

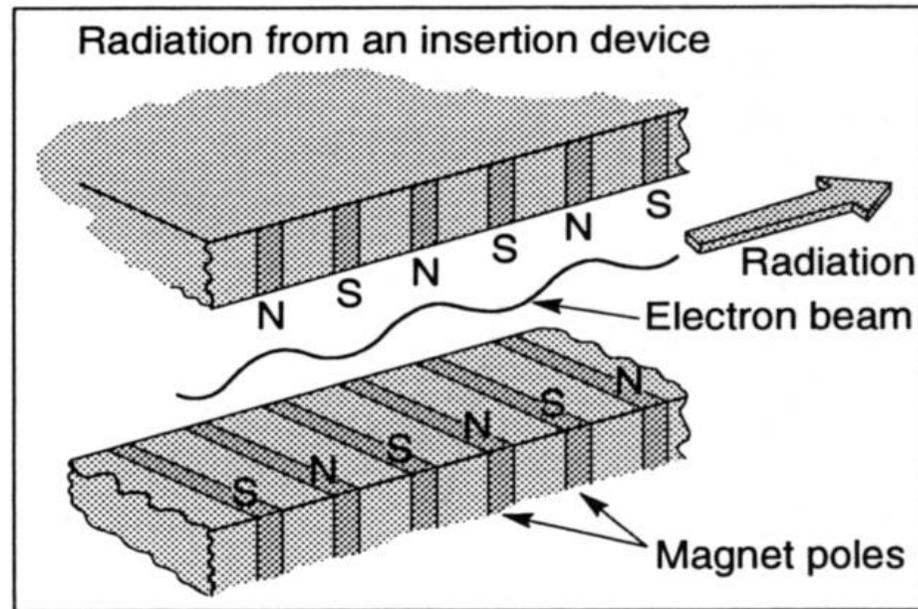
# Introduction to Insertion Devices

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# What is an Insertion Device ?



- Oscillating Magnetic field create a beam undulation
- Also called Undulators and Wigglers
- Can be 1 to 20 m long, with period 15 to 200 mm
- Operated with a small magnetic gap (5 to 15 mm)
- Use :
  - **Intense Source of Radiation in electron storage rings**
  - Control of damping times in Electron Colliders (LEP, CESR,...)
  - Reduce emittance in advanced light sources (Petra III, NSLS II)

# Table of Content

- Electron beam Dynamics
- Synchrotron radiation
- Technology

# Electron beam dynamics

# Electron Trajectory in an Insertion Device

Consider Orthogonal Frame  $Oxzs$

Electron velocity:  $\vec{v} = (v_x, v_z, v_s)$

Electron position:  $\vec{R} = (x, z, s)$

Magnetic field:  $\vec{B} = (B_x, B_z, B_s)$

Define:  $\gamma = \frac{1}{\sqrt{1 - \frac{v^2}{c^2}}}$

Lorentz Force

$$\gamma m \frac{d\vec{v}}{dt} = e\vec{v} \times \vec{B}$$

$$\Rightarrow \gamma m \frac{dv_x}{dt} = -e(v_s B_z - v_z B_s)$$

Assume:  $v_x, v_z \ll v_s \approx c$

$$\frac{v_x(s)}{c} = -\frac{e}{\gamma mc} \int_{-\infty}^s B_z(s') ds'$$
$$x(s) = -\frac{e}{\gamma mc} \int_{-\infty}^s \int_{-\infty}^{s'} B_z(s'') ds'' ds'$$

and similar expression for  $v_z(s)$  and  $z(s)$

# Electron Trajectory in a Planar Sinusoidal Undulator

$$\text{Consider } \vec{B} = (0, B_0 \sin(2\pi \frac{s}{\lambda_0}), 0)$$

$$\frac{v_x}{c} = \frac{K}{\gamma} \cos(2\pi \frac{s}{\lambda_0})$$

$$\frac{v_z}{c} = 0$$

$$\frac{v_s}{c} = 1 - \frac{1}{2\gamma^2} (1 + K^2 \cos^2(2\pi \frac{s}{\lambda_0}))$$

$$x \cong -\frac{\lambda_0}{2\pi} \frac{K}{\gamma} \sin(2\pi \frac{s}{\lambda_0})$$

with

$$K = \frac{eB_0\lambda_0}{2\pi mc} = 0.0934 B_0[T] \lambda_0[mm]$$

K is a fundamental parameter called : **Deflection Parameter**

*Example : ESRF, Energy=6GeV, Undulator  $\lambda_0 = 35$  mm,  $B_0 = 0.7$  T*

$$\Rightarrow K = 2.3, \quad \frac{K}{\gamma} = 200 \mu rad, \quad \frac{\lambda_0}{2\pi} \frac{K}{\gamma} = 1.1 \mu m !!$$

$$B_x = 0$$

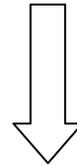
$$B_z = B_0 \cosh\left(2\pi \frac{z}{\lambda_0}\right) \cos\left(2\pi \frac{s}{\lambda_0}\right)$$

$$B_s = -B_0 \sinh\left(2\pi \frac{z}{\lambda_0}\right) \sin\left(2\pi \frac{s}{\lambda_0}\right)$$

Undulator Field Satisfying  
Maxwell Equation

$$\gamma m \frac{d\vec{v}}{dt} = e\vec{v} \times \vec{B}$$

Lorentz Force Equation



2<sup>nd</sup> Order in  $\gamma^{-1}$

$$\frac{d^2 x}{ds^2} = 0$$

$$\frac{d^2 z}{ds^2} = -\frac{1}{2} \left( \frac{eB_0}{\gamma mc} \right)^2 \frac{\lambda_0}{4\pi} \sinh\left(4\pi \frac{z}{\lambda_0}\right) \cong -\frac{1}{2} \left( \frac{eB_0}{\gamma mc} \right)^2 z$$

$$K_z = \frac{1}{2} \left( \frac{eB_0}{\gamma mc} \right)^2$$

A vertical Field Undulator is Vertically Focusing !

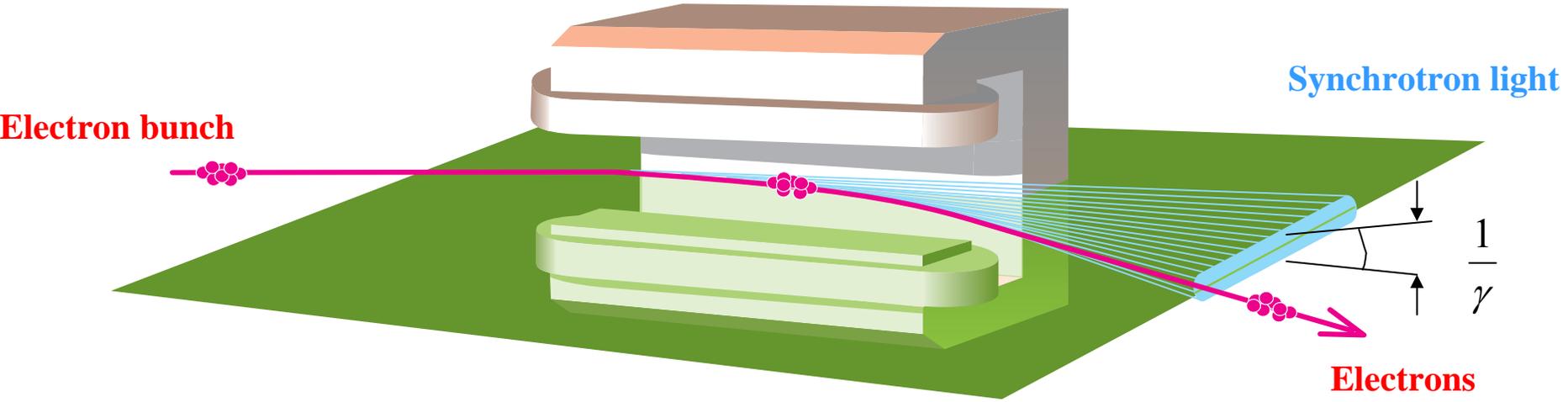
$$\frac{1}{F_z} = \int_{ID} K_z ds = \frac{1}{2} \left( \frac{eB_0}{\gamma mc} \right)^2 L$$

# Interference with the beam dynamics in the ring lattice

- An Insertion Device is the first component of a photon beamline. Its field setting is fully controlled by the users of the beamline . The change of field results in a change of beam dynamics in the whole ring.
- As far as the lattices are concerned, **Insertion devices** should ideally behave like **drift space** but the reality is different :
  - Closed Orbit distortion (by non zero field integrals=dipole error)
  - Betatron tune shift (by nominal field and by quadrupole errors)
  - Coupling (skew quadrupole errors)
  - Reduction of dynamic aperture (=>Lifetime reduction & reduced injection efficiency )
    - Through a break of the lattice periodicity
    - A change of the focusing versus injection point x,z
  - Very high field IDs may change the damping time, emittance , energy spread ...
- By combining careful manufacture, magnetic field shimming and local active corrections, many perturbations can be compensated.
- The problem of the reduction of dynamic aperture is most severe on low energy rings with many insertion devices.

# Synchrotron Radiation from an Insertion Device

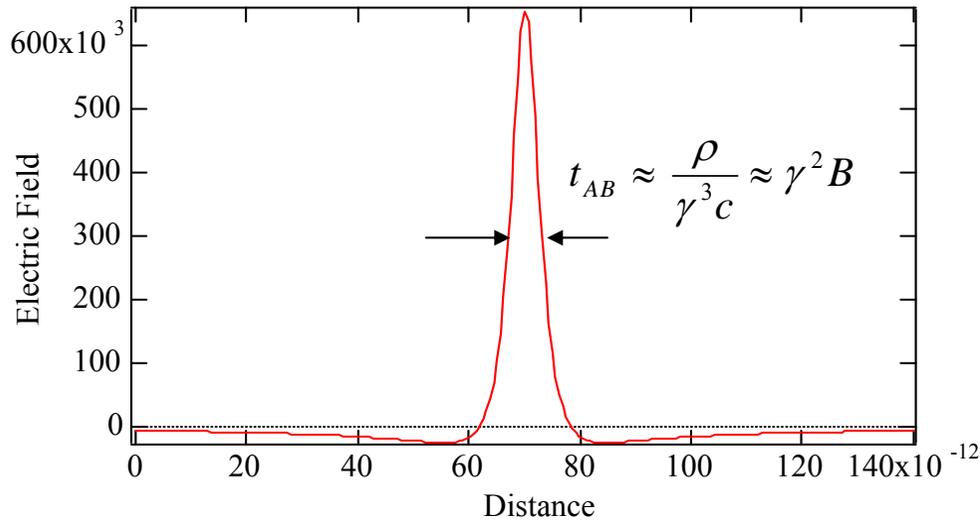
# Bending Magnet



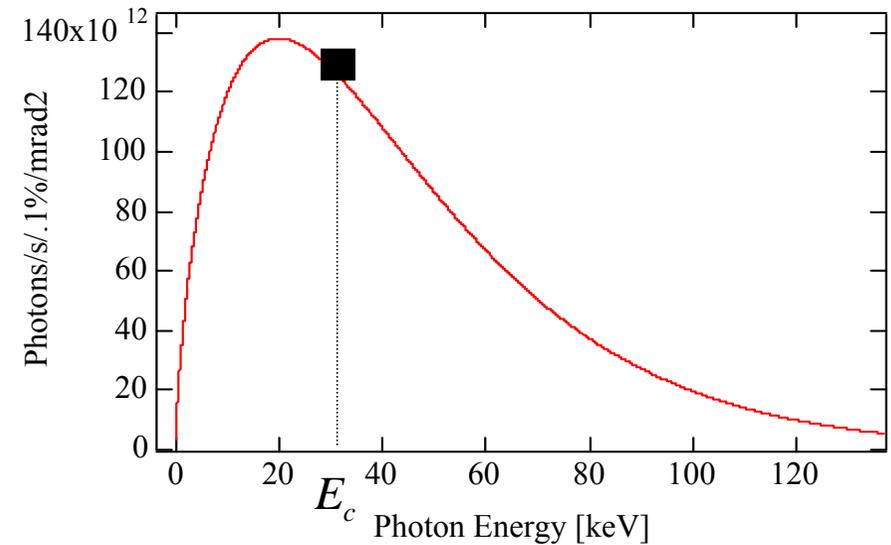
Synchrotron Radiation is emitted tangentially to the trajectory  
Inside a cone of angle  $1/\gamma$

# Radiation by a single electron

Electric field  
in the time domain



Angular spectral flux  
in frequency domain

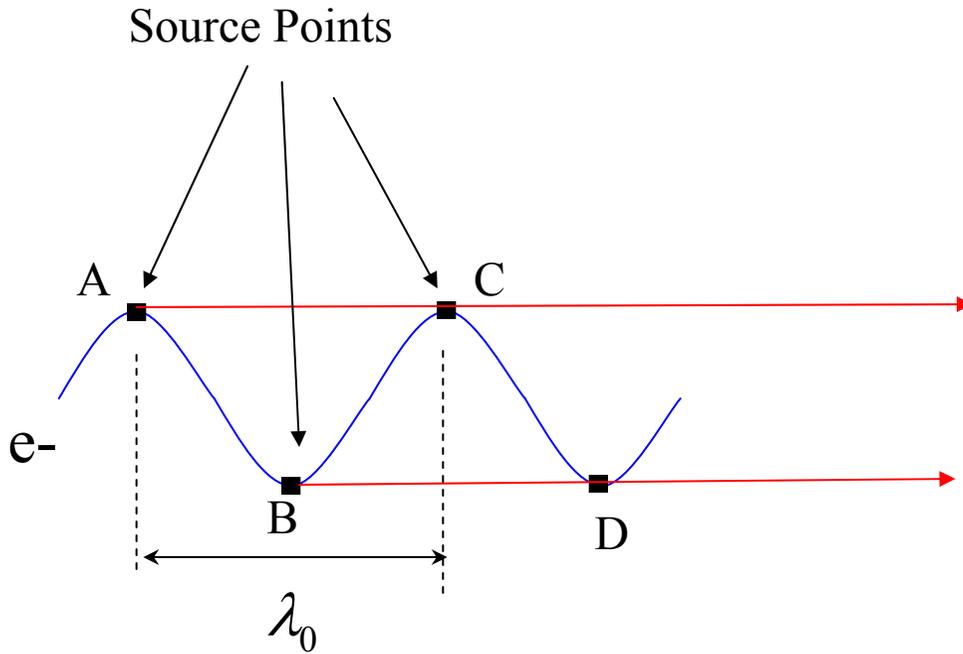


Computed for 6 GeV, I = 200 mA, B = 1 tesla

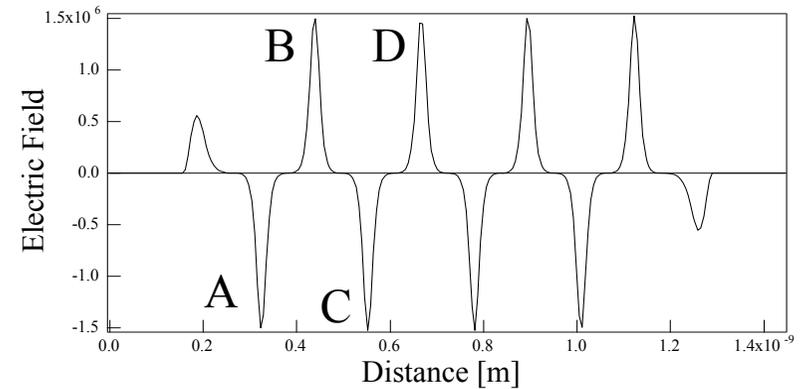
$$E_c = \frac{3hc}{4\pi} \frac{\gamma^3}{\rho} = \frac{3he}{4\pi m} \gamma^2 B$$

$$E_c [keV] = 0.665 E^2 [GeV] B [T]$$

# Undulator

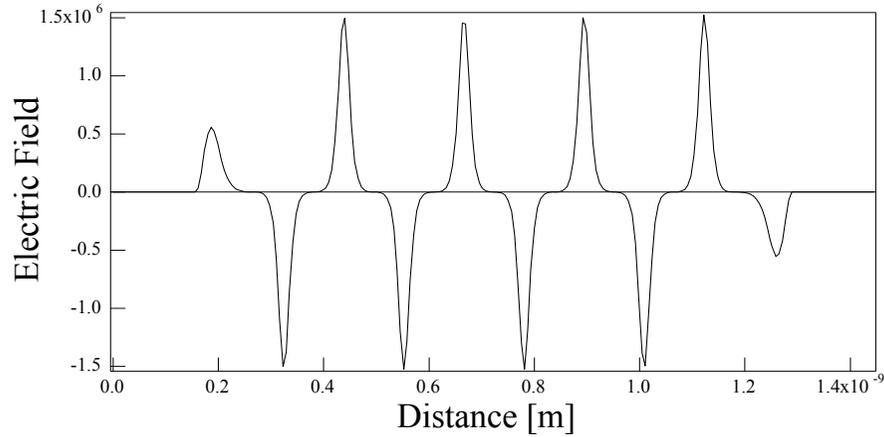


Electron trajectory

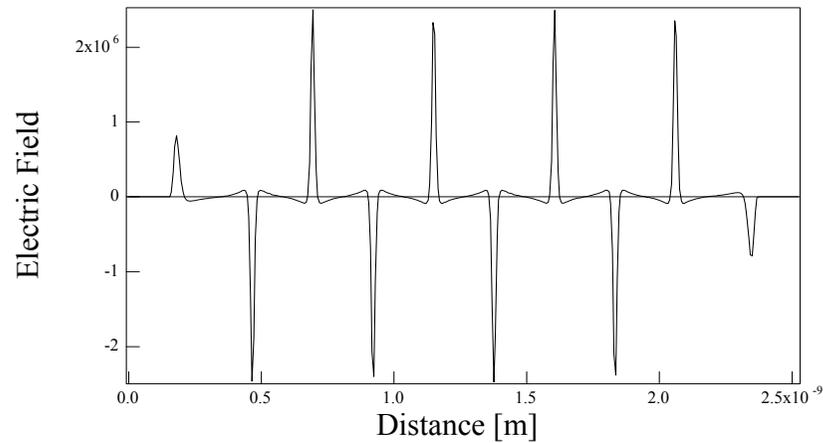
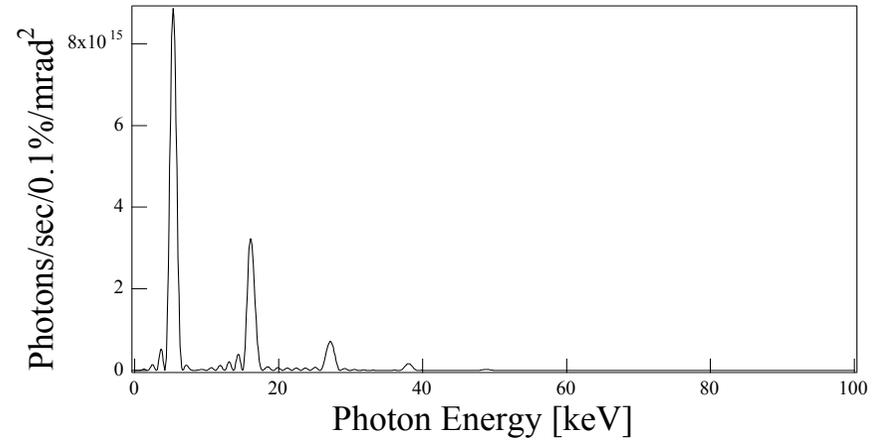


Electric field in time domain

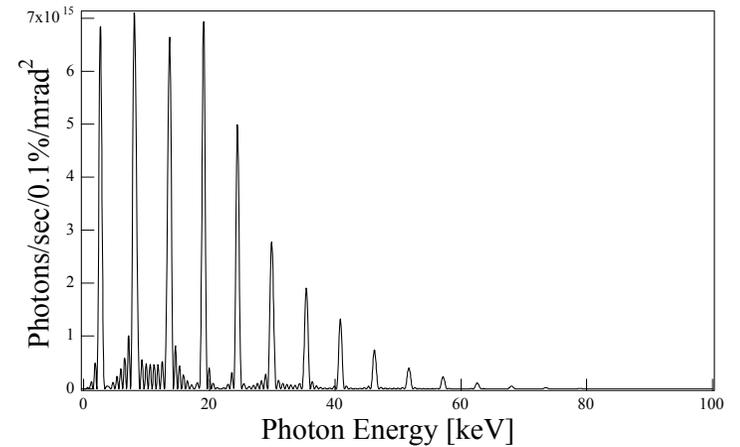
# Electric field and Spectrum vs K



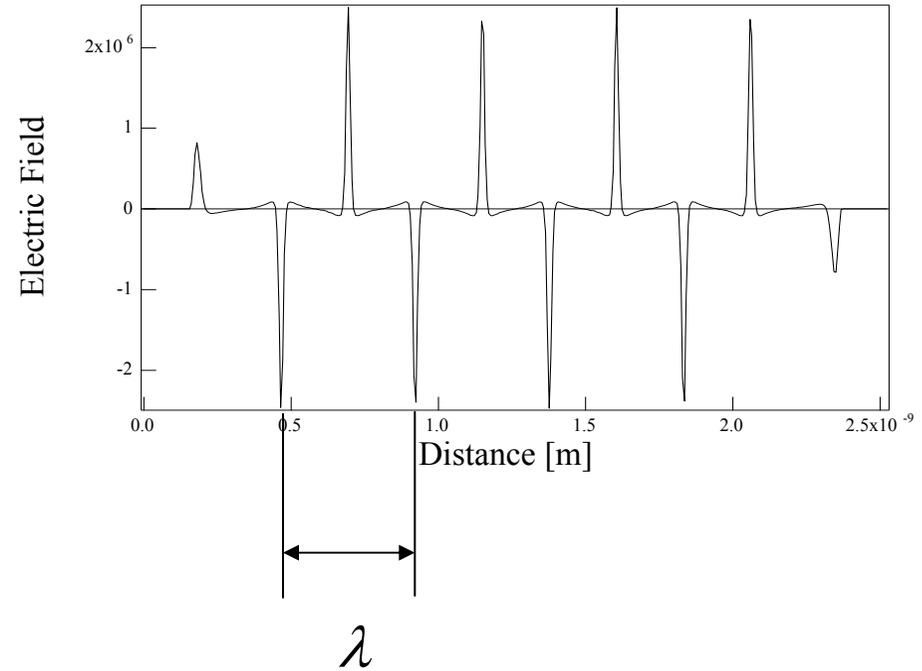
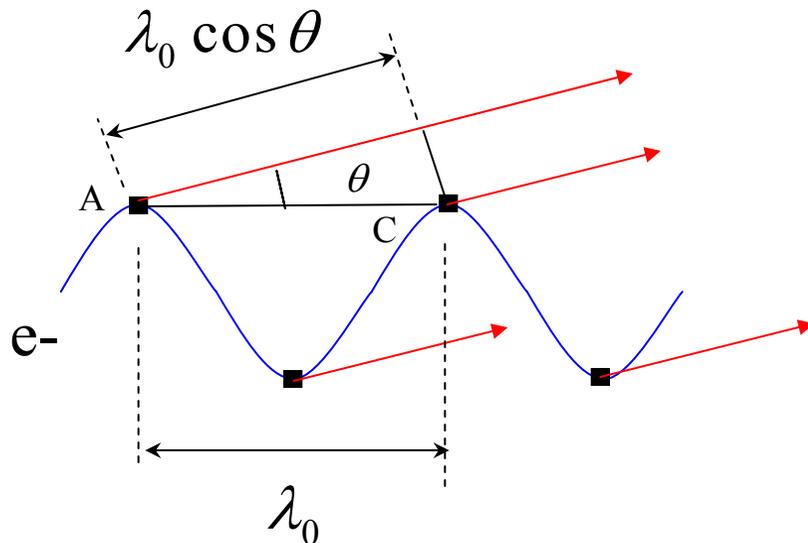
$K=1$



$K=2$



# Fundamental wavelength of the radiation field



$$t_{AC} = \frac{\lambda_0}{\langle v_s \rangle} = \frac{\lambda_0}{c(1 - \frac{1}{2\gamma^2}(1 + \frac{K^2}{2}))}$$

$$\lambda = \lambda_0 \cos \theta - ct_{AC} \cong \lambda_0 (1 - \frac{\theta^2}{2}) - \frac{\lambda_0}{(1 - \frac{1}{2\gamma^2}(1 + \frac{K^2}{2}))} \cong \frac{\lambda_0}{2\gamma^2} (1 + \frac{K^2}{2} + \gamma^2 \theta^2)$$

# Wavelength of the Harmonics

$$\lambda_n = \frac{\lambda_0}{2n\gamma^2} \left(1 + \frac{K^2}{2} + \gamma^2 \theta^2\right)$$

Equivalently, the energy  $E_n$  of the harmonics are given by

$$E_n [keV] = \frac{9.5 n E^2 [GeV]}{\lambda_0 [mm] \left(1 + \frac{K^2}{2} + \gamma^2 \theta^2\right)}$$

$\lambda_n, E_n$  : Wavelength, Energy of the  $n^{\text{th}}$  harmonic

$n = 1, 2, 3, \dots$  : Harmonic number

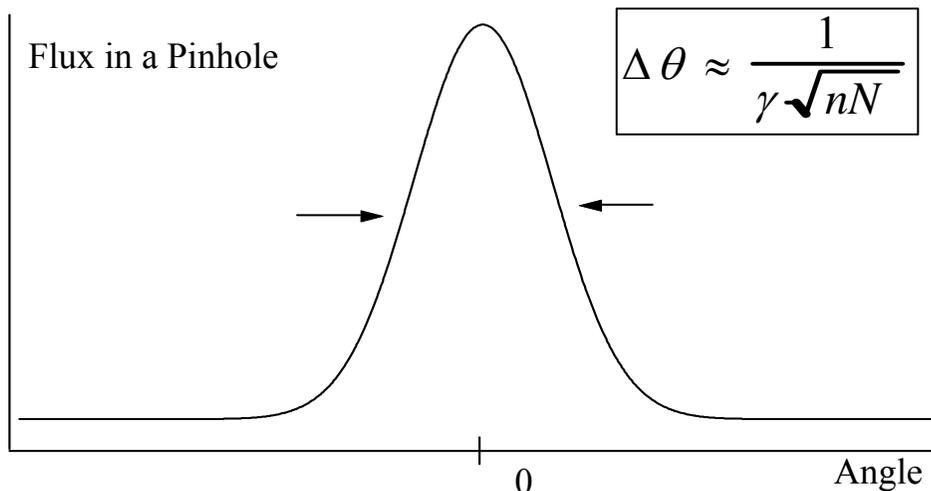
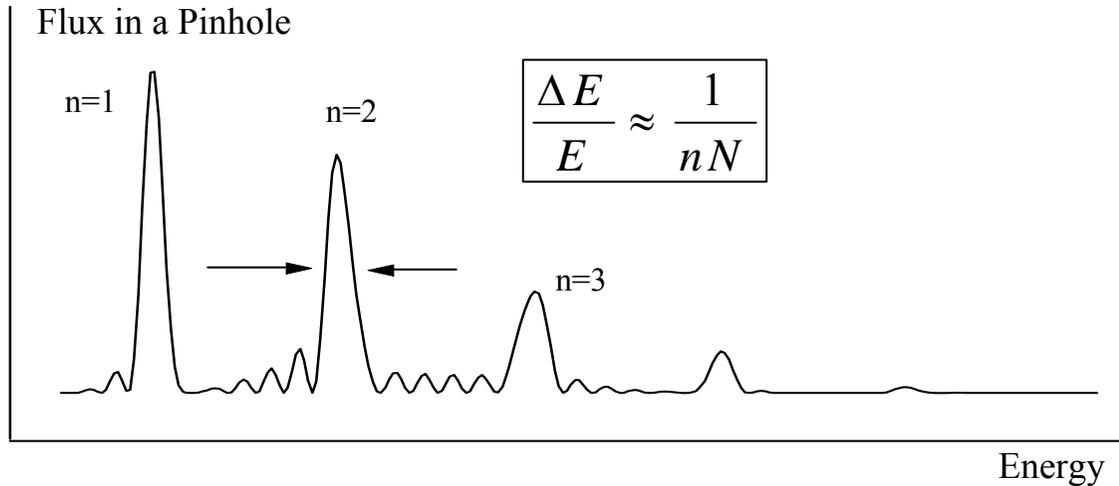
$\lambda_0$  : Undulator period

$E = \gamma mc^2$  : Electron Energy

$K$  : Deflection Parameter =  $0.0934 B_0 [T] \lambda_0 [mm]$

$\theta$  : Angle between observer direction and  $e -$  beam

# Undulator Emission by a Filament Electron Beam



$n$  : Harmonic number

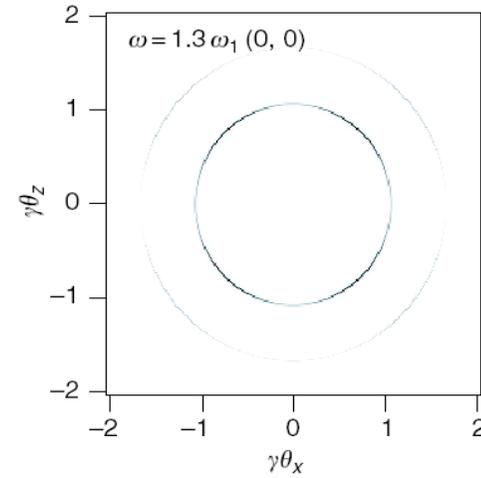
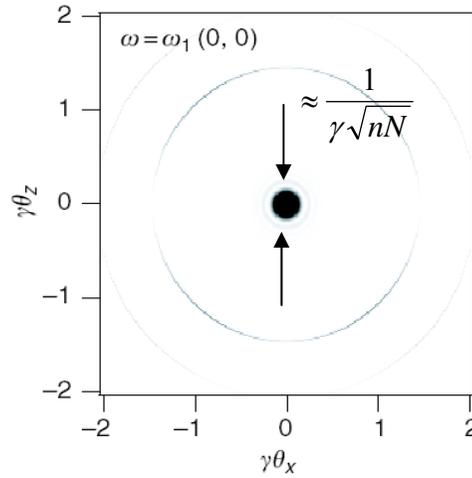
$N$  : Number of Periods

$$\gamma = \frac{1}{\sqrt{1 - \frac{v^2}{c^2}}} = \frac{E}{mc^2}$$

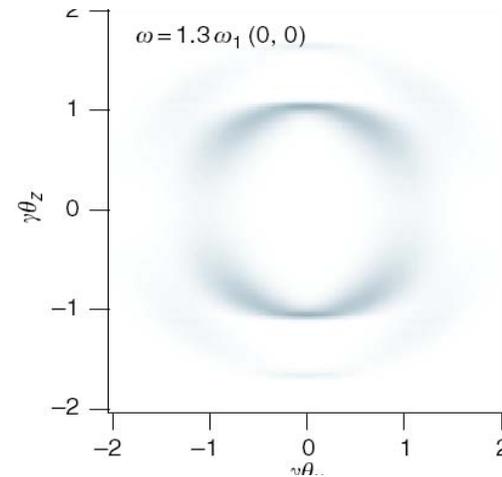
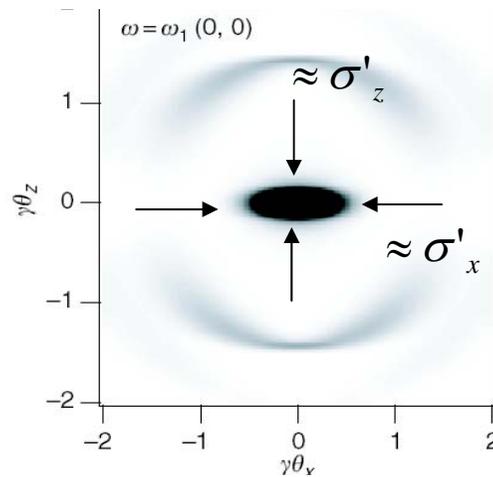
What happens if the beam presents a finite emittance (size and divergence) and finite energy spread ?

$$\lambda = \frac{\lambda_0}{2n\gamma^2} \left( 1 + \frac{K^2}{2} + \gamma^2 \theta^2 \right)$$

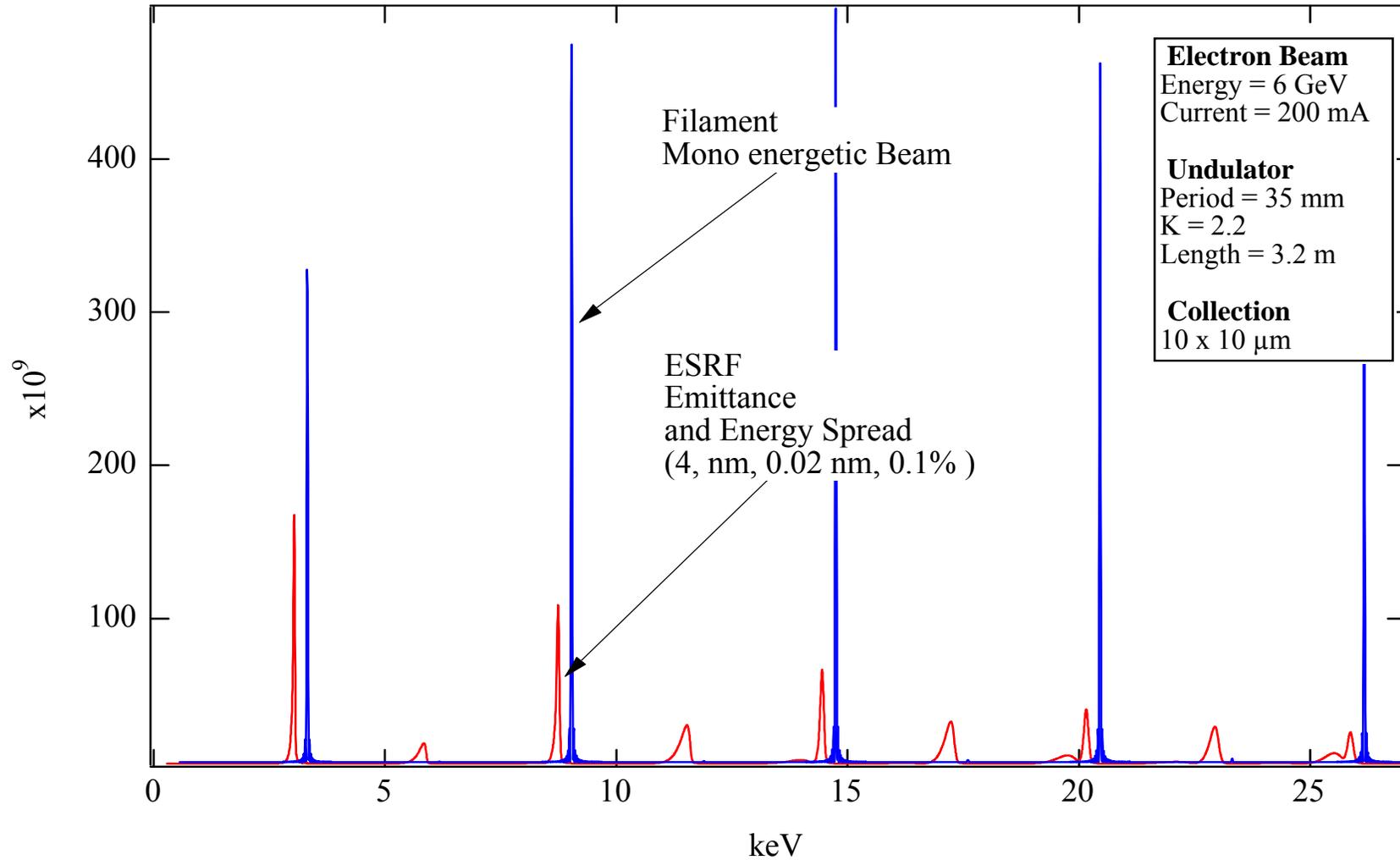
Radiation from a filament  
e- Beam at a wavelength  $\lambda$



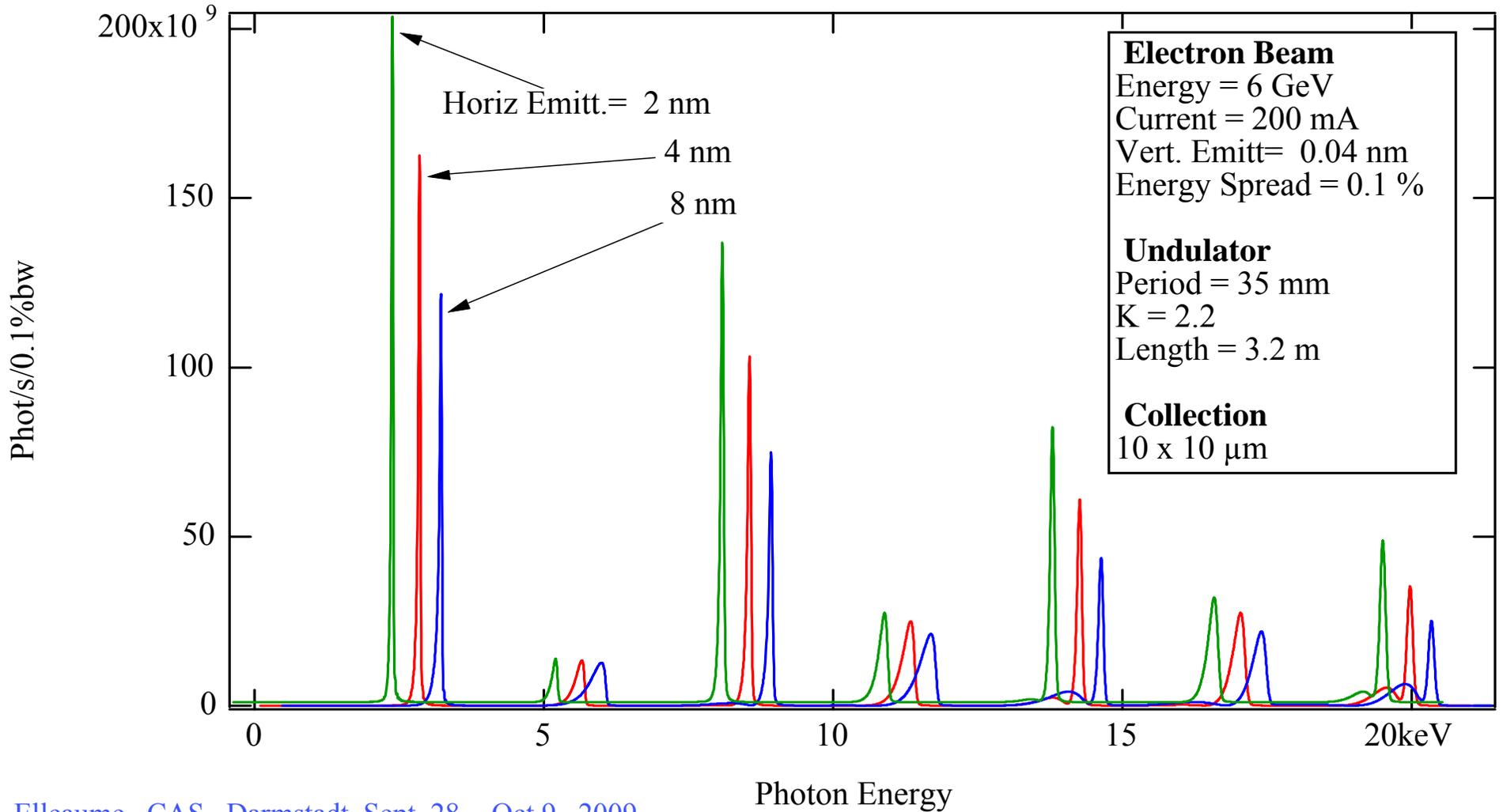
e- Beam with Finite Divergence



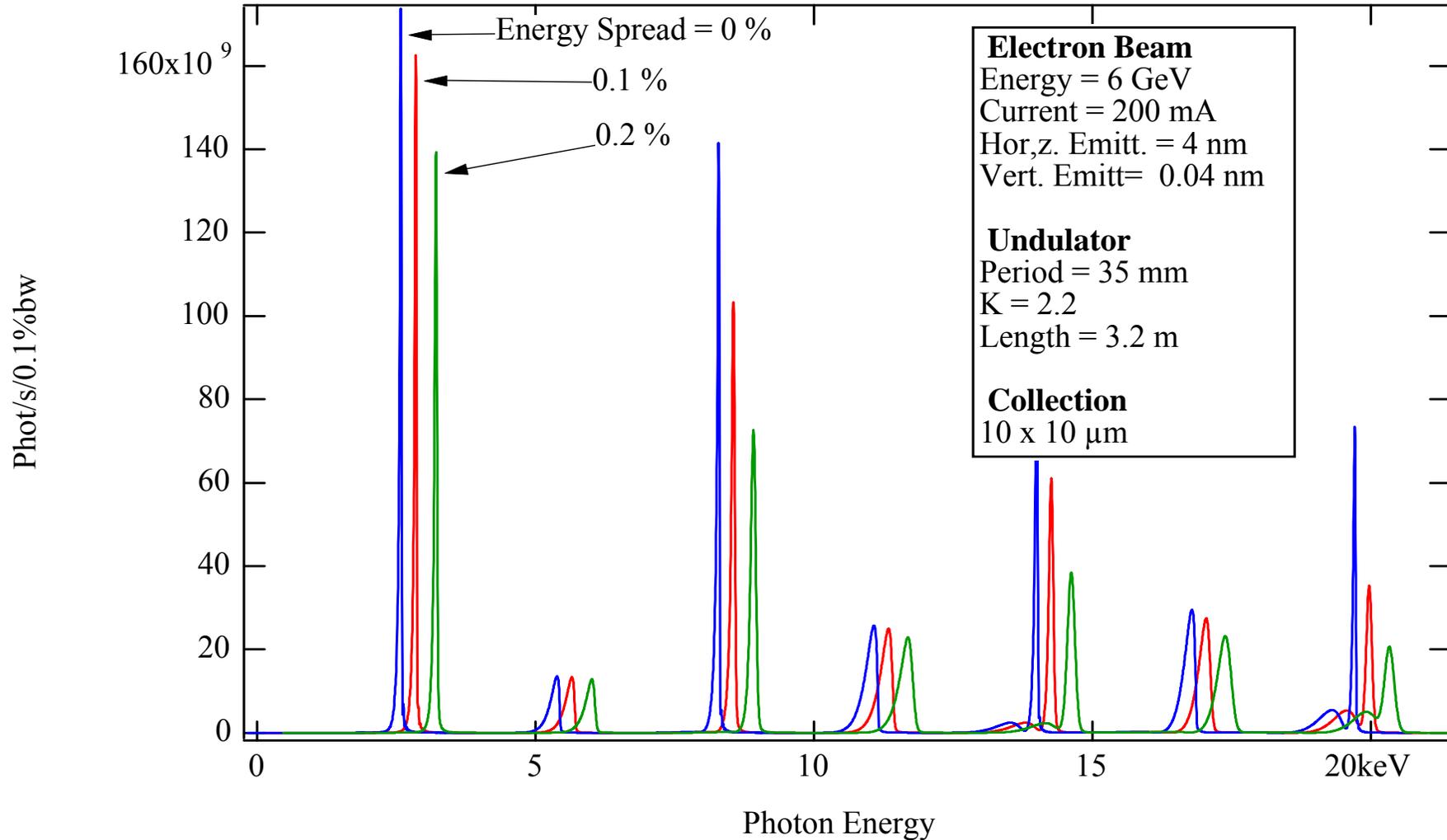
# Radiation Spectrum through a narrow aperture



# Broadening of the Harmonics by the Electron Emittance

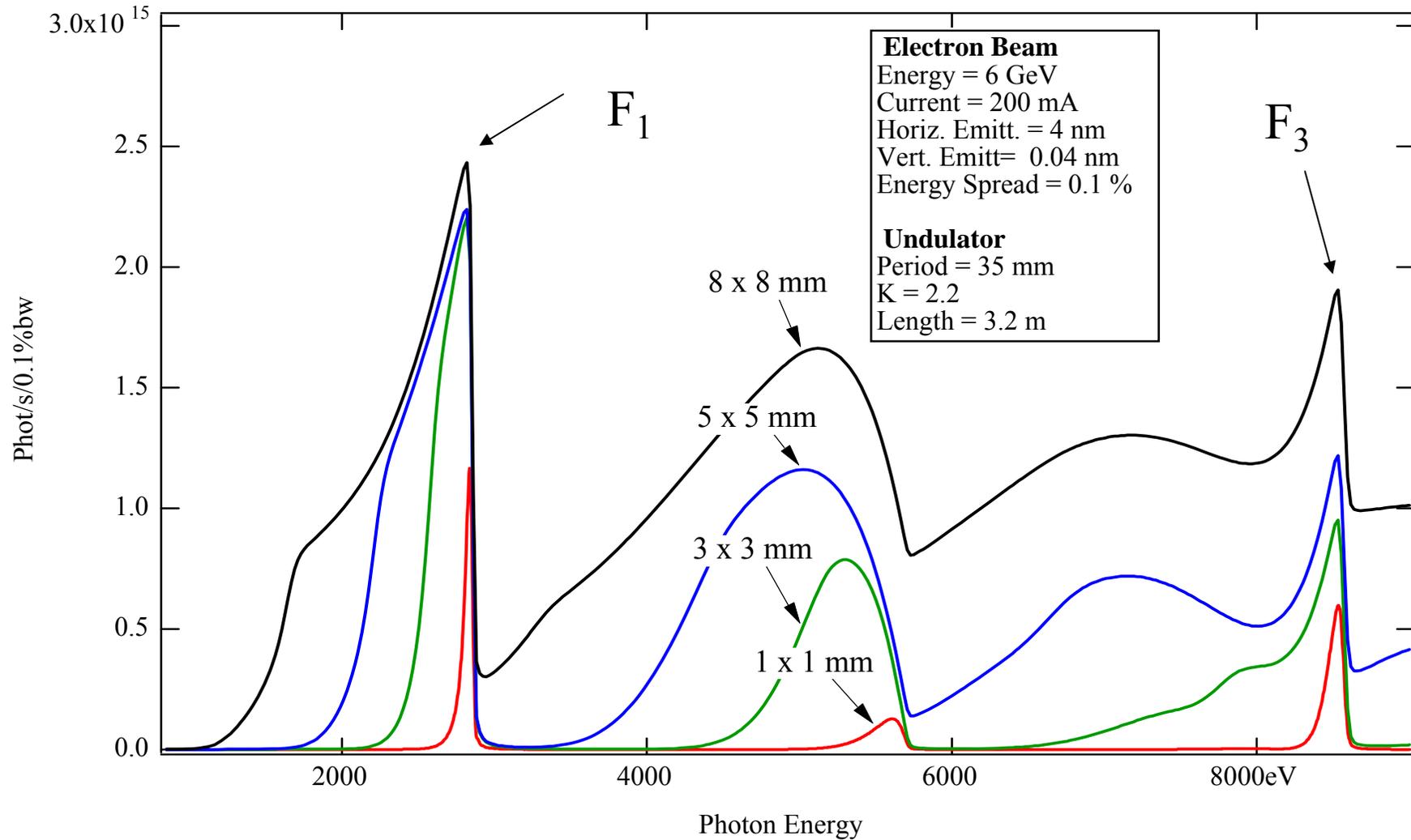


# Broadening of the Harmonics by Electron Energy Spread



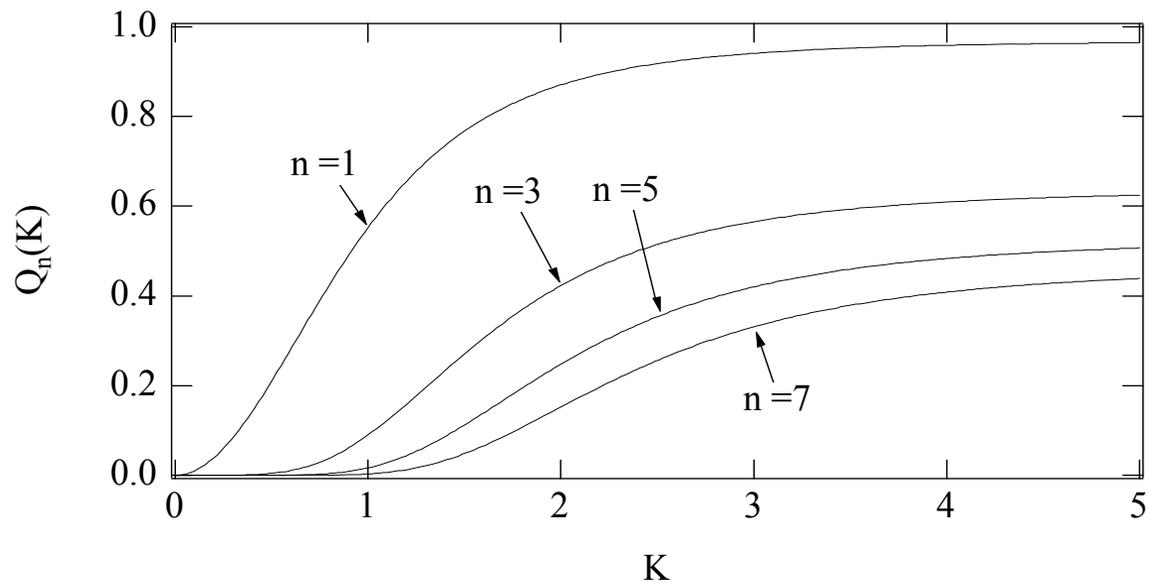
To make optimum use of the  
**Undulators, the magnet lattice of**  
synchrotron light sources should be  
designed to produce the **smallest**  
**emittance** and **smallest energy**  
**spread.**

# Collecting Undulator Radiation in a variable Aperture



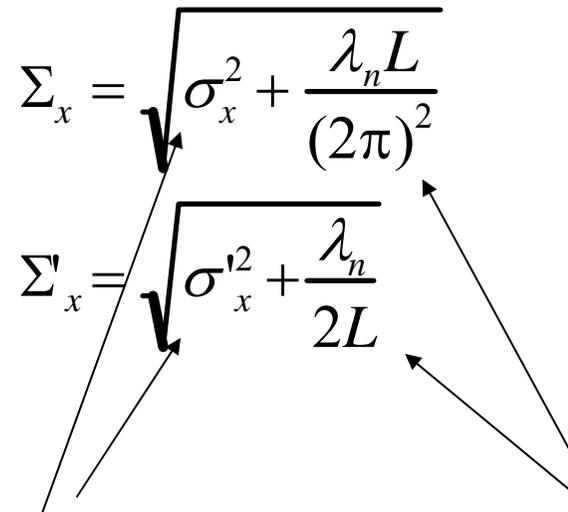
## Maximum Spectral Flux On-axis on odd harmonics

$$F_n \text{ [Ph / sec / 0.1\%]} = 1.431 \cdot 10^{14} N I[A] Q_n(K)$$



# Brilliance ( or Brightness)

$$B_n = \frac{F_n}{(2\pi)^2 \Sigma_x \Sigma'_x \Sigma_z \Sigma'_z}$$

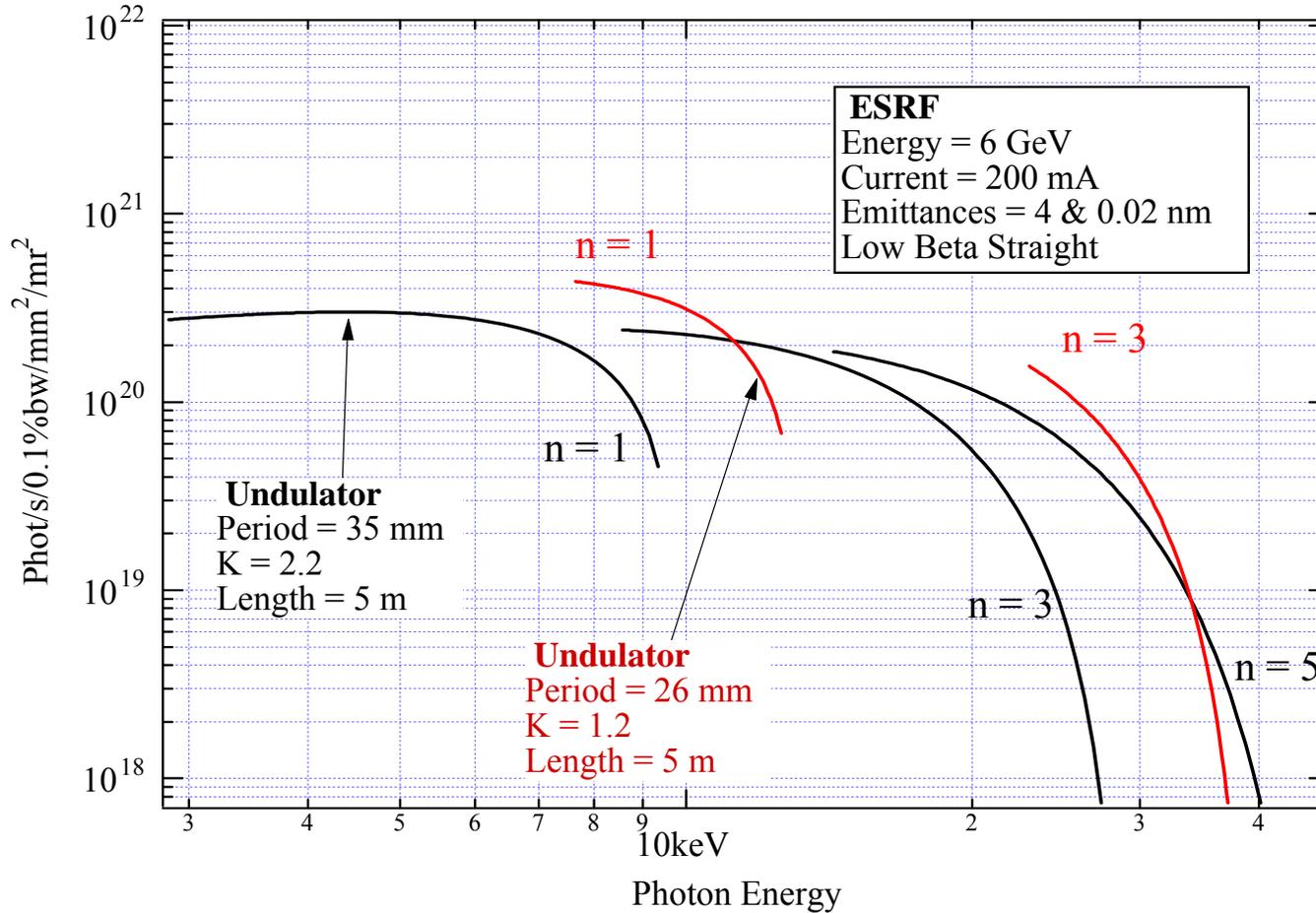
$$\Sigma_x = \sqrt{\sigma_x^2 + \frac{\lambda_n L}{(2\pi)^2}}$$
$$\Sigma'_x = \sqrt{\sigma'^2_x + \frac{\lambda_n}{2L}}$$


Electron beam

Single electron emission

$$\lambda = \frac{\lambda_0}{2n\gamma^2} \left(1 + \frac{K^2}{2}\right)$$

# Brilliance vs Photon Energy



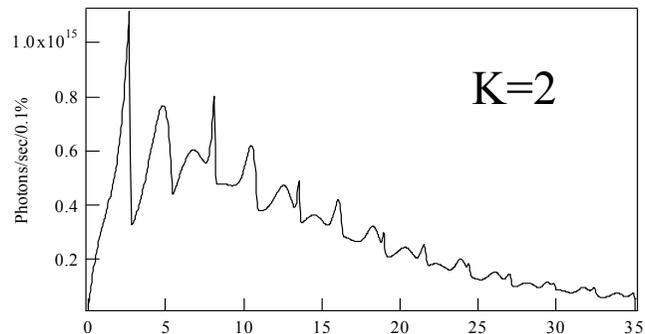
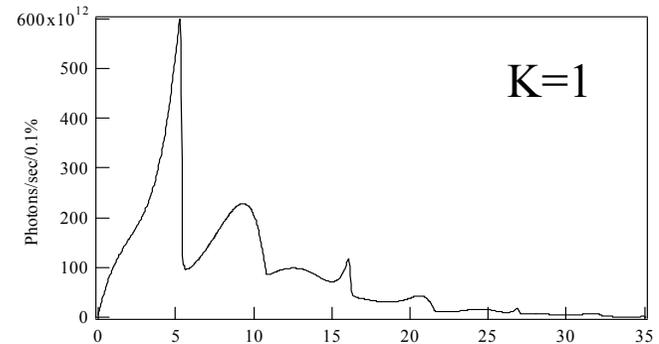
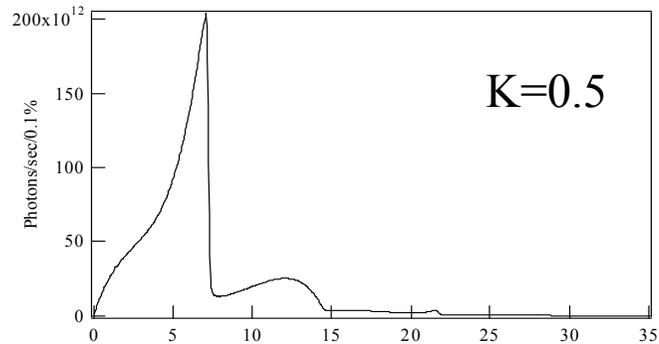
$$B_n = \frac{F_n}{(2\pi)^2 \Sigma_x \Sigma'_x \Sigma_z \Sigma'_z}$$

with

$$\Sigma_x = \sqrt{\sigma_x^2 + \frac{\lambda_n L}{(2\pi)^2}}$$

$$\Sigma'_x = \sqrt{\sigma_x'^2 + \frac{\lambda_n}{2L}}$$

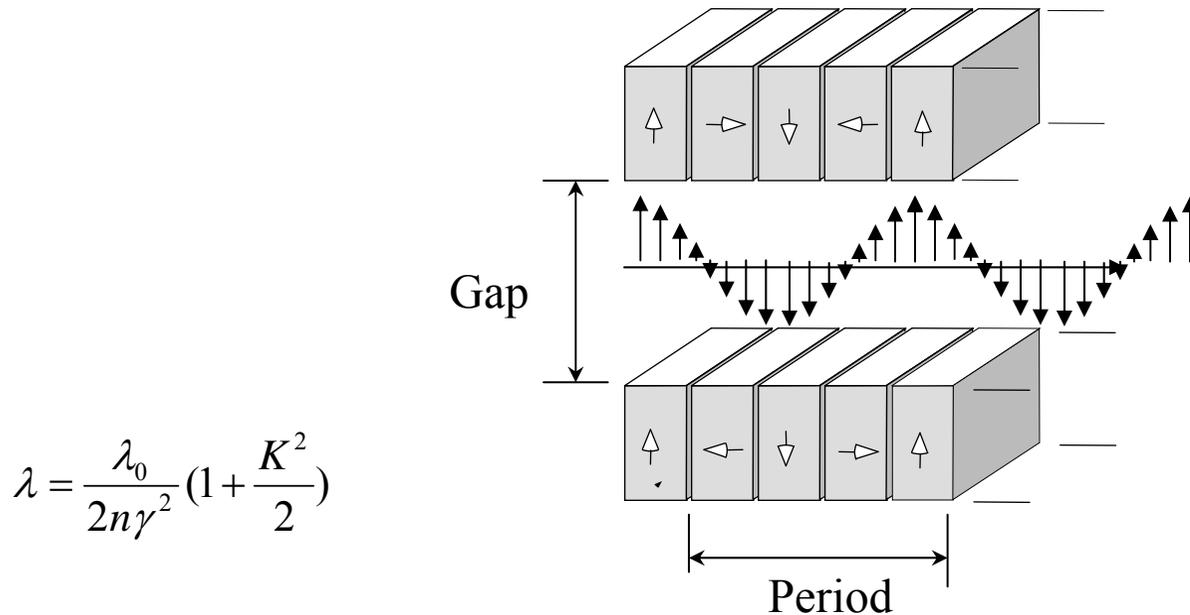
# Angle Integrated Flux



For Large  $K$ , the angle integrated spectrum from an Undulator tends toward that of a bending magnet  $\times 2N$   
 $\Rightarrow$  Such Devices are called **Wigglers**

# Technology

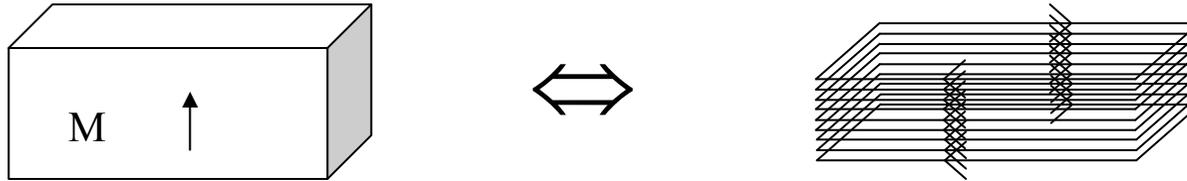
# Technology of Undulators and Wigglers



$$\lambda = \frac{\lambda_0}{2n\gamma^2} \left(1 + \frac{K^2}{2}\right)$$

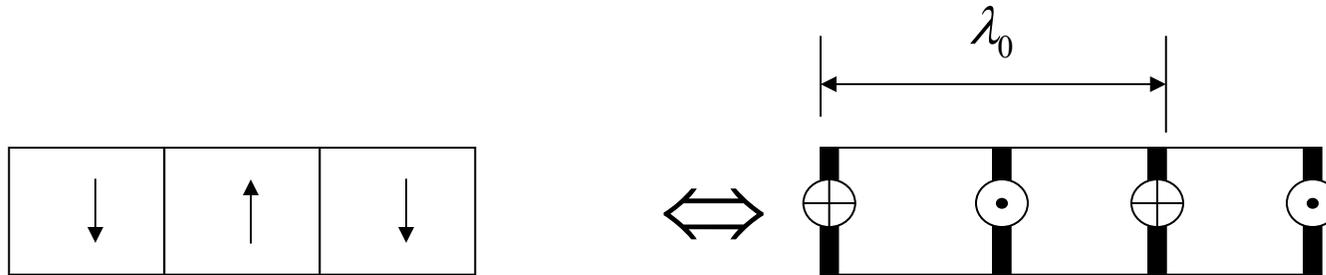
- The fundamental issue in the magnetic design of a planar undulator or wiggler is to produce a periodic field with a **high peak field** B and the **shortest period**  $\lambda_0$  within a **given aperture** (gap).
- Three type of technologies can be used :
  - Permanent magnets ( NdFeB , Sm<sub>2</sub>Co<sub>17</sub> )
  - Room temperature electromagnets
  - Superconducting electromagnets

# Magnetization is equivalent to a surface current



$$\text{Air coil with Surface Current Density [A/m]} \cong \frac{B_r [T]}{\mu_0}$$

# Periodic Array of Magnets



$$\text{Surface Current Density [A/m]} \cong \frac{2B_r [T]}{\mu_0}$$

$$\text{or Current Density [A/m}^2\text{]} \cong \frac{4B_r [T]}{\mu_0 \lambda_0}$$

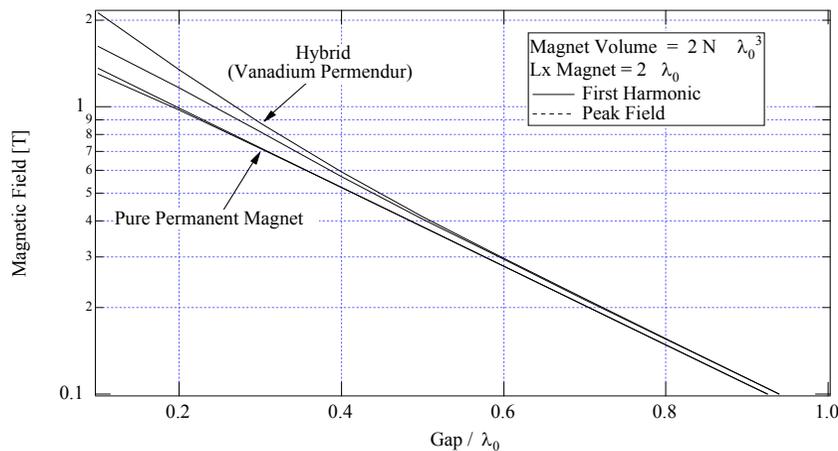
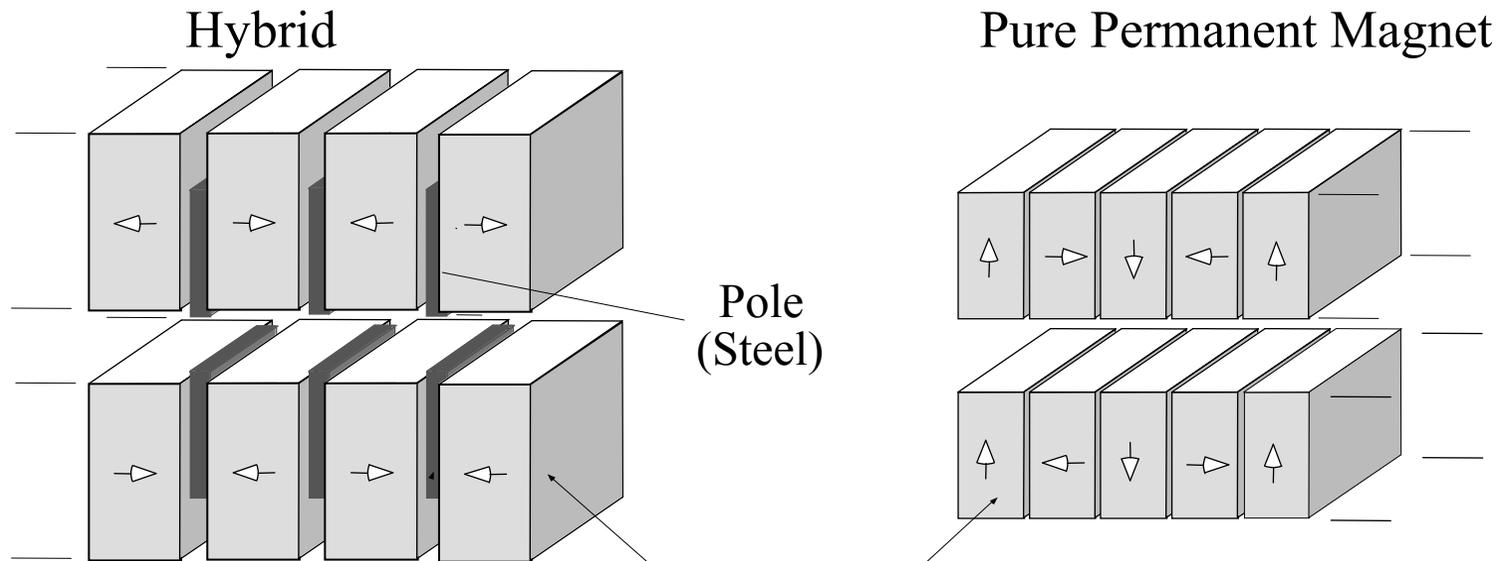
Examples:

$$B_r = 1 \text{ T} , \lambda_0 = 20 \text{ mm} \Rightarrow \text{Equiv. Current Density} = 160 \text{ A/mm}^2 !!$$

$$B_r = 1 \text{ T} , \lambda_0 = 400 \text{ mm} \Rightarrow \text{Equiv. Current Density} = 8 \text{ A/mm}^2$$

> 95 % of Insertion Devices are made of Permanent Magnets !!

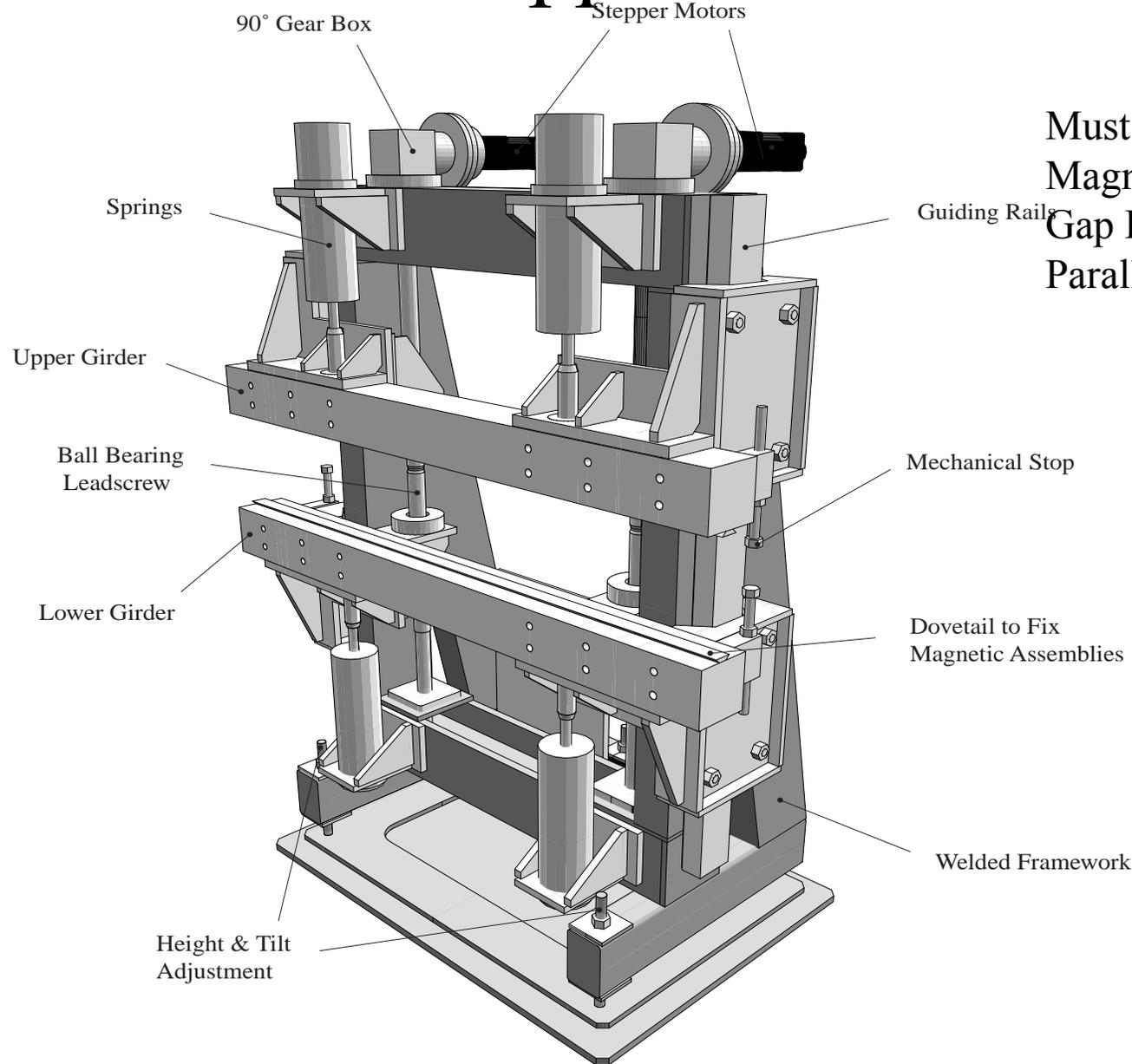
# Permanent Magnet Undulator



Magnet (NdFeB,  $\text{Sm}_2\text{Co}_{17}$ ,...)

| magnet materials            |           |                     |                 |  |
|-----------------------------|-----------|---------------------|-----------------|--|
| Material                    | $B_r$ [T] | $\mu_{r,\parallel}$ | $\mu_{r,\perp}$ | $H_{c1}$ [kA/m] $10^{-2}/^\circ\text{C}$ |
| $\text{SmCO}_5$             | 0.9–1.01  | 1.05                |                 | 1500–2400 –0.04                          |
| $\text{Sm}_2\text{CO}_{17}$ | 1.04–1.12 | 1.05–1.08           |                 | 800–2000 –0.03                           |
| NdFeB                       | 1.0–1.4   | 1.04–1.06           | 1.15–1.17       | 1000–3000 –0.10                          |

# Support Structure



Must Handle :  
Magnetic Force : 1-20 Tons  
Gap Resolution :  $< 1 \mu\text{m}$   
Parallellism  $< 20 \mu\text{m}$

# Undulators are Fundamentally **Small Gap** Devices

- For a permanent magnet undulator , shrinking all dimensions maintains the field unchanged.

- The peak field  $B_0 \propto B_r \exp(-\pi \frac{gap}{\lambda_0})$

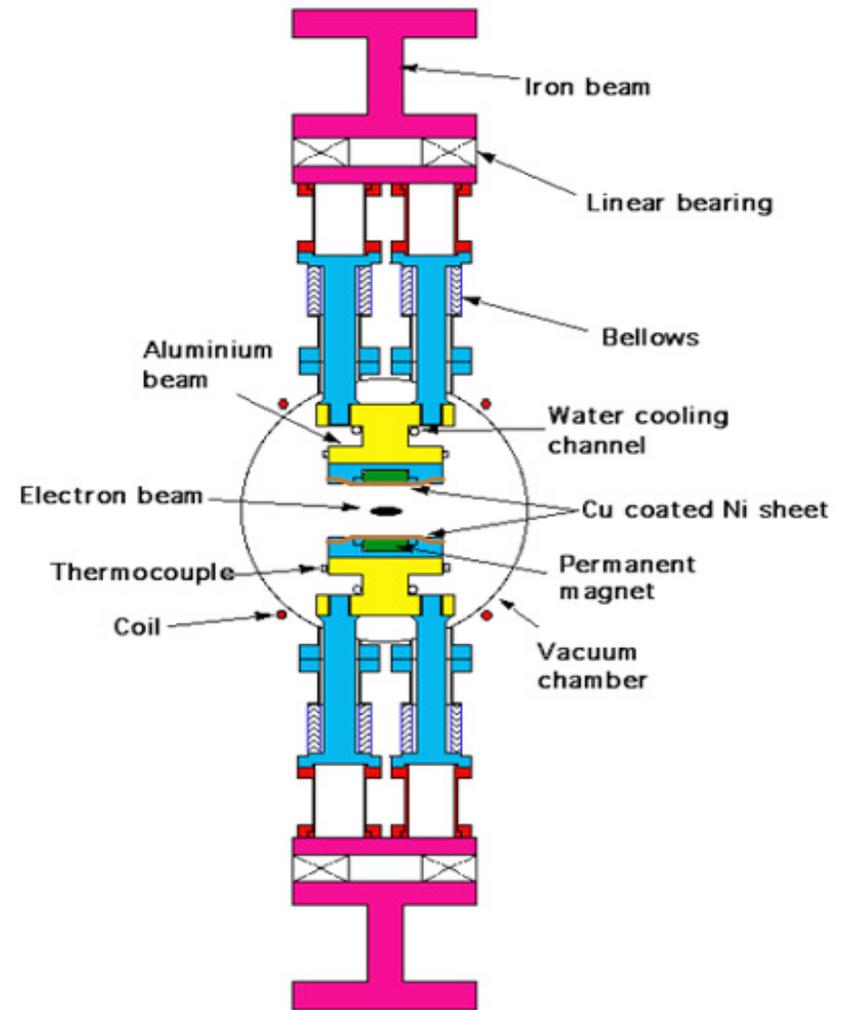
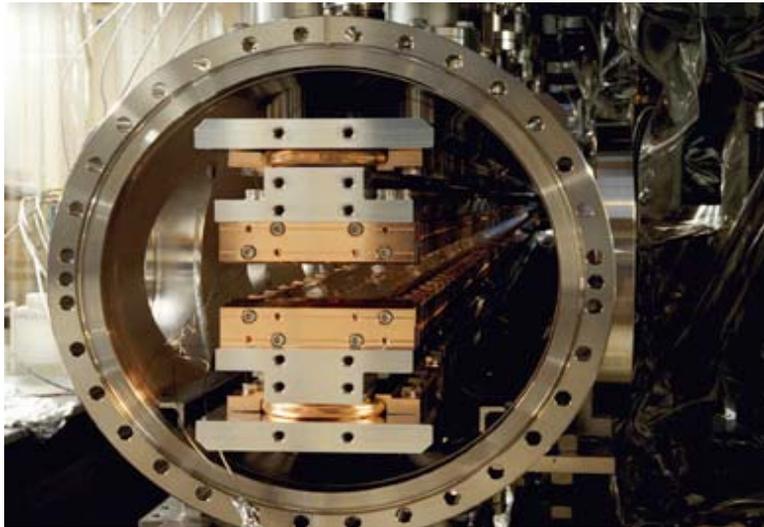
- Benefits of using small gaps Insertion Devices :

- Decrease the volume of material (cost driving)  $\sim gap^3$
- The lower the gap, the higher the energy of the harmonics of the undulator emission => the lower the electron energy required to reach the same photon energy

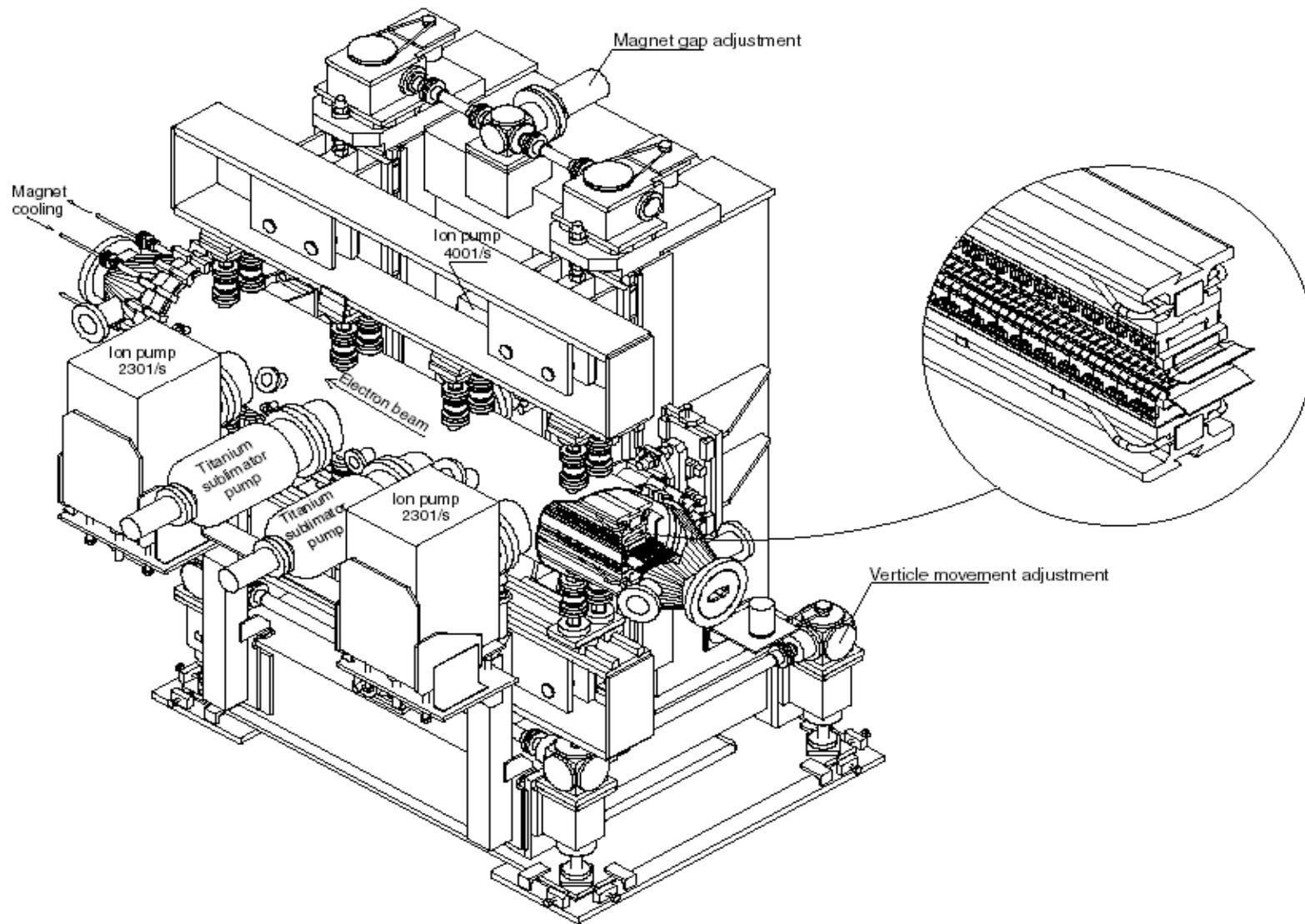
$$\lambda = \frac{\lambda_0}{2\gamma^2} \left(1 + \frac{K^2}{2}\right) \quad \text{with } K = \frac{eB_0\lambda_0}{2\pi mc}$$

- The most advanced undulators have magnet blocks in the vacuum with an operating magnetic gap of **4-6 mm !!**

# In Vacuum Permanent Magnet Undulators



SPring-8 In-Vacuum Undulator

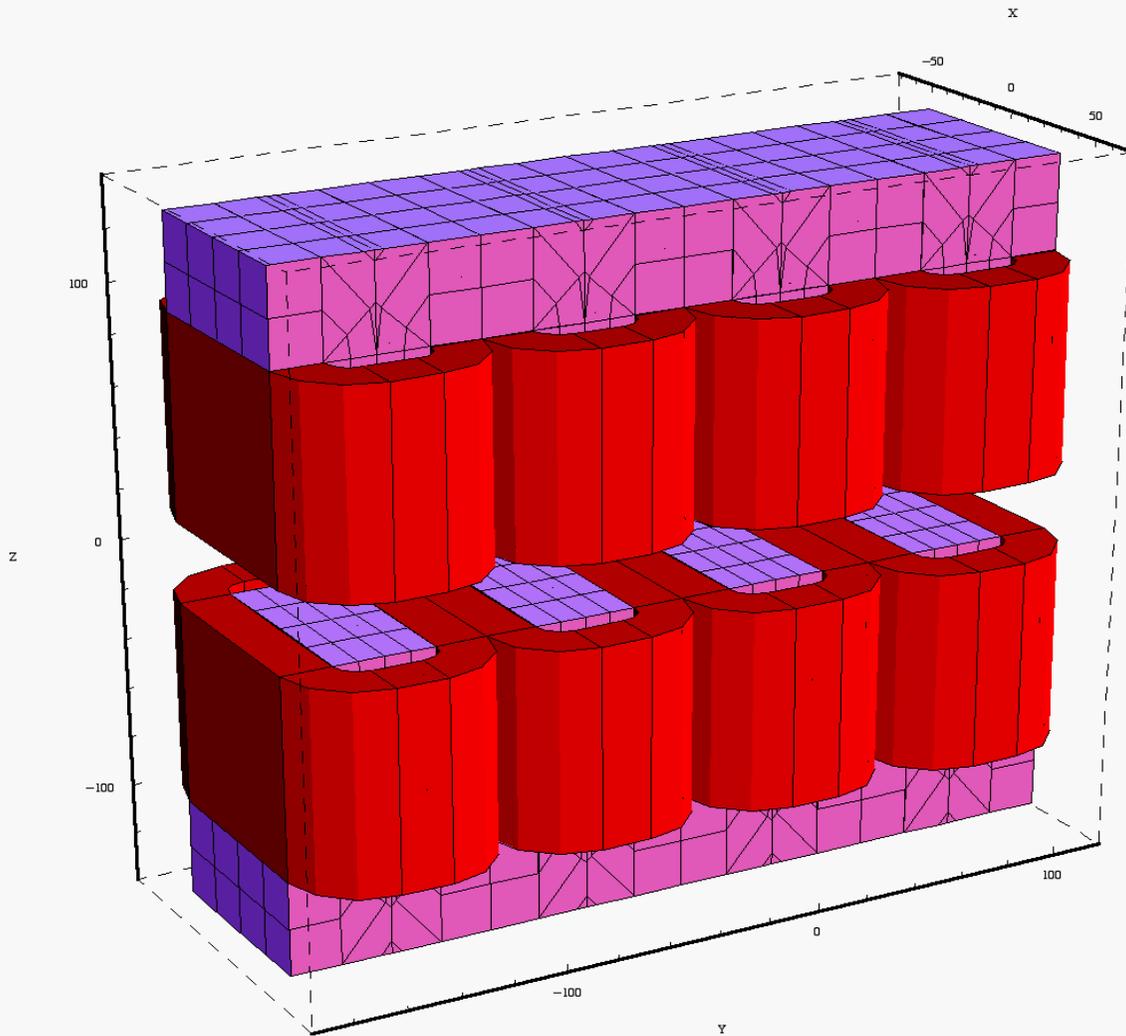


# Application : Build a pure permanent magnet undulator with NdFeB Magnets ( $B_r = 1.2$ T)

Undulator with  $K=1$  with 6 GeV energy

| Gap [mm] | B [T] | Period [mm] | Fundamental [keV]<br>@ 6 GeV | Electron Energy [GeV]<br>Fund = 15.2 keV |
|----------|-------|-------------|------------------------------|--|
| 5        | 0.72  | 15          | 15.2                         | 6.0                                      |
| 10       | 0.49  | 22          | 10.3                         | 7.3                                      |
| 15       | 0.38  | 28          | 8.2                          | 8.2                                      |

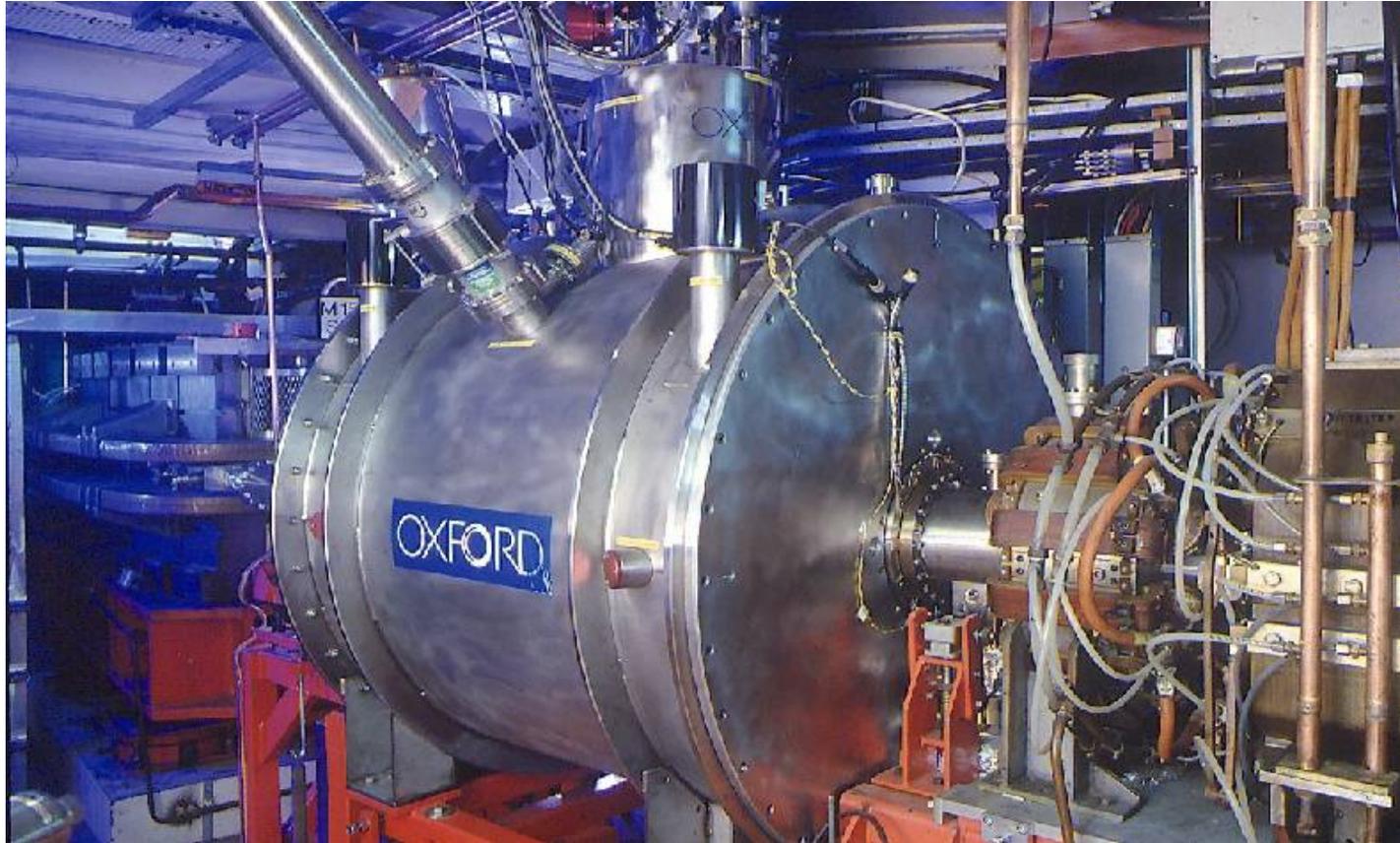
# Electro-Magnet Undulator



Current Densities  $< 20 \text{ A/mm}^2$

Lower field  
than permanent magnet  
For small period / gap

# Superconducting W wigglers



- High field : up to 10 T => Shift the spectrum to higher energies
- Complicated engineering & High costs

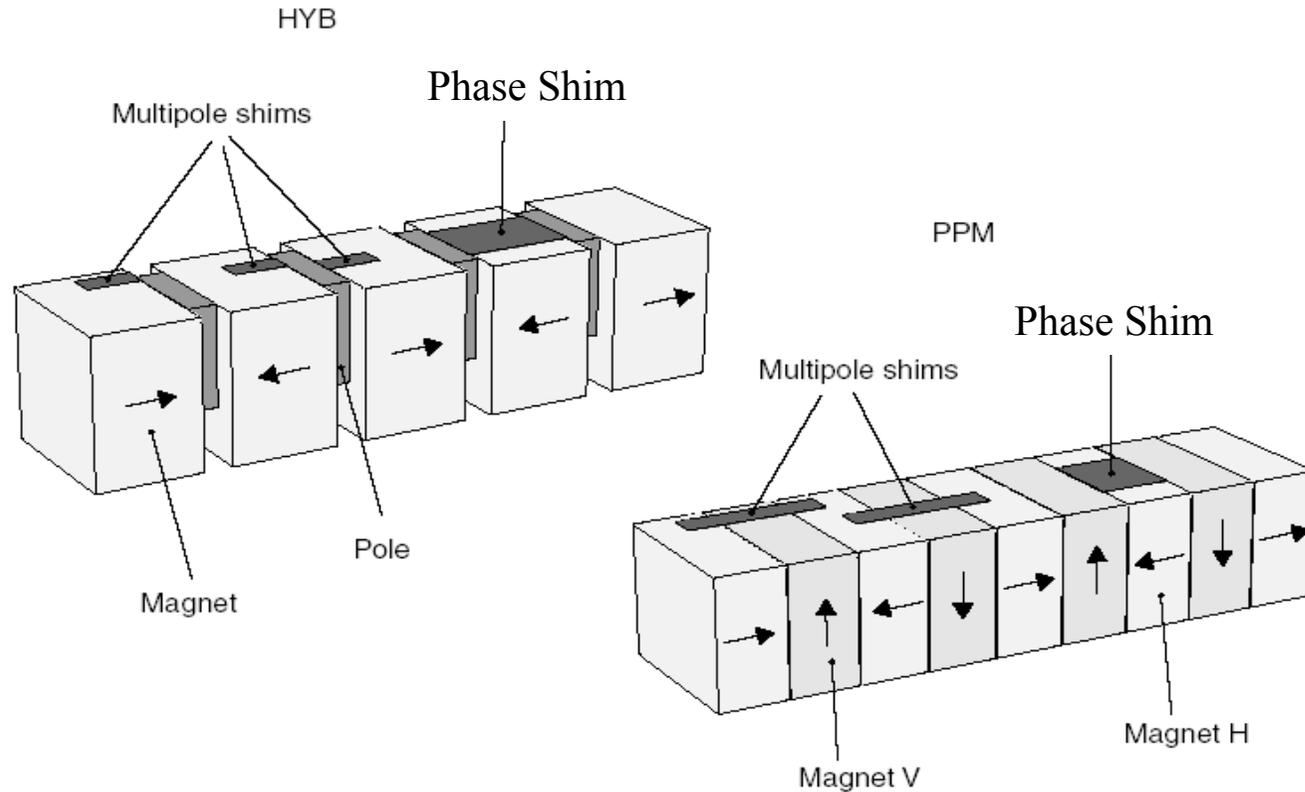
# Magnetic Field Errors in Permanent Magnet Insertion Devices :

- Field errors originate from :
  - Non uniform magnetization of the magnet blocks (poles).
  - Dimensional and Positional errors of the poles and magnet blocks.
  - Interaction with environmental magnetic field (iron frame, earth field,...)
- Important to use highly uniform magnetized blocks
  - perform a systematic characterization of the magnetization
  - Perform a pairing of the blocks to cancel errors
  - Still insufficient ...
- Two main type of field errors remain
  - Multipole Field Errors (Normal and skew dipole, quadrupole, sextupole,...).
  - Phase errors which reduce the emission on the high harmonic numbers
  - Further corrections :
    - Correction magnets
    - Shimming

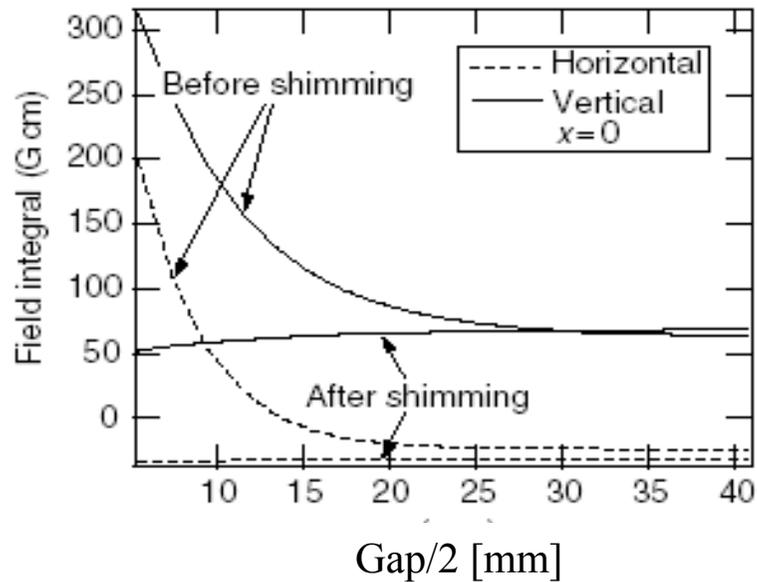
# Shimming

- **Mechanical Shimming** :
  - Moving permanent magnet or iron pole vertically or horizontally
  - Best when free space and mechanical fixation make it possible.
  
- **Magnetic Shimming** :
  - Add thin iron piece at the surface of the blocks
  - Reduce minimum gap and reduce the peak field

# Magnetic shims

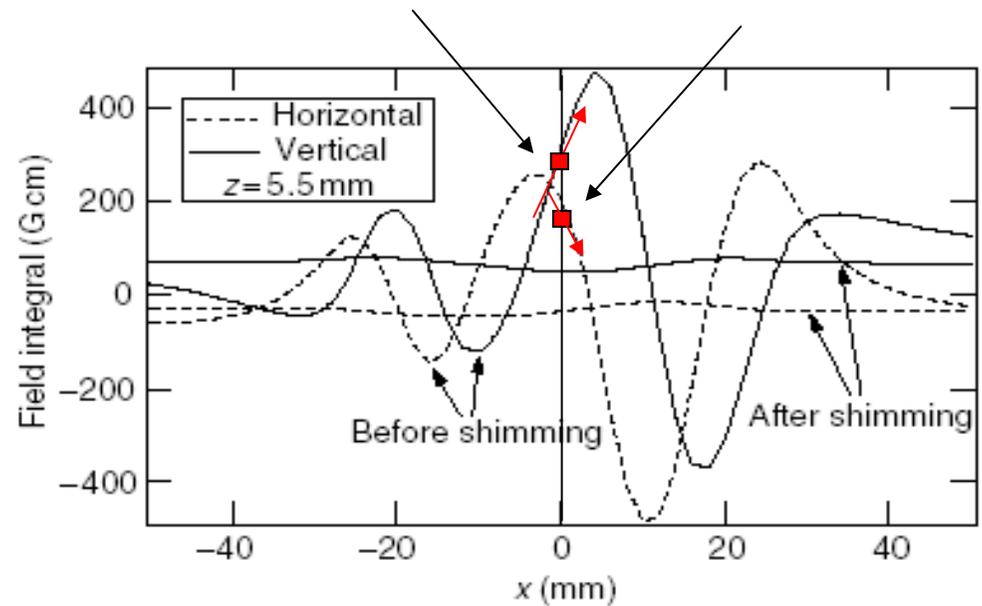


# Field Integral and Multipole Shimming



Horizontal Deflection  
 Quadrupole  
 Sextupole ...

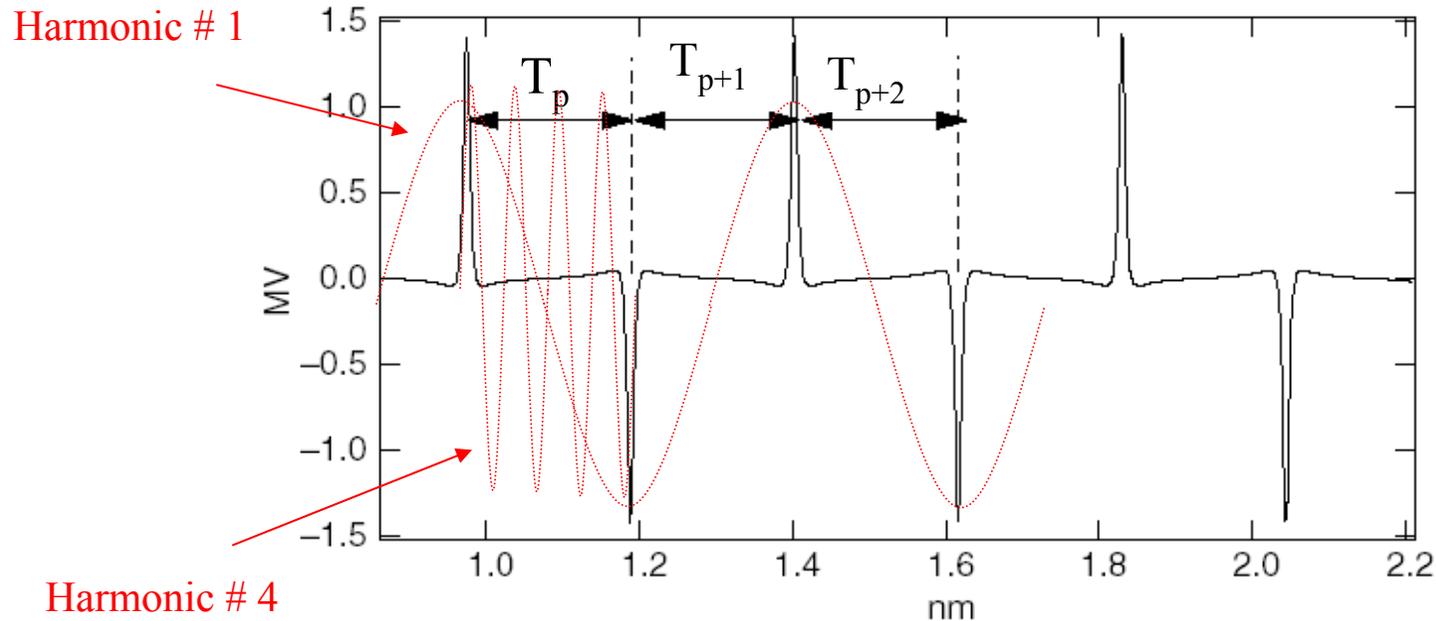
Vertical Deflection  
 Skew Quadrupole  
 Skew sextupole ...



$T_p$  : time distance between successive peaks

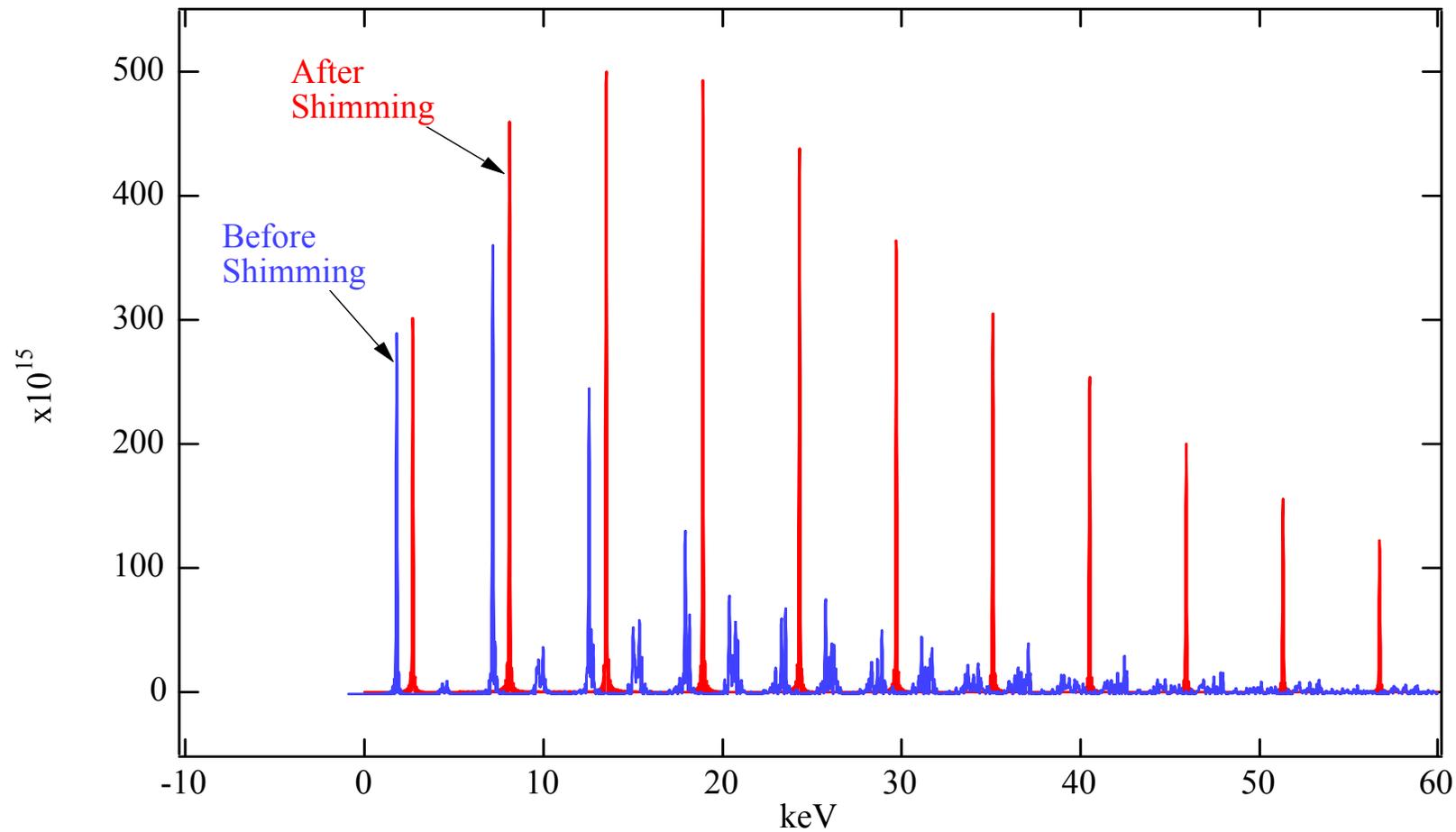
$$T_p = \frac{c\gamma^2}{\lambda_0(1 + \frac{K^2}{2})}$$

$T_p$  varies from one pole to the next due to period and peak field fluctuations



The **Phase shimming** consists of a set of local magnetic field corrections, which make  $T_p$  always identical.

# Phase Shimming and the single electron spectrum



- Learning more about **Insertion Devices**.
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