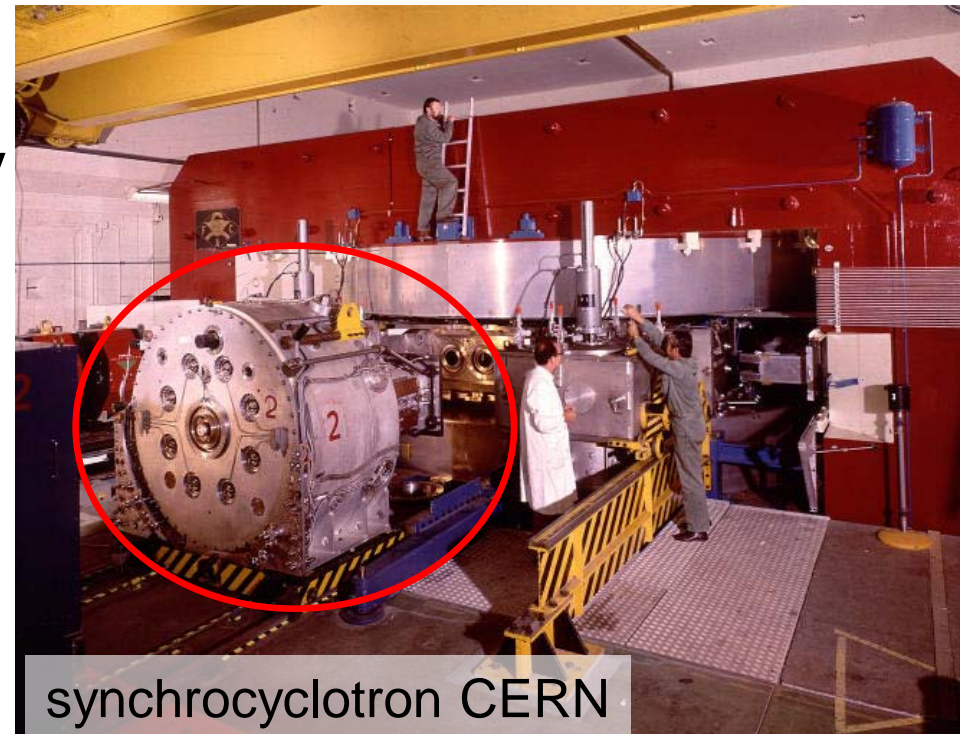


synchrocyclotron

- $\lambda/2$ transmission line with capacitive load on both ends



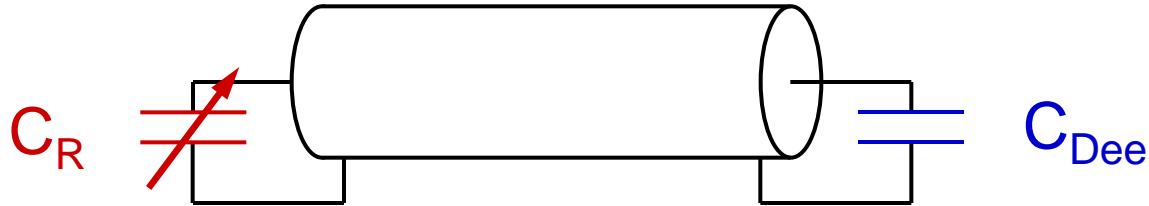
- frequency variation by variation of C_R
 - capacitance rotating in vacuum
- acceleration electrode C_{Dee}
- operational parameters
 - acceleration voltage ~ 20 kV
 - RF power 10 – 100 kW
 - self-oscillating
 - frequency swing ~ 20 %
Orsay 19 – 24 MHz
 - rep rate 100 - 400 Hz



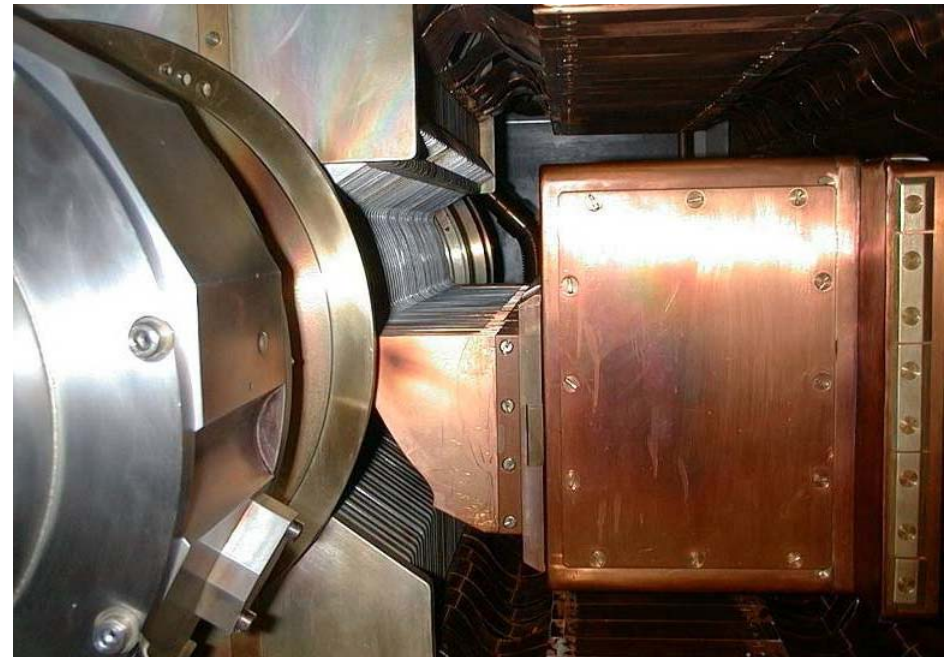
synchrocyclotron CERN

synchrocyclotron

- $\lambda/2$ transmission line with capacitive load on both ends



- frequency variation by variation of C_R
 - capacitance rotating in vacuum
- acceleration electrode C_{De}
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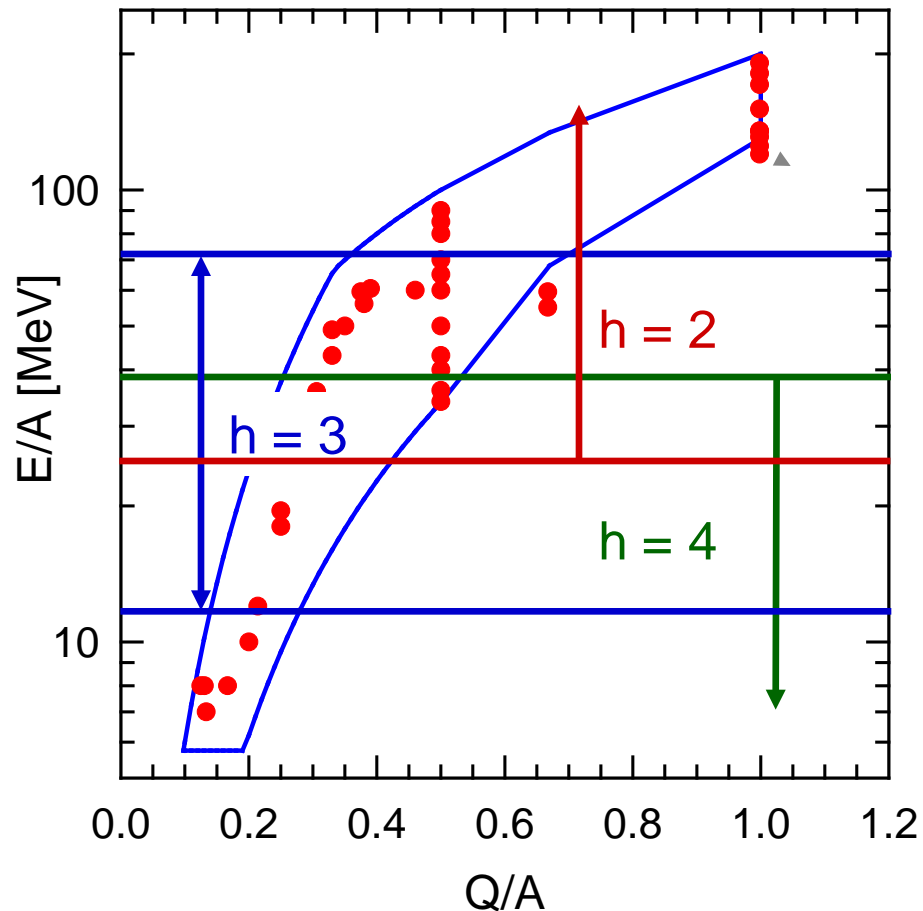
synchrocyclotron Orsay

operational parameters

- orbital frequency (non-relativistic) $\nu_{\text{orb}} = 15.2 \frac{Q}{A} \bar{B}$ [MHz]
 \bar{B} average magnetic field along orbit [T]
 Q/A charge-to-mass ratio ion
- typical values
 - compact RT cyclotrons 1 – 15 MHz
 - superconducting cyclotrons 6 – 35 MHz
 - separated sector cyclotrons 1 – 10 MHz
 - research machines
 - multi-particle
 - multi-energy
 - è large orbital frequency range
 - typical example SC AGOR-cyclotron @ KVI
 - particles protons – Pb
 - energy 190 – 5.5 MeV/nucleon
 - orbital frequency 30 - 6 MHz

operational parameters

- orbital and resonator frequency ranges incompatible
 - è use different harmonic modes (example AGOR)
 - different phasing of resonators

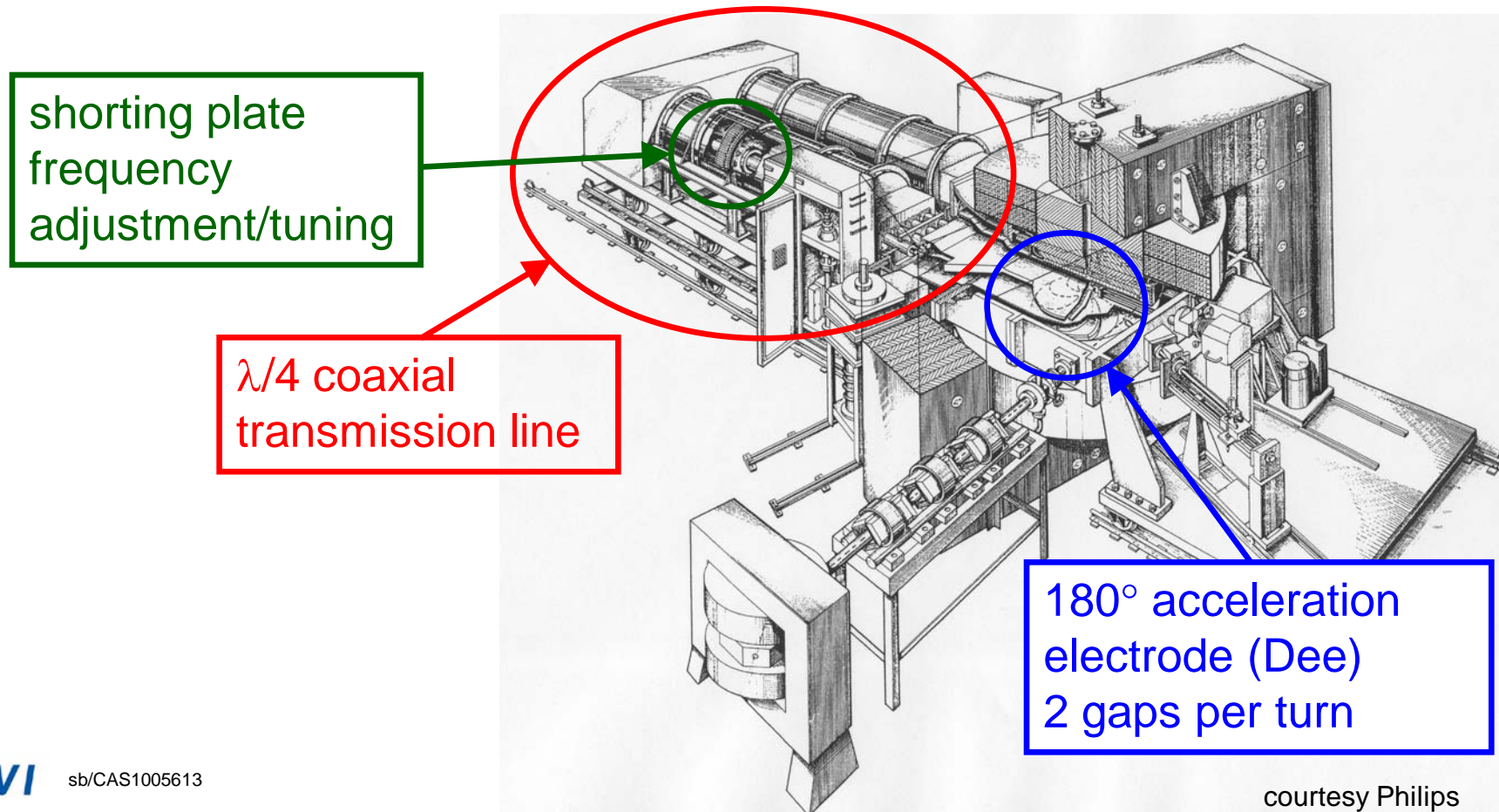


operational parameters

- orbital and resonator frequency ranges incompatible
è use different harmonic modes
- harmonic mode
 - geometry acceleration electrode è possible values
 - typical $h = 1 - 6$, max. 10
- acceleration voltage
 - typical $V = 50 - 100$ kV; max. 1000 kV
- RF power
 - typical $P = 10 - 100$ kW; max 400 kW (excl. beamloading)

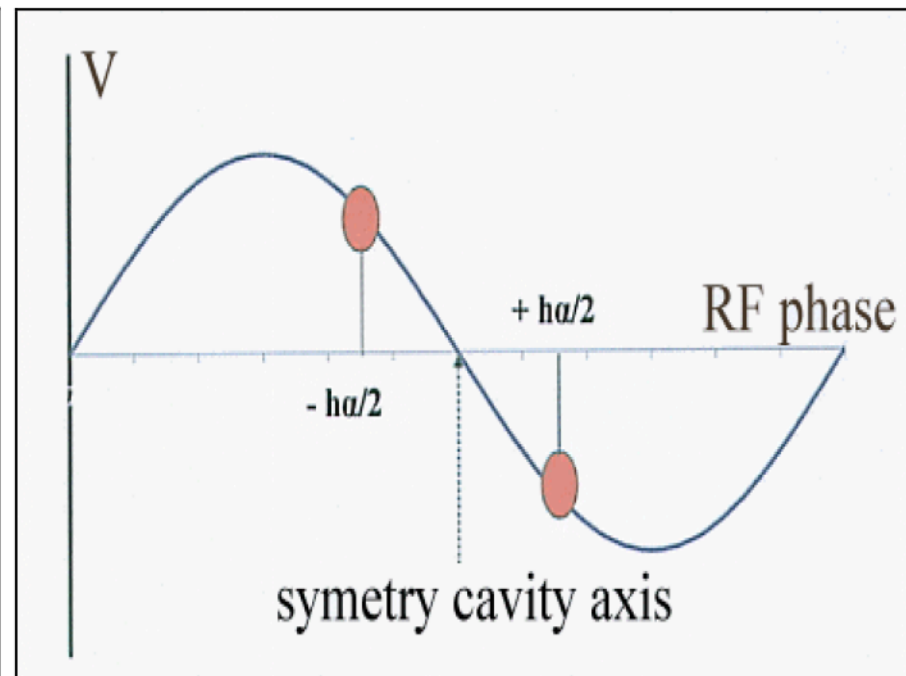
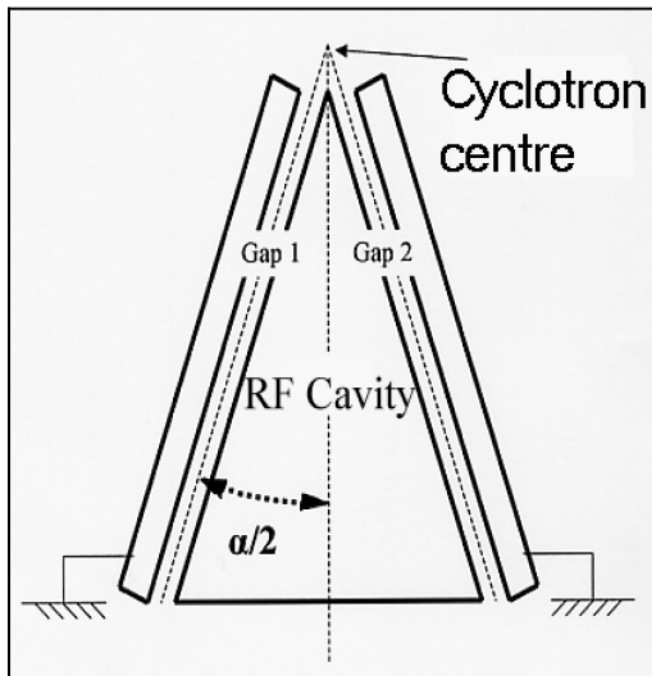
resonator types

- capacitively loaded transmission line ($\lambda/4$ or $\lambda/2$)
 - dual gap acceleration electrode
 - TEM-mode
 - most common solution



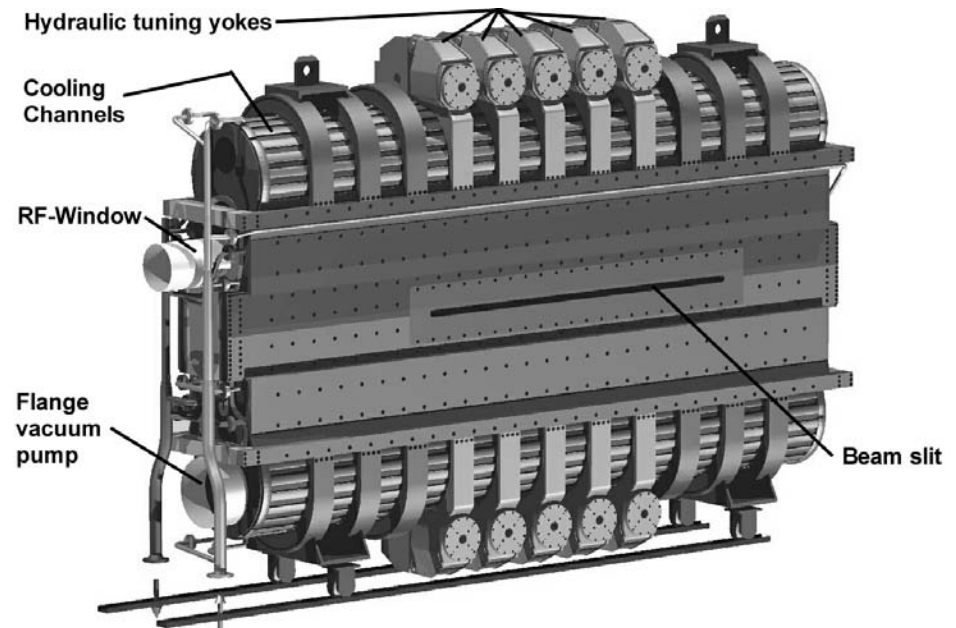
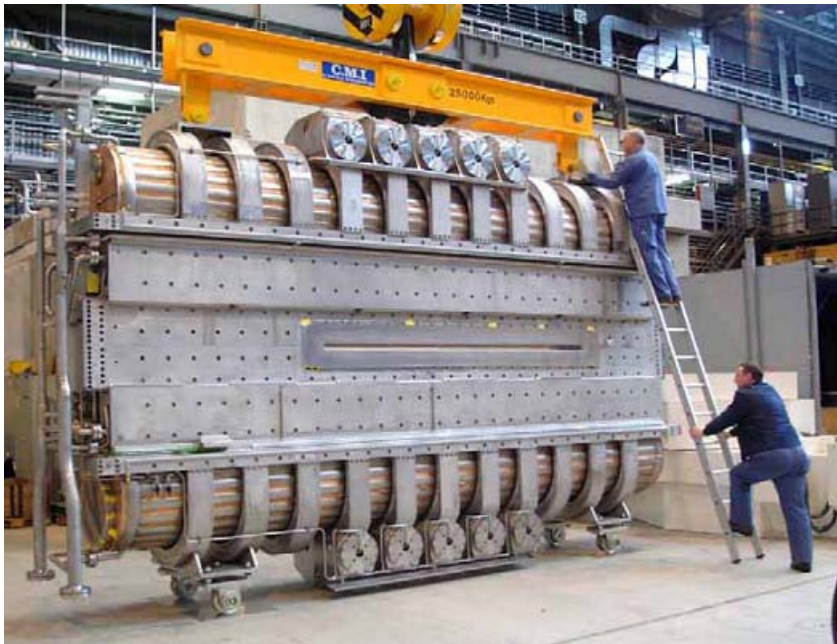
shape acceleration electrode vs. harmonic

- highest acceleration: particle passes symmetry axis for $\varphi = \pi$
 $\Delta E = -QV_D \sin(h\alpha/2) \sin(\varphi)$
- not all harmonic modes possible
e.g. $\alpha = 60^\circ$ è no acceleration for $h = 6$



resonator types

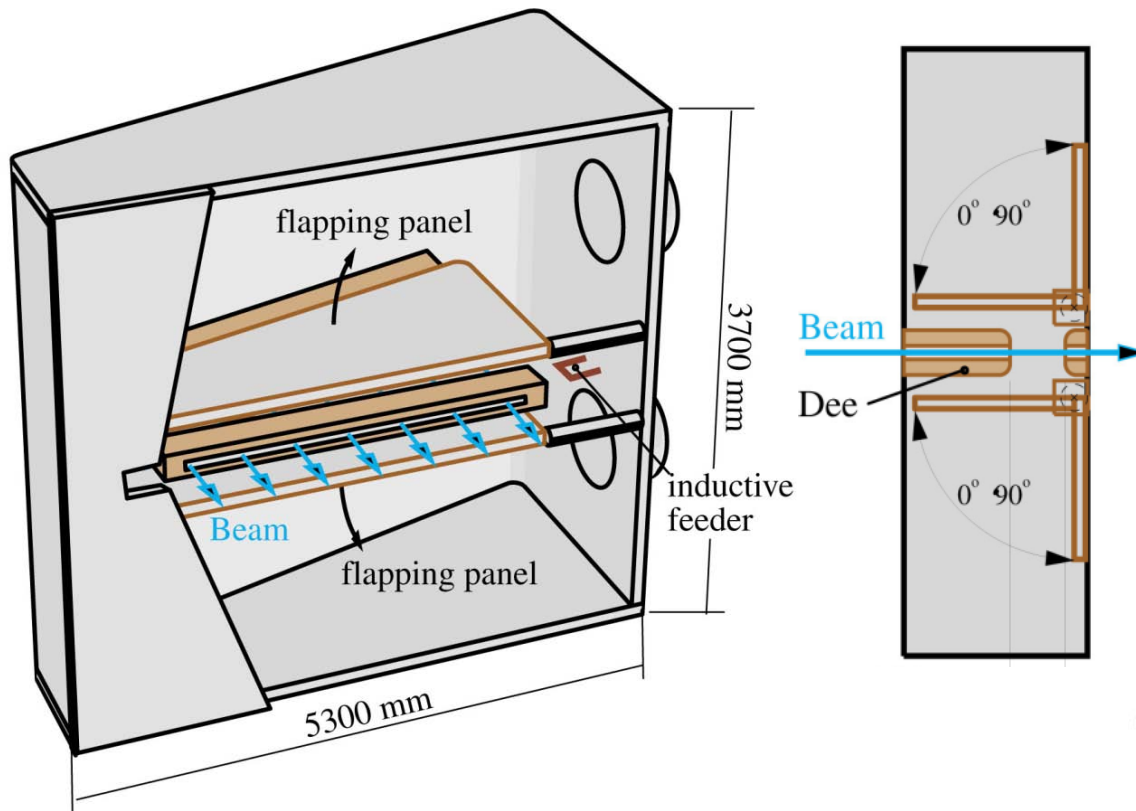
- single gap resonator
 - separated sector cyclotrons
 - used at PSI, RCNP and RIKEN
 - TE_{110} mode



resonator types

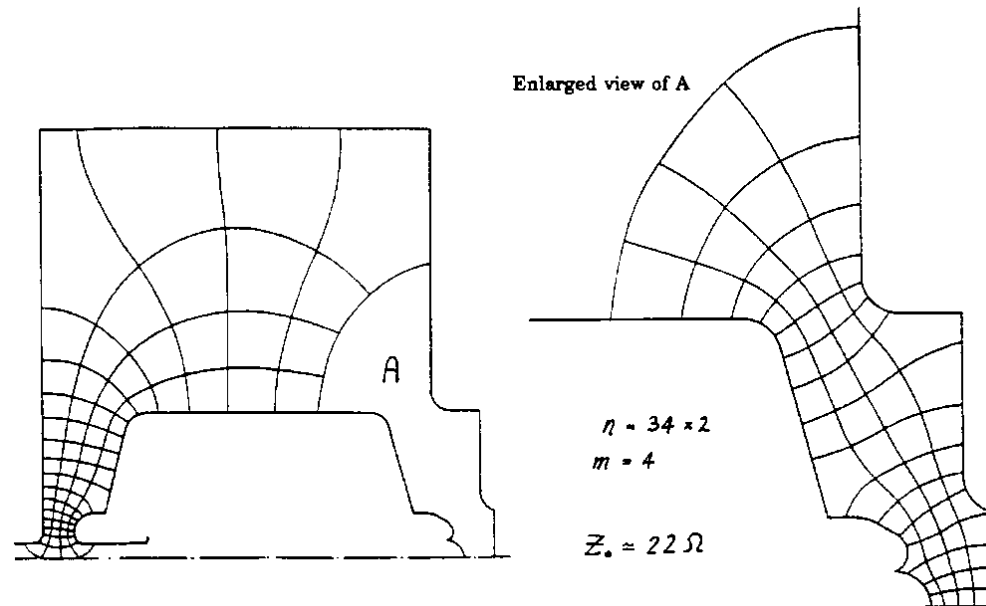
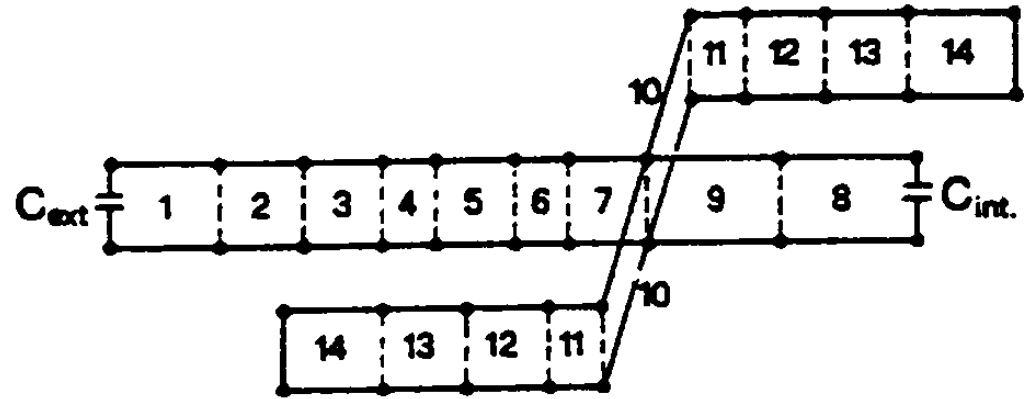
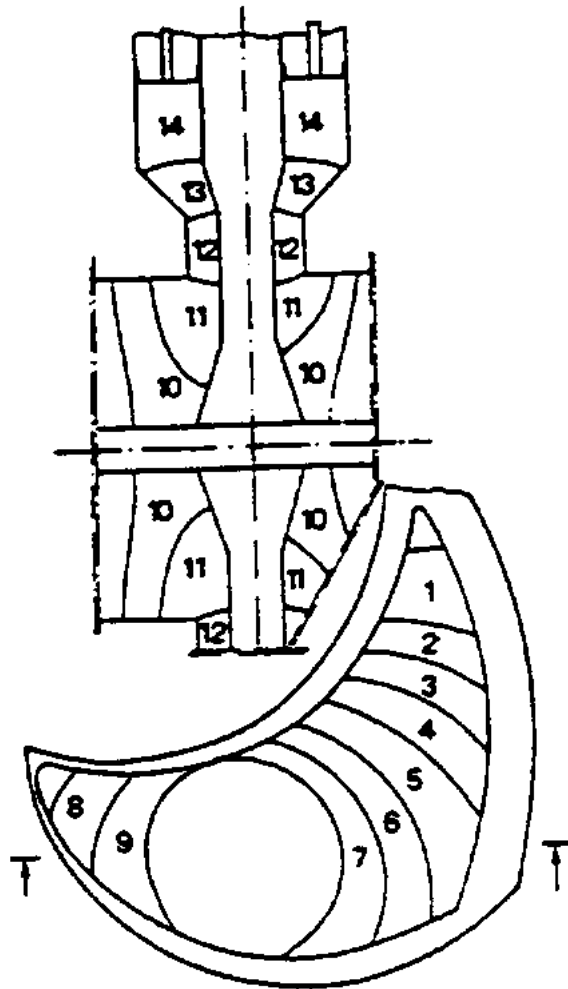
- single gap resonator
 - separated sector cyclotrons
 - used at PSI, RCNP and RIKEN SRC
 - TE_{110} mode

SRC Single Gap Type Resonator



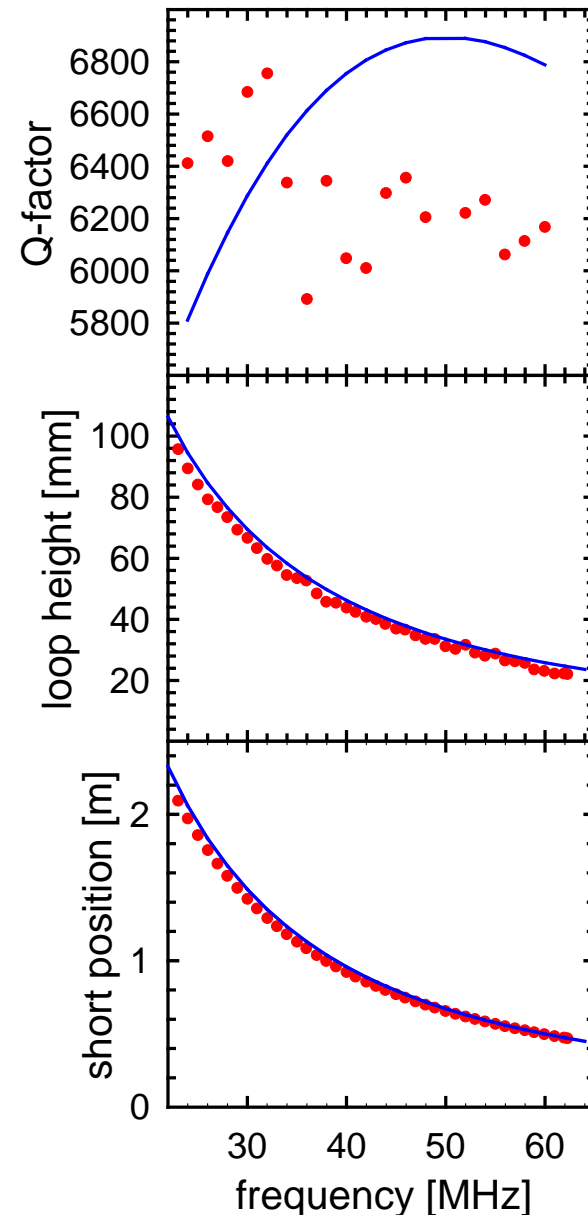
resonator design: transmission line model

- traditional approach (used until ~10 years ago)
 - validation on scale models



resonator design: transmission line model

- sufficient accuracy feasible
- design AGOR cavities
 - transmission line model
 - model measurements
 - results
 - Δ frequency < 1 MHz
range 22 – 62 MHz
 - Δ loop height < 5 mm
range 100 mm
 - Δ Q-factor/power < 10 %

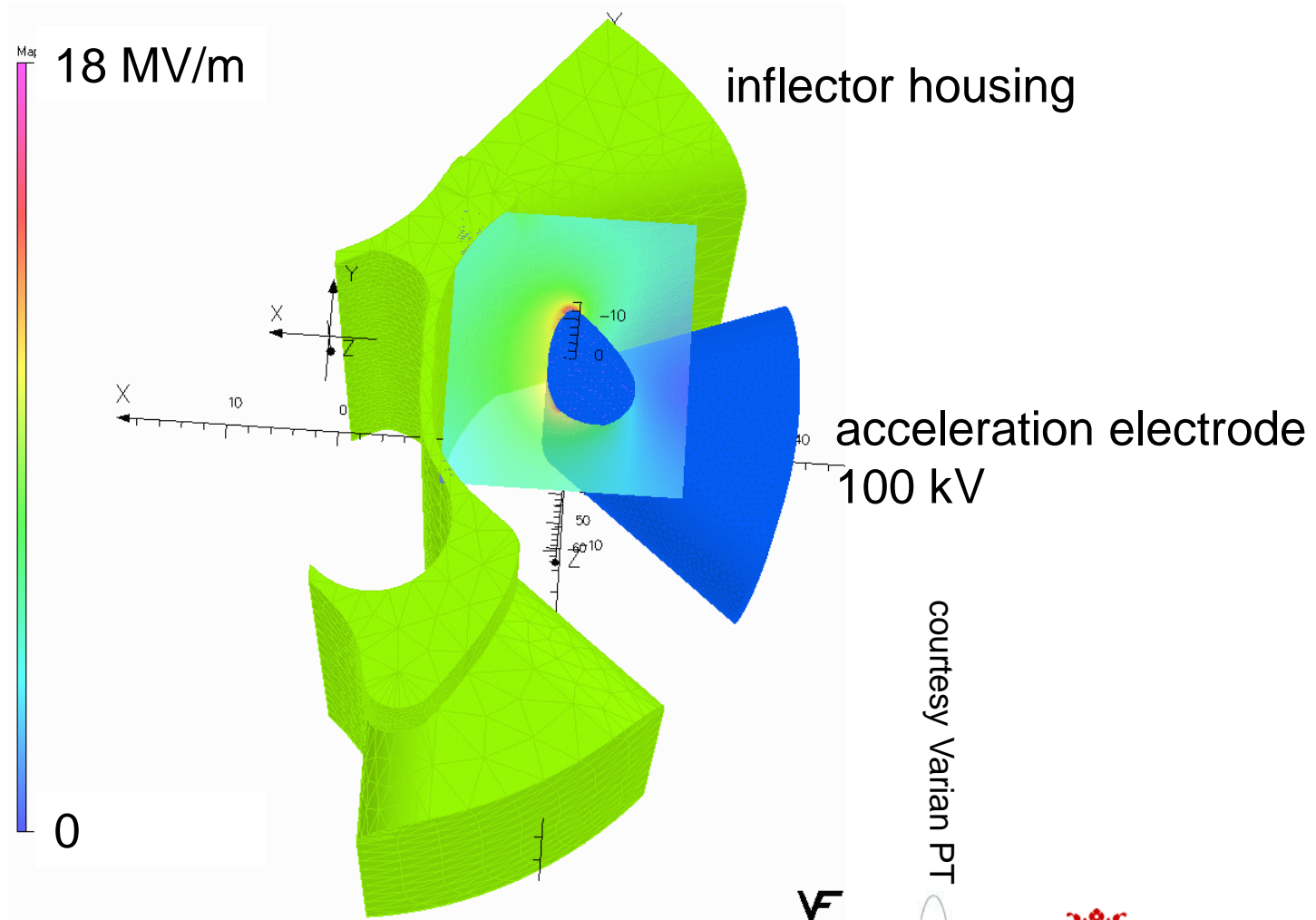


resonator design: 3D simulations

- recent trend; facilitated by computer and ICT revolution
- advantages
 - calculation of more complex resonator shapes
 - coupling with CAD-packages: input detailed geometry
 - detailed insight in current and voltage distribution
 - è better optimization of
 - cooling
 - peak fields (breakdown probability)
 - detailed maps RF-field for trajectory calculations
 - higher accuracy resonance parameters
 - coupling with thermal and mechanical simulations (deformation)
 - better insight in higher order modes
- disadvantages
 - less insight in critical parameters
 - initial stages design significantly slower
 - large computing power required

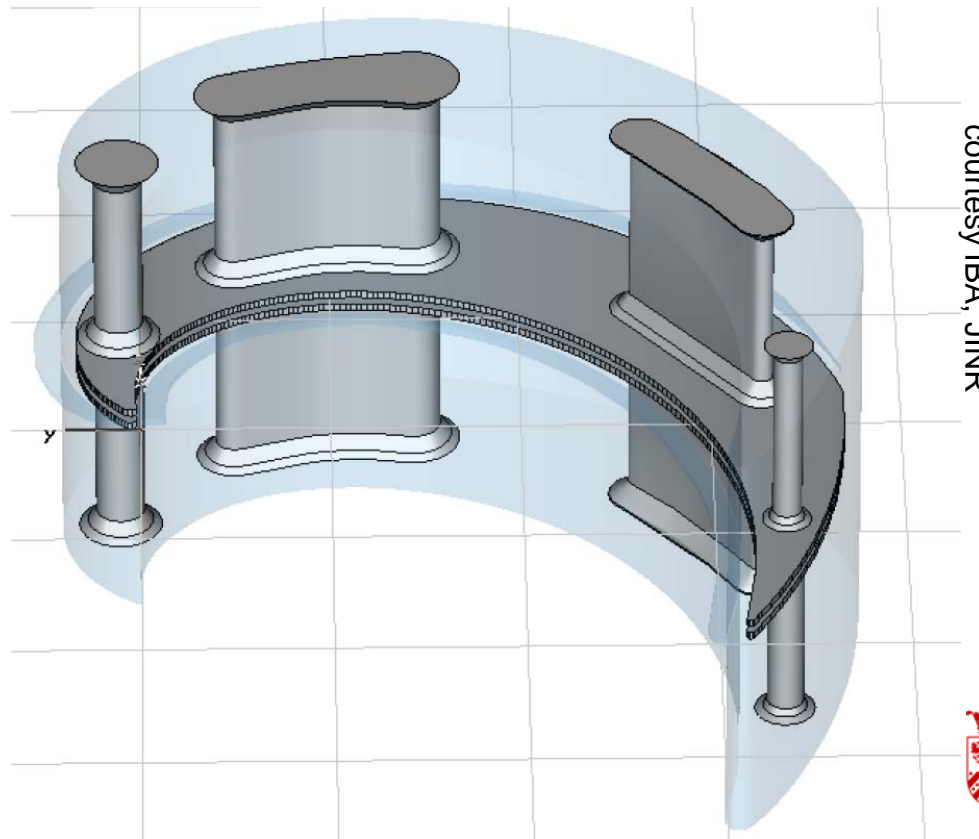
resonator design: 3D simulations

- optimization electric fields AGOR central region
 - reduce breakdown frequency



resonator design: 3D simulations

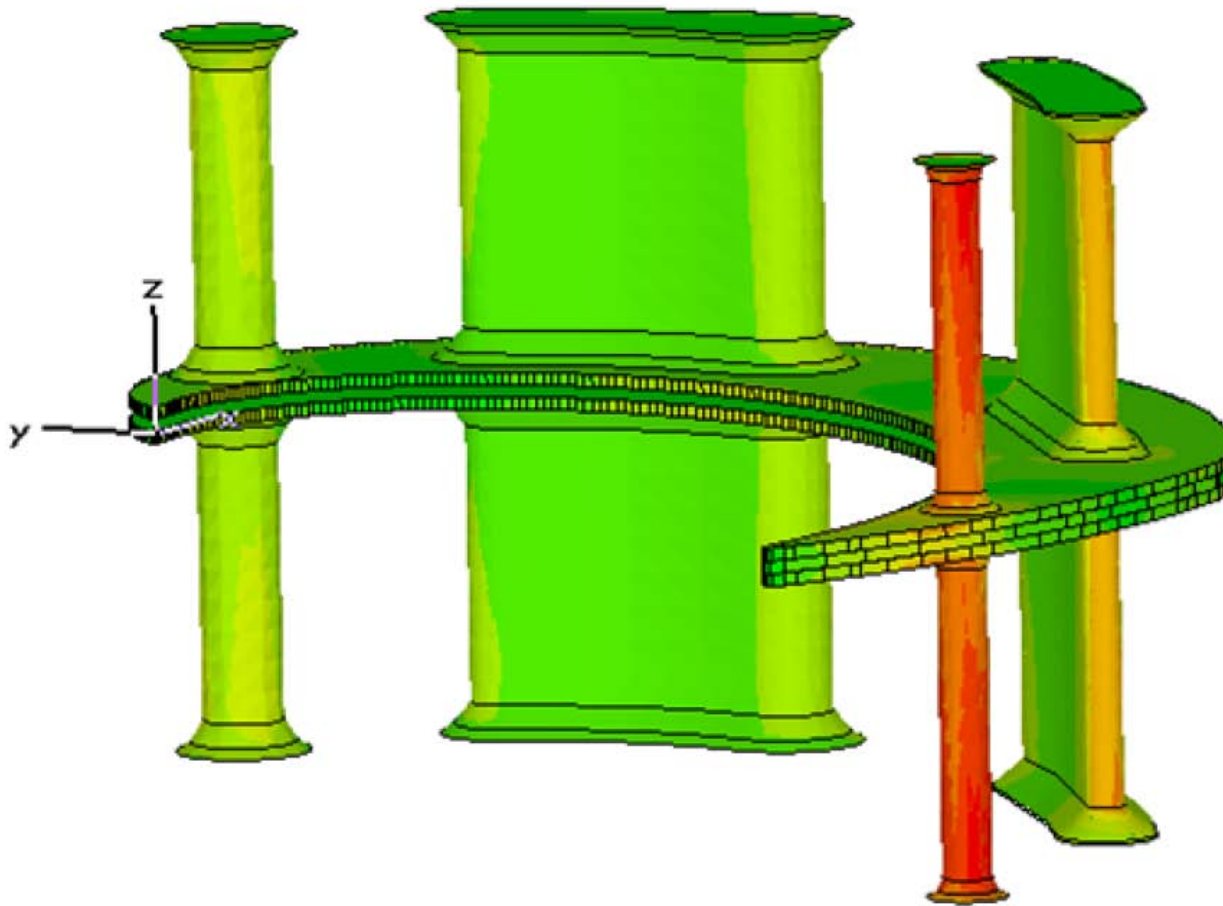
- 75 MHz resonator for 400 MeV/nucleon ^{12}C cyclotron IBA
- 4 parallel transmission line cavities
 - optimized voltage distribution
 - suppression higher order modes along Dee
 - mechanical stiffness



courtesy IBA, JINR

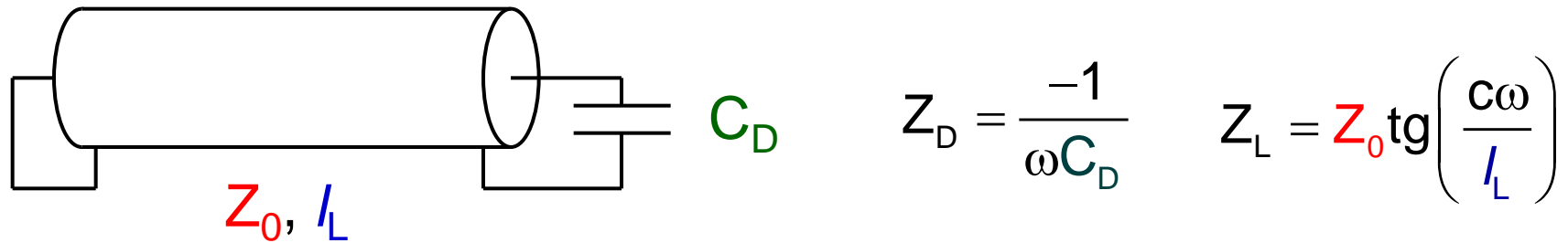
resonator design: 3D simulations

- 75 MHz resonator for 400 MeV/nucleon ^{12}C cyclotron IBA



courtesy IBA, JINR

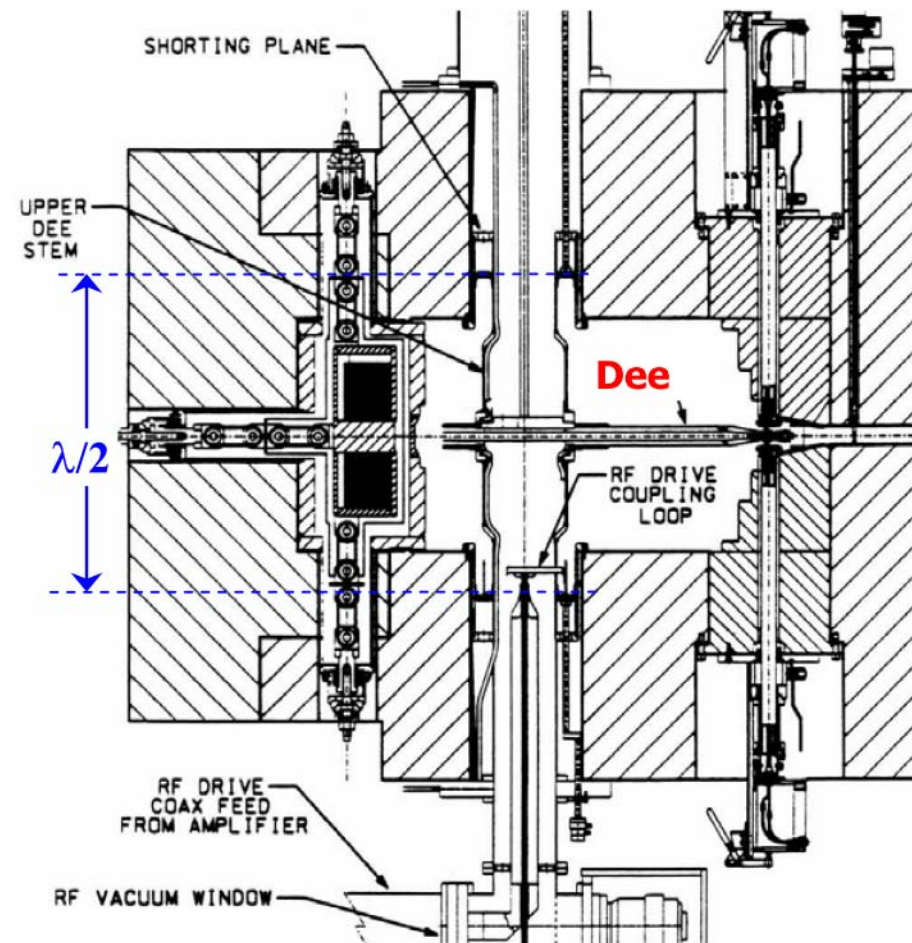
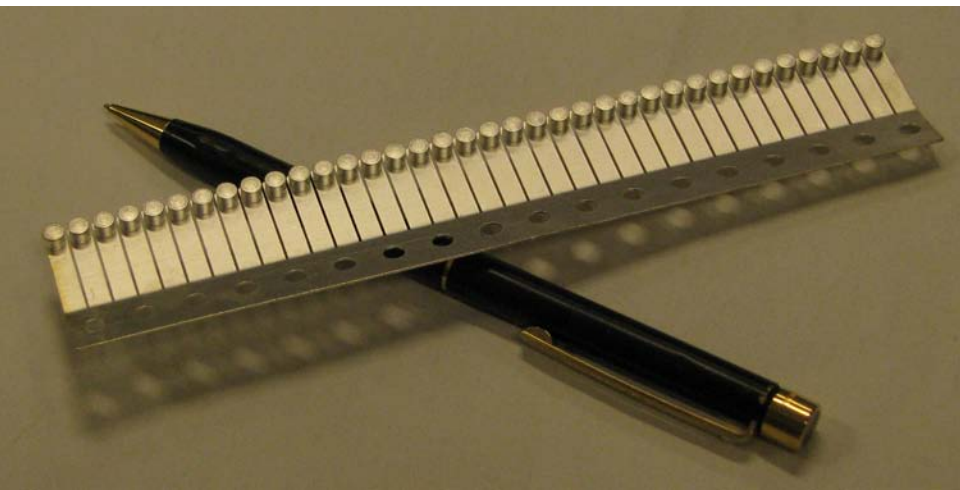
frequency tuning transmission line resonator



- resonance condition $Z_D = -Z_L$
- transmission line resonators
 - length transmission line
è mobile short
 - characteristic impedance transmission line
è mobile panel, plunger
 - capacitance acceleration electrode
è mobile panel
- combination of techniques for coarse and fine tuning

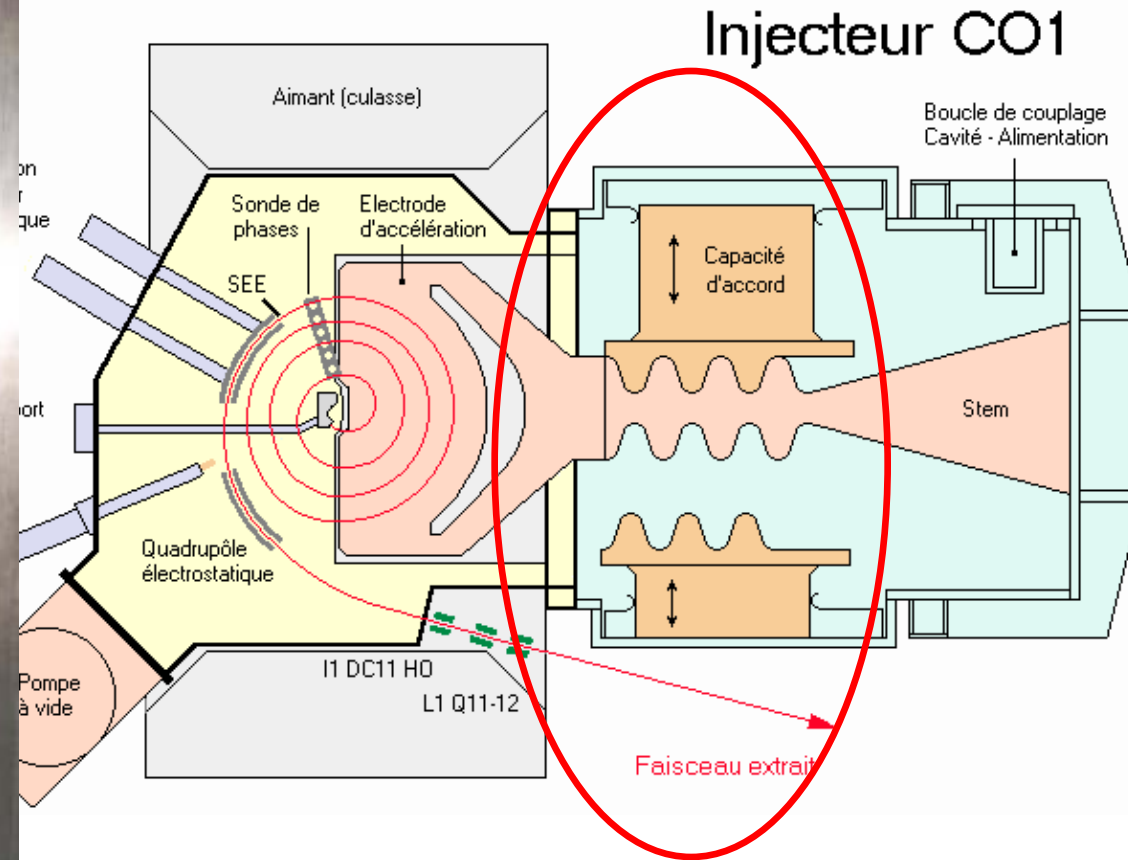
frequency tuning: VARIAN PT cyclotron

- frequency adjustment and tuning with sliding shorts
 - move both to retain symmetry
 - **move under power**
- è high performance contacts
 - silver plated CuBe spring
 - carbon-silver contact grain
 - 50 A per contact at 60 MHz
 - development GANIL/AGOR



frequency tuning: GANIL injector cyclotron

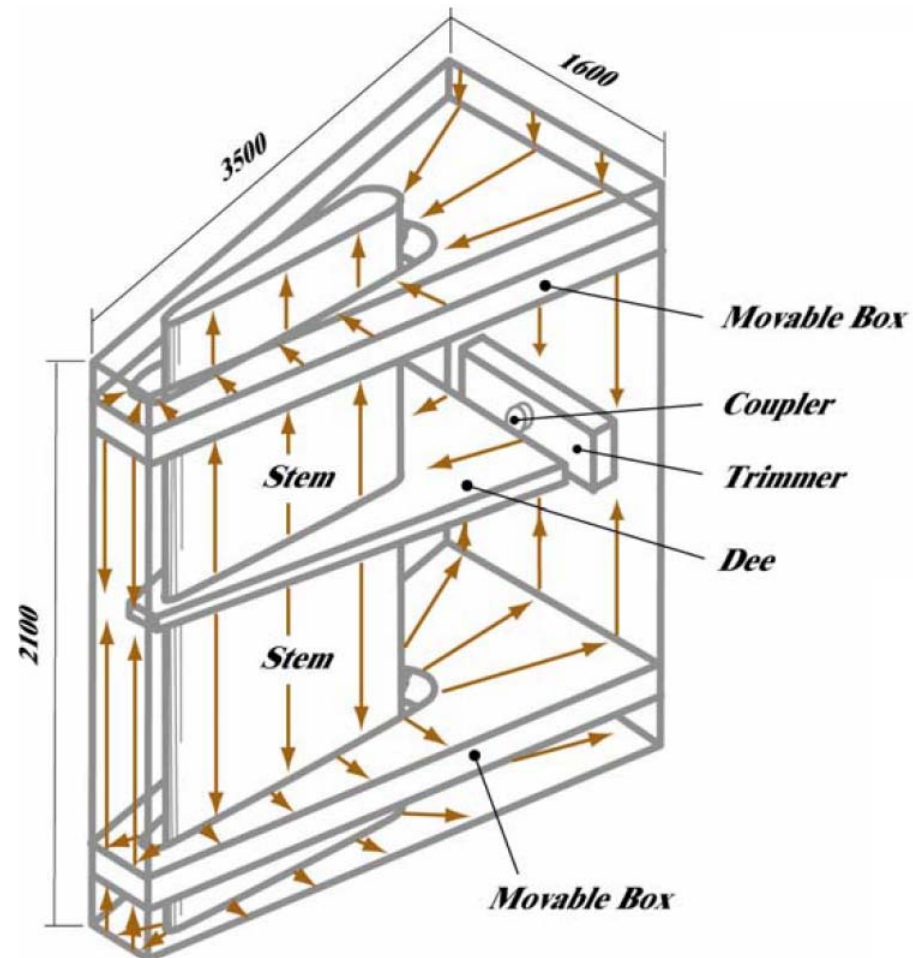
- change characteristic impedance transmission line



frequency tuning: RIKEN ring cyclotron

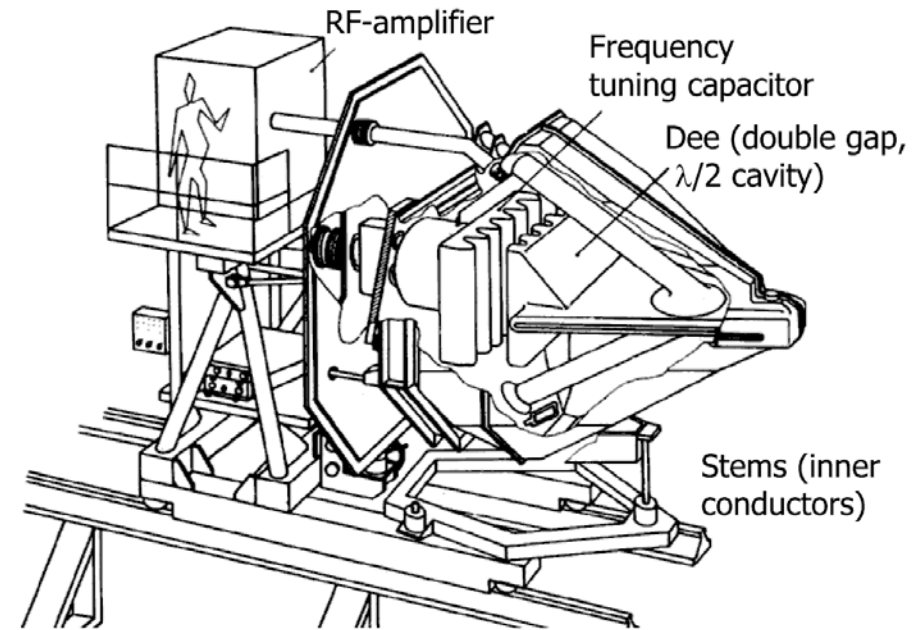
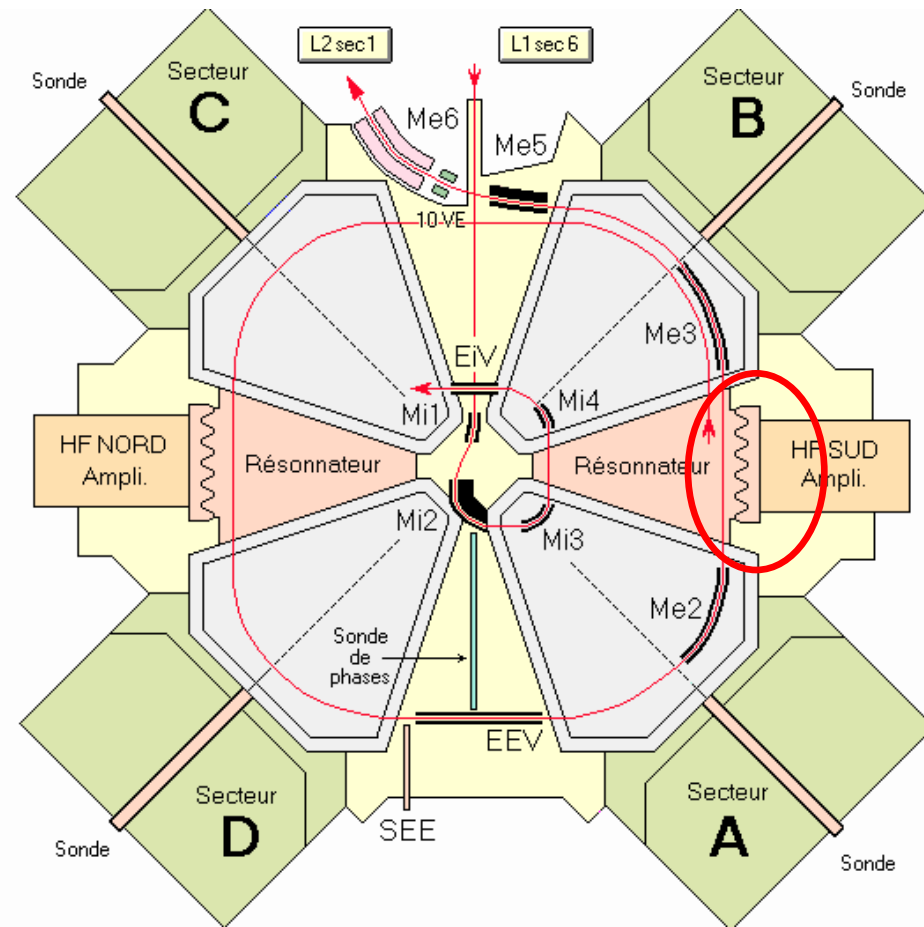
- change of characteristic impedance at different location
 - no high current density contacts on stem
 - box to median plane: more capacitance \Rightarrow lower frequency
 - box to outside: less inductance \Rightarrow higher frequency

- resonator characteristics
 - 18 – 45 MHz
 - 300 kV @ 45 MHz
 - 150 kW @ 45 MHz



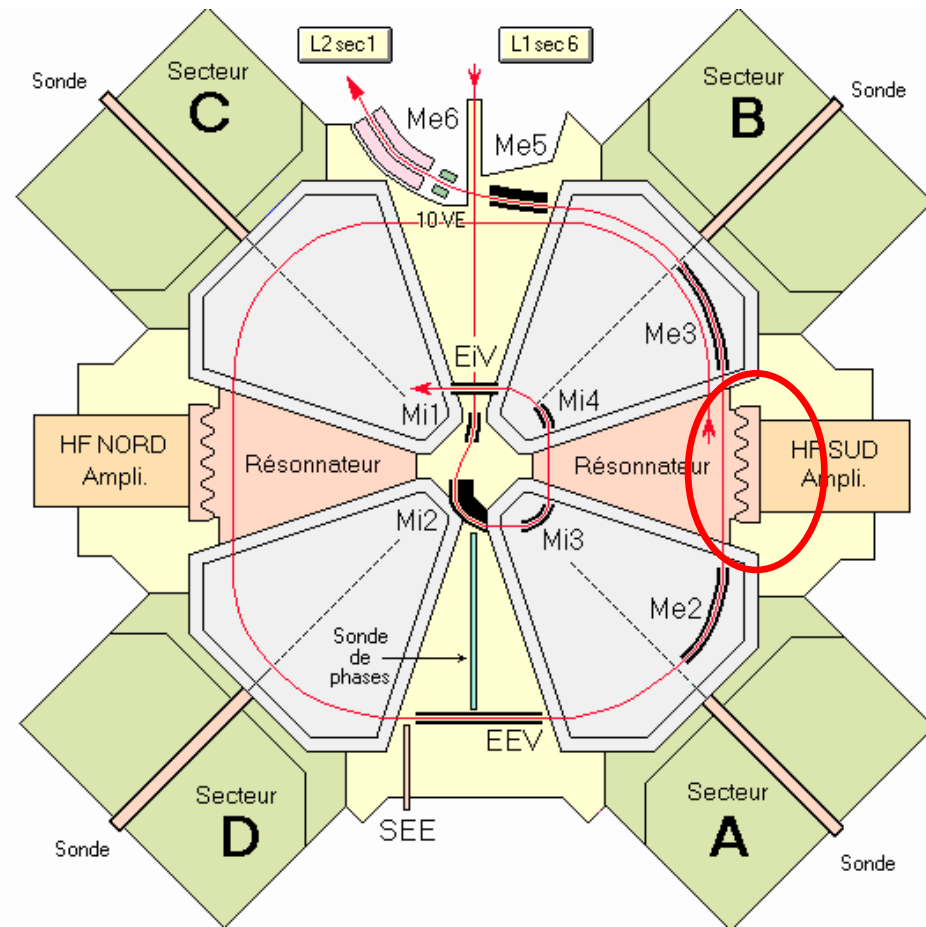
frequency tuning: GANIL main cyclotron

- change capacitance
acceleration electrode



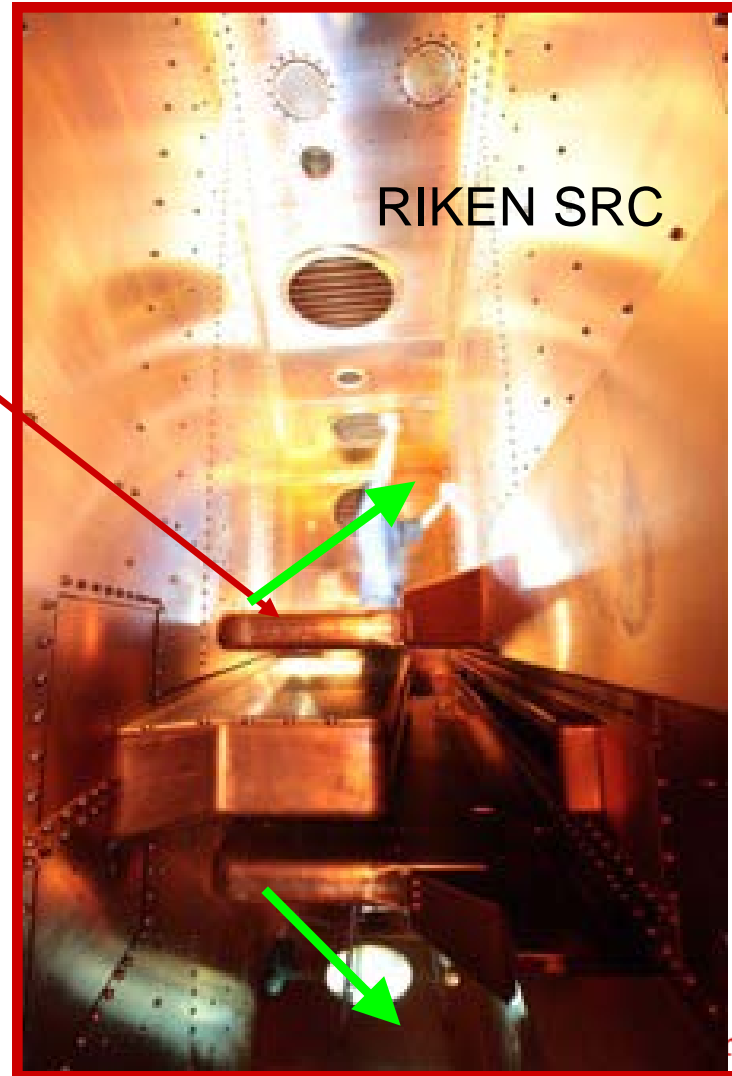
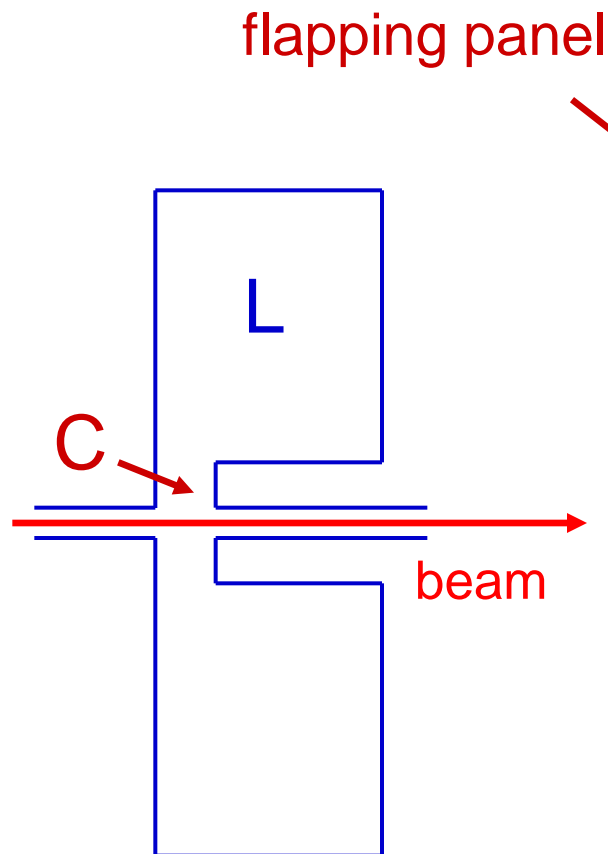
frequency tuning: GANIL main cyclotron

- change capacitance
acceleration electrode



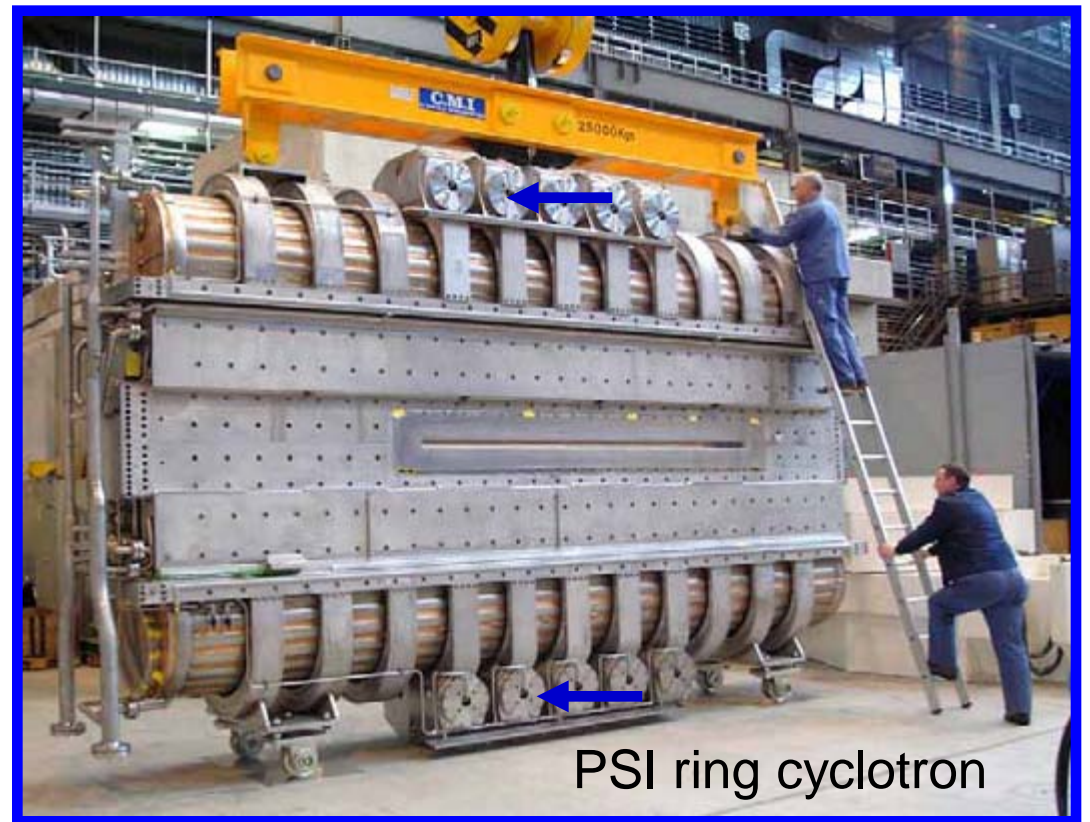
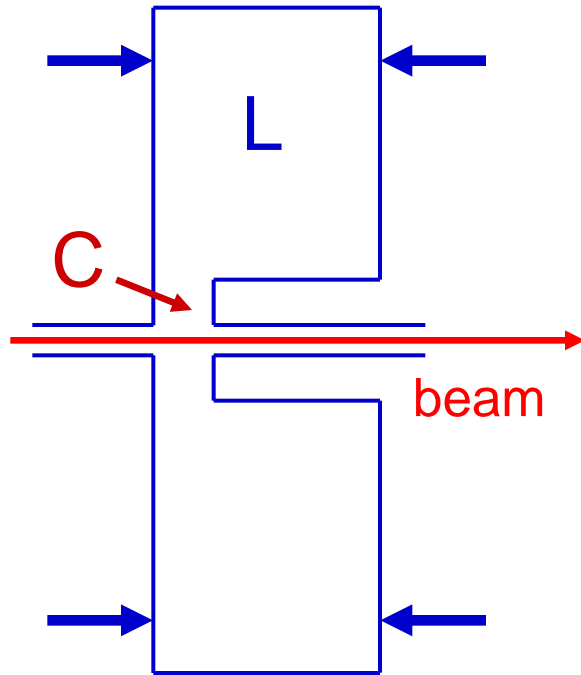
frequency tuning: single gap resonator

- basically two options
 - gap capacitance
 - chamber inductance



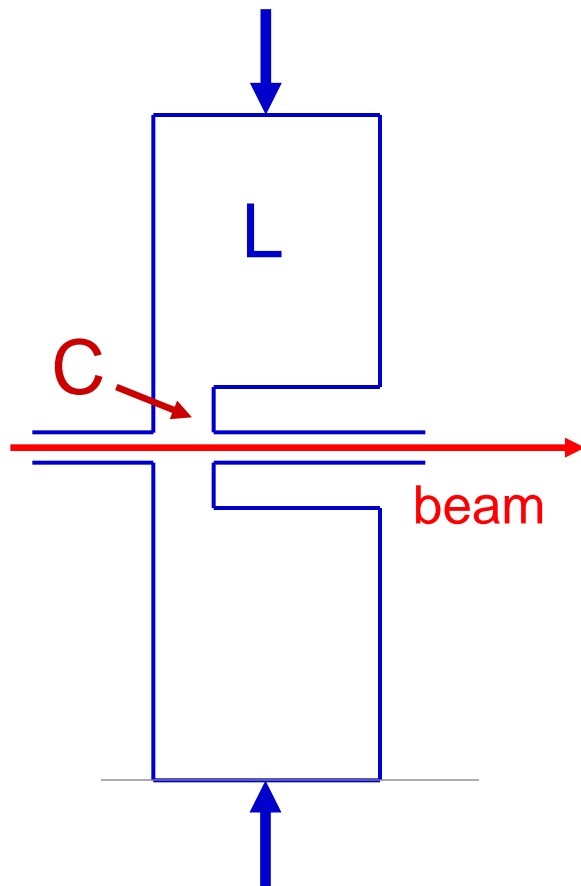
frequency tuning: single gap resonator

- basically two options
 - gap capacitance
 - chamber inductance

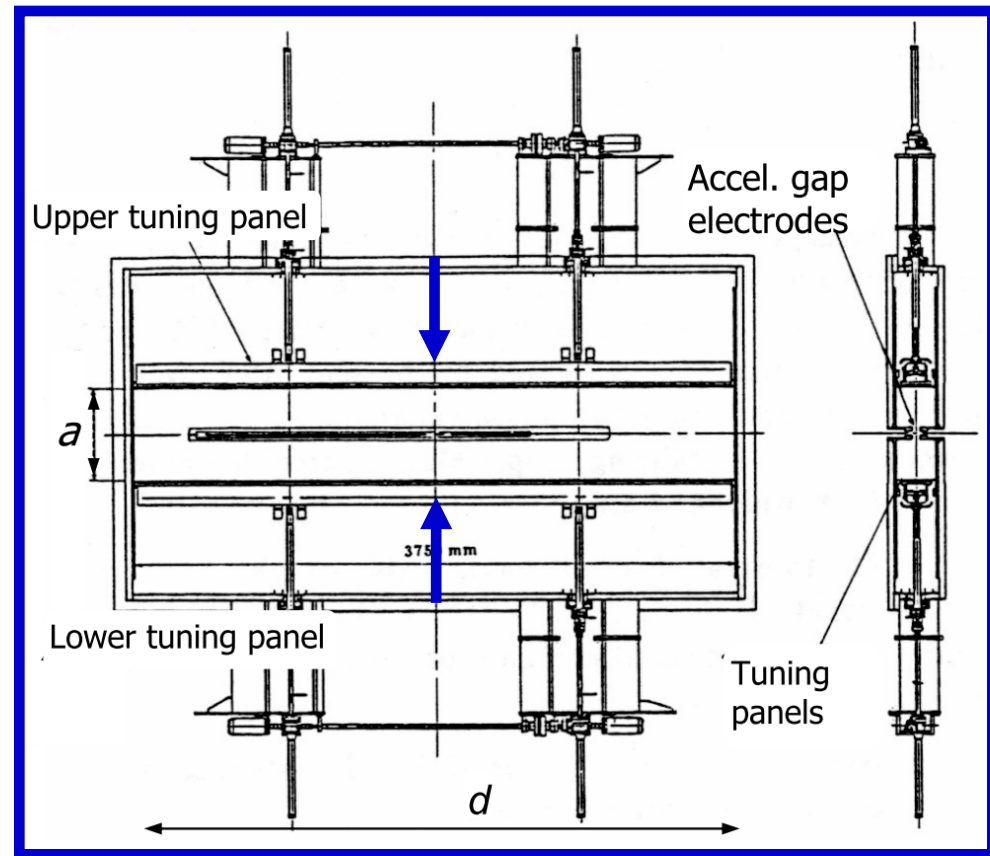


frequency tuning: single gap resonator

- basically two options
 - gap capacitance
 - chamber inductance

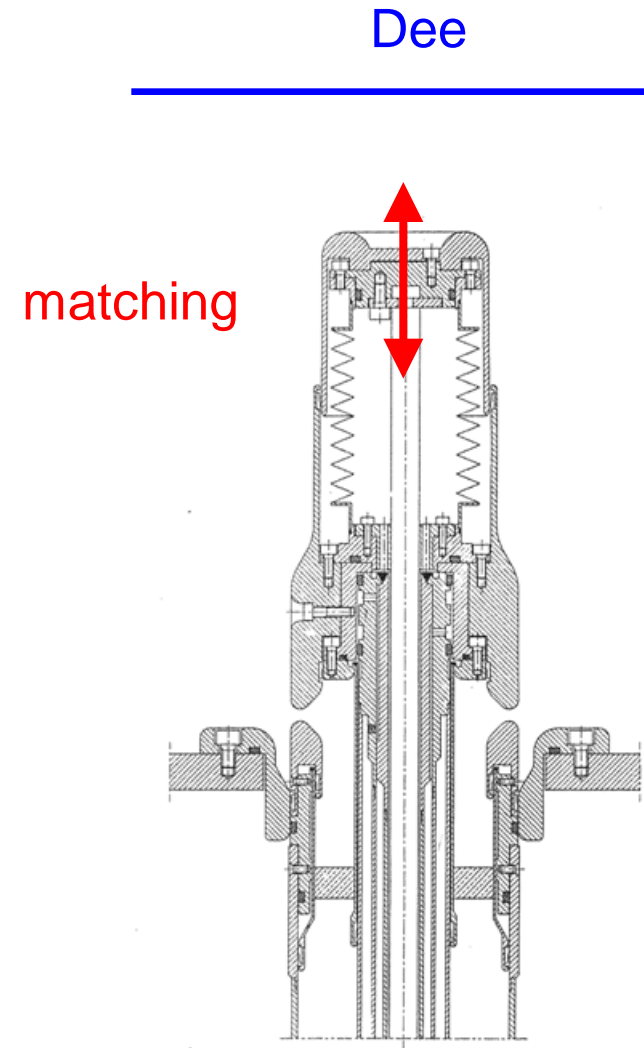


RCNP ring cyclotron



power coupling: capacitive

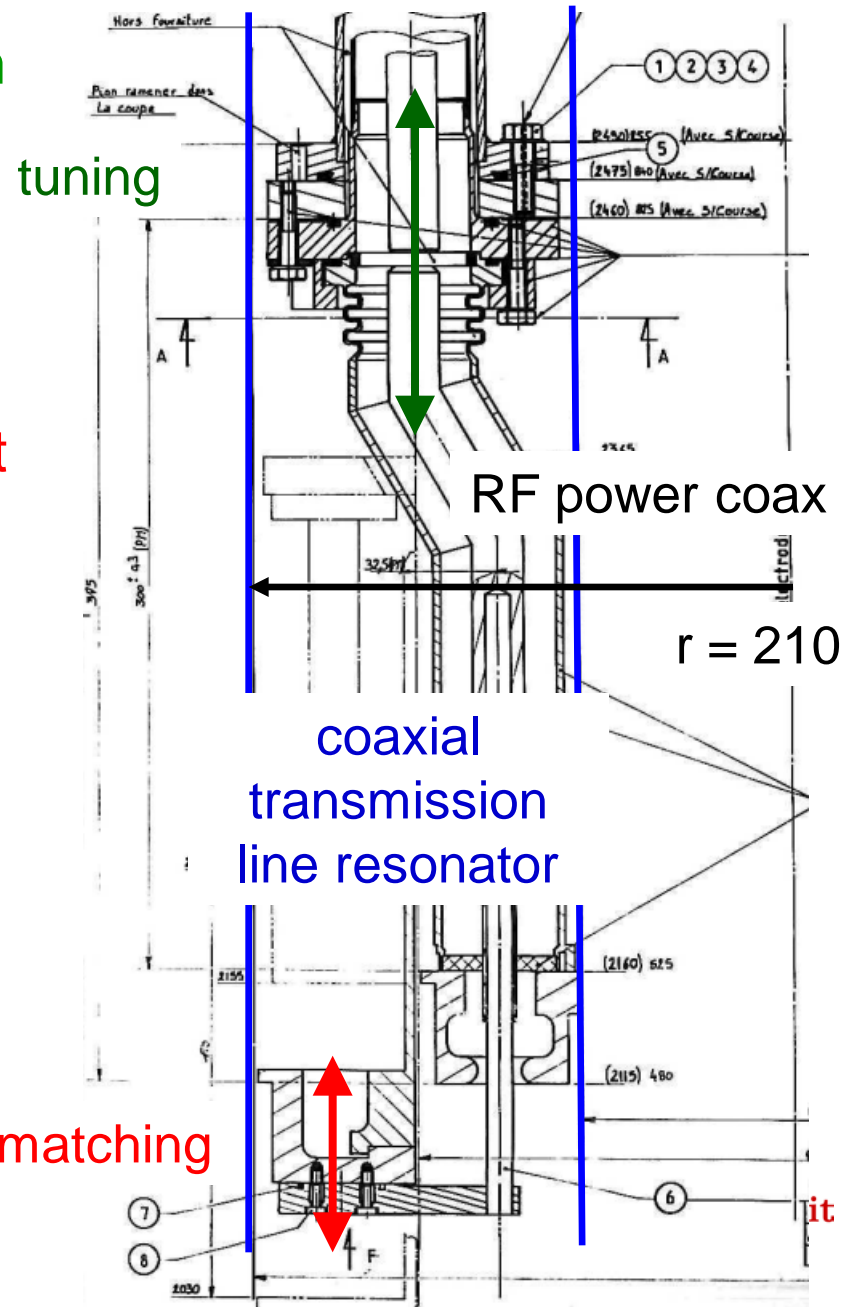
- simple mechanics
- also applicable for tuning control
- high voltage
 - insulator
 - discharge



power coupling: inductive

- low voltage è insulator no problem
- multipactor
- variable frequency resonator:
complex mechanics
- high current rotating/sliding contact

AGOR, Groningen



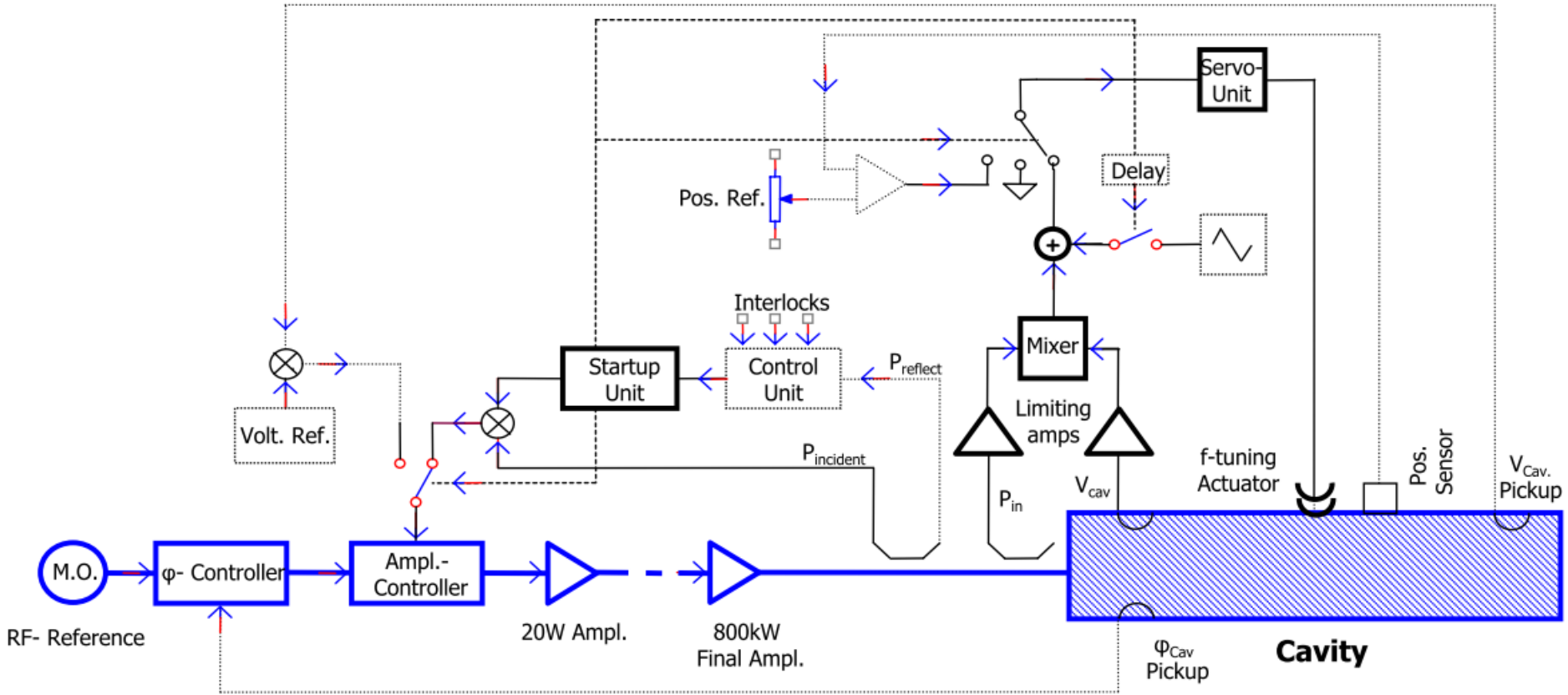
RF controls

- controlled parameters
 - amplitude acceleration voltage
 - phase acceleration phase
 - required when using several independent resonators
 - resonator tuning
 - high intensity: possibly matching (beam loading)
- measured parameters
 - amplitude acceleration voltage
 - phase acceleration voltage
 - phase incident wave – acceleration voltage
 - reflected power

RF controls: design issues

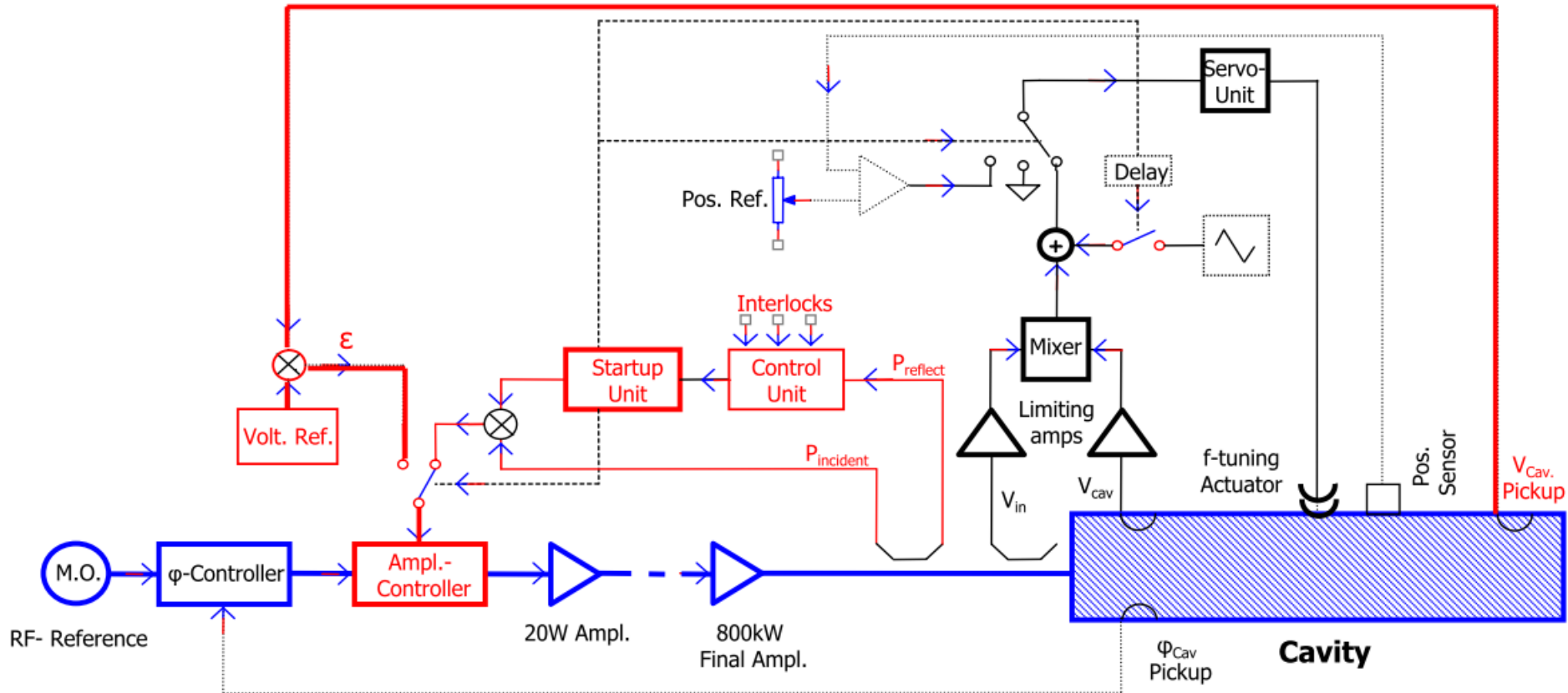
- pick-up probes
 - mechanical stability
- pick-up electronics
 - large amplitude and frequency range
- error signal processing
 - high gain for phase and amplitude stability
 - compensation resonator response
- grounds loop via RF circuitry

RF controls: overview



courtesy Peter Sigg, PSI

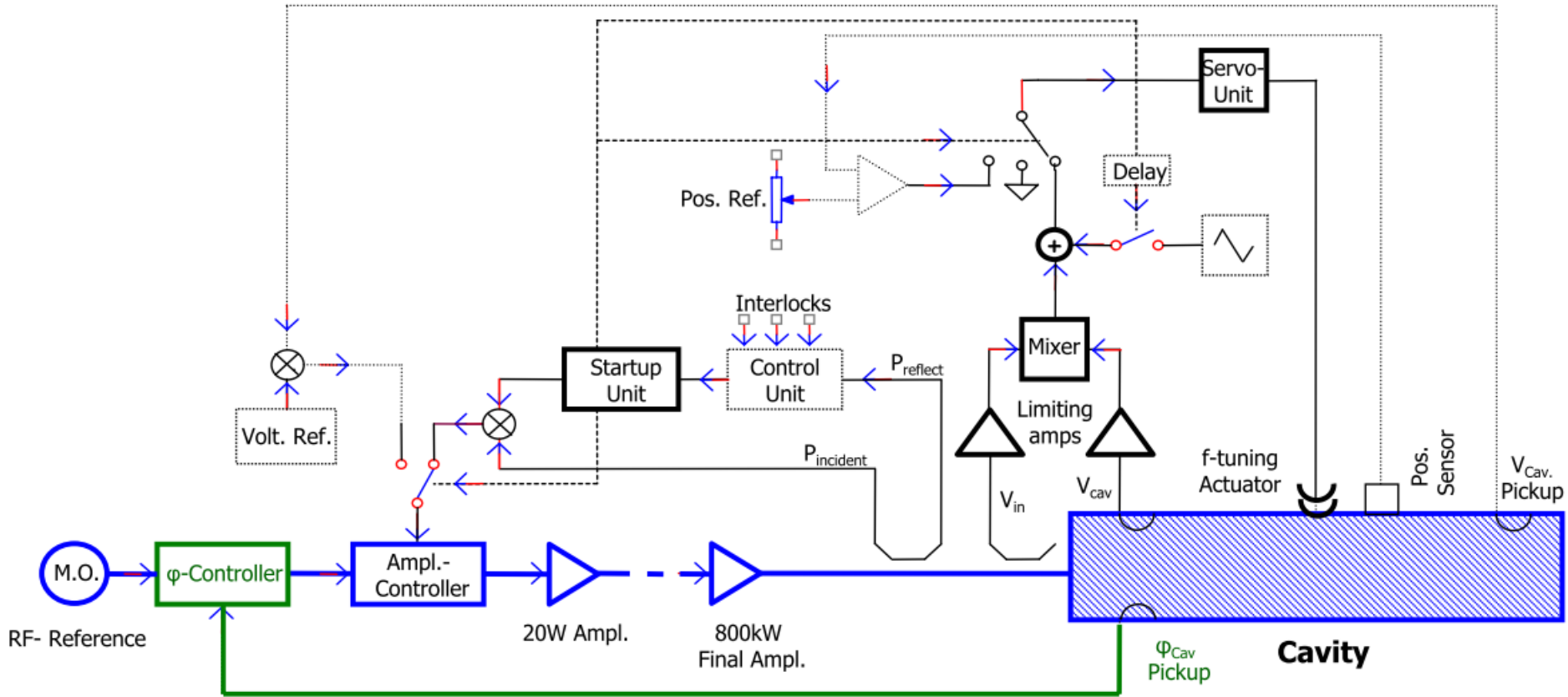
RF controls: amplitude



courtesy Peter Sigg, PSI

- power pulse at start-up to pass through multipactor region
- amplitude stability $<10^{-4}$

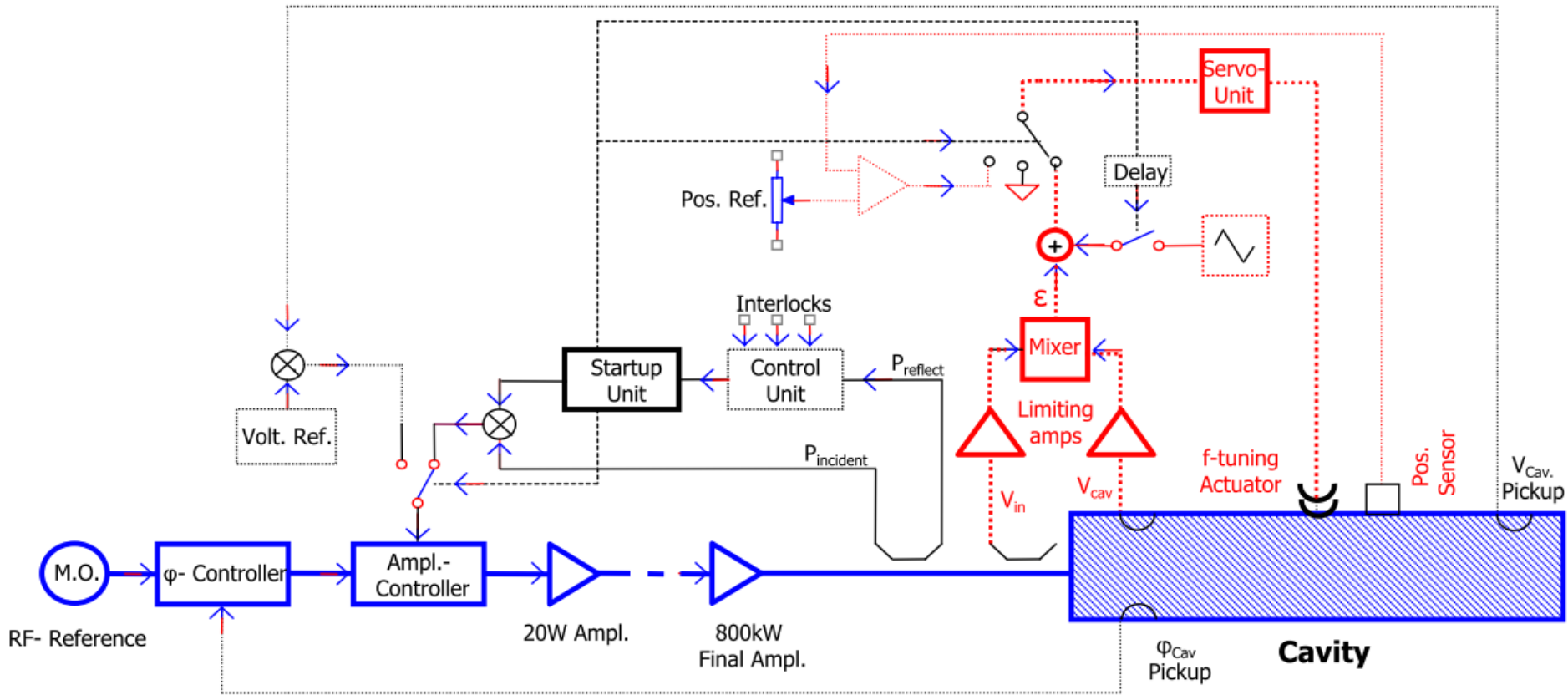
RF controls: phase



courtesy Peter Sigg, PSI

- essential for multi-resonator system
- phase stability $< 0.1^\circ$

RF controls: tuning



courtesy Peter Sigg, PSI

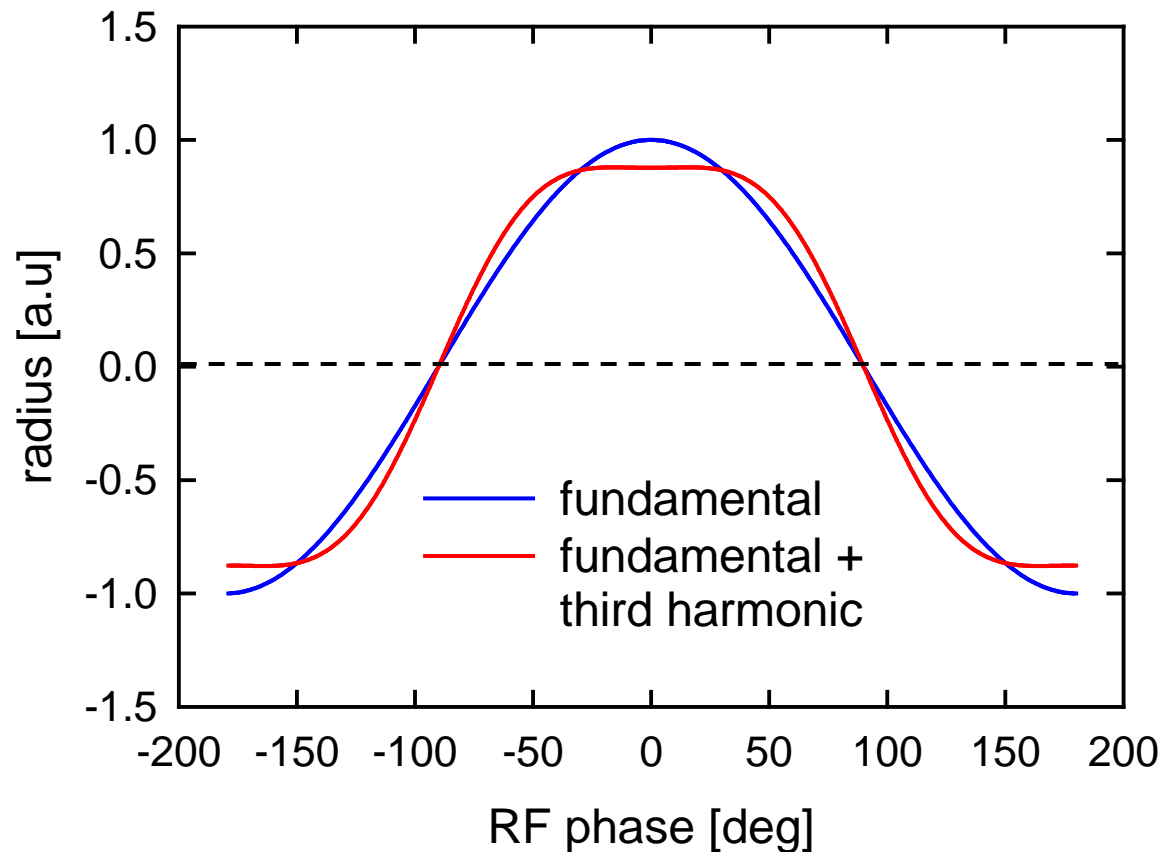
- bandwidth typ. 1 Hz

flattopping with higher harmonic

- cyclotron: no phase stability (always on transition)
 - $\Delta\varphi$ translates into ΔE
 - è radial bunch broadening, overlapping turns
 - increased by fieldimperfections: acceleration on slope
- add odd higher harmonic of RF voltage
 - è reduced energyspread
 - è compensate longitudinal space charge force
- flat topping resonator extracts power from beam
 - è complex voltage and phase control @ high beam intensity

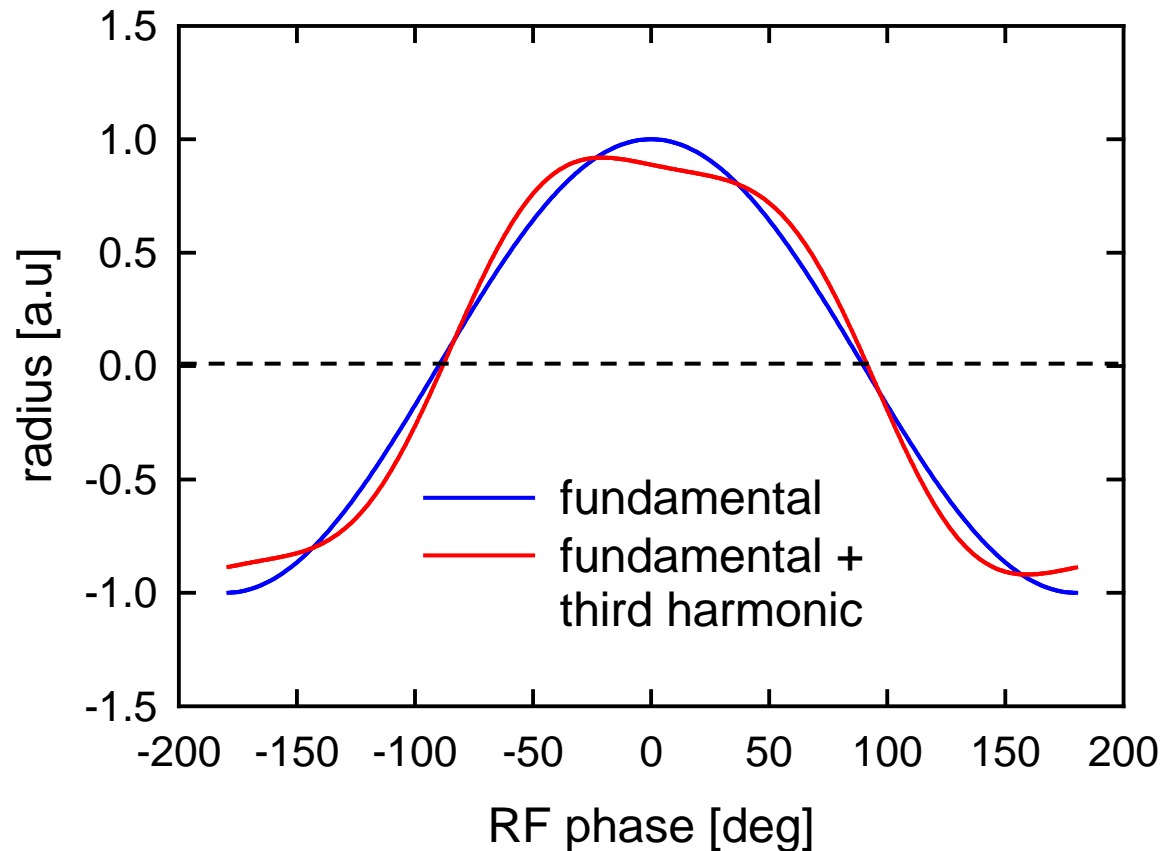
flattopping with higher harmonic

- accommodate larger bunchwidth and isochronism deviations



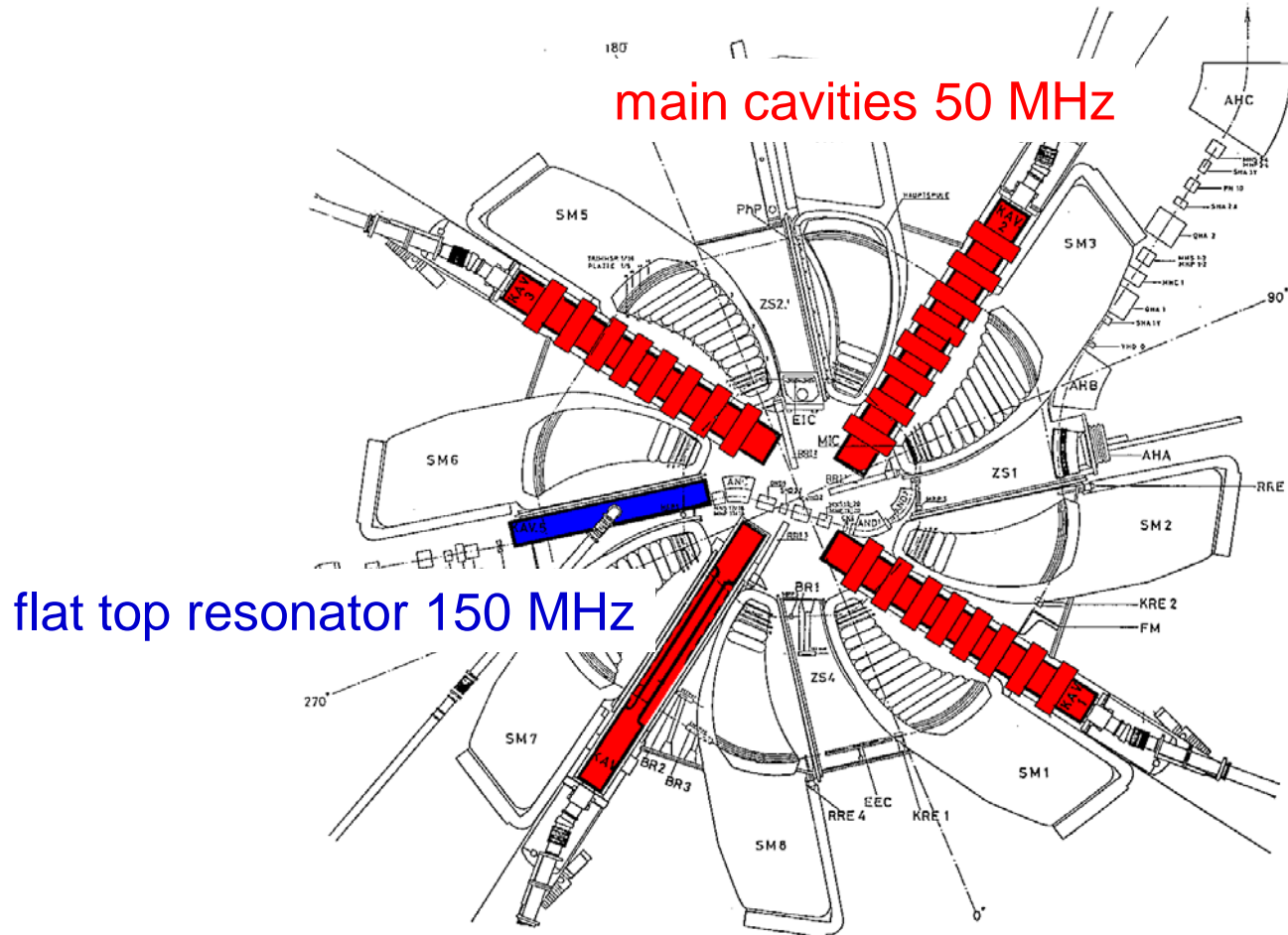
flattopping with higher harmonic

- accommodate larger bunchwidth and isochronism deviations
- compensate longitudinal phase space force
 - phase and amplitude intensity dependent



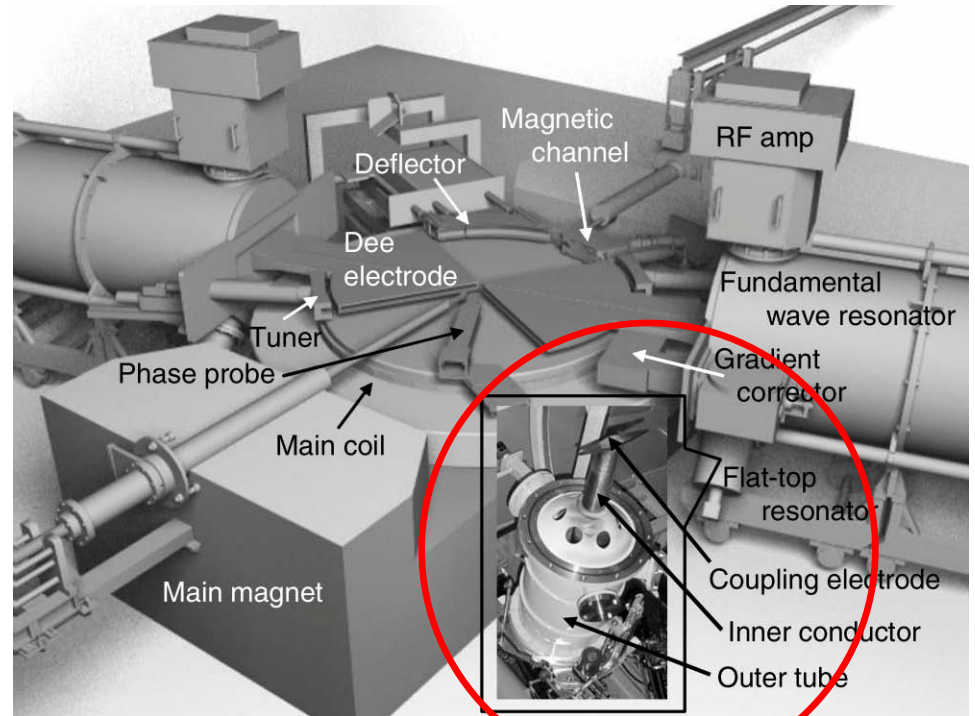
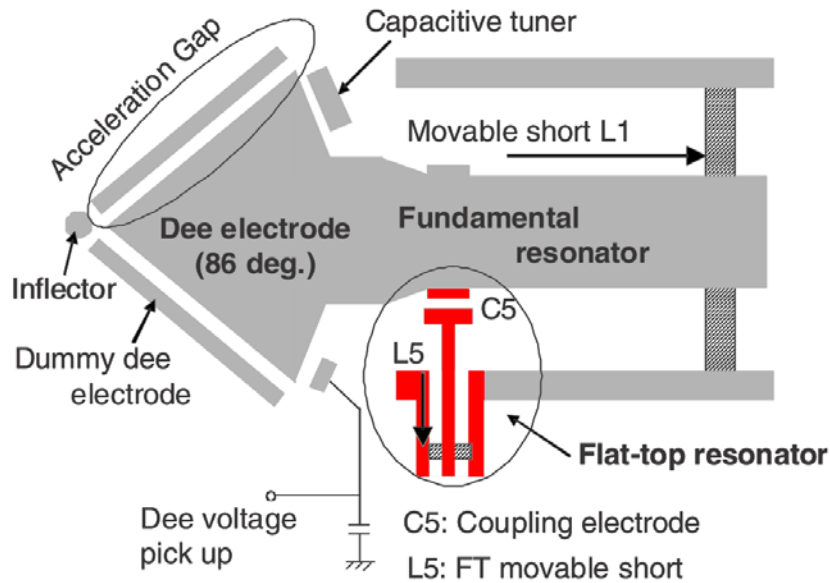
flattopping with higher harmonics

- PSI, RIKEN, RCNP: separate higher harmonic resonator



flattopping with higher harmonic

- JAERI AVF cyclotron: higher harmonic superimposed



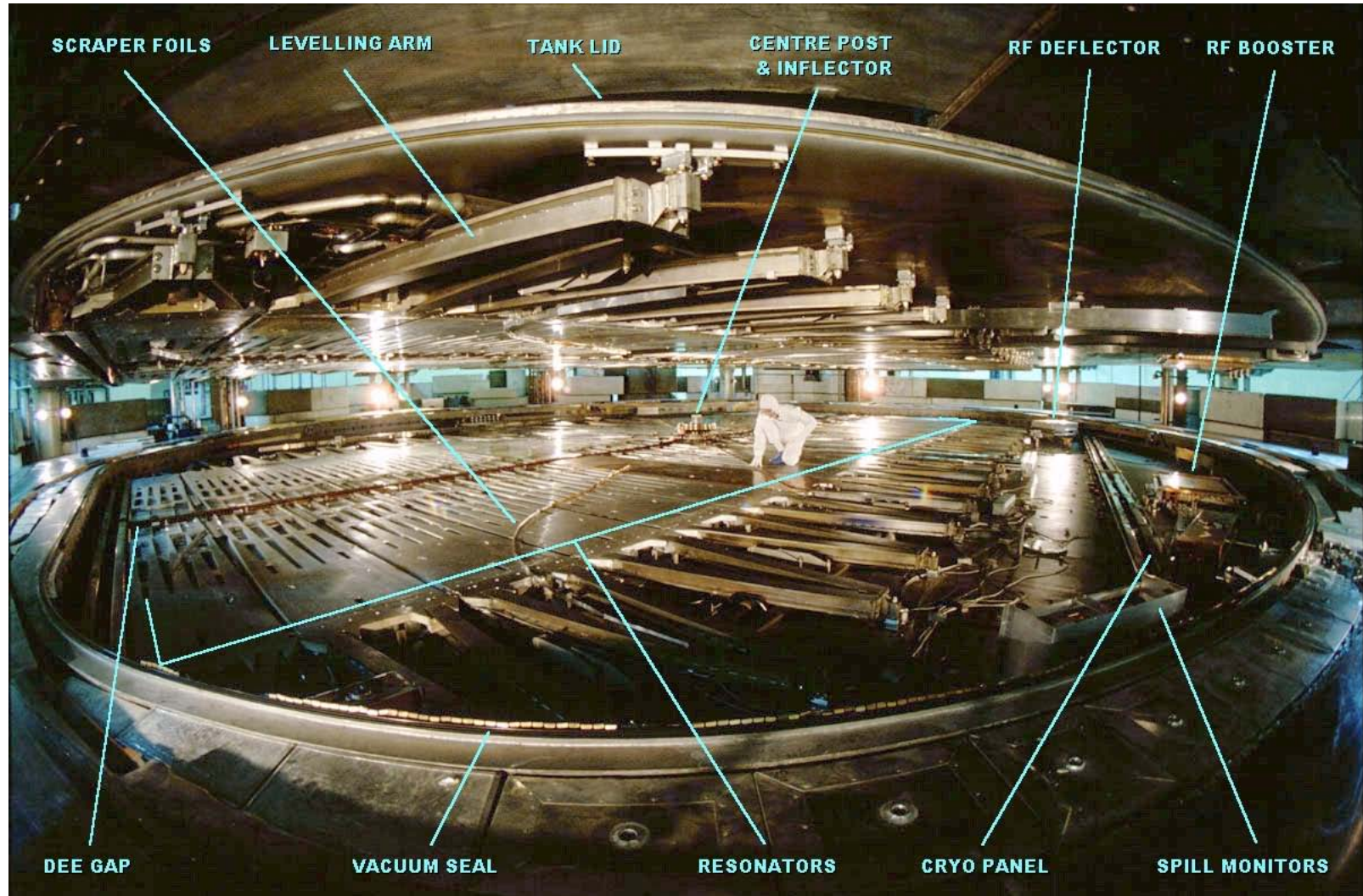
some examples: TRIUMF

- beam 200 μA 520 MeV H^-



some examples: TRIUMF

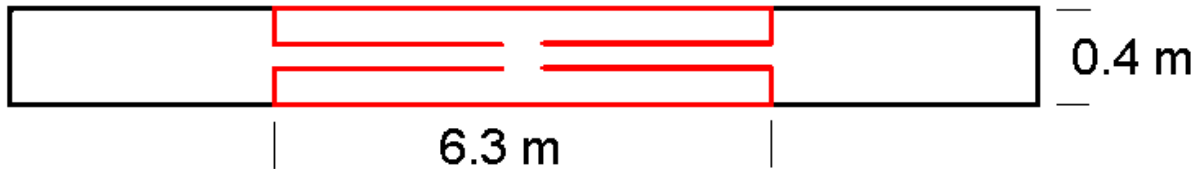
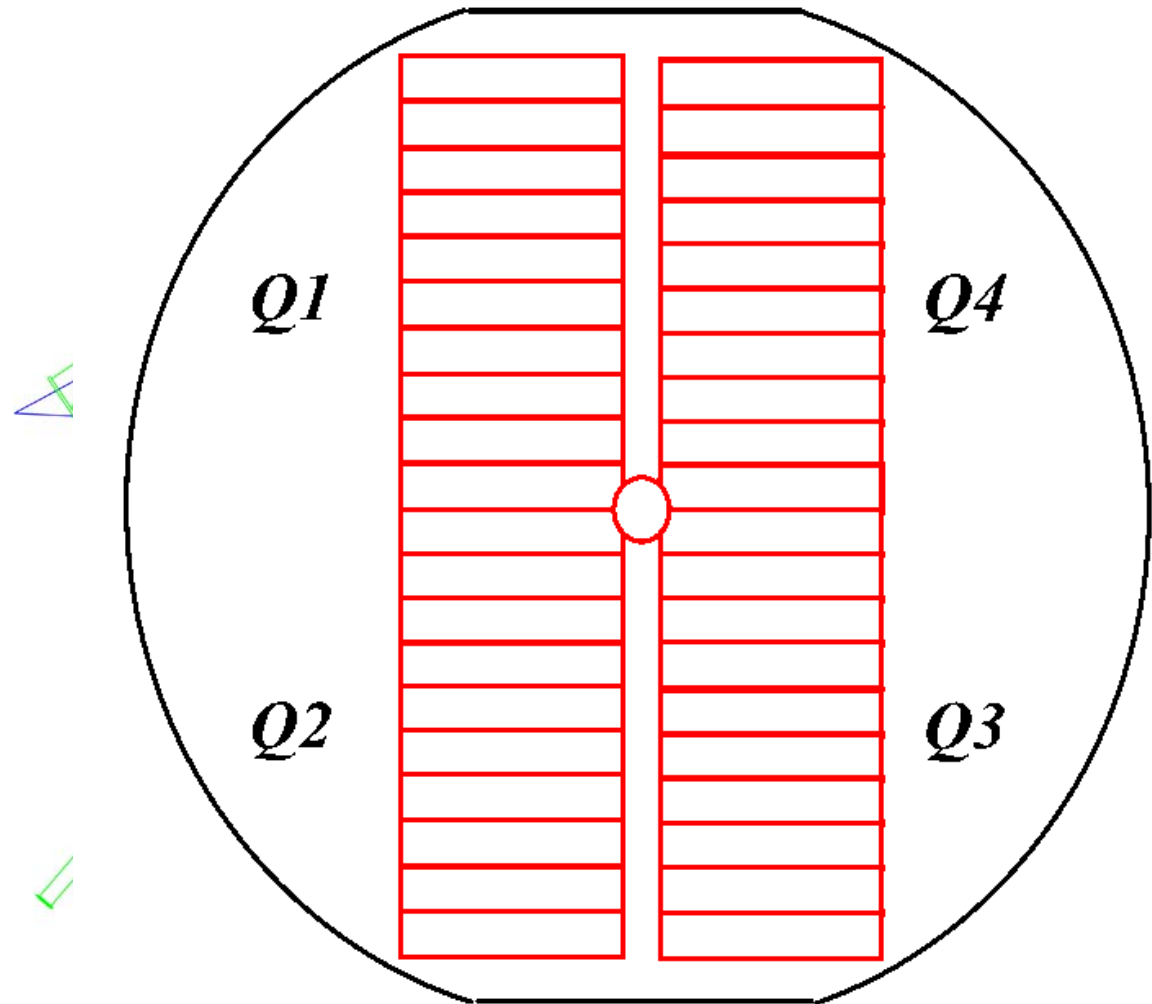
- beam 200 μA 520 MeV H^-



some examples: TRIUMF

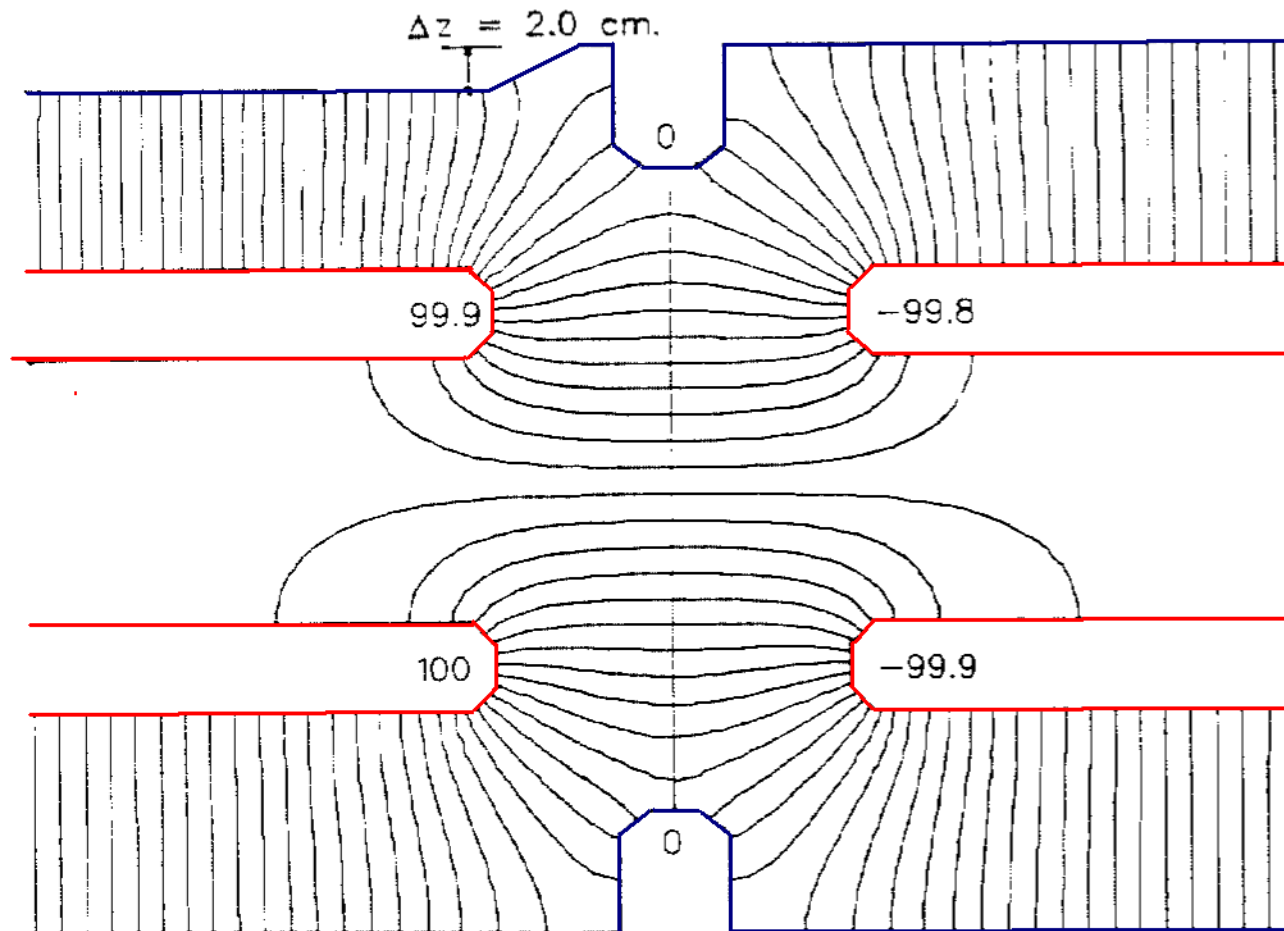
- 80 23 MHz $\lambda/4$ resonators
 - 2 x 20 above median plane
 - 2 x 20 below median plane
- excitation scheme
 - above – below inductive coupling; 0-mode
 - adjacent capacitive coupling; 0-mode
 - left – right capacitive coupling; π -mode
- inductive coupling; RF power 1.2 MW
- tuning by resonator deformation

some examples: TRIUMF



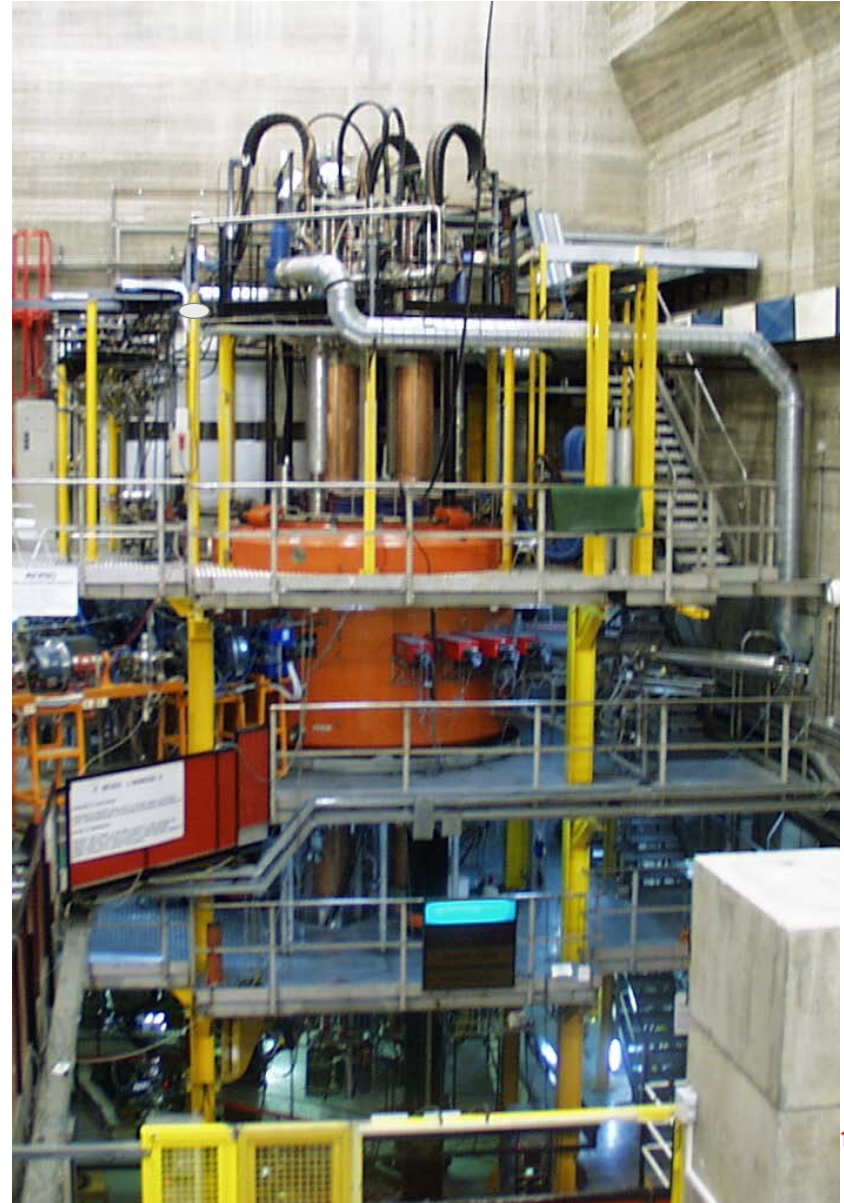
some examples: TRIUMF

- electric field distribution in accelerating gap



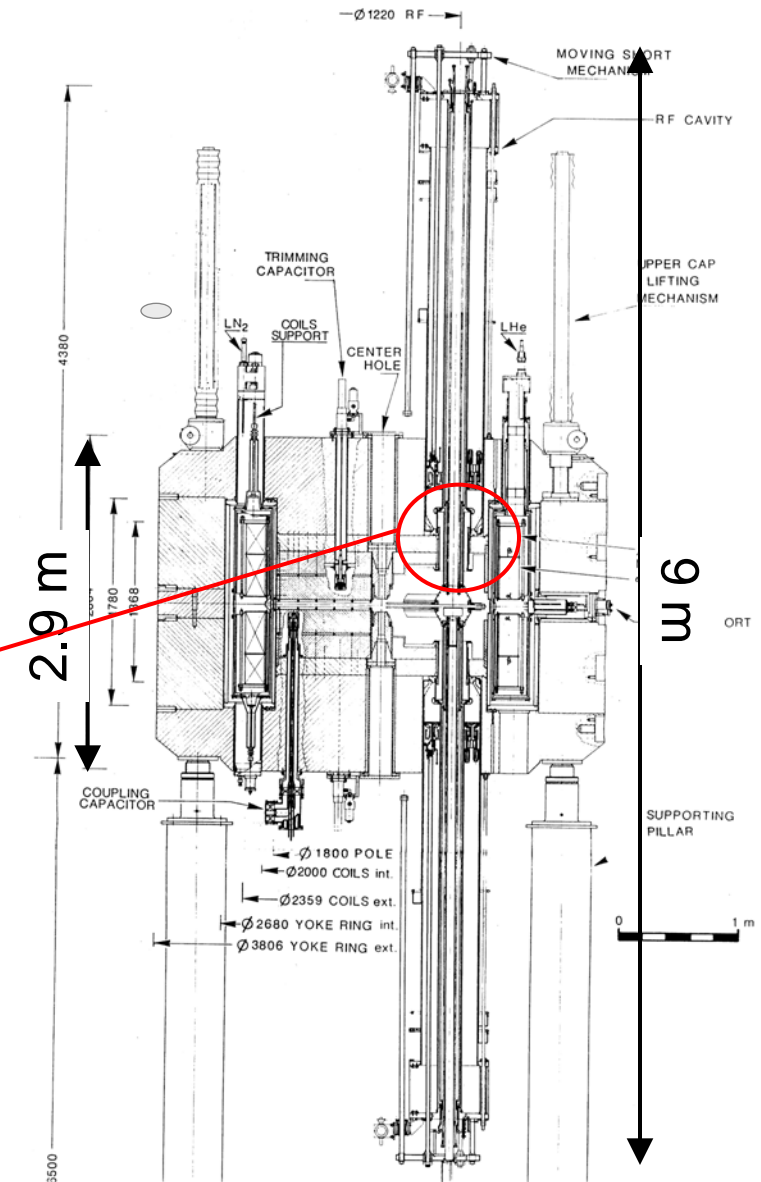
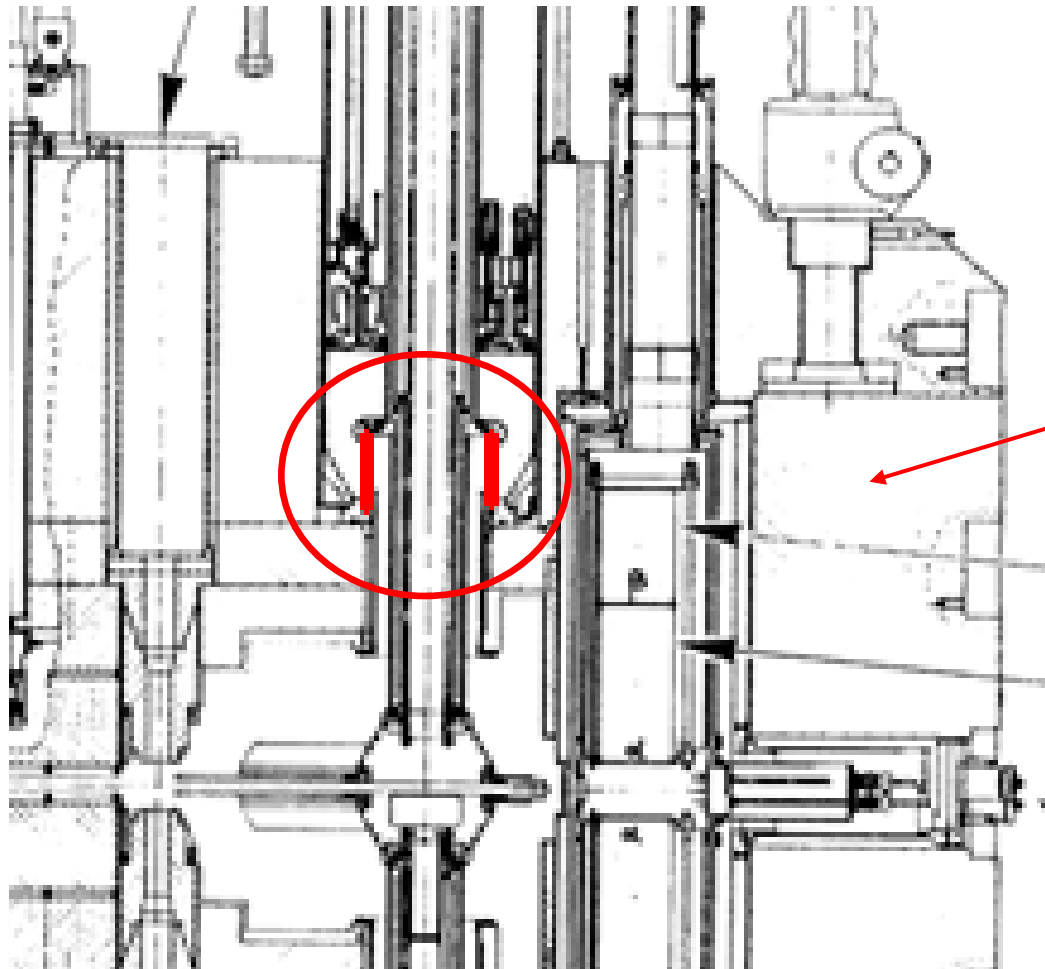
some examples: LNS SC cyclotron

- three 15 – 48 MHz $\lambda/2$ resonators



some examples: LNS SC cyclotron

- three 15 – 48 MHz $\lambda/2$ resonators
 - vacuum feedthrough issue: E || B



some examples: LNS SC cyclotron

- inter-resonator coupling in center
- not operating in Eigenmode
 - power transfer between resonators è perturbation

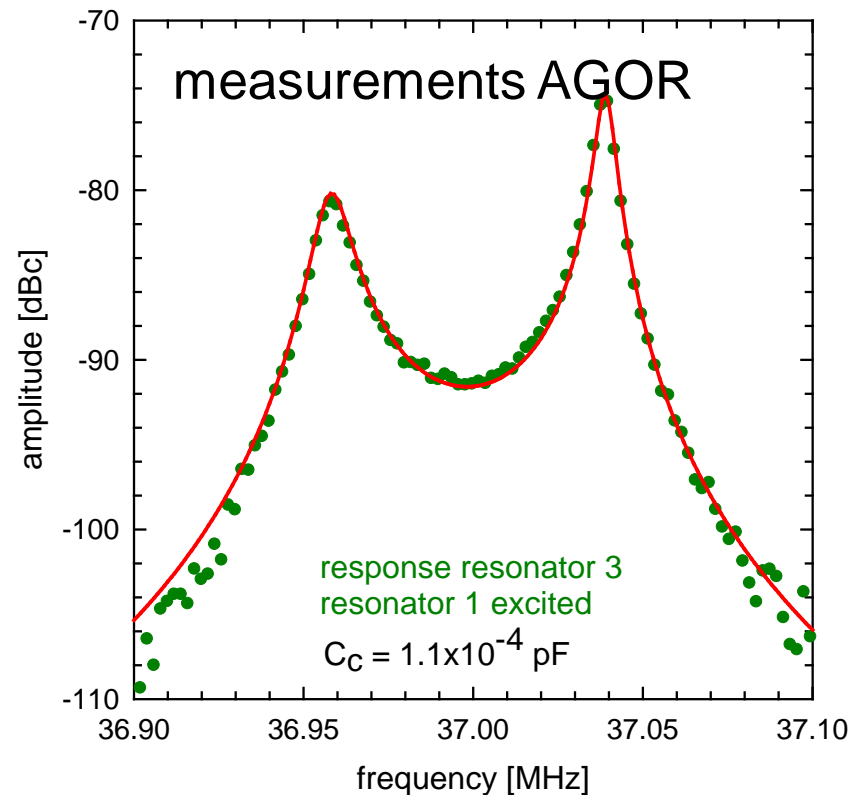


some examples: LNS SC cyclotron

- inter-resonator coupling in center
 - not operating in normal mode ($h = 3$)
 - power transfer between resonators è perturbation
 - some numbers
 - reactive power resonator $P_R = 100 \text{ MW}$
 - electrode voltage $V_D = 100 \text{ kV}$
 - operating frequency $\nu = 40 \text{ MHz}$
 - reactive power coupling $1.75 V^2 \omega C_c$
 4.4 MW/pF
- è minimize coupling capacitance
achievable value $C_c \leq 10^{-3} \text{ pF}$

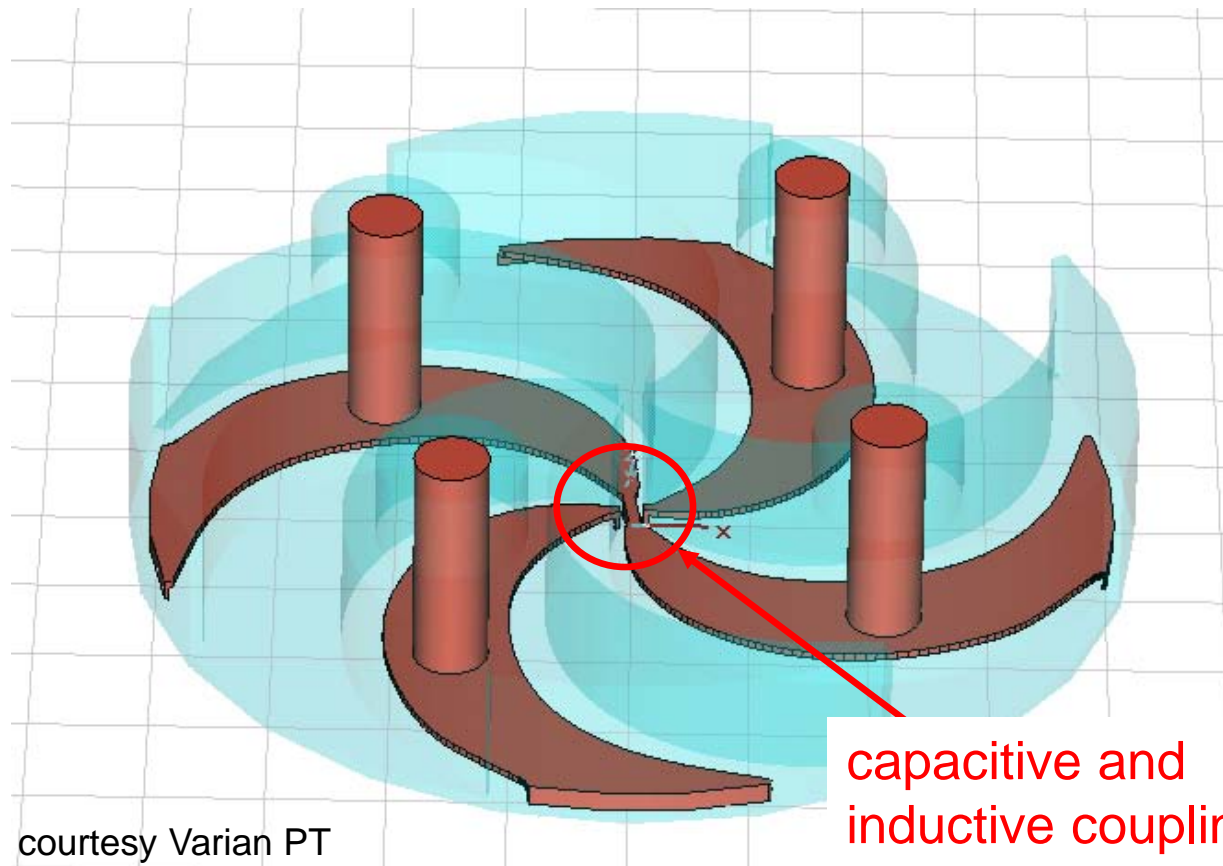
some examples: LNS SC cyclotron

- inter-resonator coupling in center
- not operating in normal mode ($h = 3$)
 - power transfer between resonators è perturbation è minimize coupling capacitance
achievable value $C_c \leq 10^{-3}$ pF



some examples: VARIAN PT cyclotron

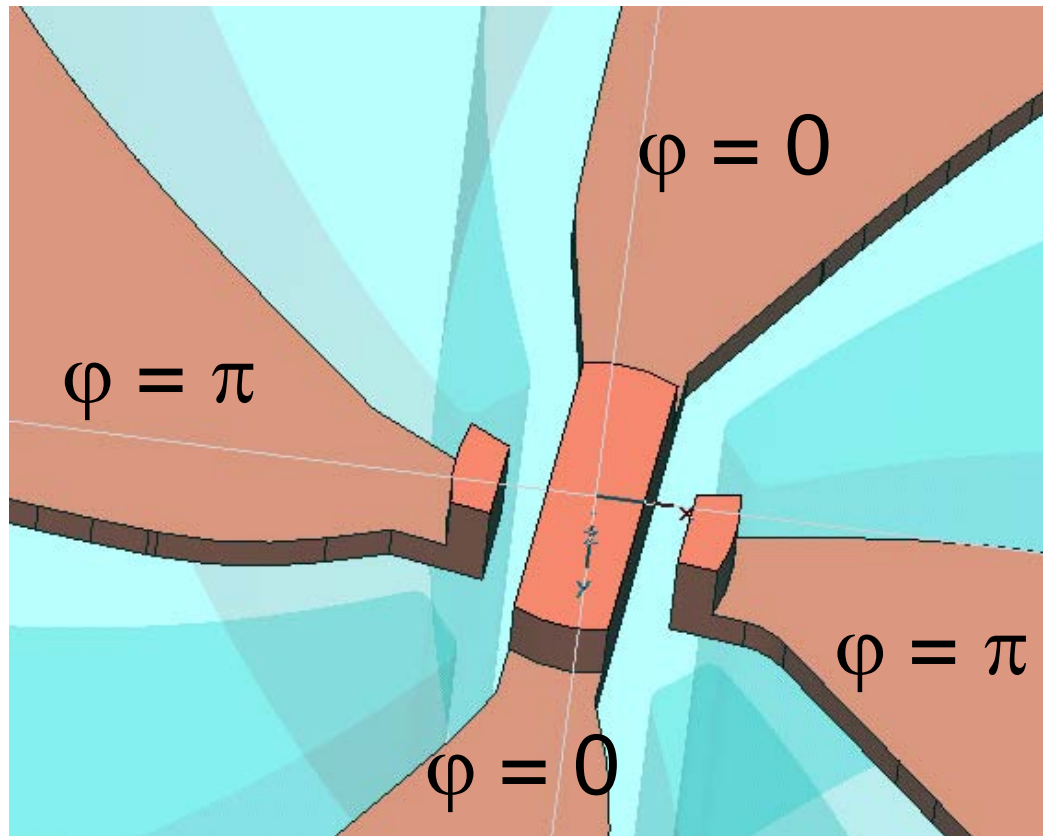
- 250 MeV protons
- 4 coupled $\lambda/2$ resonators; 1 amplifier



capacitive and
inductive coupling
between resonators

some examples: VARIAN PT cyclotron

- 250 MeV protons
- 4 coupled $\lambda/2$ resonators driven via one power coupler
 - 4 Eigenmodes; only three can be excited
 - push-pull mode



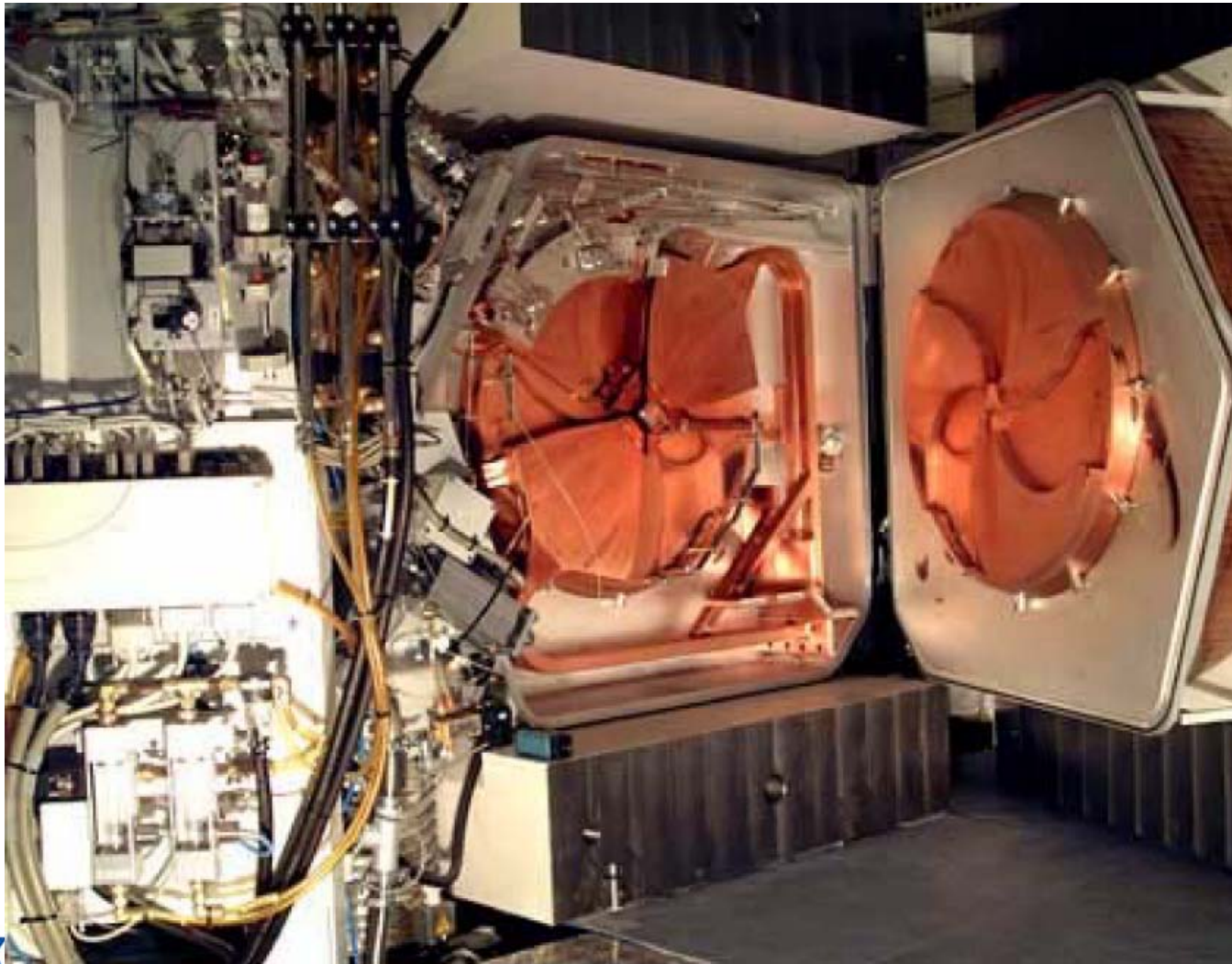
courtesy Varian PT

some examples: VARIAN PT cyclotron

- 250 MeV protons
- 4 coupled $\lambda/2$ resonators driven via one power coupler
 - 4 Eigenmodes; only three can be excited
 - push-pull mode
- complex tuning control
 - control parameters: 4 positions sliding short
 - error signals
 - phase drive power – resonator 1
 - 3 voltage ratios resonator 1 – resonator 2; 3 and 4
 - 4 x 4 transfer matrix not diagonal
 - è no independent servo loops

example: PET isotope production cyclotron

- 2 MHz $\lambda/4$ resonators; π -mode for protons, 0-mode for deuterons



courtesy GE

conclusions

- wide range of applications
 - isotope production
 - nuclear physics; radioactive beam production
 - meson factory; spallation neutron source
- wide range of beams and energies
 - protons up to uranium
 - 1.5 MeV/nucleon – 590 MeV/nucleon
- large dynamic range in intensity and beam power
 - <1 nA – 5 mA
 - <1 W – 1.3 MW
- compact cyclotrons, separated sector cyclotrons
- extraction radius 0.2 – 8 m

è large variety of RF systems

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