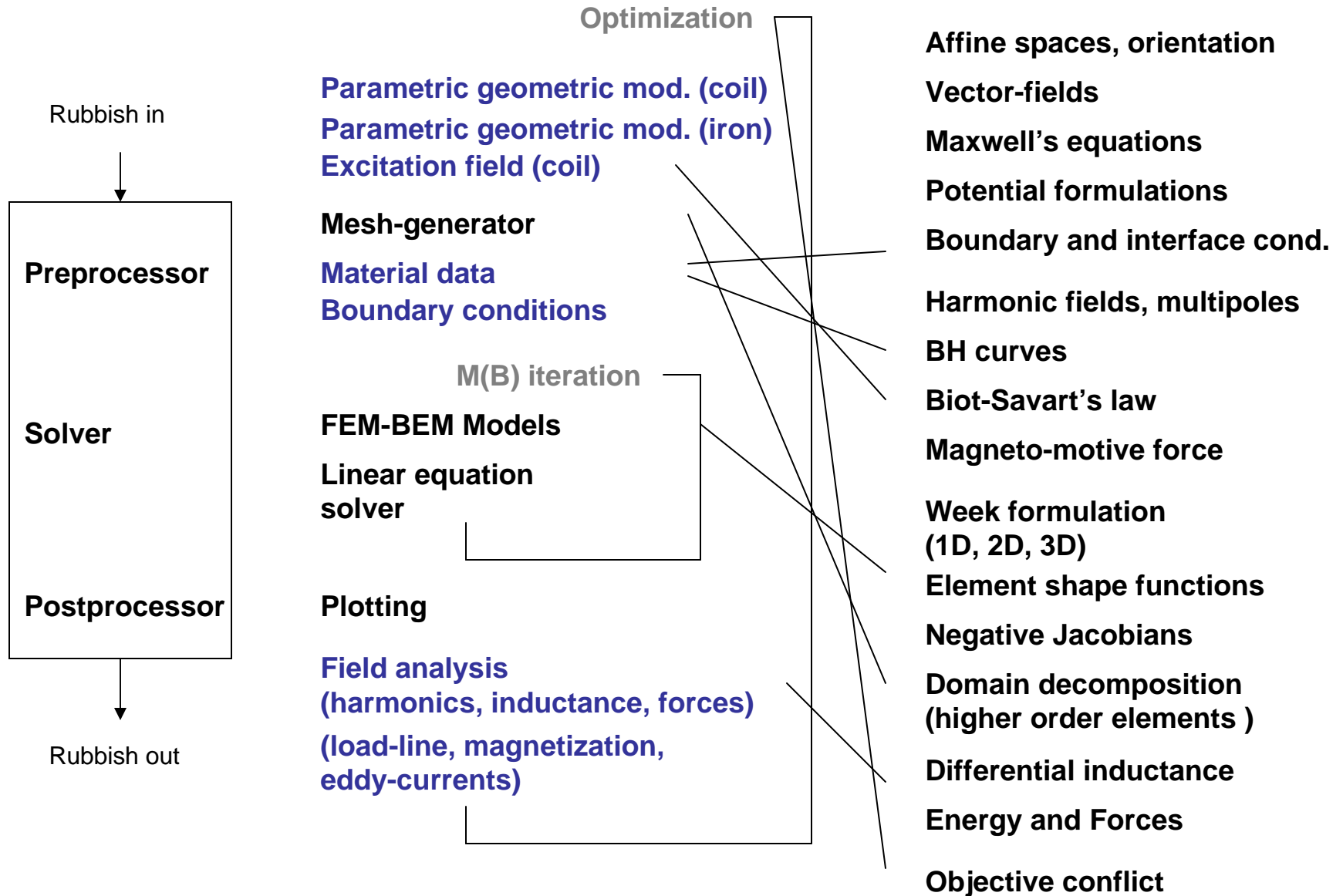


# Foundations of Analytical and Numerical Field Computation

Stephan Russenschuck  
CERN, TE-MCS, 1211 Geneva, Switzerland



**Cockpit 1.1** [/home/russ/Genetic/geneblock\_postp.data]

Parameter	Value
GAP 2	8.2445
GAP 3	14.989
GAP 4	3.6634
PHIO 1	3.5556

Objective function: 0.18887E+04

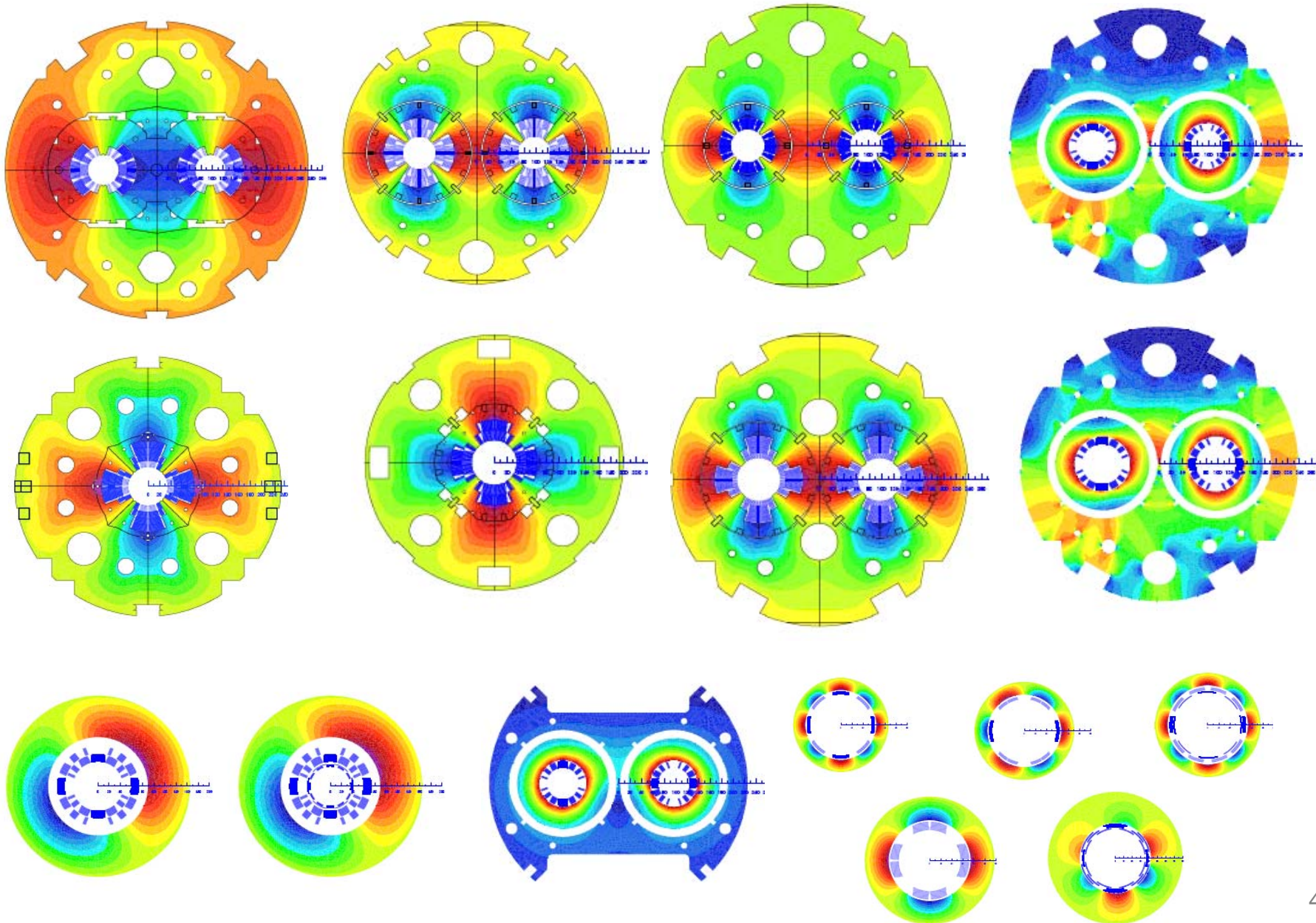
**Xhermes** - [/home/russ/analyfort/C\_core\_saturation]

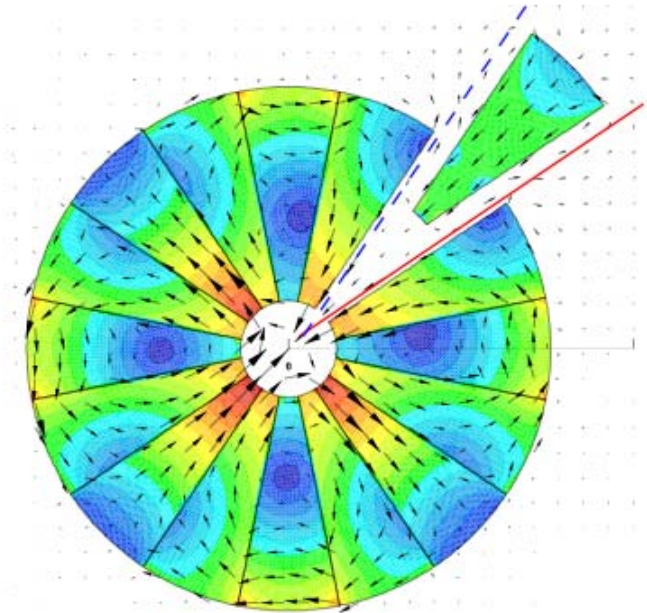
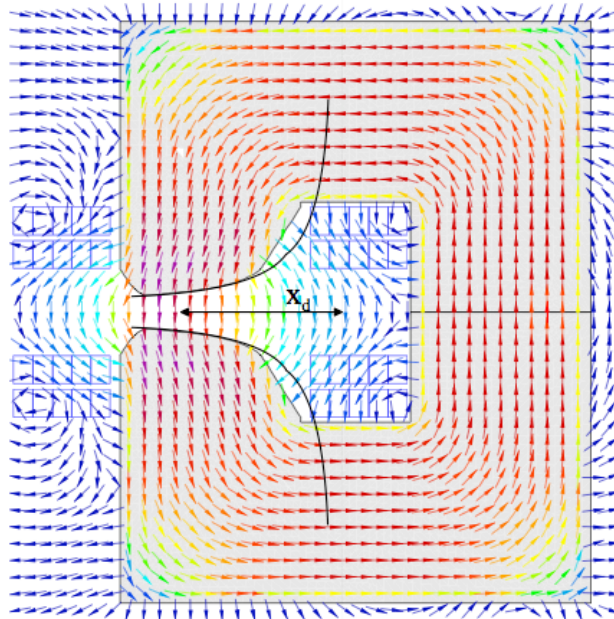
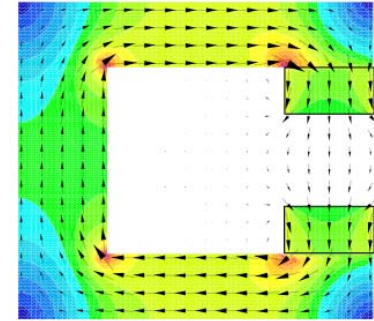
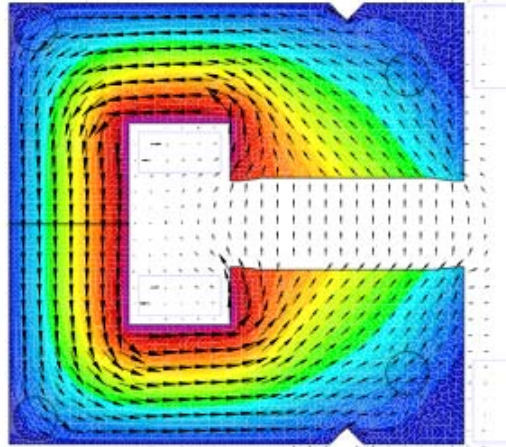
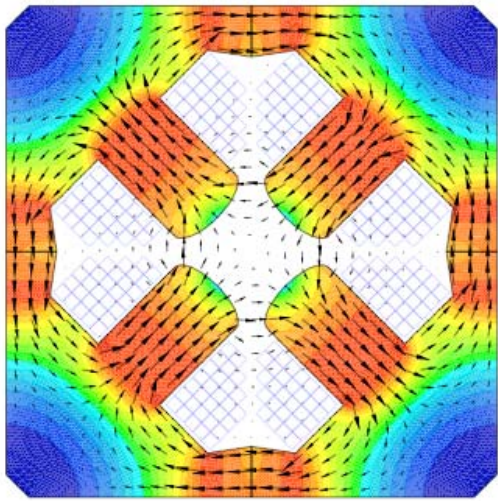
Full Graph | Run ROXIE

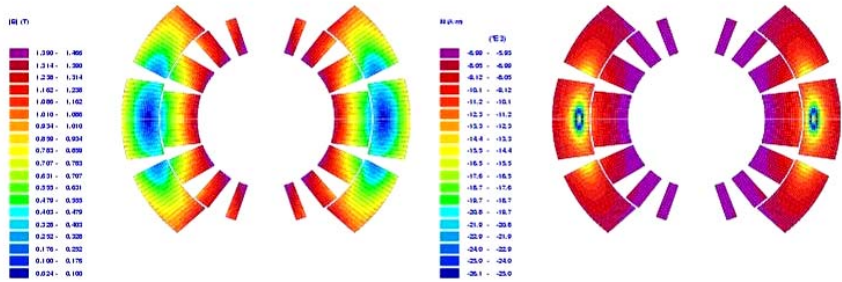
```
Version 1.29/04 of HIGZ started
PLOTTING OF CONVERGENCE:
FIRST OBJECTIVE RED, SECOND BLUE,
THIRD MAGENTA, ALL OTHERS BLACK

*****
*          END OF THIS ROXIE CALCULATION          *
*****
```

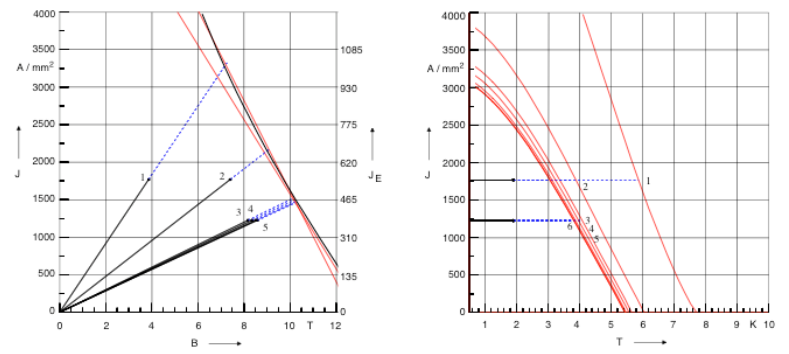
roxie run completed ok (Time elapsed 00:00:06). Click on Close to continue.



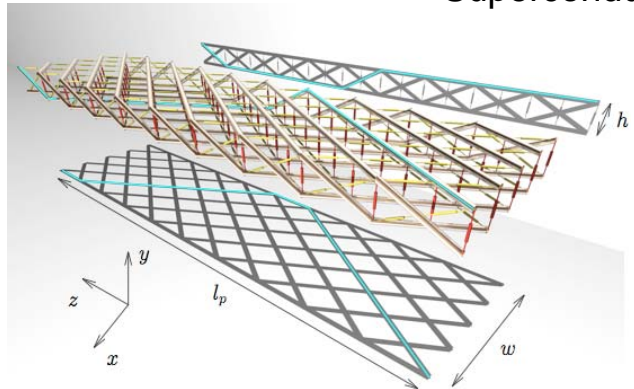




Superconductor magnetization



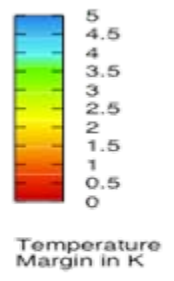
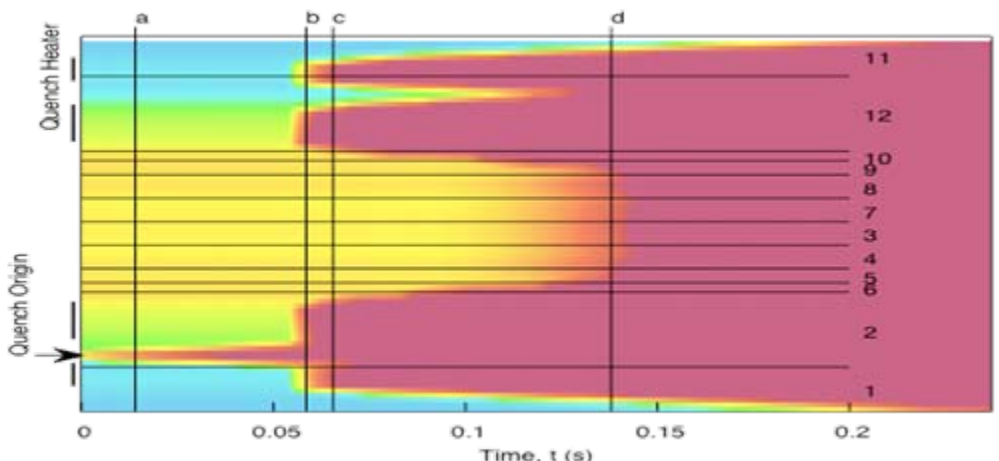
Load lines



Cable eddy currents

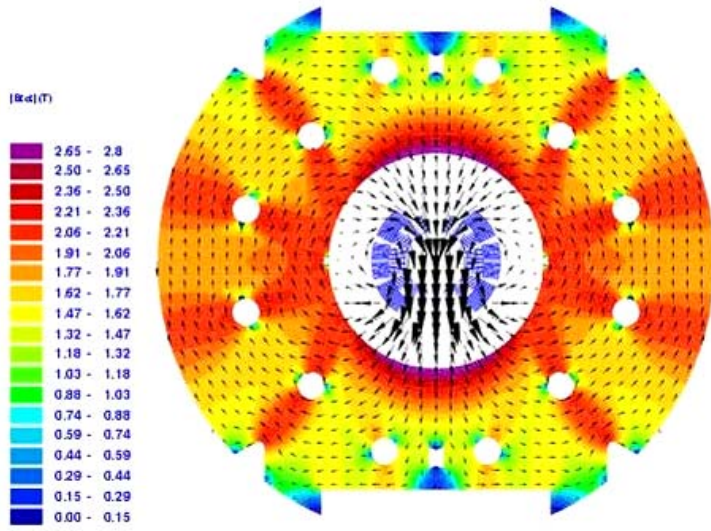


End-spacer design

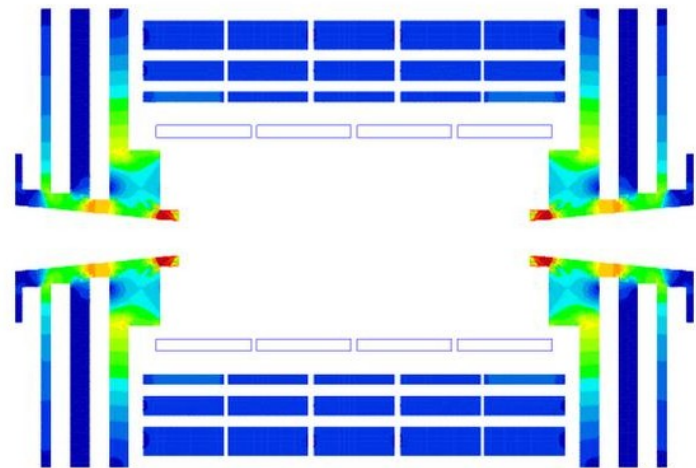
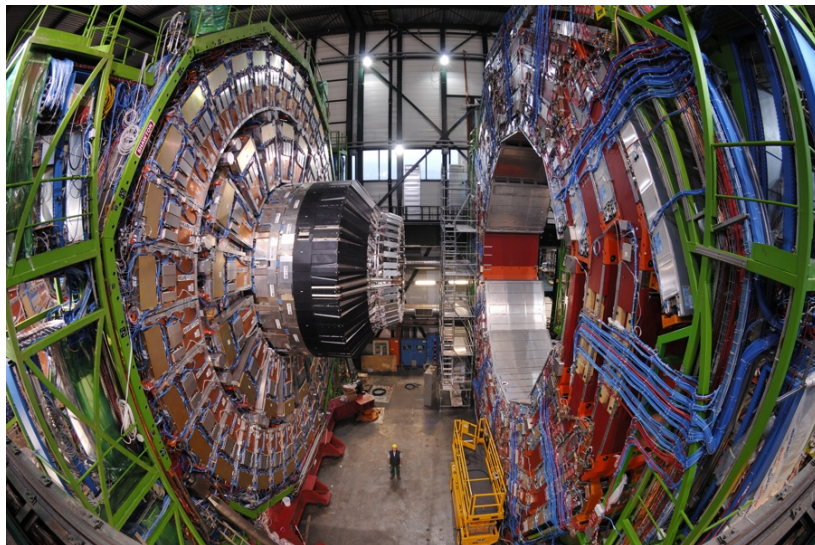


Quench simulation

- ➔ This is not a ROXIE user's course, nor does it present syntax of any commercial software
- ➔ We glance at the foundations of FEM and BEM (basically for a 1-D example)
- ➔ But we want to give a deeper understanding of what the potential problems and limitations of both of semi-analytical and numerical field computation are
  - We provide questions to be asked at your next software user's meeting
- ➔ We discuss pre- and post-processing that can, if necessary, be appended to commercial solvers using modern script languages
  - To this end, we show examples from the ROXIE code



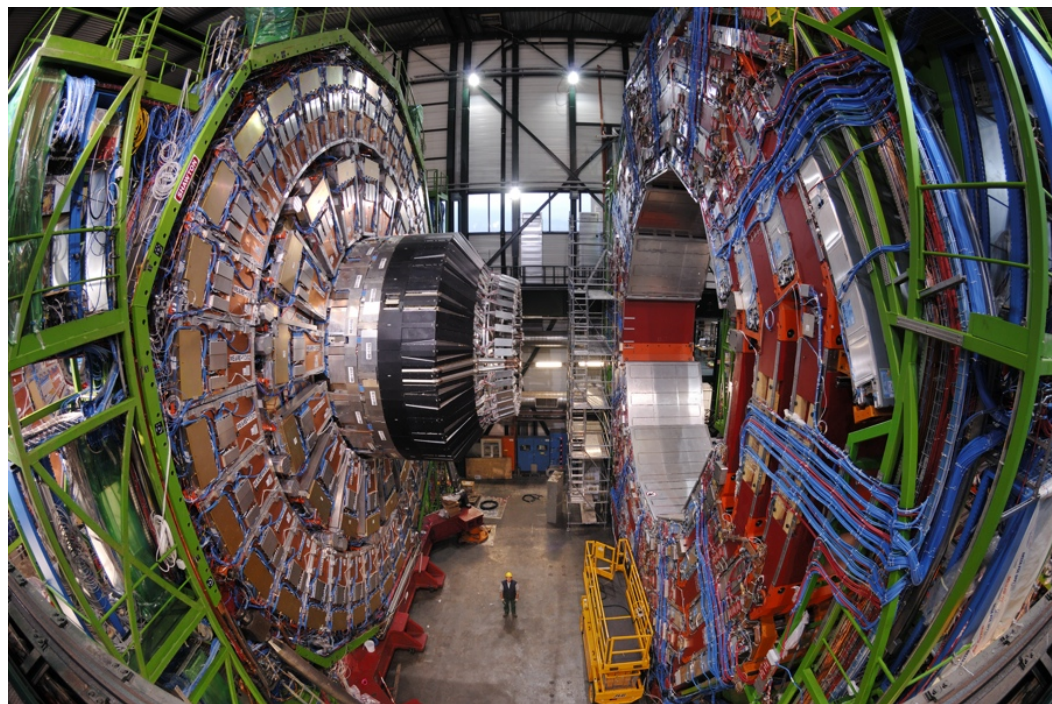
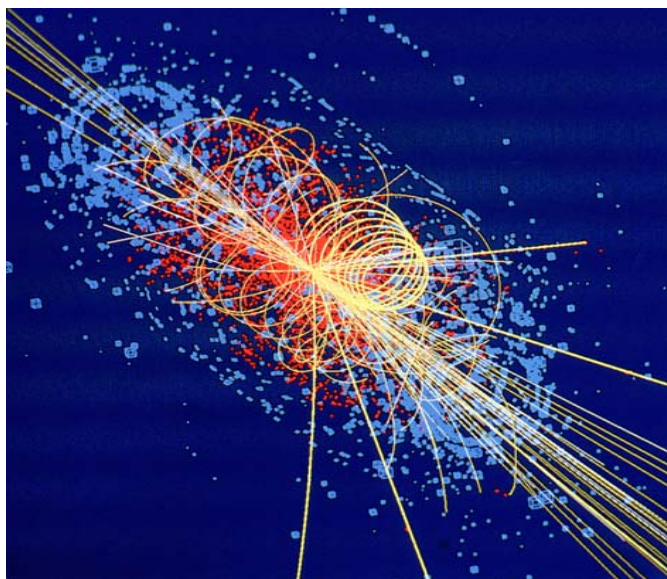
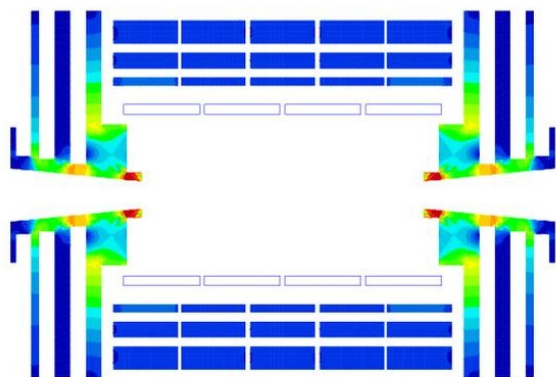
$B = 8.33 \text{ T}$     $B_S = 7.77 \text{ T}$



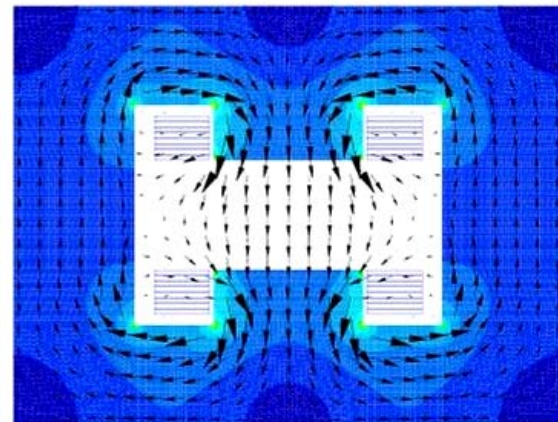
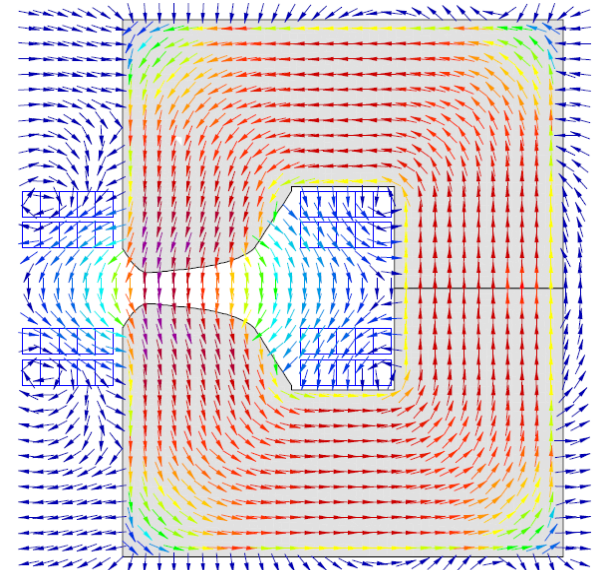
$B = 4 \text{ T}$

$B_S = 3.69 \text{ T}$





$$S = R(1 - \cos \frac{\alpha}{2}) \approx \frac{R\alpha^2}{8} = \frac{QBL^2}{8p}$$



$N \cdot I = 24000 \text{ A}$

$B_1 = 0.3 \text{ T}$

$B_s = 0.065 \text{ T}$

Fill.fac. 0.98

War es ein Gott der diese Zeichen schrieb,  
die mit geheimnisvoll verborg'nem Trieb  
die Kraefte der Natur um mich enthuelen  
und mir das Herz mit stiller Freude fuellen.

Ludwig Boltzmann

Was it a god whose inspirations  
led him to write these fine equations,  
nature's field to me he shows  
and so my heart with pleasure glows.

Translation by J.P. Blewett

$$\int_{\partial a} \vec{H} \cdot d\vec{s} = \int_a \vec{J} \cdot d\vec{a} + \frac{d}{dt} \int_a \vec{D} \cdot d\vec{a}$$

$$\int_{\partial a} \vec{E} \cdot d\vec{s} = -\frac{d}{dt} \int_a \vec{B} \cdot d\vec{a}$$

$$\int_{\partial V} \vec{B} \cdot d\vec{a} = 0$$

$$\int_{\partial V} \vec{D} \cdot d\vec{a} = \int_V \rho dV$$

$$dH = J + \partial_t D$$

$$dE = -\partial_t B$$

$$dB = 0$$

$$dD = \rho$$

$$V_m(\partial a) = I(a) + \frac{d}{dt} \Psi(a)$$

$$U(\partial a) = -\frac{d}{dt} \Phi(a)$$

$$\Phi(\partial V) = 0$$

$$\Psi(\partial V) = Q(V)$$

$$\text{curl} \vec{H} = \vec{J} + \partial_t \vec{D}$$

$$\text{curl} \vec{E} = -\partial_t \vec{B}$$

$$\text{div} \vec{B} = 0$$

$$\text{div} \vec{D} = \rho$$

$$\mathcal{B} = V \cdot \nabla u$$

$$\mathcal{E} = V \cdot \dot{\rho} \mathcal{B} - \mathcal{H} - \nabla \psi$$

$$\mathcal{C} = c\mathcal{E} + \mathcal{D}$$

$$\mathcal{B} = \mathcal{H} + 4\pi \mathcal{J}$$

$$4\pi c = V \cdot \nabla \mathcal{H}$$

$$\mathcal{D} = \frac{1}{4\pi} \kappa \mathcal{E}$$

$$a = \frac{\partial H}{\partial y} - \frac{\partial G}{\partial z}$$

$$b = \frac{\partial F}{\partial z} - \frac{\partial H}{\partial x}$$

$$c = \frac{\partial G}{\partial x} - \frac{\partial F}{\partial y}$$

$$P = -\frac{\partial F}{\partial t} - \frac{\partial \phi}{\partial x}$$

$$Q = -\frac{\partial G}{\partial t} - \frac{\partial \phi}{\partial y}$$

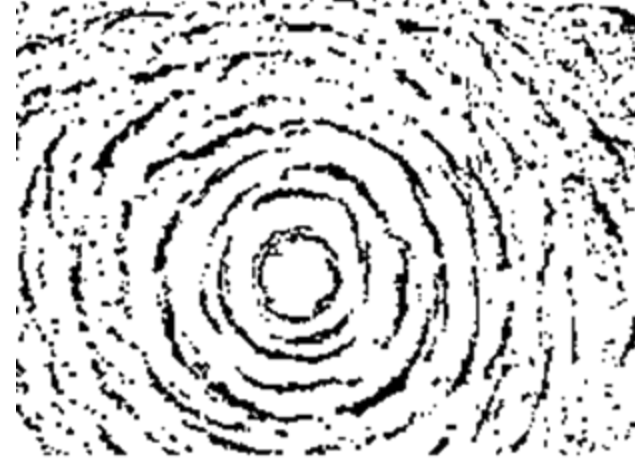
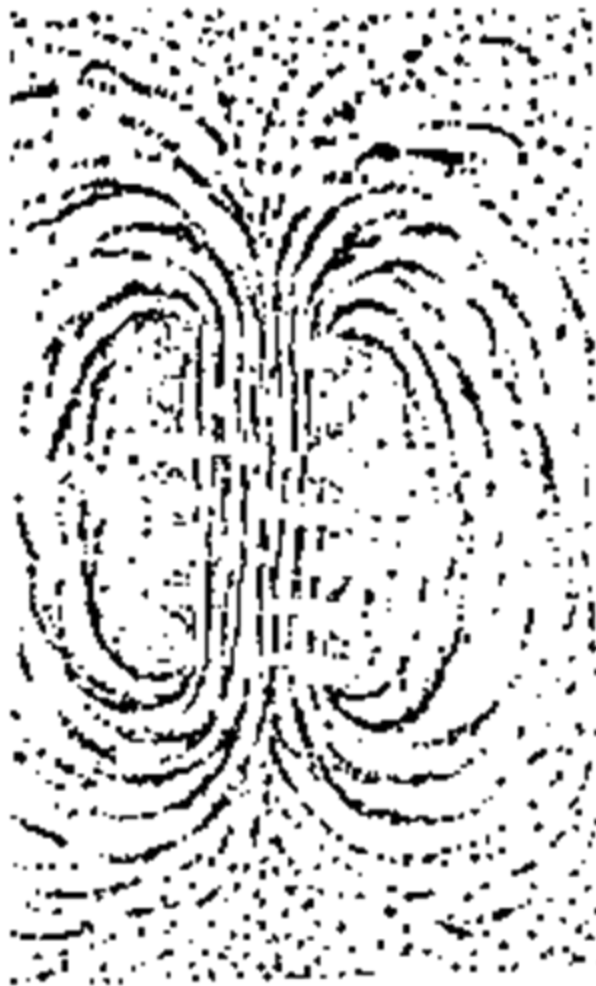
$$R = -\frac{\partial H}{\partial t} - \frac{\partial \phi}{\partial z}$$

$$p + \frac{\partial f}{\partial t} = \frac{\partial \gamma}{\partial y} - \frac{\partial \beta}{\partial z}$$

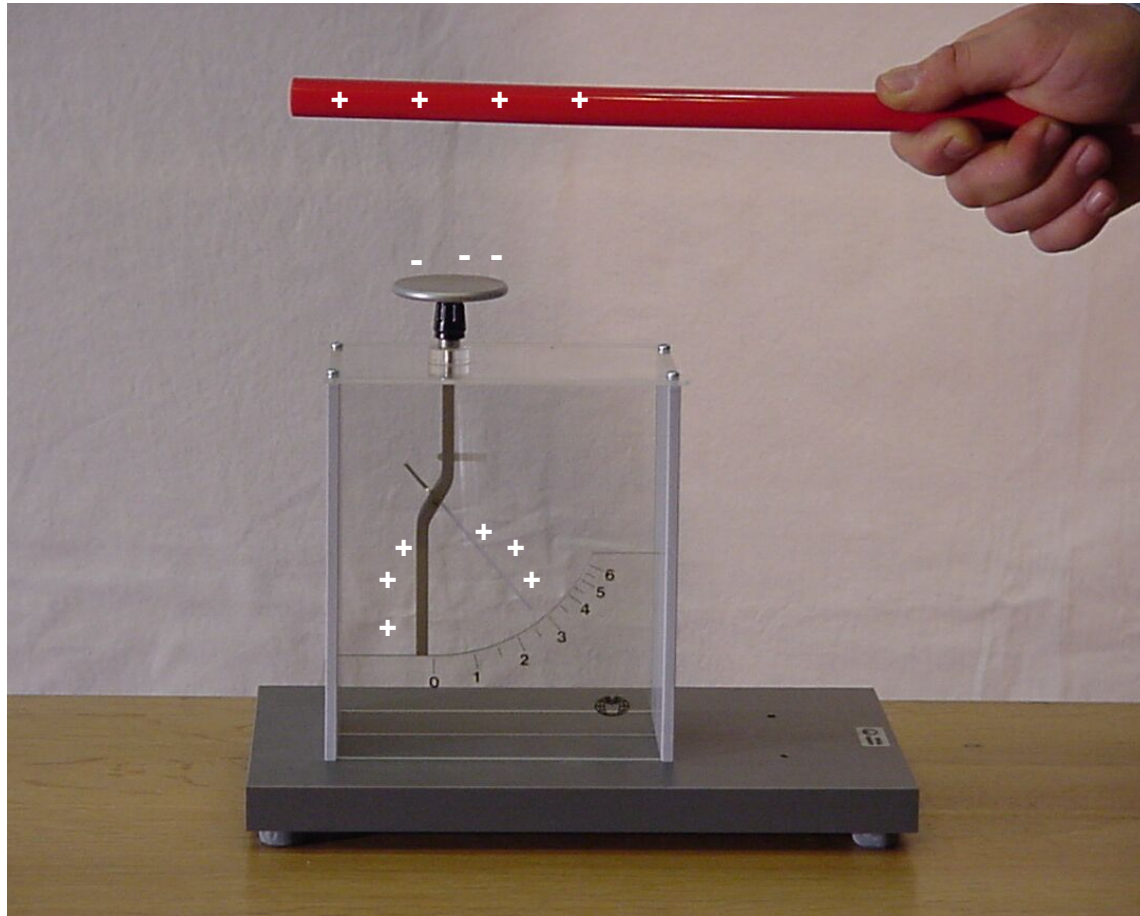
$$q + \frac{\partial g}{\partial t} = \frac{\partial \alpha}{\partial z} - \frac{\partial \gamma}{\partial x}$$

$$r + \frac{\partial h}{\partial t} = \frac{\partial \beta}{\partial x} - \frac{\partial \alpha}{\partial y}$$

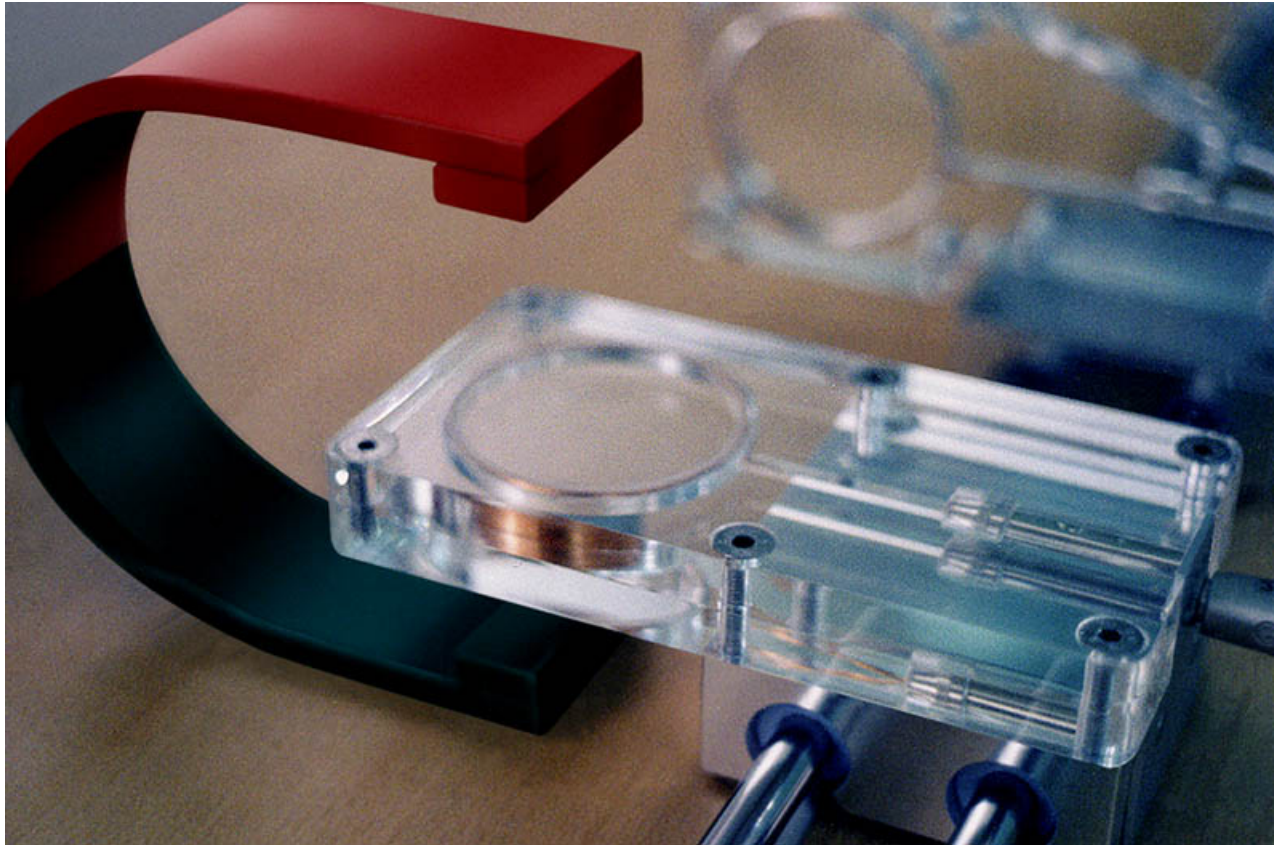
$$\rho = \frac{\partial f}{\partial x} + \frac{\partial g}{\partial y} + \frac{\partial h}{\partial z}$$



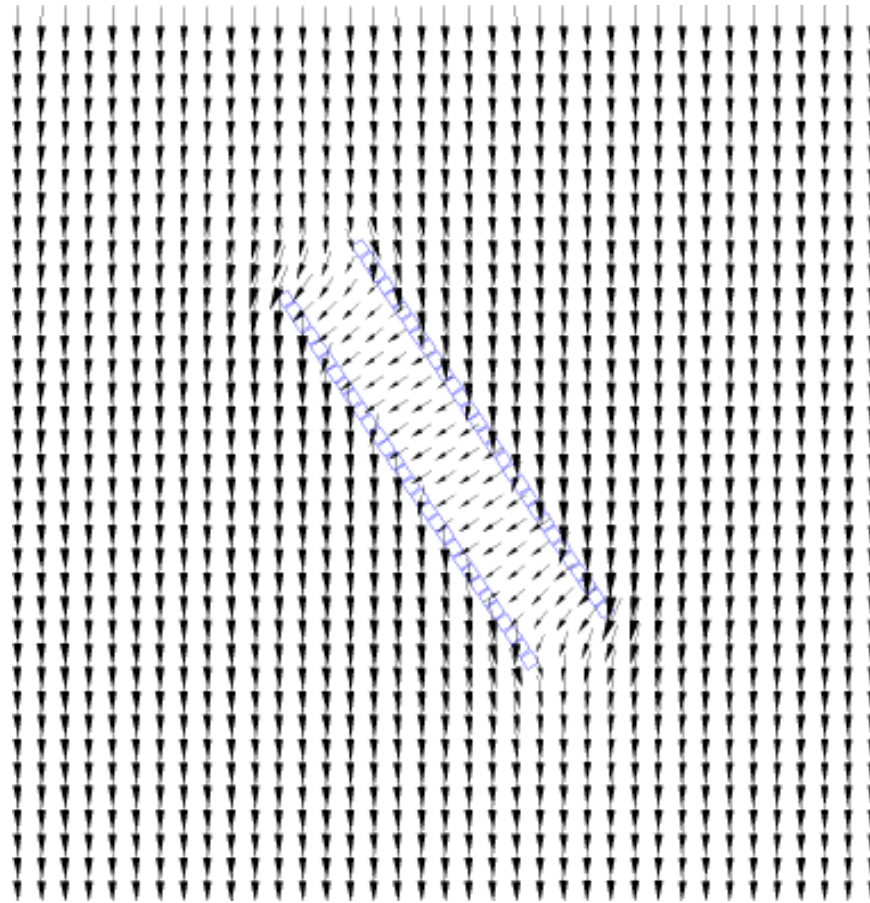
$$\Phi(\partial V) = 0$$



$$\Psi(\partial V) = Q(V)$$



$$U(\partial a) = -\frac{d}{dt}\Phi(a)$$



$$V_m(\partial a) = I(a)$$



Ampere  $V_m(\partial a) = I(a) + \frac{d}{dt}\psi(a)$

Faraday  $U(\partial a) = -\frac{d}{dt}\Phi(a)$

Flux conservation  $\Phi(\partial V) = 0$

Gauss  $\psi(\partial V) = Q(V)$

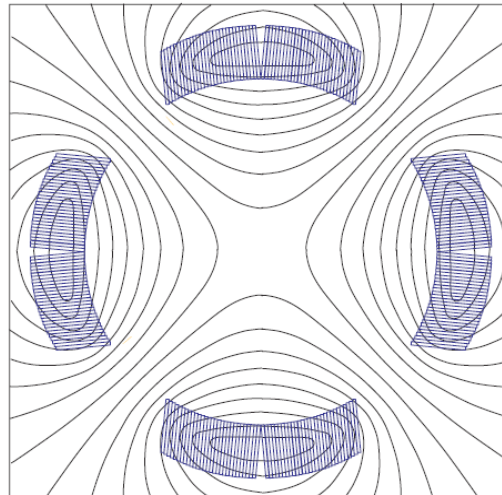
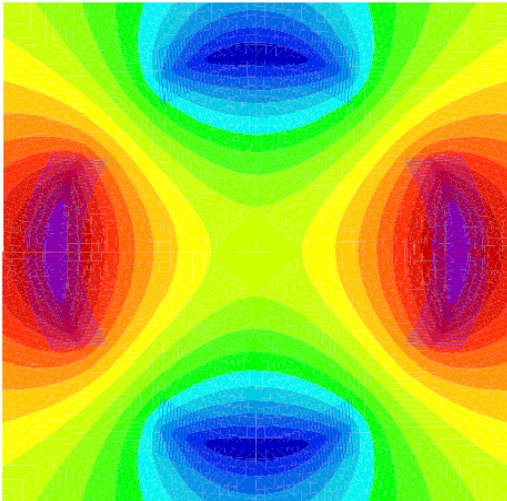
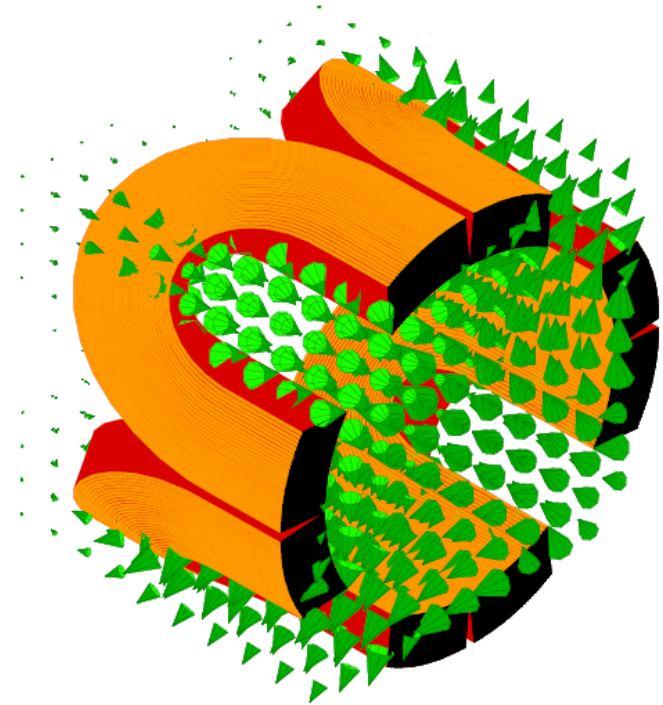
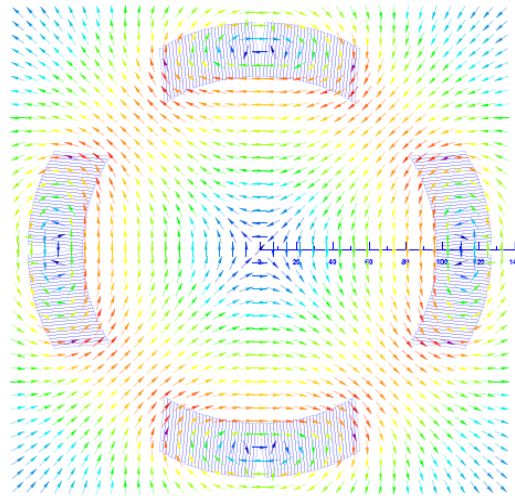
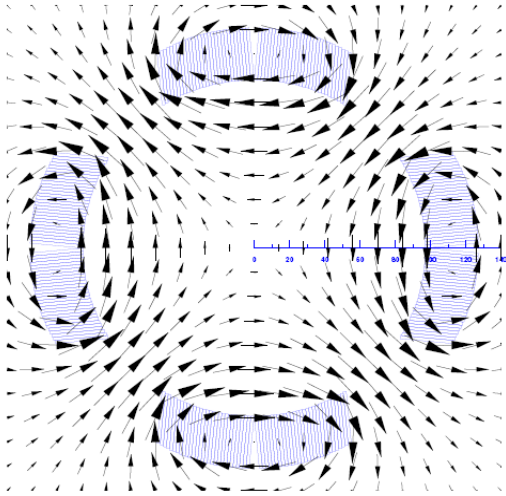
Conservation of charge / Kirchhoff law

$$V_m(\partial(\partial V)) = 0 = I(\partial V) + \frac{d}{dt}Q(V)$$

**For its unworthy of excellent men  
to loose hours like slaves in the labour of calculation  
which could safely be regulated to anyone else if  
machines were used**

**Gottfried Wilhelm Leibnitz (1646-1716)**

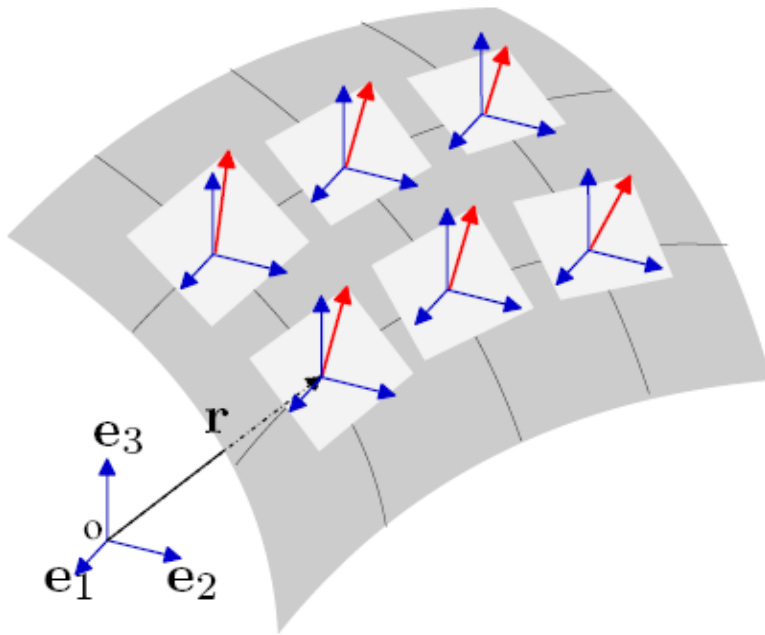
SI-unit	Relation	SI-unit
1A	$V_m(s) = \int_s \mathbf{H} \cdot d\mathbf{s}$	$1\text{A} \cdot \text{m}^{-1}$
1V	$U(s) = \int_s \mathbf{E} \cdot d\mathbf{s}$	$1\text{V} \cdot \text{m}^{-1}$
$1\text{V} \cdot \text{s}$	$\Phi(a) = \int_a \mathbf{B} \cdot d\mathbf{a}$	$1\text{V} \cdot \text{s} \cdot \text{m}^{-2}$
$1\text{A} \cdot \text{s}$	$\Psi(a) = \int_a \mathbf{D} \cdot d\mathbf{a}$	$1\text{A} \cdot \text{s} \cdot \text{m}^{-2}$
1A	$I(a) = \int_a \mathbf{J} \cdot d\mathbf{a}$	$1\text{A} \cdot \text{m}^{-2}$
$1\text{A} \cdot \text{s}$	$Q(V) = \int_V \rho \cdot dV$	$1\text{A} \cdot \text{s} \cdot \text{m}^{-3}$



$$\mathbf{a} : \Omega \rightarrow \mathbb{R}^3 : \mathbf{r} \mapsto \mathbf{a}(\mathbf{r}) : \mathbf{a}(\mathbf{r}) = (a^1(\mathbf{r}), a^2(\mathbf{r}), a^3(\mathbf{r}))$$

$$\mathcal{V}(\Omega) := C^\infty(\Omega, \mathbb{R}^3)$$

$\Omega \subset \mathbb{R}^3$



$$\phi : \Omega \rightarrow \mathbb{R} : \phi \mapsto \phi(\mathbf{r})$$

$$\mathcal{S}(\Omega) := C^\infty(\Omega, \mathbb{R})$$

$$\int_{\partial a} \mathbf{H} \cdot d\mathbf{s} = \int_a \mathbf{J} \cdot d\mathbf{a} + \frac{d}{dt} \int_a \mathbf{D} \cdot d\mathbf{a},$$

$$\int_{\partial a} \mathbf{E} \cdot d\mathbf{s} = -\frac{d}{dt} \int_a \mathbf{B} \cdot d\mathbf{a},$$

$$\int_{\partial V} \mathbf{B} \cdot d\mathbf{a} = 0,$$

$$\int_{\partial V} \mathbf{D} \cdot d\mathbf{a} = \int_V \rho dV.$$

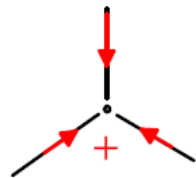
$$V_m(\partial a) = I(a) + \frac{d}{dt} \Psi(a),$$

$$U(\partial a) = -\frac{d}{dt} \Phi(a),$$

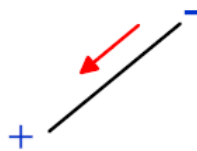
$$\Phi(\partial V) = 0,$$

$$\Psi(\partial V) = Q(V).$$

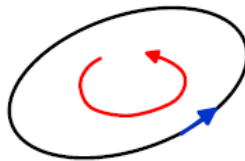
## Inner orientation



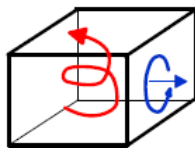
Point:  
A positive point is oriented as a sink



Line/Edge:  
Selecting a vector pointing in forward direction

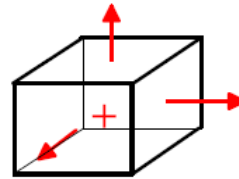


Surface:  
Sense of rotation

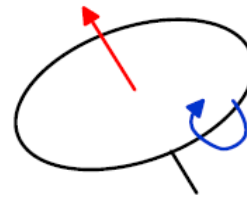


Volume:  
Sense of a screw

## Outer orientation



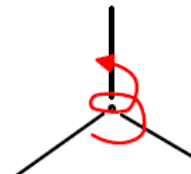
Volume:  
Choice of outward normals



Surface:  
Crossing direction of a line

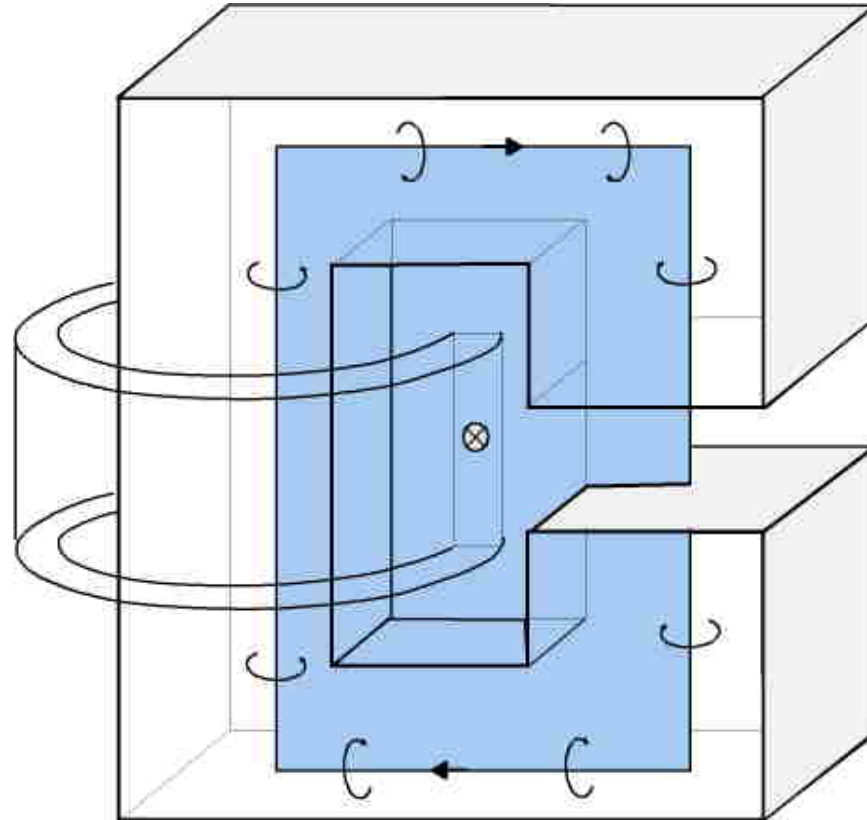


Line/Edge:  
Direction of circulation of a surface around this line



Point:  
The inner orientation of the volume containing the point

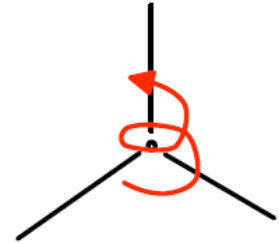
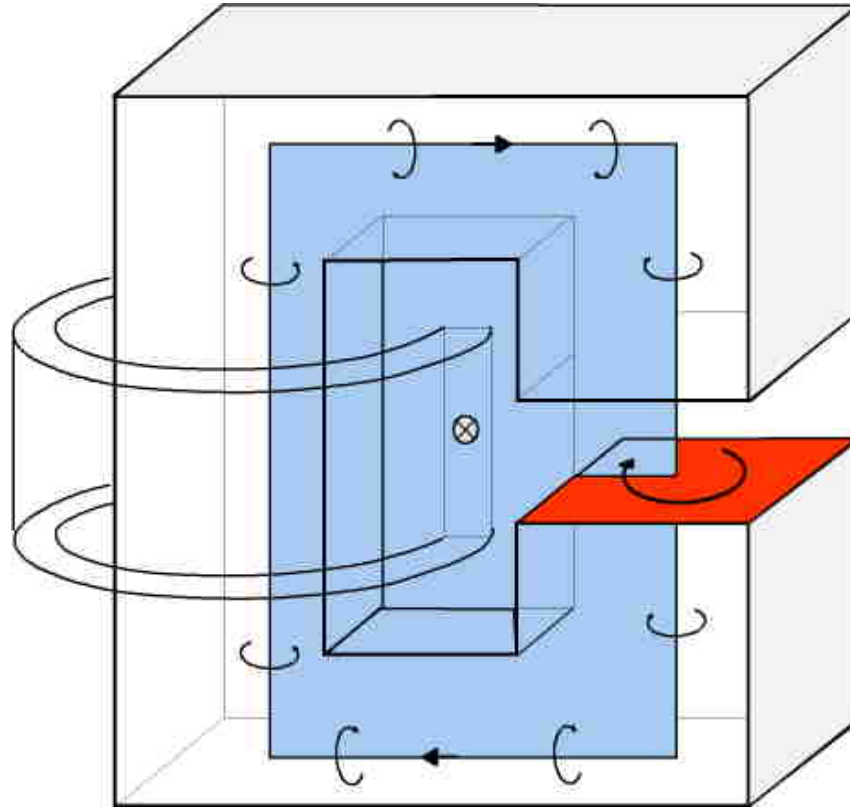
$$\int_{\partial a} \mathbf{H} \cdot d\mathbf{s} = \int_a \mathbf{J} \cdot d\mathbf{a}$$



$$\Phi(a) = \int_a \mathbf{B} \cdot d\mathbf{a}$$



$$\int_{\partial a} \mathbf{H} \cdot d\mathbf{s} = \int_a \mathbf{J} \cdot d\mathbf{a}$$



Embedding into oriented ambient space  
(Origin, coordinates)

$$\Phi(a) = \int_a \mathbf{B} \cdot d\mathbf{a}$$



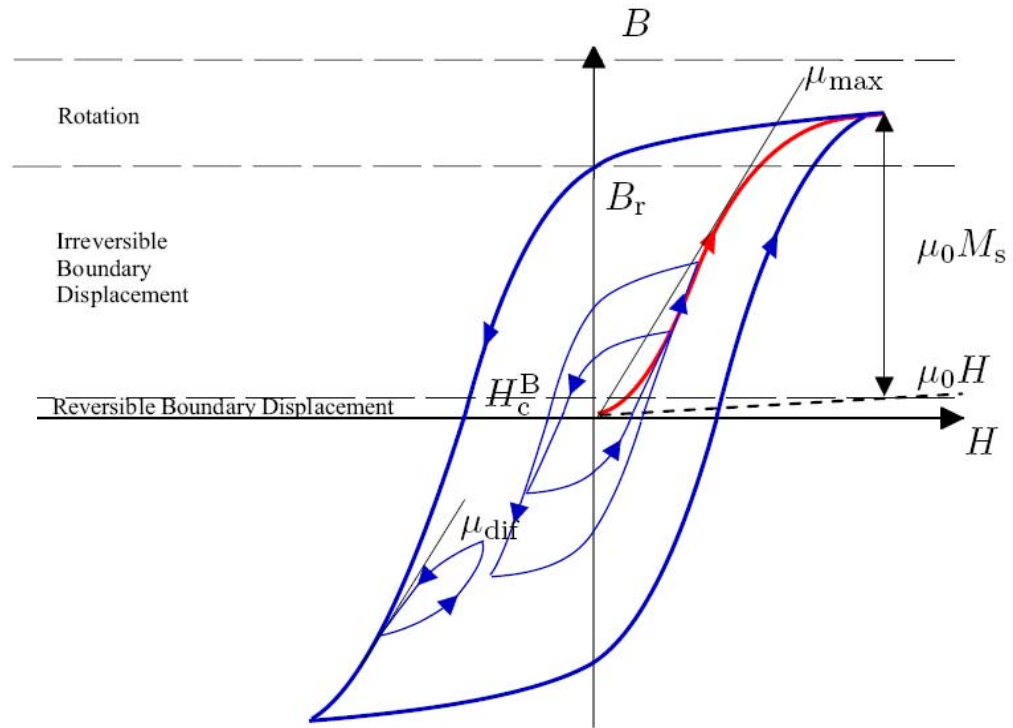
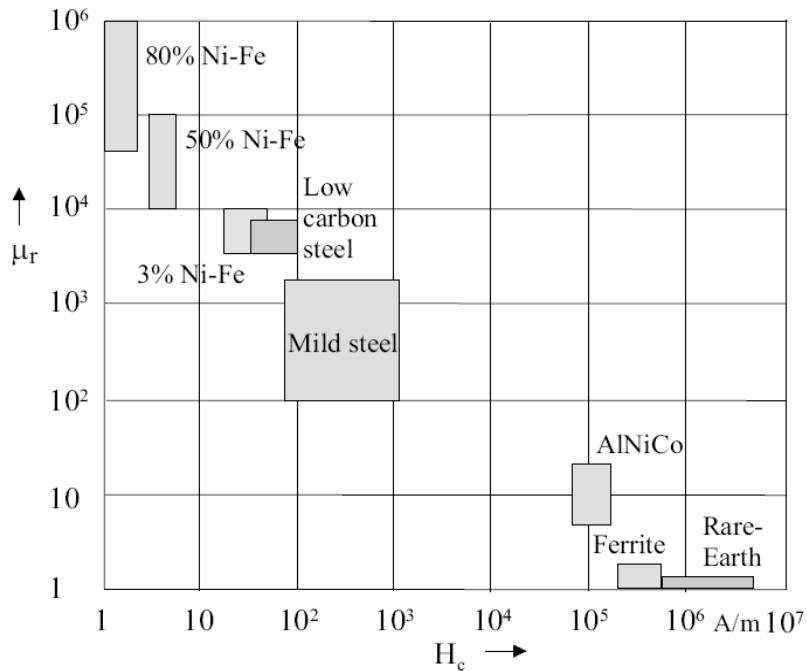
$$\mathbf{B} = \mu \mathbf{H} \quad \mathbf{D} = \epsilon \mathbf{E} \quad \mathbf{J} = \kappa \mathbf{E}$$

Permeability:  $[\mu] = 1 \text{ V} \cdot \text{s} \cdot \text{A}^{-1} \cdot \text{m}^{-1} = 1 \text{ H} \cdot \text{m}^{-1}$

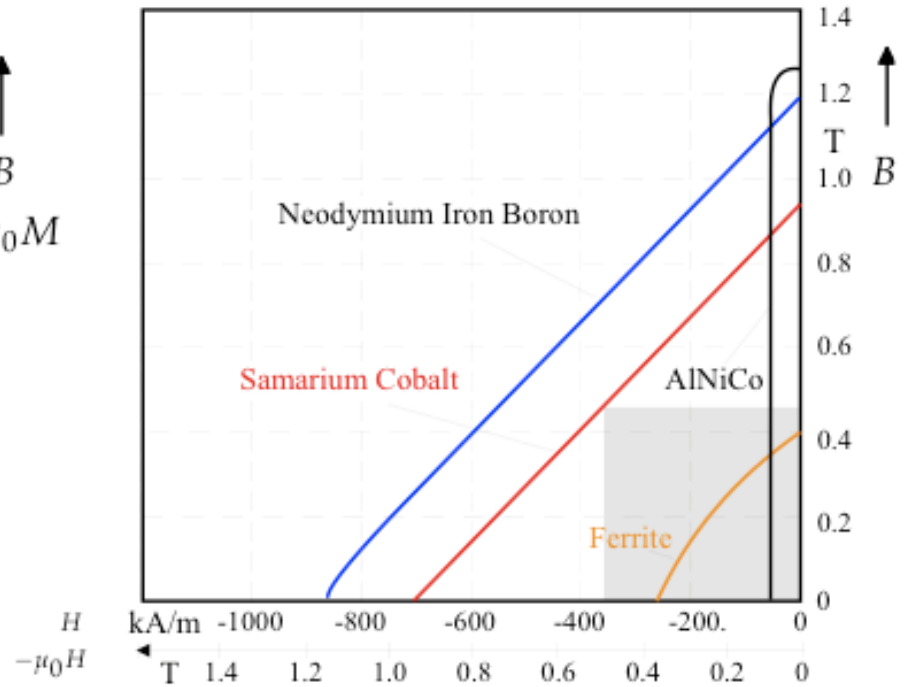
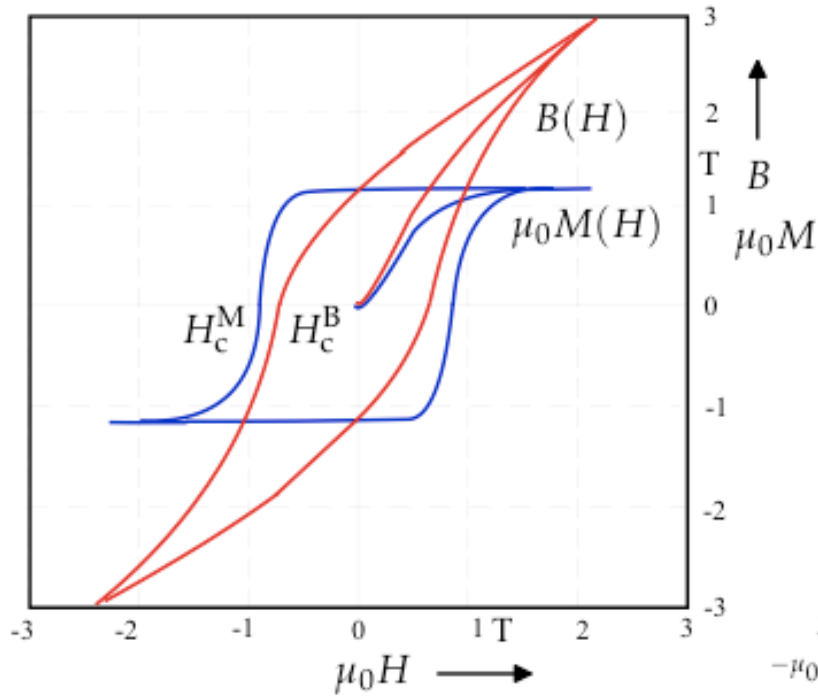
Permittivity:  $[\epsilon] = 1 \text{ A} \cdot \text{s} \cdot \text{V}^{-1} \cdot \text{m}^{-1}$

Conductivity:  $[\kappa] = 1 \text{ A} \cdot \text{V}^{-1} \cdot \text{m}^{-1}$

Linear (field independent), homogeneous (position independent), isotropic (direction independent) and stationary media. The material parameters may depend on the spatial position.



$$\mathbf{B} = \mu_0 \mathbf{H} + \mathbf{P}_{mag}(\mathbf{H}) = \mu_0 (\mathbf{H} + \mathbf{M}(\mathbf{H}))$$



$$H = \frac{NI}{2\pi r}$$

$$\mu = \frac{\bar{B}}{H}$$

$$\bar{H} = \frac{NI}{2\pi(r_2 - r_1)} \ln \frac{r_2}{r_1}$$

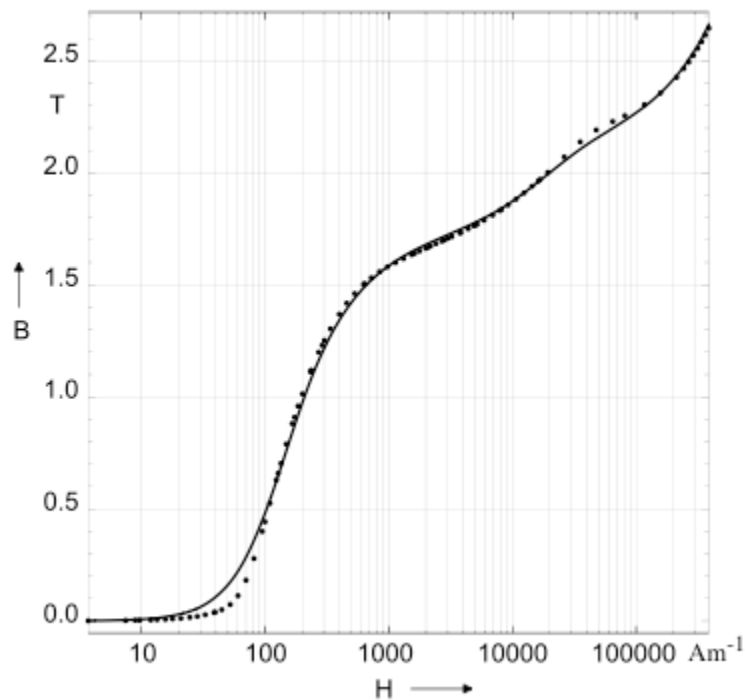
$$U = \frac{d}{dt} \Phi = \frac{d}{dt} \bar{B} a$$

$$\bar{B} = \bar{B}_{\text{meas.}} + B_{\text{corr.}}$$



Temperature T K	Stress MPa	Coercive field $H_c^B$ $A \cdot m^{-1}$	Remanence $B_r$ T	max $\mu_r$
300	0	68.4	1.07	5900
77	0	79.6	1.12	5600
4.2	0	85.1	1.06	4800
4.2	20	110.	0.67	2460

**Always check conditions of measurements**



$$L\left(\frac{H}{a}\right) := \coth\left(\frac{H}{a}\right) - \left(\frac{a}{H}\right)$$

$$M(H) = M_a L\left(\frac{H}{a}\right) + M_b \tanh\left(\frac{|H|}{b}\right) L\left(\frac{H}{b}\right)$$

**Always fulfilling the smoothness requirements for M(B)  
and Newton-Raphson iterative solvers**

Closed domain (2-D or 3-D) will be denoted as  $\Omega$ . Boundary  $\Gamma = \partial\Omega$  with  $\Gamma = \Gamma_H \cup \Gamma_B$

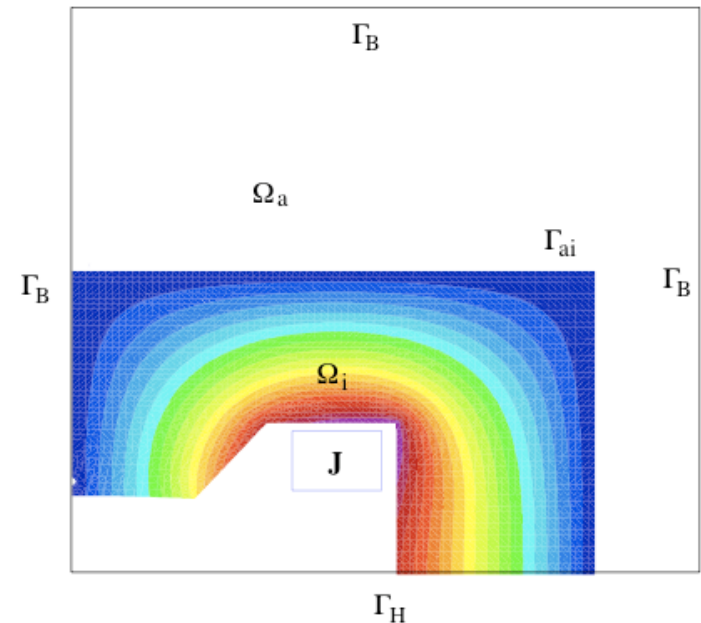
On  $\Gamma_B$  the normal component of the magnetic flux density is prescribed (symmetry planes parallel to the field, on far boundaries etc.)

$$B_n = \mathbf{B} \cdot \mathbf{n} = \sigma_{\text{mag}} \quad \text{on } \Gamma_B$$

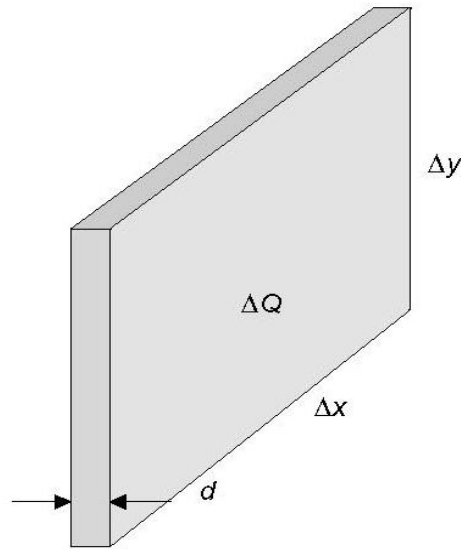
On  $\Gamma_H$  of the boundary the tangential components of the magnetic field are prescribed. In general

$$\mathbf{H} \times \mathbf{n} = \boldsymbol{\alpha} \quad \text{on } \Gamma_H$$

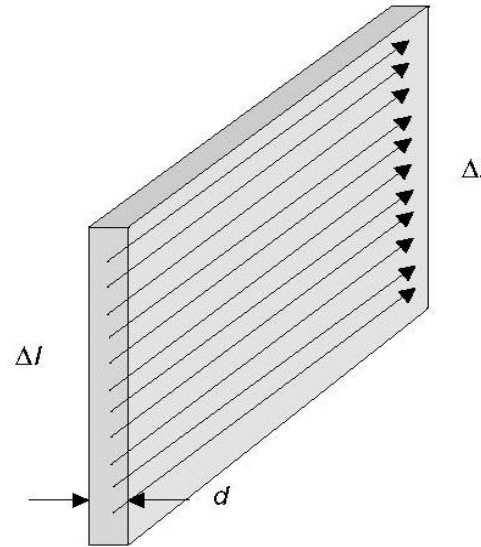
$$\mathbf{H}_t = \mathbf{0} \quad \rightarrow \quad \mathbf{n} \times (\mathbf{H} \times \mathbf{n}) = \mathbf{0}$$





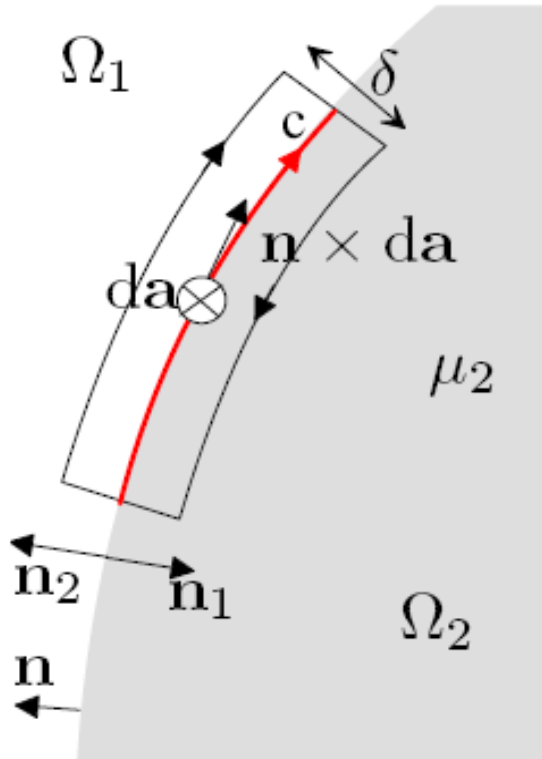


Thin layer with  $\rho_{\text{mag}}$   
 $\Delta Q = \Delta x \Delta y d \rho_{\text{mag}}$   
 $\rho_{\text{mag}} \rightarrow \infty$  and  $d \rightarrow 0$   
 $\sigma_{\text{mag}} = d \rho_{\text{mag}}$   
 $[\sigma_{\text{mag}}] = 1 \text{ V}\cdot\text{s}/\text{m}^2$



Thin layer with  $J$   
 $\Delta I = J d \Delta l$   
 $J \rightarrow \infty$  and  $d \rightarrow 0$   
 $\alpha = J d$   
 $[\alpha] = 1 \text{ A}\cdot\text{m}^{-1}$

**Fictitious quantities to define boundary values**



$$\int_{\partial a} \mathbf{H} \cdot d\mathbf{s} = \int_a \mathbf{J} \cdot d\mathbf{a} \quad \delta \rightarrow 0$$

$$\int_{s_2} \mathbf{H}_2 \cdot d\mathbf{s} + \int_{s_1} \mathbf{H}_1 \cdot d\mathbf{s} = - \int_c (\mathbf{n} \times \boldsymbol{\alpha}) \cdot d\mathbf{s}$$

$$\int_c (\mathbf{H}_1 - \mathbf{H}_2) \cdot d\mathbf{s} = - \int_c (\mathbf{n} \times \boldsymbol{\alpha}) \cdot d\mathbf{s}$$

Holds for any curve  $c$  if the integrands are equal, except for a possible normal component  $\lambda \mathbf{n}$

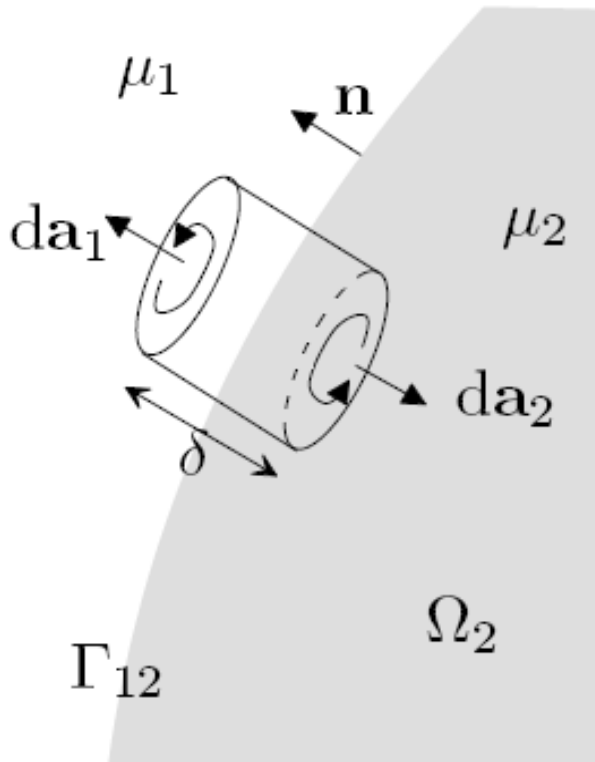
$$(\mathbf{H}_1 - \mathbf{H}_2) + \lambda \mathbf{n} = -\mathbf{n} \times \boldsymbol{\alpha}$$

With  $\mathbf{n} \times (\mathbf{n} \times \boldsymbol{\alpha}) = (\mathbf{n} \cdot \boldsymbol{\alpha})\mathbf{n} - (\mathbf{n} \cdot \mathbf{n})\boldsymbol{\alpha} = -\boldsymbol{\alpha}$

$$\boldsymbol{\alpha} = (\mathbf{H}_1 - \mathbf{H}_2) \times \mathbf{n}$$

$$= [\mathbf{H} \times \mathbf{n}]_{12}$$

$$\mathbf{H}_{t1} = \mathbf{H}_{t2} \quad \equiv \quad (\mathbf{H}_1 - \mathbf{H}_2) \times \mathbf{n} = \mathbf{0} \quad \equiv \quad [\mathbf{H} \times \mathbf{n}]_{12} = \mathbf{0}$$



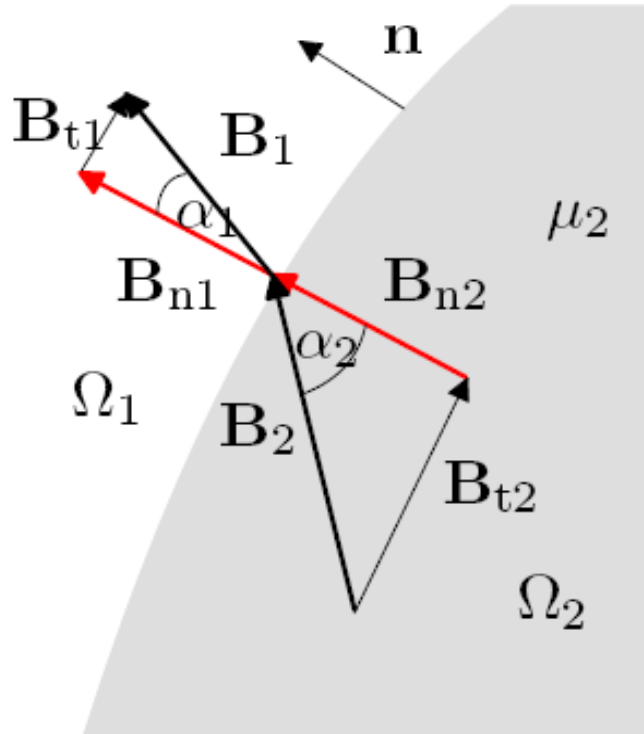
$$\int_{\partial V} \mathbf{B} \cdot d\mathbf{a} = 0 \quad \delta \rightarrow 0$$

$$\begin{aligned} \int_a \sigma_{\text{mag}} da &= \int_a \mathbf{B}_1 \cdot d\mathbf{a}_1 + \mathbf{B}_2 \cdot d\mathbf{a}_2 \\ &= \int_a (\mathbf{B}_1 - \mathbf{B}_2) \cdot \mathbf{n}_1 da \end{aligned}$$

Holds for any surface  $a$  if

$$\begin{aligned} \sigma_{\text{mag}} &= (\mathbf{B}_1 - \mathbf{B}_2) \cdot \mathbf{n} \\ &= [\mathbf{B} \cdot \mathbf{n}]_{12} \end{aligned}$$

$$B_{n1} = B_{n2} \quad \equiv \quad (\mathbf{B}_1 - \mathbf{B}_2) \cdot \mathbf{n} = 0 \quad \equiv \quad [\mathbf{B} \cdot \mathbf{n}]_{12} = 0$$

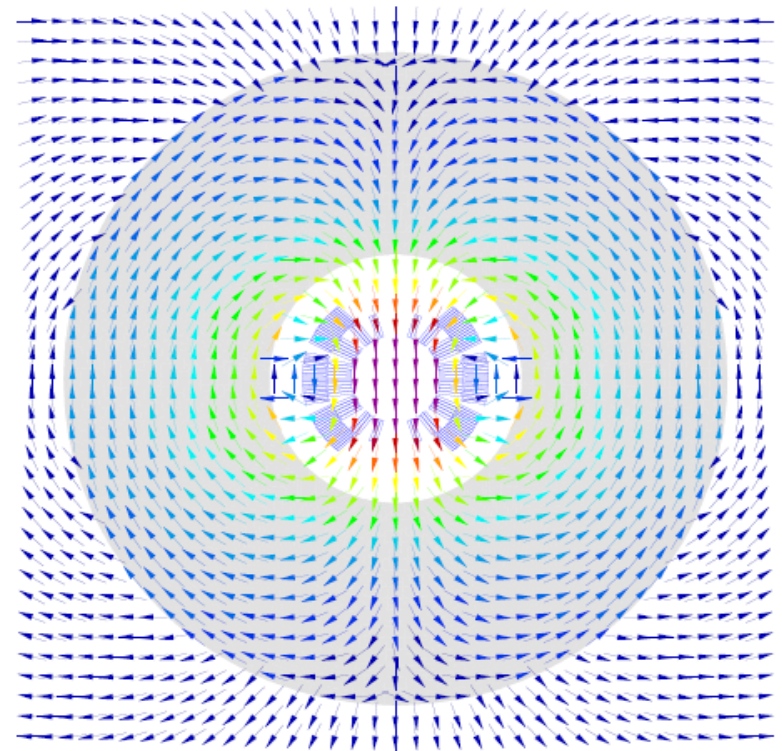
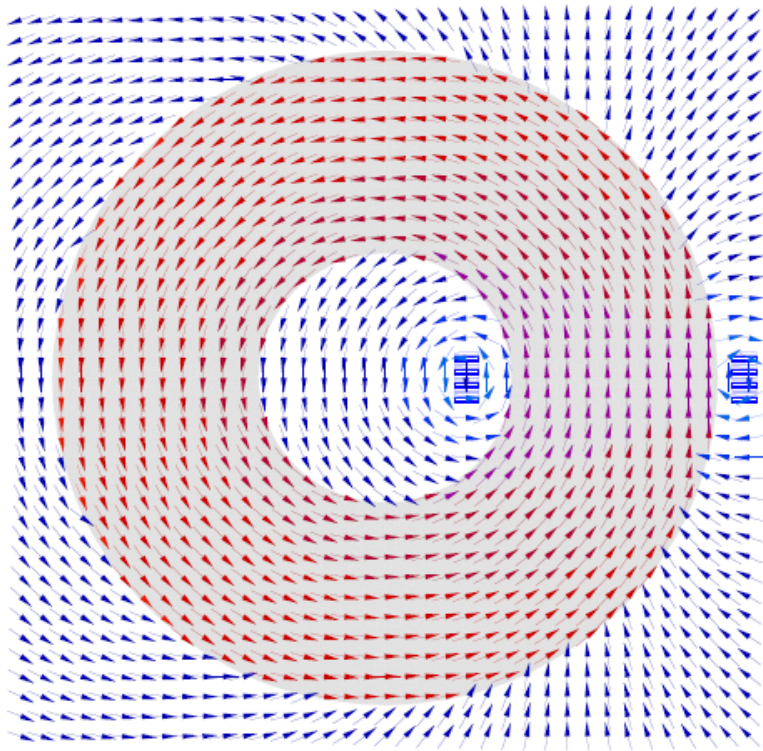


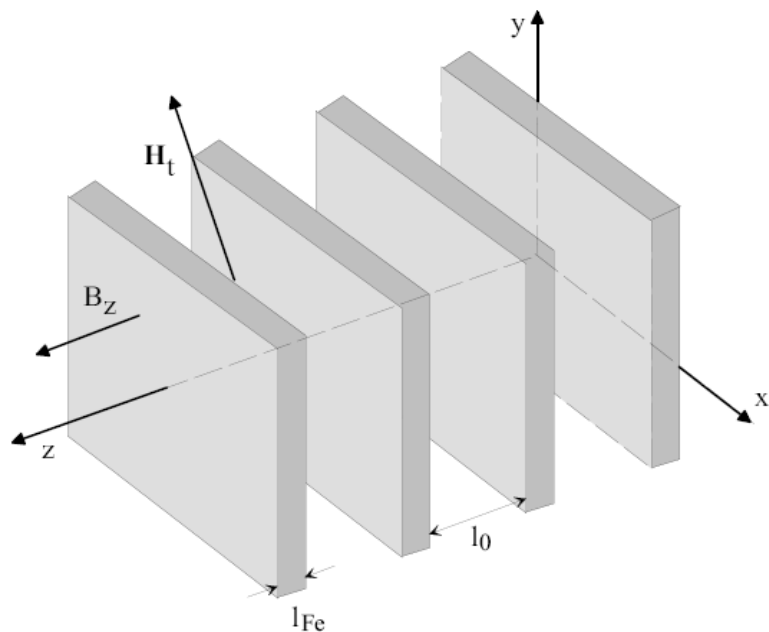
No surface currents:

$$\frac{\tan \alpha_1}{\tan \alpha_2} = \frac{\frac{B_{t1}}{B_{n1}}}{\frac{B_{t2}}{B_{n2}}} = \frac{\mu_1 H_{t1}}{\mu_2 H_{t2}} = \frac{\mu_1}{\mu_2}$$

$$\mu_2 \gg \mu_1$$

$$\alpha_1 \approx 0 \quad \text{or} \quad \alpha_2 \approx \pi/4$$





$$H_t^0 = H_t^{Fe} = \bar{H}_t$$

$$\bar{B}_t = \frac{1}{l_{Fe} + l_0} (l_{Fe} \mu \bar{H}_t + l_0 \mu_0 \bar{H}_t)$$

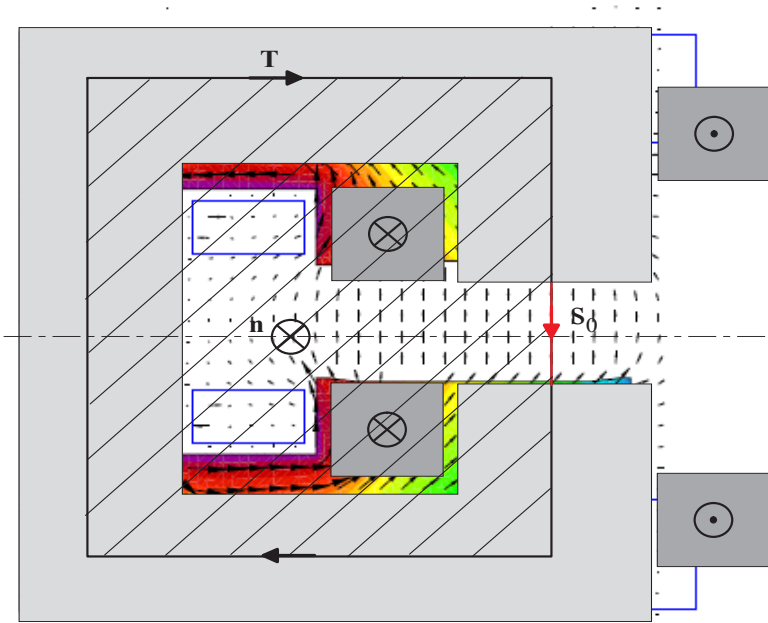
$$B_z^0 = B_z^{Fe} = \bar{B}_z$$

$$\bar{H}_z = \frac{1}{l_{Fe} + l_0} \left( l_{Fe} \frac{\bar{B}_z}{\mu} + l_0 \frac{\bar{B}_z}{\mu_0} \right)$$

$$\lambda = \frac{l_{Fe}}{l_{Fe} + l_0}$$

$$\bar{\mu}_t = \lambda \mu + (1 - \lambda) \mu_0$$

$$\bar{\mu}_z = \left( \frac{\lambda}{\mu} + \frac{1 - \lambda}{\mu_0} \right)^{-1}$$



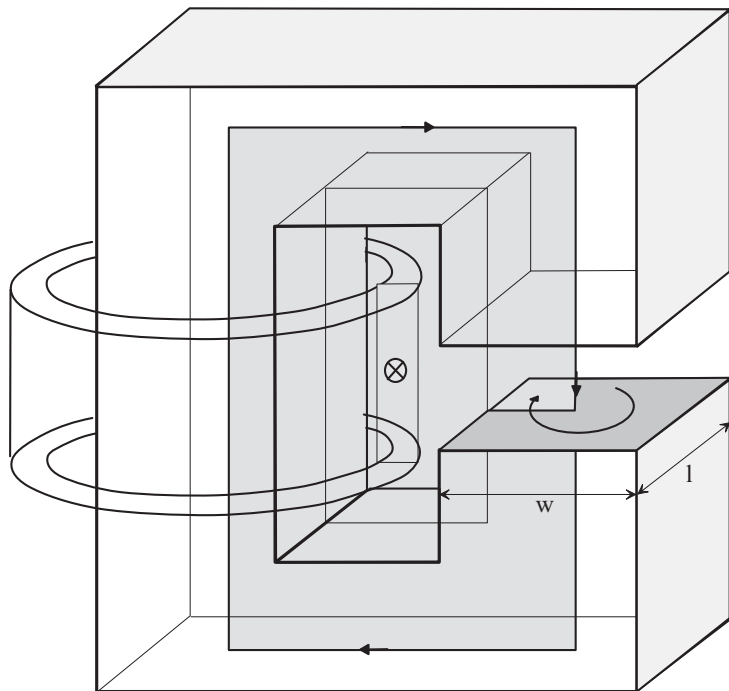
$$\int_{\partial a} \mathbf{H} \cdot d\mathbf{s} = \int_a \mathbf{J} \cdot d\mathbf{a}$$

$$\int_{\partial a} \mathbf{H} \cdot \mathbf{T} ds = \int_a \mathbf{J} \cdot \mathbf{n} da$$

$$H_i s_i + H_0 s_0 = N I$$

$$\frac{1}{\mu_0 \mu_r} B_i s_i + \frac{1}{\mu_0} B_0 s_0 = N I$$

$$B_0 = \frac{\mu_0 N I}{s_0}$$



$$\sum_{i=0}^n H_i s_i = N I$$

$$H_i = \frac{B_i}{\mu_i} = \frac{\Phi}{a_i \mu_i}$$

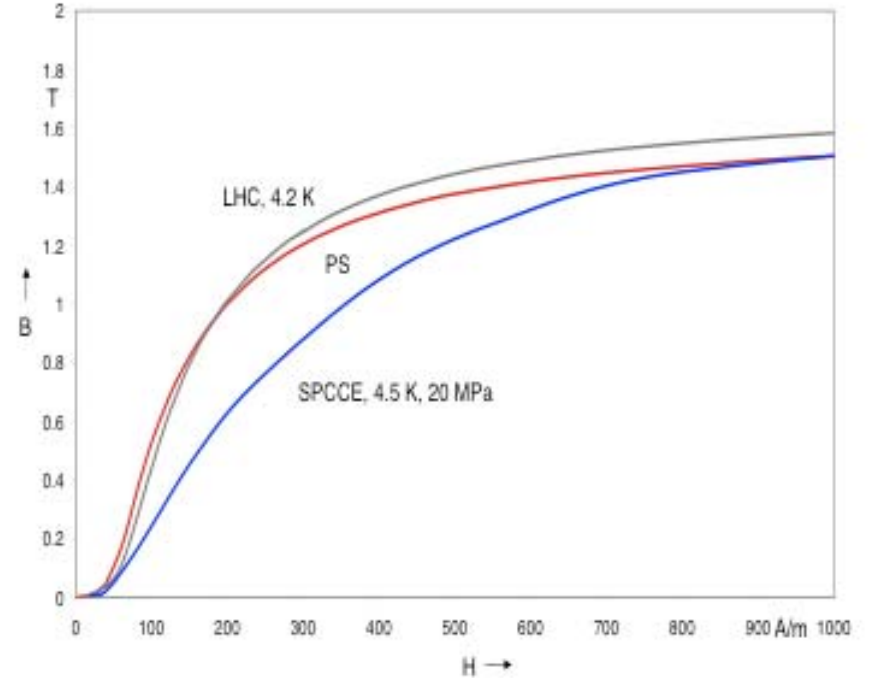
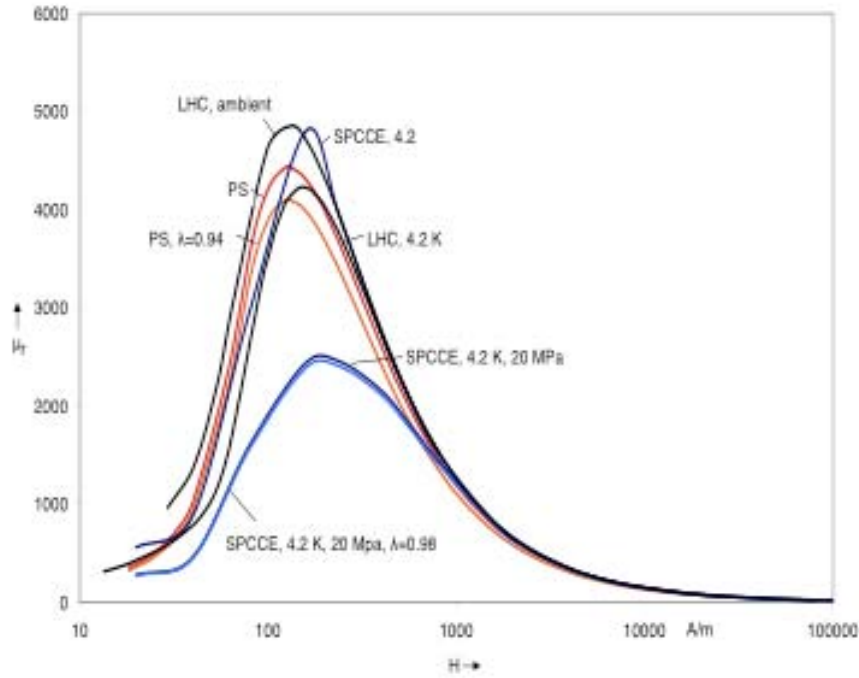
$$\Phi \sum_{i=0}^n \frac{s_i}{a_i \mu_i} = N I = V_m$$

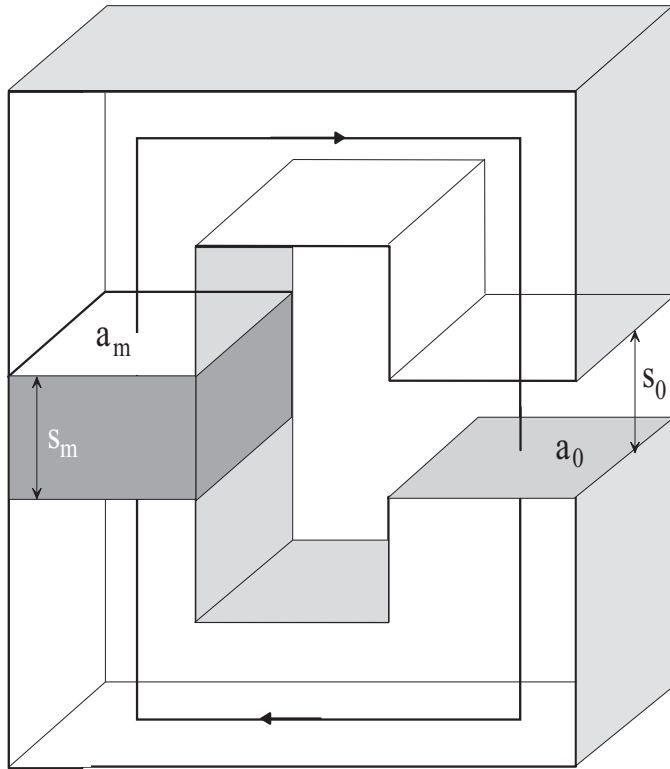
$$\text{Ohm's law: } I \sum_{i=0}^n \frac{s_i}{a_i \kappa_i} = U$$

$$N I = \Phi \sum_{i=0}^n \frac{s_i}{a_i \mu_i} = \Phi \left( \frac{s_0}{a_0 \mu_0} + \sum_{i=1}^n \frac{s_i}{a_i \mu_i} \right)$$

**Conclusion: Magnet with big air-gap is stabilized against variations in permeability**







$$H_0 s_0 + H_m s_m = 0$$

$$B_m a_m = B_0 a_0 = \mu_0 H_0 a_0$$

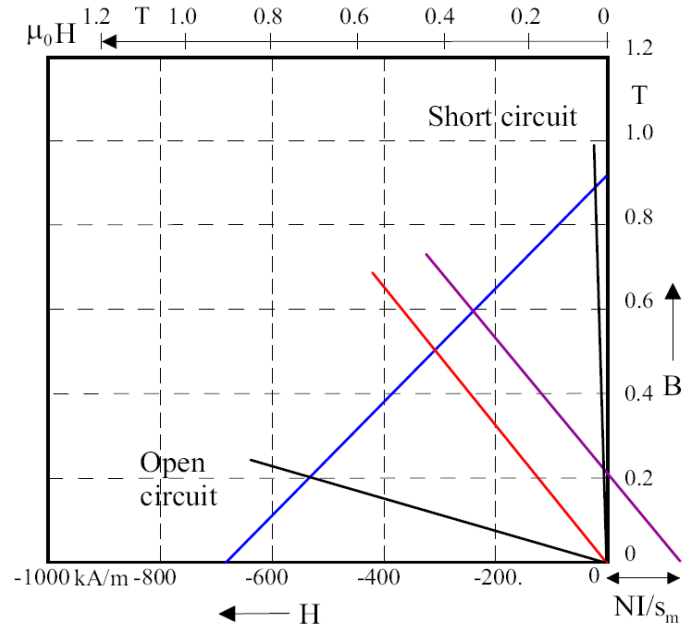
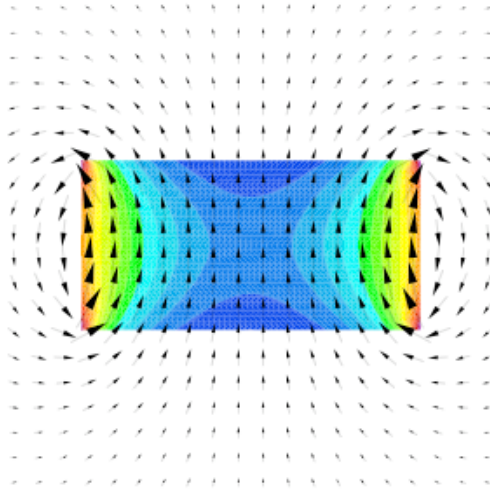
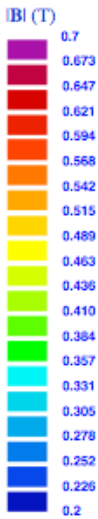
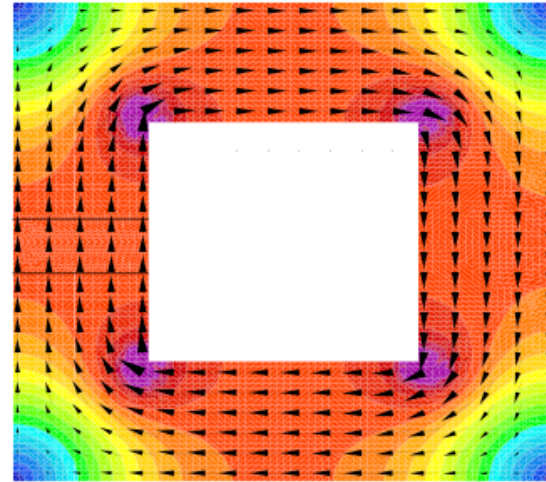
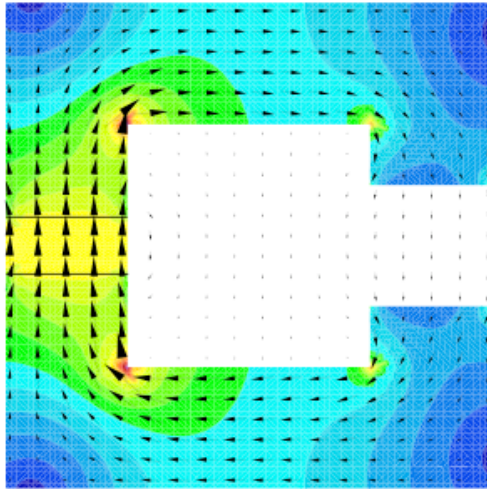
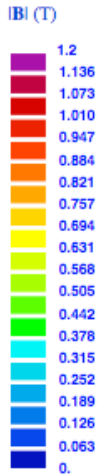
$$H_0 s_0 = -H_m s_m,$$

$$\frac{1}{\mu_0} B_m \frac{a_m}{a_0} s_0 = -H_m s_m,$$

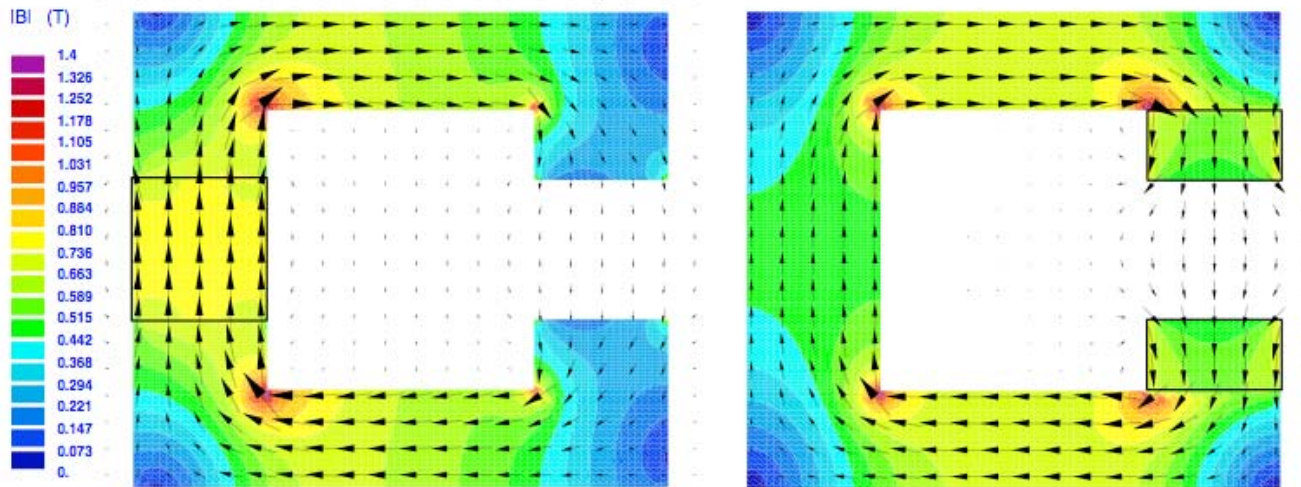
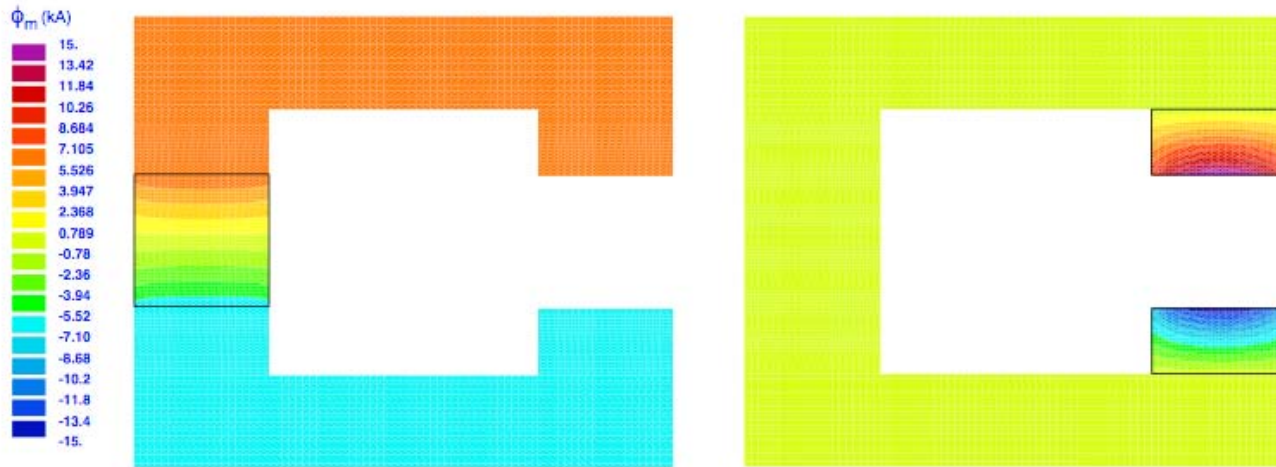
$$B_m = -\mu_0 \frac{s_m a_0}{s_0 a_m} H_m,$$

$$\frac{B_m}{\mu_0 H_m} = -\frac{s_m a_0}{s_0 a_m} = P$$

$$s = \frac{B_m}{H_m} = \mu_0 P = -\mu_0 \frac{s_m a_0}{s_0 a_m} = \mu_0 \frac{M(1-N)}{H_m - NM}$$

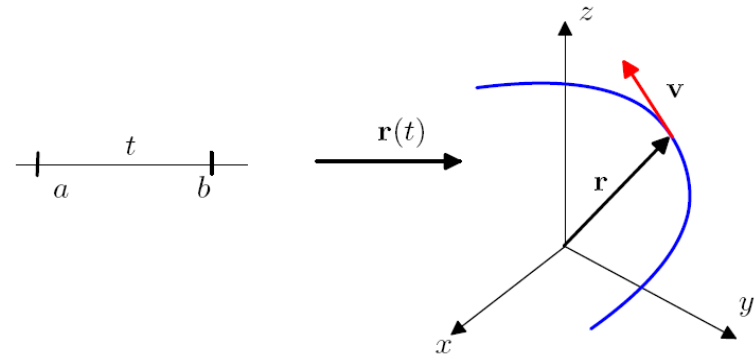


$$s = \frac{B_m}{H_m} = \mu_0 P = -\mu_0 \frac{s_m a_0}{s_0 a_m}$$



Space curve with  $\mathbf{r}(t) = (x(t), y(t), z(t))$   
 parametrized such that  $\mathbf{r}(0) = P$ .

1-smooth scalar field  $\phi : E_3 \rightarrow R : \mathbf{r} \mapsto \phi(\mathbf{r})$   
 expressed as  $\phi(x, y, z)$ , then  $\phi(\mathbf{r}(t))$  at  
 parameter (time)  $t$ .



$$\partial_{\mathbf{v}}\phi = \frac{\partial\phi}{\partial v} = \frac{d}{dt}[\phi(\mathbf{r} + t\mathbf{v})]_{t=0} = \lim_{t \rightarrow 0} \frac{\phi(\mathbf{r} + t\mathbf{v}) - \phi(\mathbf{r})}{t}$$

$$\partial_{\mathbf{e}_x}\phi = \frac{\partial\phi(x, y, z)}{\partial x} = \lim_{\Delta x \rightarrow 0} \frac{\phi(x + \Delta x, y, z) - \phi(x, y, z)}{\Delta x}$$

$$\partial_{\mathbf{v}}\phi = \frac{d}{dt}\phi(\mathbf{r}(t)) = \frac{\partial\phi}{\partial x} \frac{dx}{dt} + \frac{\partial\phi}{\partial y} \frac{dy}{dt} + \frac{\partial\phi}{\partial z} \frac{dz}{dt} = \text{grad } \phi \cdot \mathbf{v}$$

$$\text{grad } \phi = \frac{\partial\phi}{\partial x} \mathbf{e}_x + \frac{\partial\phi}{\partial y} \mathbf{e}_y + \frac{\partial\phi}{\partial z} \mathbf{e}_z$$

$$\nabla = \frac{\partial}{\partial x} \mathbf{e}_x + \frac{\partial}{\partial y} \mathbf{e}_y + \frac{\partial}{\partial z} \mathbf{e}_z$$

$$\Delta = \nabla^2 = \nabla \cdot \nabla = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

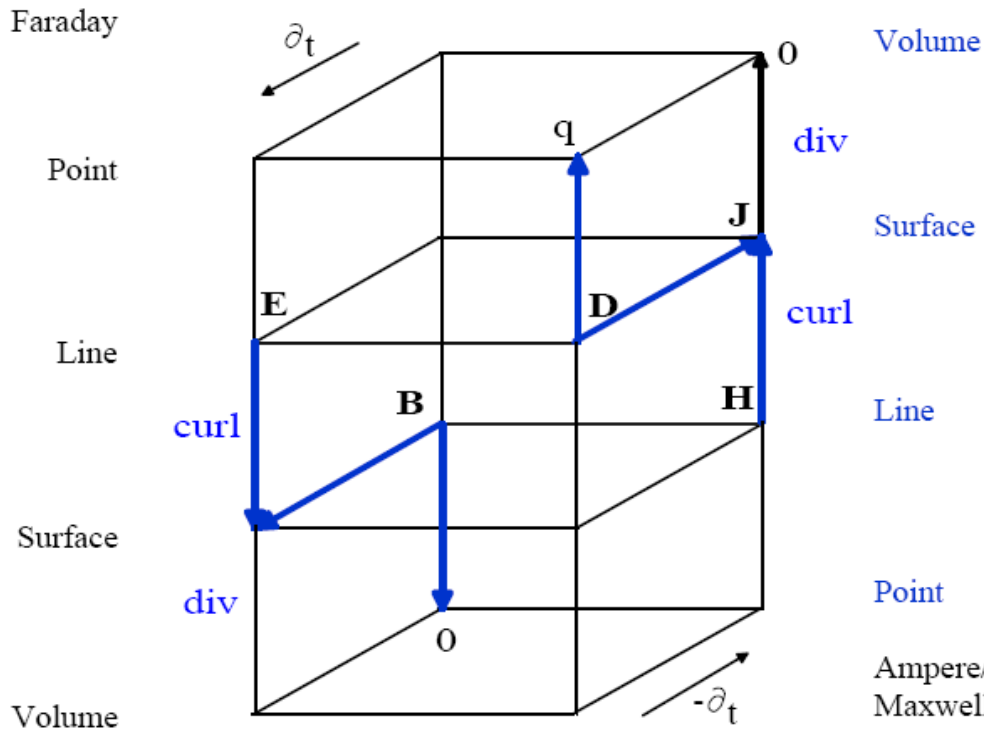
$$\nabla \phi = \text{grad } \phi = \frac{\partial \phi}{\partial x} \mathbf{e}_x + \frac{\partial \phi}{\partial y} \mathbf{e}_y + \frac{\partial \phi}{\partial z} \mathbf{e}_z$$

$$\nabla \cdot \mathbf{a} = \text{div } \mathbf{a} = \frac{\partial a_x}{\partial x} + \frac{\partial a_y}{\partial y} + \frac{\partial a_z}{\partial z}$$

$$\nabla \times \mathbf{a} = \text{curl } \mathbf{a} = \left( \frac{\partial a_z}{\partial y} - \frac{\partial a_y}{\partial z} \right) \mathbf{e}_x + \left( \frac{\partial a_x}{\partial z} - \frac{\partial a_z}{\partial x} \right) \mathbf{e}_y + \left( \frac{\partial a_y}{\partial x} - \frac{\partial a_x}{\partial y} \right) \mathbf{e}_z$$

$$\begin{aligned} \nabla^2 \mathbf{A} &= \left( \frac{\partial^2 A_x}{\partial x^2} + \frac{\partial^2 A_x}{\partial y^2} + \frac{\partial^2 A_x}{\partial z^2} \right) \mathbf{e}_x + \left( \frac{\partial^2 A_y}{\partial x^2} + \frac{\partial^2 A_y}{\partial y^2} + \frac{\partial^2 A_y}{\partial z^2} \right) \mathbf{e}_y + \\ &\left( \frac{\partial^2 A_z}{\partial x^2} + \frac{\partial^2 A_z}{\partial y^2} + \frac{\partial^2 A_z}{\partial z^2} \right) \mathbf{e}_z = (\nabla^2 A_x) \mathbf{e}_x + (\nabla^2 A_y) \mathbf{e}_y + (\nabla^2 A_z) \mathbf{e}_z \end{aligned}$$

**Conclusion: This is horrible, so let's try the geometric approach**



$$\mathbf{v} \cdot \text{grad } \phi = \lim_{s \rightarrow 0} \frac{\phi(P_2) - \phi(P_1)}{s}$$

$$\text{div } \mathbf{g} = \lim_{V \rightarrow 0} \frac{\int_{\partial V} \mathbf{g} \cdot d\mathbf{a}}{V}$$

$$\mathbf{n} \cdot \text{curl } \mathbf{g} = \lim_{a \rightarrow 0} \frac{\int_{\partial a} \mathbf{g} \cdot d\mathbf{s}}{a}$$

$$\int_a \text{curl} \vec{g} \cdot d\vec{a} = \int_{\partial a} \vec{g} \cdot d\vec{s}$$

$$\int_V \text{div} \vec{g} dV = \int_{\partial V} \vec{g} \cdot d\vec{a}$$

$$\int_{\partial a} \vec{H} \cdot d\vec{s} = \int_a \vec{J} \cdot d\vec{a} + \frac{d}{dt} \int_a \vec{D} \cdot d\vec{a}$$

$$\int_{\partial a} \vec{E} \cdot d\vec{s} = -\frac{d}{dt} \int_a \vec{B} \cdot d\vec{a}$$

$$\int_{\partial V} \vec{B} \cdot d\vec{a} = 0$$

$$\int_{\partial V} \vec{D} \cdot d\vec{a} = \int_V \rho dV$$

$$\int_a \text{curl} \vec{H} \cdot d\vec{a} = \int_a (\vec{J} + \frac{\partial}{\partial t} \vec{D}) \cdot d\vec{a}$$

$$\int_a \text{curl} \vec{E} \cdot d\vec{a} = -\int_a \frac{\partial}{\partial t} \vec{B} \cdot d\vec{a}$$

$$\int_V \text{div} \vec{B} dV = 0$$

$$\int_V \text{div} \vec{D} dV = \int_V \rho dV$$

$$\text{curl} \vec{H} = \vec{J} + \partial_t \vec{D}$$

$$\text{curl} \vec{E} = -\partial_t \vec{B}$$

$$\text{div} \vec{B} = 0$$

$$\text{div} \vec{D} = \rho$$



$$\int_V \operatorname{div} \operatorname{curl} \mathbf{g} dV = \int_{\partial V} \operatorname{curl} \mathbf{g} \cdot d\mathbf{a} = \int_{\partial(\partial V)} \mathbf{g} \cdot d\mathbf{s} = 0$$

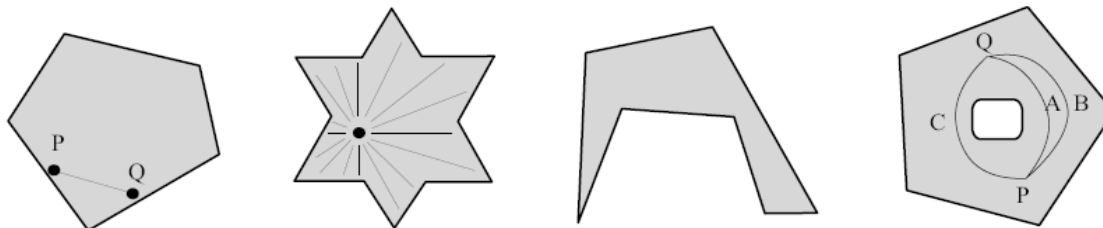
$$\int_a \operatorname{curl} \operatorname{grad} \phi \cdot d\mathbf{a} = \int_{\partial a} \operatorname{grad} \phi \cdot d\mathbf{s} = \phi|_{\partial(\partial a)} = 0$$

A curl free smooth vector field  $\mathbf{h} \in \mathcal{V}(\Omega)$  over an open star shaped domain  $\Omega \subset \mathbb{R}^3$  can always be expressed by a (smooth) scalar potential  $\phi \in \mathcal{S}(\Omega)$ .

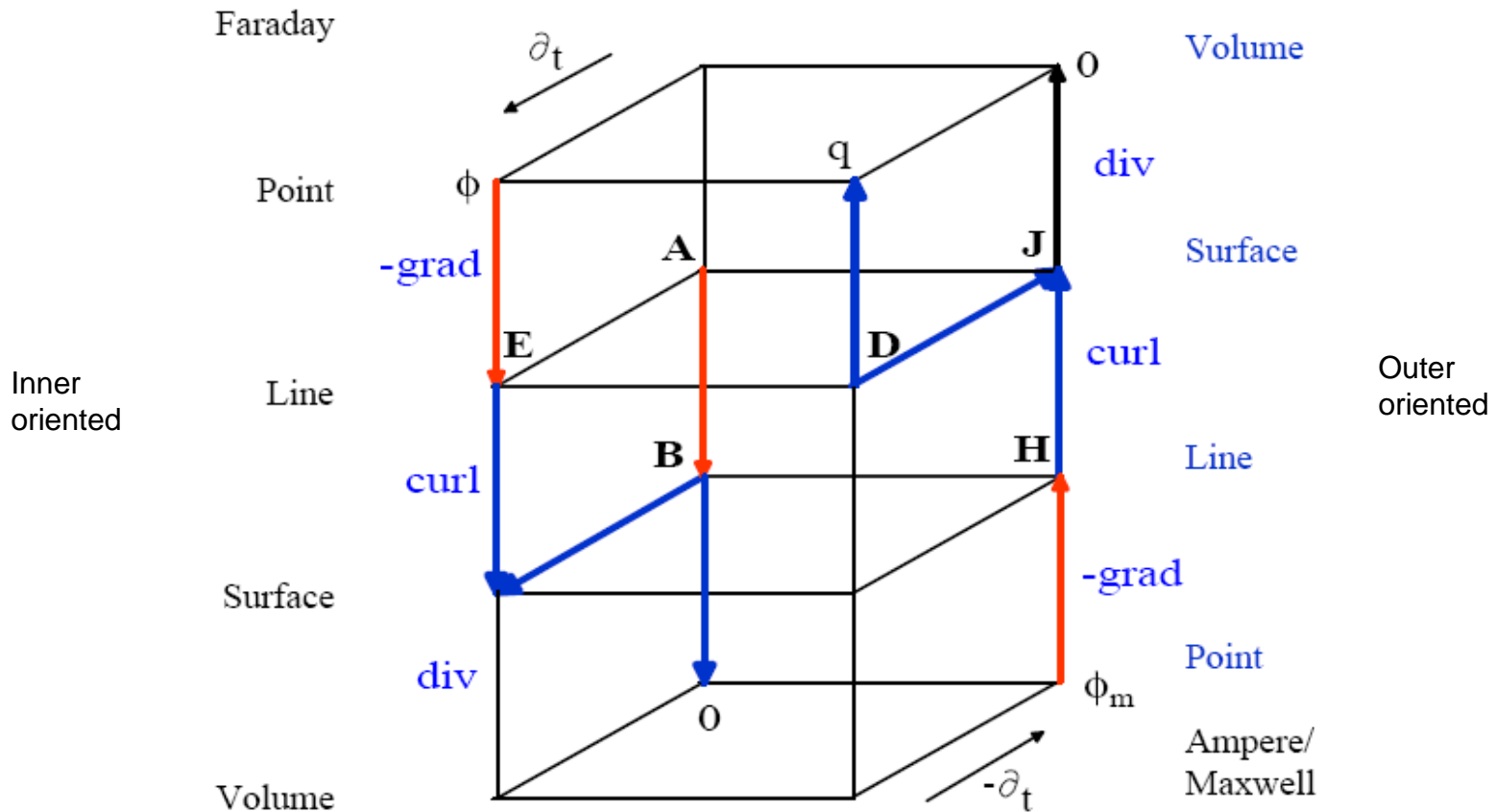
$$\operatorname{curl} \mathbf{h} = 0 \quad \rightarrow \quad \mathbf{h} = \operatorname{grad} \phi.$$

A source free, smooth vector field  $\mathbf{b} \in \mathcal{V}(\Omega)$  over an open star shaped domain  $\Omega \subset \mathbb{R}^3$  can always be expressed by a (smooth) vector potential  $\mathbf{a} \in \mathcal{V}(\Omega)$ .

$$\operatorname{div} \mathbf{b} = 0 \quad \rightarrow \quad \mathbf{b} = \operatorname{curl} \mathbf{a}.$$



In 3D: also connected boundaries

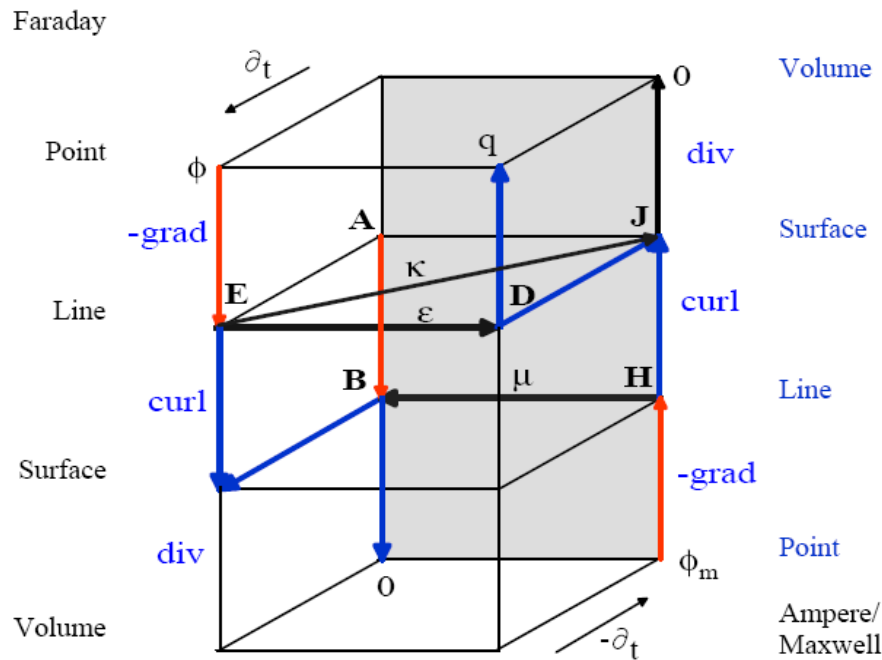


**Would be even more symmetric with magnetic monopoles**

$$\text{curl } \frac{1}{\mu} \text{curl } \mathbf{A} = \mathbf{J} \quad \frac{1}{\mu} \text{curl } \text{curl } \mathbf{A} = 0 \quad \nabla^2 \mathbf{A} - \text{grad } \text{div } \mathbf{A} = 0 \quad \nabla^2 A_z = 0$$

**Constant permeability and no sources**

**Only for Cartesian components**



$$\text{div } \mu \text{grad } \phi_m = 0 \quad \mu_0 \text{div } \text{grad } \phi_m = 0 \quad \nabla^2 \phi_m = 0$$

**No sources**

$$\nabla^2 A_z = -\mu_0 J_z \quad \text{in } \Omega_a \qquad \nabla^2 A_z = 0 \quad \text{in } \Omega_a, \mathbf{J} = 0$$

$$r^2 \frac{\partial^2 A_z}{\partial r^2} + r \frac{\partial A_z}{\partial r} + \frac{\partial^2 A_z}{\partial \varphi^2} = 0 \quad \text{in } \Omega_a, \mathbf{J} = 0$$

$$A_z = R(r)\phi(\varphi)$$

$$\begin{aligned} \downarrow \\ \frac{\partial A_z}{\partial r} &= \frac{\partial R(r)}{\partial r} \phi(\varphi), \\ \frac{\partial^2 A_z}{\partial r^2} &= \frac{\partial^2 R(r)}{\partial r^2} \phi(\varphi), \\ \frac{\partial^2 A_z}{\partial \varphi^2} &= \frac{\partial^2 \phi(\varphi)}{\partial \varphi^2} R(r). \end{aligned}$$

$$\underbrace{\frac{1}{R(r)} \left( r^2 \frac{\partial^2 R(r)}{\partial r^2} + r \frac{\partial R(r)}{\partial r} \right)}_{n^2} = \underbrace{-\frac{1}{\phi(\varphi)} \frac{\partial^2 \phi(\varphi)}{\partial \varphi^2}}_{n^2}$$

$$\begin{aligned} \downarrow \\ r^2 \frac{d^2 R(r)}{dr^2} + r \frac{dR(r)}{dr} - n^2 R(r) &= 0 \\ \frac{d^2 \phi(\varphi)}{d\varphi^2} + n^2 \phi(\varphi) &= 0 \end{aligned}$$

**How do you solve differential equations: Look them up in a book**

$$R(r) = \mathcal{E} r^n + \mathcal{F} r^{-n},$$

$$\phi(\varphi) = \mathcal{G} \sin n\varphi + \mathcal{H} \cos n\varphi.$$

$$\begin{aligned} A_z(r, \varphi) &= \sum_{n=1}^{\infty} (\mathcal{E}_n r^n + \mathcal{F}_n r^{-n}) (\mathcal{G}_n \sin n\varphi + \mathcal{H}_n \cos n\varphi) \\ &= \sum_{n=1}^{\infty} r^n (\mathcal{C}_n \sin n\varphi - \mathcal{D}_n \cos n\varphi) \end{aligned}$$

$$B_r(r, \varphi) = \frac{1}{r} \frac{\partial A_z}{\partial \varphi} = \sum_{n=1}^{\infty} n r^{n-1} (\mathcal{C}_n \cos n\varphi + \mathcal{D}_n \sin n\varphi),$$

$$B_\varphi(r, \varphi) = -\frac{\partial A_z}{\partial r} = -\sum_{n=1}^{\infty} n r^{n-1} (\mathcal{C}_n \sin n\varphi - \mathcal{D}_n \cos n\varphi).$$

**What have we won? If we know the field at a reference radius, we know it everywhere inside**

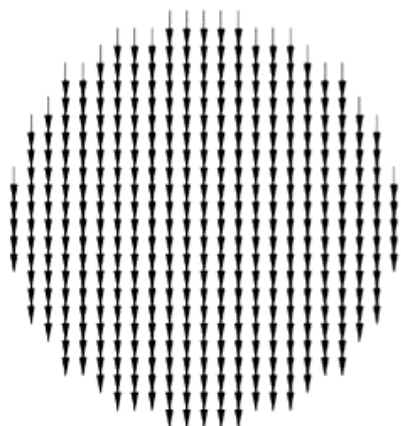
$$A_n = nr_0^{n-1}C_n \quad \text{and} \quad B_n = nr_0^{n-1}D_n$$

$$B_r(r_0, \varphi) = \sum_{n=1}^{\infty} (B_n \sin n\varphi + A_n \cos n\varphi) = B_N \sum_{n=1}^{\infty} (b_n \sin n\varphi + a_n \cos n\varphi)$$

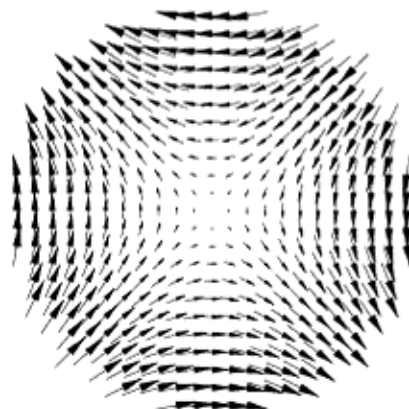
$$B_\varphi(r_0, \varphi) = \sum_{n=1}^{\infty} (B_n \cos n\varphi - A_n \sin n\varphi) = B_N \sum_{n=1}^{\infty} (b_n \cos n\varphi - a_n \sin n\varphi)$$

$$A_n(r_1) = \left(\frac{r_1}{r_0}\right)^{n-1} A_n(r_0), \quad B_n(r_1) = \left(\frac{r_1}{r_0}\right)^{n-1} B_n(r_0).$$

$$b_n(r_1) = \frac{B_n(r_1)}{B_N(r_1)} = \frac{\left(\frac{r_1}{r_0}\right)^{n-1} B_n(r_0)}{\left(\frac{r_1}{r_0}\right)^{N-1} B_N(r_0)} = \left(\frac{r_1}{r_0}\right)^{n-N} b_n(r_0),$$

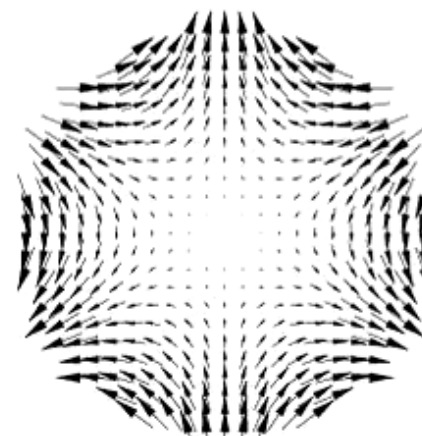


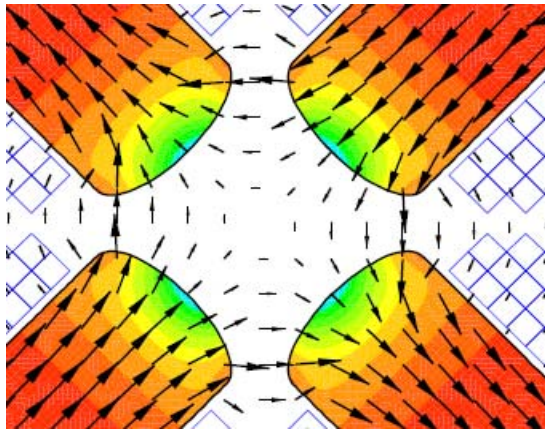
$$\begin{aligned}
 B_r &= C_1 \cos \varphi + \mathcal{D}_1 \sin \varphi \\
 B_\varphi &= -C_1 \sin \varphi + \mathcal{D}_1 \cos \varphi \\
 B_x &= C_1 \\
 B_y &= \mathcal{D}_1
 \end{aligned}$$



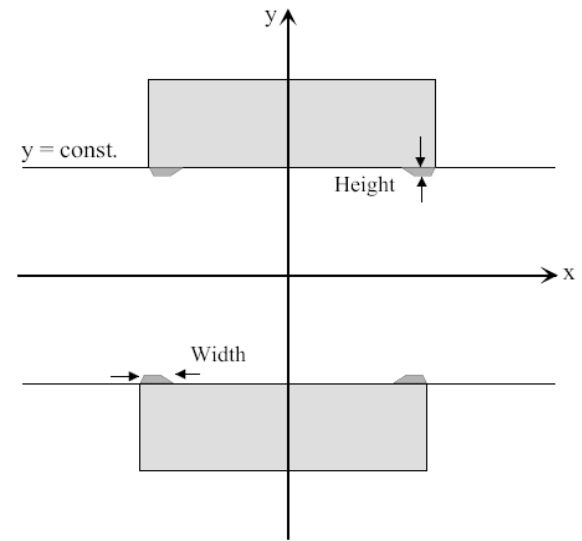
$$\begin{aligned}
 B_r &= 2C_2 r \cos 2\varphi + 2\mathcal{D}_2 r \sin 2\varphi \\
 B_\varphi &= -2C_2 r \sin 2\varphi + 2\mathcal{D}_2 r \cos 2\varphi \\
 B_x &= 2C_2 x + 2\mathcal{D}_2 y \\
 B_y &= -2C_2 y + 2\mathcal{D}_2 x
 \end{aligned}$$

$$\begin{aligned}
 B_r &= 3C_3 r^2 \cos 3\varphi + 3\mathcal{D}_3 r^2 \sin 3\varphi \\
 B_\varphi &= -3C_3 r^2 \sin 3\varphi + 3\mathcal{D}_3 r^2 \cos 3\varphi \\
 B_x &= 3C_3(x^2 - y^2) + 6\mathcal{D}_3 xy \\
 B_y &= -6C_3 xy + 3\mathcal{D}_3(x^2 - y^2)
 \end{aligned}$$

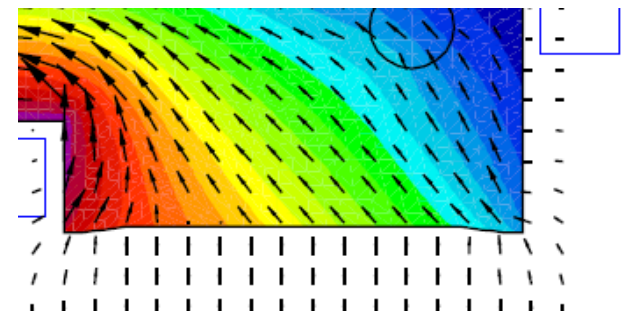
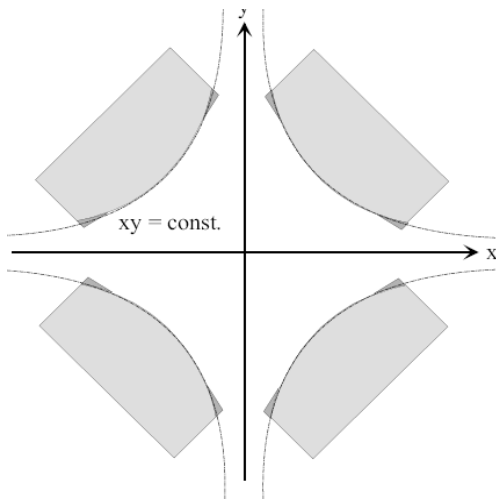




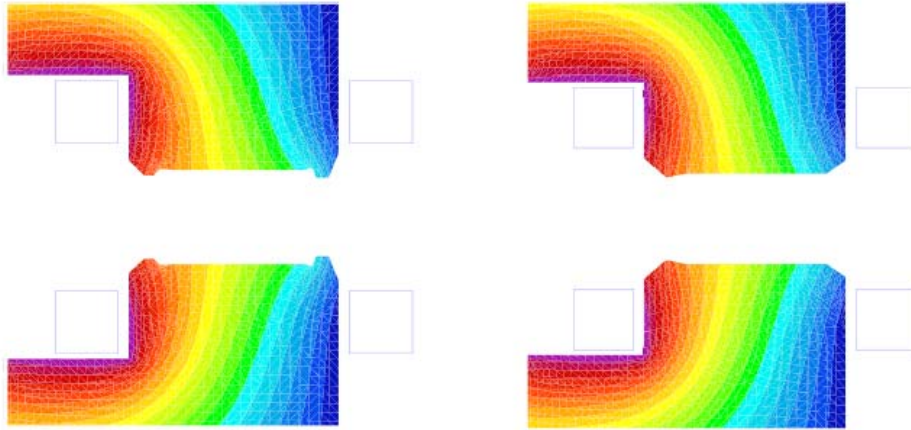
$$\phi_m = C_1 x + D_1 y$$



$$\phi_m = C_2(x^2 - y^2) + 2D_2xy$$

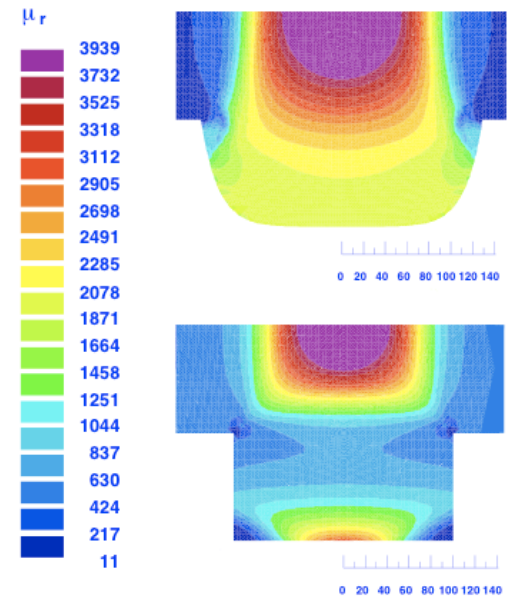
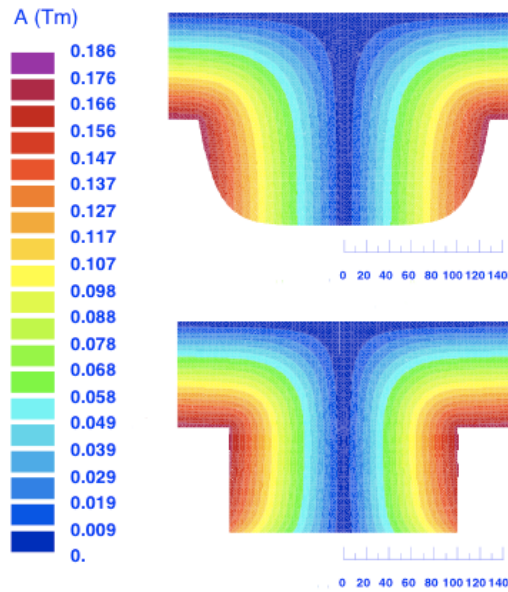






### Pole shimming

### Rogowski profiles



$$\nabla^2 \Phi_m(x, y, z) = \frac{\partial^2 \Phi_m(x, y, z)}{\partial x^2} + \frac{\partial^2 \Phi_m(x, y, z)}{\partial y^2} + \frac{\partial^2 \Phi_m(x, y, z)}{\partial z^2} = 0$$

$$\bar{\Phi}_m(x, y) = \int_{-z_0}^{z_0} \Phi_m(x, y, z) dz$$

$$\nabla^2 \bar{\Phi}_m(x, y) = \frac{\partial^2 \bar{\Phi}_m(x, y)}{\partial x^2} + \frac{\partial^2 \bar{\Phi}_m(x, y)}{\partial y^2} = 0$$

**Sufficient condition:** Integration path is extended far enough away from (into) the magnet so that the axial component of the field has dropped to zero.

$$\frac{\partial^2 \bar{\Phi}_m}{\partial x^2} + \frac{\partial^2 \bar{\Phi}_m}{\partial y^2} = \int_{-z_0}^{z_0} \left( \frac{\partial^2 \Phi_m}{\partial x^2} + \frac{\partial^2 \Phi_m}{\partial y^2} \right) dz = \int_{-z_0}^{z_0} \left( -\frac{\partial^2 \Phi_m}{\partial z^2} \right) dz = -\frac{\partial \Phi_m}{\partial z} \Big|_{-z_0}^{z_0} = H_z|_{-z_0} - H_z|_{z_0}$$

**Caution:** Always use long measurement coils, or don't apply the scaling laws