

# Computational Methods in Accelerator Physics

## An introduction (1)

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([http://cern.ch/Werner.Herr/lectures/baden\\_comp1.pdf](http://cern.ch/Werner.Herr/lectures/baden_comp1.pdf))



# Where are computational methods needed ?



## Studies of Beam Dynamics

- Design and simulation of an accelerator
- Control and operation



- (
- Design of accelerator equipment
  - Magnets, RF cavities ...
  - Vacuum components, cryogenics
- )



# Steps of accelerator design

- Definition of basic parameters according to requirements
- Design of machine layout and optics
- Analysis of its (local and global) properties, evaluation of performance
- Stability of beams:
  - Single particle stability
  - Multi particle behaviour
- Process may be iterative



# Accelerator design with an optics program

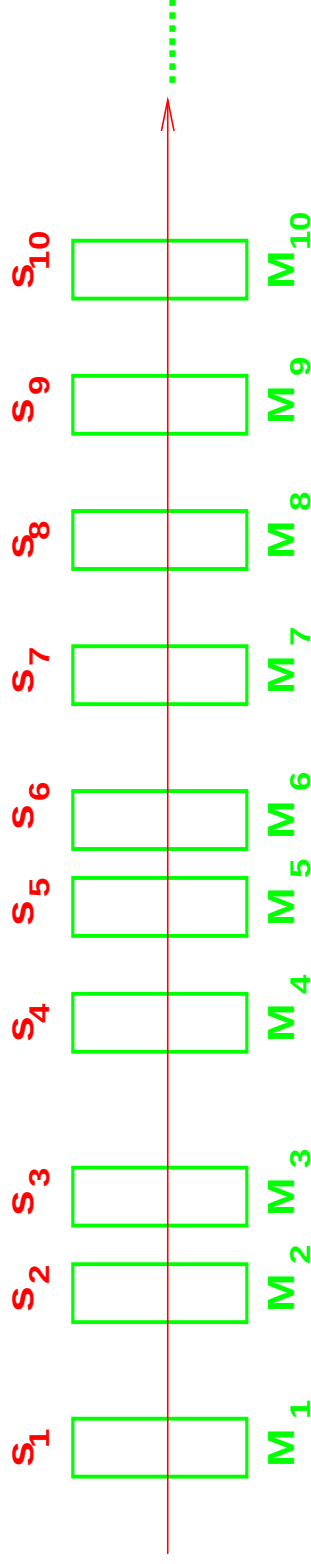
- It needs: Description of machine in standard format
- It does: Optics calculations
  - Linear and non-linear optics computations
  - Linear corrections
  - Non-linear and chromatic corrections
- Parameter matching



# How does an **accelerator** look like to a computer ?

- Basically as it looks like to a particle:

- ➡ A (finite) sequence of machine elements  $\mathcal{M}$  at longitudinal positions  $s_1, s_2, s_3, \dots$ :

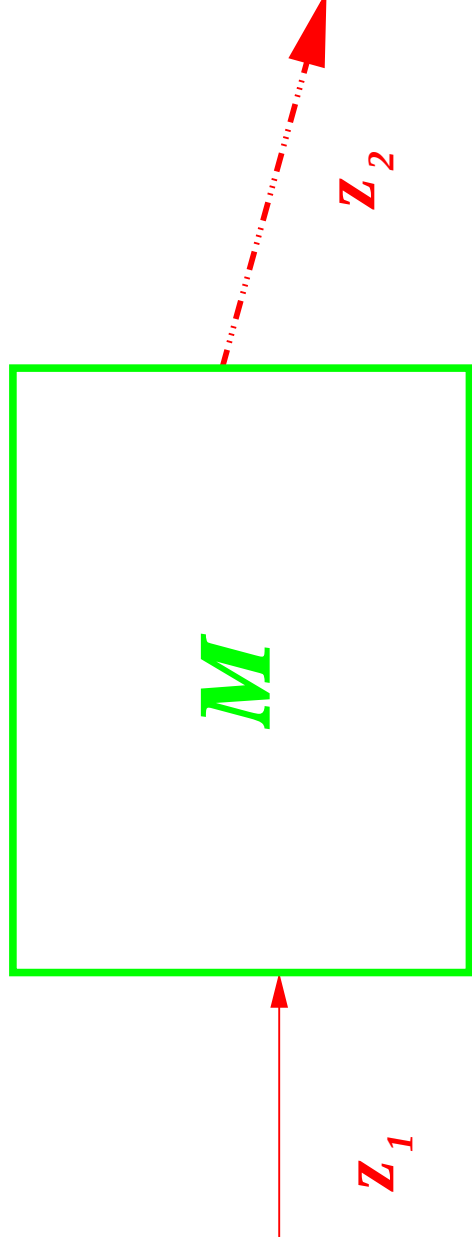


- All elements together make the ring or a beam line



# How does an element look like to a computer ?

- Each element  $\mathcal{M}$  acts on the beam in a deterministic way



- In general:  $\vec{z}_2 \neq \vec{z}_1$



# What is $\mathcal{M}$ ? It can represent:

- A single machine element
- magnet: dipole, quadrupole
- vacuum chamber
- collimators
- RF cavity
- monitors
- drift
- .....



## It can also represent:

- Several machine elements combined, (i.e. part of a ring made of **n** elements:  $\mathcal{M}_{part}$ )

$$\mathcal{M}_{part} = \mathcal{M}_1 \circ \mathcal{M}_2 \circ \dots \circ \mathcal{M}_n$$

- The whole machine (e.g. complete turn in a ring with **N** elements,  $\mathcal{M}_{ring}$ )

$$\mathcal{M}_{ring} = \mathcal{M}_1 \circ \mathcal{M}_2 \circ \dots \circ \mathcal{M}_N$$

- Many turns in a ring ( $\mathbf{M} = \mathcal{M}_{ring}^n$ )





# How is an **element** described to a computer ?

- Let  $\vec{z}_1, \vec{z}_2$  describe a quantity (coordinates, beam sizes ...) before and after the element
- Take an machine element (e.g. magnet) and build a mathematical object  $\mathcal{M}$  for this quantity
  - $\mathcal{M}$  describes the element in terms of **this** quantity
  - In general:  $\vec{z}_2 = \mathcal{M} \circ \vec{z}_1$
  - $\mathcal{M}$  is a so-called **MAP**
- All MAPS connect the pieces together to make a ring (or beam line)



# MAPS transform coordinates through an element

- 4 coordinates needed for 2 dimensions (off momentum effects ignored)

- Coordinate vector:  $\vec{z} = (x, x' = \frac{\delta x}{\delta s}, y, y' = \frac{\delta y}{\delta s})$

- $\mathcal{M}$  transforms the coordinates  $\vec{z}_1(s_1)$  at position  $s_1$  to new coordinates  $\vec{z}_2(s_2)$  at position  $s_2$ :

$$\vec{z}_2(s_2) = \mathcal{M} \circ \begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_2} = \mathcal{M} \circ \begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_1} = \vec{z}_1(s_1)$$

... or OPTICAL functions

■ 6 optical functions needed for 2 dimensions:

$$\vec{\nu}_2(s_2) = \begin{pmatrix} \beta_x \\ \alpha_x \\ \gamma_x \\ \beta_y \\ \alpha_y \\ \gamma_y \end{pmatrix}^{s_2} = \mathcal{M} \circ \begin{pmatrix} \beta_x \\ \alpha_x \\ \gamma_x \\ \beta_y \\ \alpha_y \\ \gamma_y \end{pmatrix}^{s_1} = \mathcal{M} \circ \vec{\nu}_1(s_1)$$

## How does $\mathcal{M}$ look like ?

The map  $\mathcal{M}$  describes **local** properties of a machine element and can be:

- A simple linear matrix or transformation
- High order integration algorithm
- Derived from **local** Hamiltonian
- A computer program, subroutine etc.
- Any "description" to go from  $\vec{z}_1$  to  $\vec{z}_2$
- Can in principle be **VERY** abstract !



# Simple examples (linear, one dimensional)

(Matrix formulation for **linear**\* elements)

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_2} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} \circ \begin{pmatrix} x \\ x' \end{pmatrix}_{s_1}$$

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{s_2} = \begin{pmatrix} m_{11}^2 & -2m_{11}m_{12} & m_{12}^2 \\ -m_{11}m_{21} & m_{11}m_{22} + m_{12}m_{21} & -m_{12}m_{22} \\ m_{21}^2 & -2m_{21}m_{22} & m_{22}^2 \end{pmatrix} \circ \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{s_1}$$

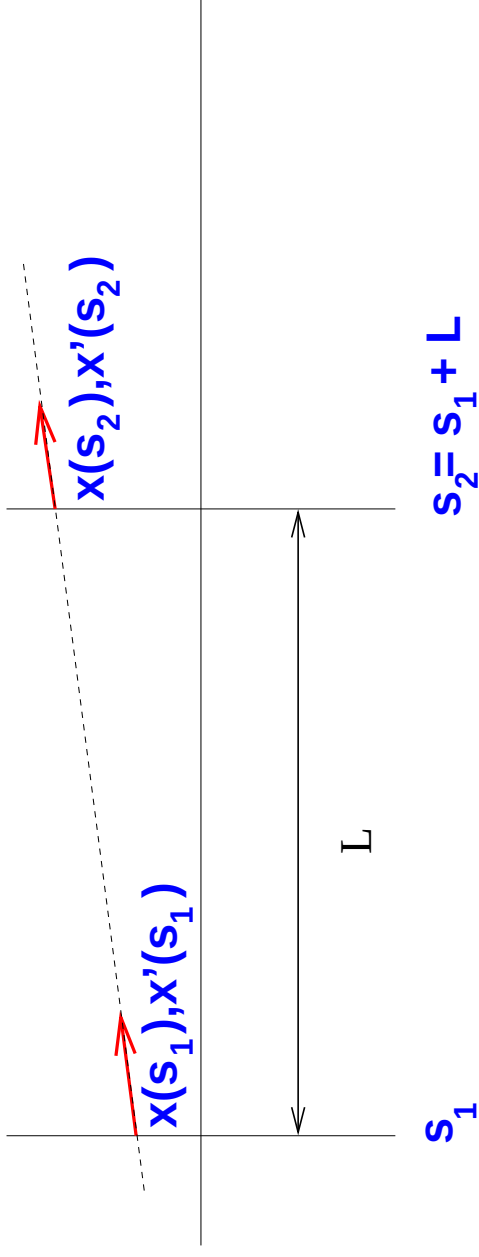
→ The maps become so-called transport matrices

\* Its effect depends on  $x$  or  $x'$  only or is constant



# Transformation of coordinates (one dimension)

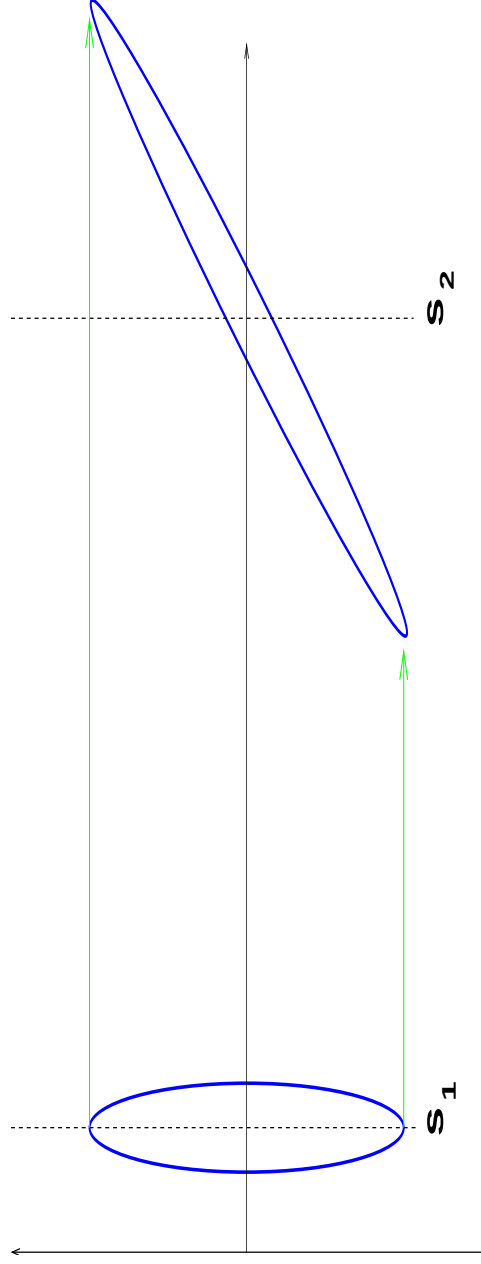
Drift space of length  $L = s_2 - s_1$ :



$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_2} = \begin{pmatrix} x \\ x' \end{pmatrix}_{s_1} + \begin{pmatrix} x' \cdot L \\ 0 \end{pmatrix}_{s_1} = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix}_{s_1} \circ \begin{pmatrix} x \\ x' \end{pmatrix}_{s_1}$$

# Transformation of beam ellipse

Drift space of length  $L = s_2 - s_1$ :



$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{s_2} = \begin{pmatrix} 1 & -2L & L^2 \\ 0 & 1 & -L \\ 0 & 0 & 1 \end{pmatrix} \circ \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{s_1} = \begin{pmatrix} \beta_0 - 2L\alpha_0 + L^2\gamma_0 \\ \alpha_0 - L\gamma_0 \\ \gamma_0 \end{pmatrix}_{s_2}$$


## Simple examples (one dimensional)

Focusing quadrupole of length  $L$  and strength  $K$ :

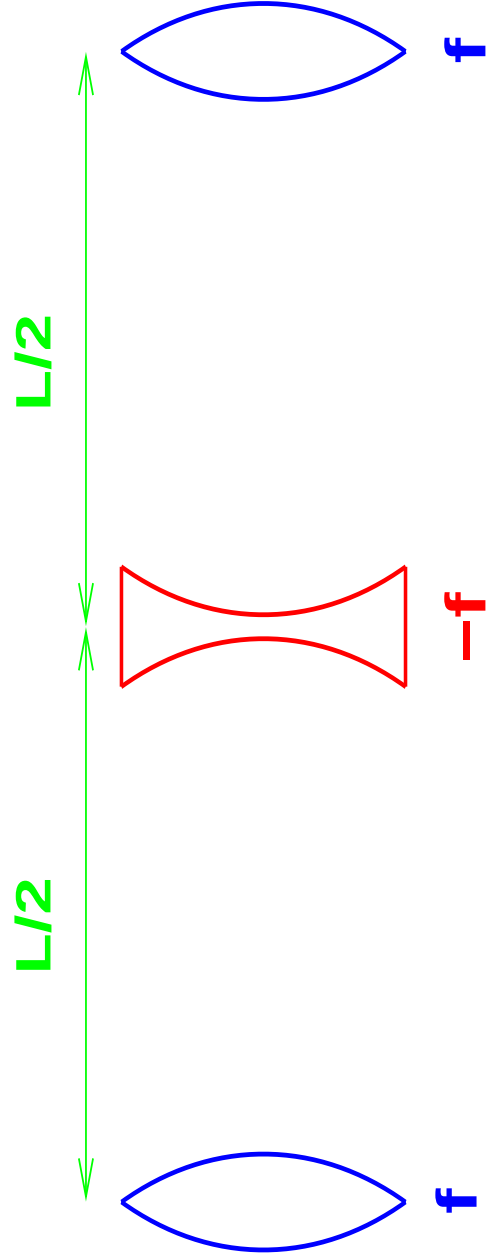
$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_2} = \begin{pmatrix} \cos(L \cdot K) & \frac{1}{K} \cdot \sin(L \cdot K) \\ K \cdot \sin(L \cdot K) & \cos(L \cdot K) \end{pmatrix} \circ \begin{pmatrix} x \\ x' \end{pmatrix}_{s_1}$$

Quadrupole with short length  $L$  (i.e.:  $1 \gg L^2 \cdot K^2$ )

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_2} = \begin{pmatrix} 1 & 0 \\ K^2 \cdot L (= -\frac{1}{f}) & 1 \end{pmatrix} \circ \begin{pmatrix} x \\ x' \end{pmatrix}_{s_1}$$



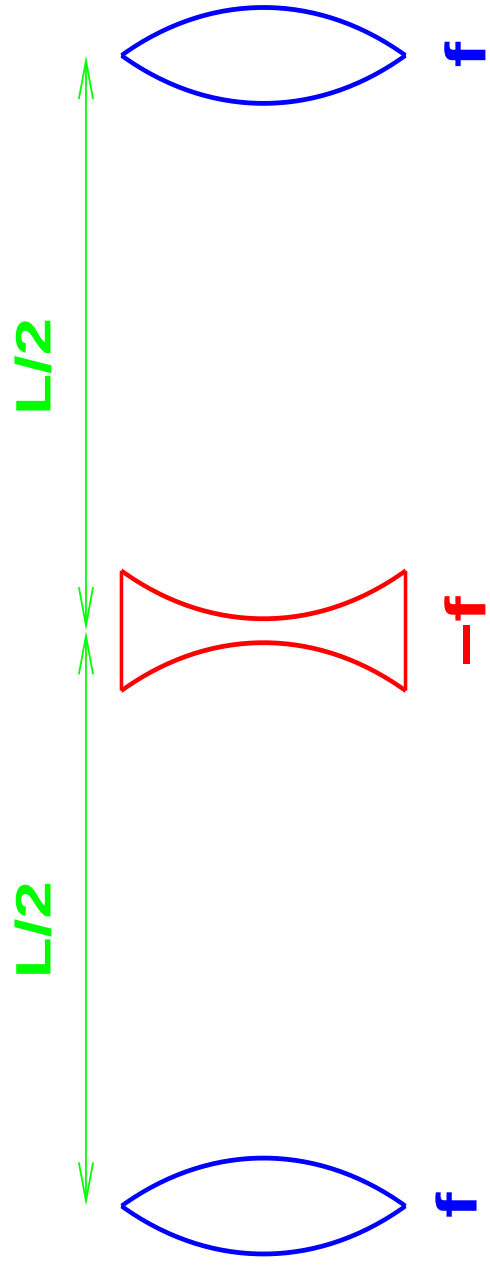
# Composition of elements (FODO cell)



$$\mathcal{M}_{cell} = \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{pmatrix} \circ \begin{pmatrix} 1 & L/2 \\ 0 & 1 \end{pmatrix} \circ \begin{pmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{pmatrix} \circ \begin{pmatrix} 1 & L/2 \\ 0 & 1 \end{pmatrix}$$



# Composition of elements (FODO cell)



$$\mathcal{M}_{cell} = \begin{pmatrix} 1 + \frac{L}{2f} & L + \frac{L^2}{4f} \\ -\frac{L}{2f^2} & 1 - \frac{L}{2f} - \frac{L^2}{4f^2} \end{pmatrix}$$



# Computer program for optics calculation

- It reads the sequence of elements of a machine (their order, their positions ..)
- It reads properties of the elements, i.e. type (dipole, quadrupole, drift ...)
- It reads strength of the elements
- It sets up the maps (matrices)
- An example is Methodical Accelerator Design (from CERN) but there are many more !



# Simplest machine description (MAD format)

```
// description of elements and their strengths
// dipoles and quadrupoles only ...
    mb: dipole,    l=6.0, angle=0.03570;
    qf: quadrupole, l=3.0, k1= 0.013426;
    qd: quadrupole, l=3.0, k1=-0.013426;

// centre position of elements in the ring
start:    at=0;
qf.1: qf, at=1.5000e+00;
mb: mb,   at=9.0000e+00;
mb: mb,   at=1.9000e+01;
qd.1: qd, at=2.6500e+01;
mb: mb,   at=3.4000e+01;
mb: mb,   at=4.4000e+01;
qf.2: qf, at=5.1500e+01;
...
end:      at=2.2000e+03;
```

→ Construct a MAP for each element from this data

## The next step

Set up a sequence of MAPS:

$\mathcal{M}_1$  [QUADRUPOLE, L=3.0, STR=K1, START=0.0]  
 $\mathcal{M}_2$  [DRIFT, L=3.0, START=3.0]  
 $\mathcal{M}_3$  [DIPOLE, L=6.0, STR=ANGLE, START=6.0]  
 $\mathcal{M}_4$  [DRIFT, L=4.0, START=12.0]  
 $\mathcal{M}_5$  [DIPOLE, L=6.0, STR=ANGLE, START=16.0]  
 $\mathcal{M}_6$  [DRIFT, L=3.0, START=22.0]  
 $\mathcal{M}_7$  [QUADRUPOLE, L=3.0, STR=-K1, START=25.0]  
 $\mathcal{M}_8$  [DRIFT, L=3.0, START=28.0]  
 $\mathcal{M}_9$  [DIPOLE, L=6.0, STR=ANGLE, START=31.0]  
 $\mathcal{M}_{10}$  [DRIFT, L=4.0, START=37.0]  
 $\mathcal{M}_{11}$  [DIPOLE, L=6.0, STR=ANGLE, START=41.0]  
....

## Putting the ”pieces” together

Starting from a position  $s_0$  and applying all maps (for  $N$  elements) in sequence around a ring with circumference  $C$  to get the **One-Turn-Map** (OTM) for the position  $s_0$  (for one dimension only):

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_0 + C} = \mathcal{M}_1 \circ \mathcal{M}_2 \circ \dots \circ \mathcal{M}_N \circ \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

$$\Rightarrow \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0 + C} = \mathcal{M}_{ring}(s_0) \circ \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$



## Putting the "pieces" together

If **all** maps are matrices (i.e. only linear elements)

→ Always true in the first step !

→ The One-Turn-Map is a MATRIX:

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_0 + C} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} \circ \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

→ After all multiplications we get the One-Turn-Map which depends on the starting point  $s_0$ .



# The analysis of the results

What can we do with the One-Turn-Matrix ?

We can express the One-Turn-Matrix  $\mathcal{M}_{ring}(s_0)$  in terms of Courant-Snyder parameters:

We know that  $\mathcal{M}_{ring}(s_0)$  for one dimension must be:

$$\mathcal{M}_{ring}(s_0) \equiv \begin{pmatrix} \cos \mu + \alpha(s_0) \sin \mu & \beta(s_0) \sin \mu \\ -\gamma(s_0) \sin \mu & \cos \mu - \alpha(s_0) \sin \mu \end{pmatrix}$$

and we also know that (for a ring):

$$\alpha(s_0 + C) \equiv \alpha(s_0), \quad \beta(s_0 + C) \equiv \beta(s_0), \quad \gamma(s_0 + C) \equiv \gamma(s_0)$$





# The first optics calculations

Comparison of:

$$\begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} = \mathcal{M}_1 \circ \mathcal{M}_2 \circ \dots \circ \mathcal{M}_N$$

and :

$$\mathcal{M}_{ring}(s_0) = \begin{pmatrix} \cos \mu + \alpha(s_0) \sin \mu & \beta(s_0) \sin \mu \\ -\gamma(s_0) \sin \mu & \cos \mu - \alpha(s_0) \sin \mu \end{pmatrix}$$

gives optical functions at position  $s_0$ :

- $\beta(s_0), \alpha(s_0), \gamma(s_0)$  (depend on position  $s_0$ )
- $\mu$  is independent of  $s_0$ :  $(2\pi Q)$



## We have now:

- Values for  $\beta_x, \beta_y, \alpha_x, \dots$  etc. at the position  $s_0$
- Tunes for both planes

## The next step:

- Starting from initial optical (Twiss) functions at  $s_0$ , transforming  $\beta_x, \beta_y, \alpha_x, \dots$  through the lattice gives functions at all positions  $s$ .
- Question: what are the  $\beta$ -functions etc. of a linear accelerator or a beam line ???



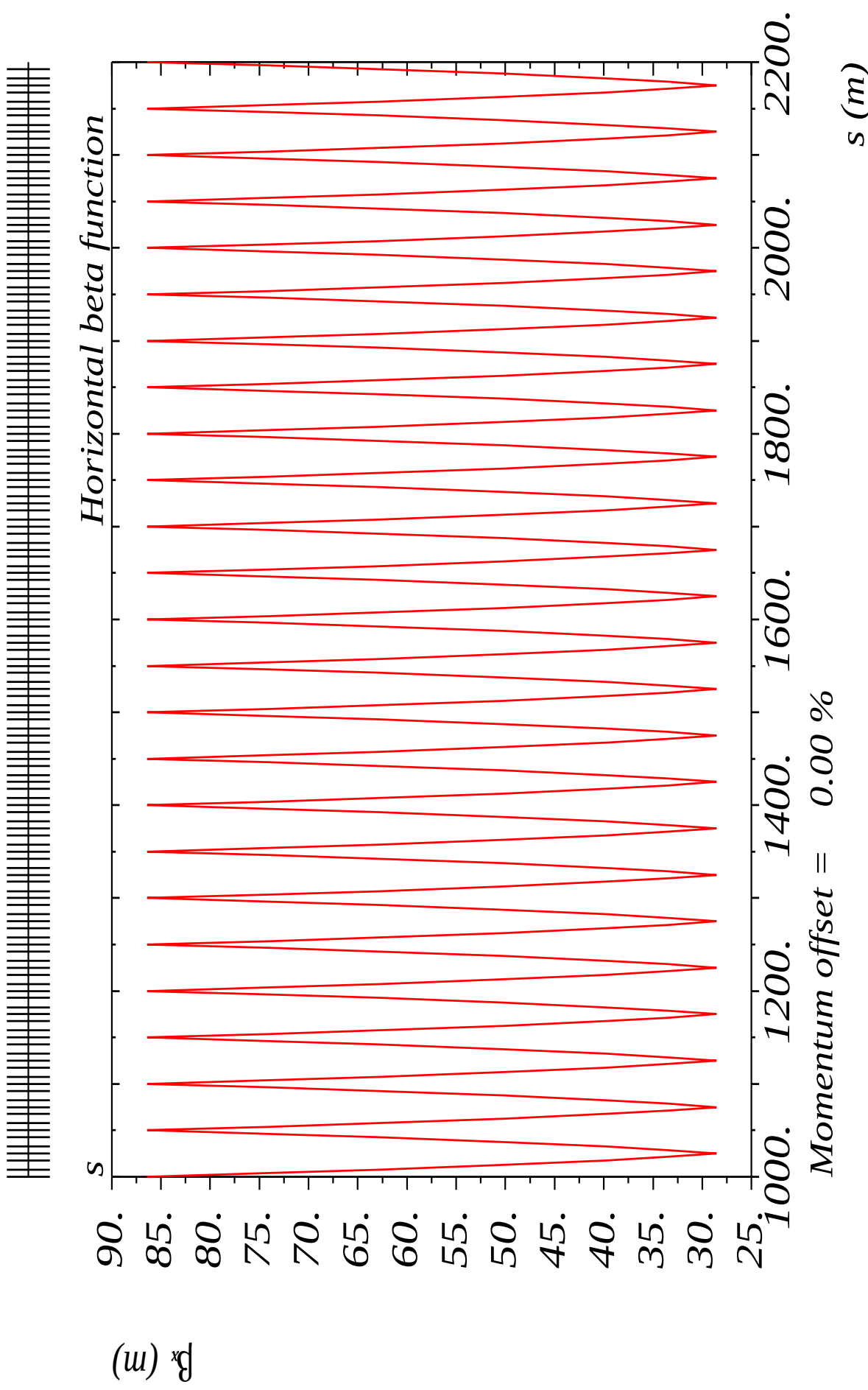
# Computation of optical functions around the ring

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} m_{11}^2 & -2m_{11}m_{12} & m_{12}^2 \\ -m_{11}m_{21} & m_{11}m_{22} + m_{12}m_{21} & -m_{12}m_{22} \\ m_{21}^2 & -2m_{21}m_{22} & m_{22}^2 \end{pmatrix} \circ \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{s_0}$$

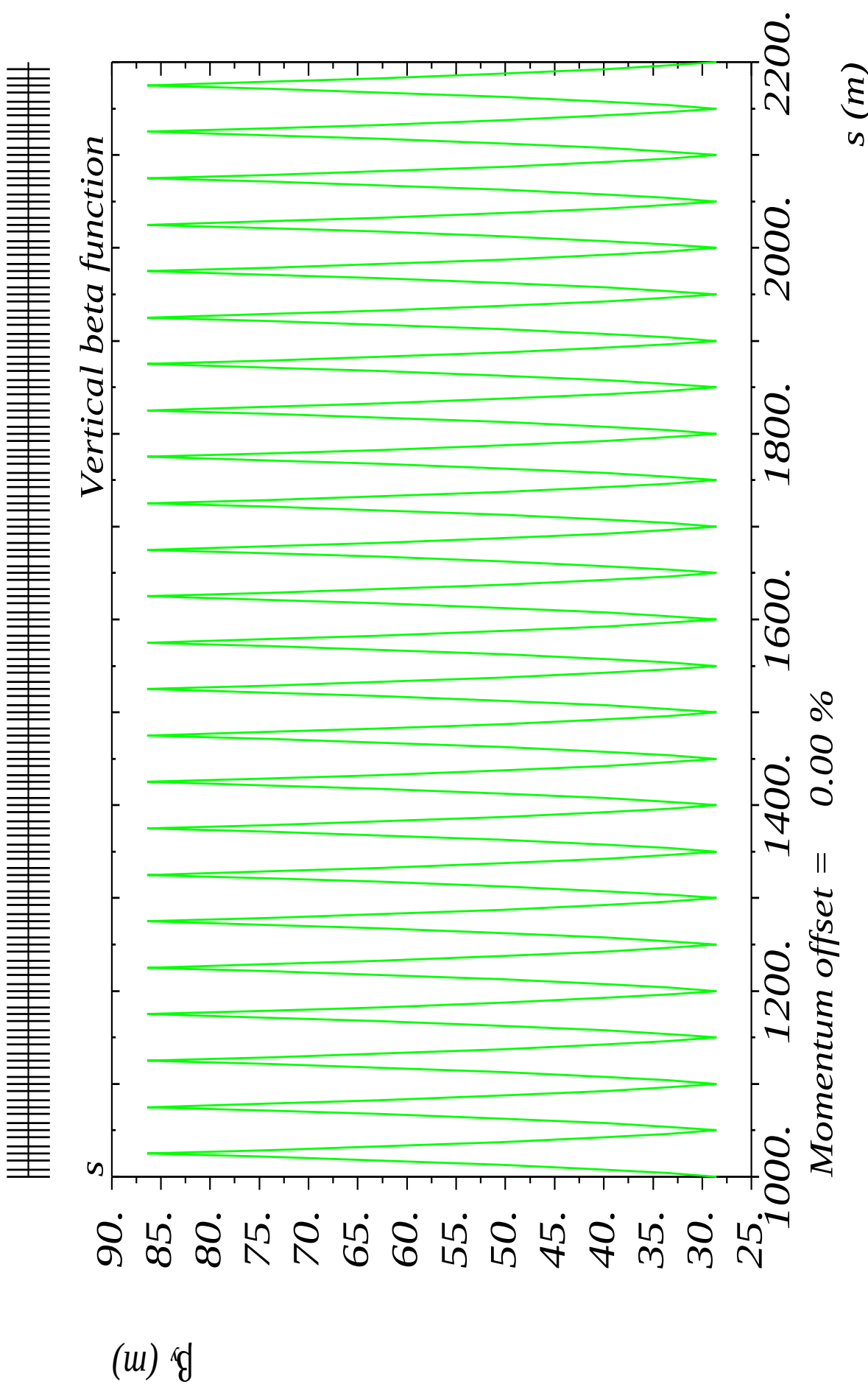
Successive application of matrices give Twiss functions at each element around the ring and at each position  $s \rightarrow$



# Optical functions (horizontal $\beta$ ):



# Optical functions (vertical $\beta$ ):



# Why do I spend so much time on $\mathcal{M}_{ring}$ ?

- Because it is very useful:
- Courant-Snyder ansatz (formalism) assumes motion is linearly stable, periodic, confined, and has a closed orbit.
- The OTM  $\mathcal{M}_{ring}$  contains all information about global behaviour in the ring, i.e. stability, tune,  $\beta$ , closed orbit etc.
- No need for assumptions



# Why do I spend so much time on $\mathcal{M}_{ring}$ ?

- $\mathcal{M}_{ring}$  or  $\mathcal{M}_{part}$  allow the analysis of imperfections (and their correction !)
- ”Straightforward” to formally extend it to complicated (e.g. non-linear) problems - additional tools and concepts needed (invariants, fixpoints, normal forms etc.)



## (Interlude I: Fixed Points)

- Certain points in phase space  $\vec{z}_1$  repeat itself after  $n$  completed turns

$$\mathcal{M}_{ring}^n \circ \vec{z}_1 = \vec{z}_2 \equiv \vec{z}_1$$

- Defines a **Fixed Point** of order  $n$
- Fixed Point of order **1** is the **closed orbit**
- Stability requires existence of such a fixed point
- Closed orbit is found (or not !) in optics programs by searching for the first order fixed point





## Extension to two dimensions

- Can be written as separate equations, or:
- Extend vectors for coordinates or optical parameters
- Extend transfer maps/matrices

$$\begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_2} = \begin{pmatrix} m_{11} & m_{12} & 0 & 0 \\ m_{21} & m_{22} & 0 & 0 \\ 0 & 0 & m_{33} & m_{34} \\ 0 & 0 & m_{43} & m_{44} \end{pmatrix} \circ \begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_1}$$



# Extension to two dimensions

■ The horizontal and vertical motion can be coupled:

➡ Additional elements in matrix

$$\begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_2} = \begin{pmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{pmatrix} \circ \begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_1}$$



## Off momentum effects

- Introduces longitudinal motion and off momentum trajectories

Strength  $k$  of element modified by non-zero  $\frac{\Delta p}{p}$ :

$$k \Rightarrow k / (1 + \frac{\Delta p}{p})$$

- Closed orbit and tune are usually different for non-zero  $\frac{\Delta p}{p}$

→ Dispersion

→ Chromatic effects



# Going to three dimensions

Formally extended by adding two new variables:

$\Delta s = c\Delta t$ : longitudinal displacement with respect to reference particle

$\frac{\Delta p}{p}$ : relative momentum difference with respect to reference particle

$$\begin{pmatrix} x \\ x' \\ y \\ y' \\ c\Delta t \\ \frac{\Delta p}{p} \end{pmatrix}_{s_2} = \begin{pmatrix} m_{11} & m_{12} & m_{13} & m_{14} & m_{15} & m_{16} \\ m_{21} & m_{22} & m_{23} & m_{24} & m_{25} & m_{26} \\ m_{32} & m_{32} & m_{33} & m_{34} & m_{35} & m_{36} \\ m_{42} & m_{42} & m_{43} & m_{44} & m_{45} & m_{46} \\ m_{32} & m_{32} & m_{33} & m_{34} & m_{55} & m_{56} \\ m_{62} & m_{62} & m_{63} & m_{64} & m_{65} & m_{66} \end{pmatrix} \begin{pmatrix} x \\ x' \\ y \\ y' \\ c\Delta t \\ \frac{\Delta p}{p} \end{pmatrix}_{s_1}$$

## (Interlude II: Symplecticity)

- Not all possible maps are allowed !
- Requires for a matrix  $\mathcal{M} \xrightarrow{\text{purple}} \mathcal{M}^t \cdot \mathcal{S} \cdot \mathcal{M} = \mathcal{S}$

with:

$$\mathcal{S} = \begin{pmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{pmatrix}$$

- It basically means:  $\mathcal{M}$  is area preserving and

$$\lim_{n \rightarrow \infty} \mathcal{M}^n = \text{finite}$$



## Introducing non-linear elements

Effect of a (short) quadrupole depends **linearly** on amplitude (re-written from the matrix form):

$$\begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_2} = \begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_1} + \begin{pmatrix} 0 \\ k_1 \cdot x_{s_1} \\ 0 \\ k_1 \cdot y_{s_1} \end{pmatrix}$$

→  $\vec{z}(s_2) = \mathbf{M} \cdot \vec{z}(s_1)$

→  $\mathbf{M}$  is a matrix



# Non-linear elements (e.g. sextupole)

Effect of a (thin) sextupole with strength  $k_2$  is:

$$\begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_2} = \begin{pmatrix} x \\ x' \\ y \\ y' \end{pmatrix}_{s_1} + \begin{pmatrix} 0 \\ k_2 \cdot (x_{s_1} \cdot y_{s_1}) \\ 0 \\ \frac{1}{2}k_2 \cdot (x_{s_1}^2 - y_{s_1}^2) \end{pmatrix}$$

→  $\vec{z}(s_2) = \mathcal{M} \circ \vec{z}(s_1)$

→  $\mathcal{M}$  is **not** a matrix, i.e. cannot be expressed by matrix multiplication



# Non-linear elements

Cannot be written in linear matrix form !  
We need something like:

$$\begin{aligned} x = & R_{11} \cdot x + R_{12} \cdot x' + \\ & + T_{111} \cdot x^2 + T_{112} \cdot xx' + T_{122} \cdot x'^2 + \\ & + T_{113} \cdot xy + T_{114} \cdot xy' + \dots \\ & + \dots \end{aligned}$$

and the equivalent for all other variables ...





## Higher order MAPS:

Definition of a **second** order map  $\mathcal{A}_2$  (Taylor expansion):

Let's call it :  $\mathcal{A}_2 = [R, T]$ , defined as (for :  $j = 1 \dots 4$ ) :

$$z_j(s_2) = \sum_{k=1}^4 R_{jk} z_k(s_1) + \sum_{k=1}^4 \sum_{l=1}^4 T_{jkl} z_k(s_1) z_l(s_1)$$

Higher orders can be defined as needed ...

$$\mathcal{A}_3 = [R, T, U] \quad \Longrightarrow \quad \sum_{k=1}^4 \sum_{l=1}^4 \sum_{m=1}^4 U_{jklm} z_k(s_1) z_l(s_1) z_m(s_1)$$



## Second order MAPS composition:

Assume now 2 maps of second order:

$$\mathcal{A}_2 = [R^A, T^A] \quad \text{and} \quad \mathcal{B}_2 = [R^B, T^B]$$

the combined second order map

$$\mathcal{C}_2 = \mathcal{A}_2 \circ \mathcal{B}_2 \quad \text{is} \quad \mathcal{C}_2 = [R^C, T^C] \quad \text{with:}$$

$$R^C = R^A \cdot R^B$$

and (after truncation of higher order terms !!):

$$T_{ijk}^C = \sum_{l=1}^4 R_{il}^B T_{ljk}^A + \sum_{l=1}^4 \sum_{m=1}^4 T_{ilm}^B R_{lj}^A R_{mk}^A$$



## (Interlude II: Symplecticity)

- Not all possible maps are allowed !
- Requires for a matrix  $\mathcal{M} \xrightarrow{\text{purple}} \mathcal{M}^t \cdot \mathcal{S} \cdot \mathcal{M} = \mathcal{S}$

with:

$$\mathcal{S} = \begin{pmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{pmatrix}$$

- It basically means:  $\mathcal{M}$  is area preserving and

$$\lim_{n \rightarrow \infty} \mathcal{M}^n = \text{finite}$$



# Symplecticity for higher order MAPS

- Truncated Taylor expansions are not matrices !!
- It is the associated Jacobian matrix  $\mathcal{J}$  which must fulfil the symplecticity condition:

$$\mathcal{J}_{ik} = \frac{\delta z_2^i}{\delta z_1^k}$$

$$\mathcal{J} \text{ must fulfil: } \mathcal{J}^t \cdot \mathcal{S} \cdot \mathcal{J} = \mathcal{S}$$

- In general:  $\mathcal{J}_{ik} \neq \text{const}$   $\rightarrow$  for truncated Taylor map can be difficult to fulfil for all  $z$



## (Interlude III: Other higher order MAPS)

There are other types of higher order maps:

- Lie transformations (always symplectic for any order, ideal for tracking, easy to analyse)
- Symplectic integration algorithms
- whatever ...

→ Intermediate level school ... !



# Matching optical functions

- Modify machine optics to get desired properties around the machine or in specific places
- For example you may want special conditions
  - for equipment: RF, collimators, diagnostics
  - for experiments: in colliding beam machines
- Algorithms to adjust parameters and layout
  - This process is called MATCHING !
  - Available in most optics programs (for lines and circular machines)



# Matching optical functions

In general:  $\vec{\nu}(\beta_x(s), \alpha_x(s) \dots) = f(\mathcal{M}_1, \mathcal{M}_2, \dots, \mathcal{M}_n)$   
optical functions depend on **all** maps, i.e. strengths and layout.

- Matching can change all parameters (strengths, positions ...)
- Additional constraints may be:
  - Tunes, chromaticities
  - Hardware parameters
  - $\hat{\beta}_x$ , etc.

## Example: matching of tunes Q (MAD language)

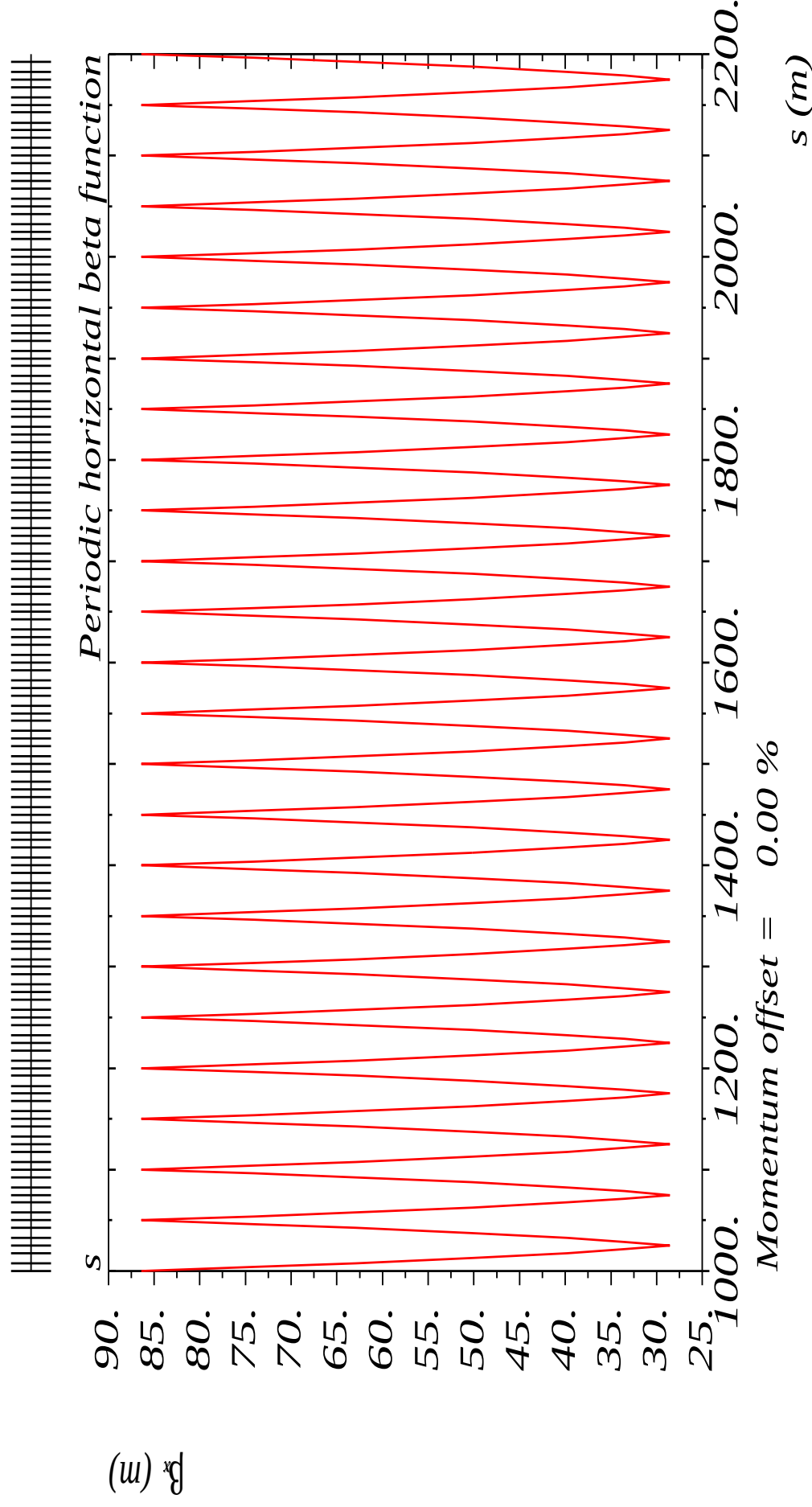
```
match;  
    vary,name=kqf, step=0.00001;  
    vary,name=kqd, step=0.00001;  
    global,QX=7.420;  
    global,QY=7.380;  
endmatch;
```

- The strengths of main quadrupoles are varied
- Computes the new strengths



# Local adjustment of optical functions

■ Small  $\beta_x$  needed for an experiment



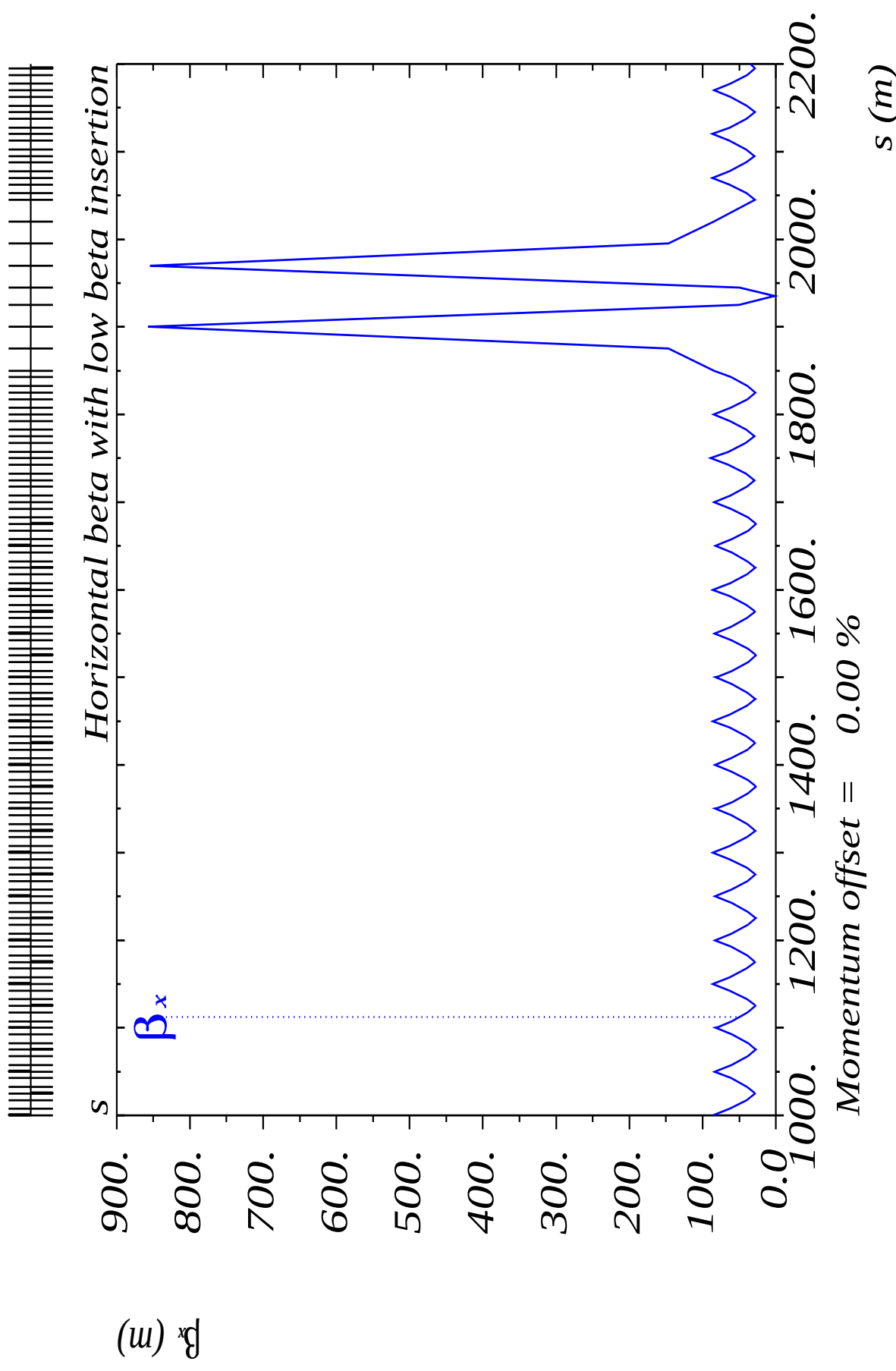
## Example: matching of $\beta$ -functions (MAD language - simplified !)

- Allow a few quadrupoles to be changed

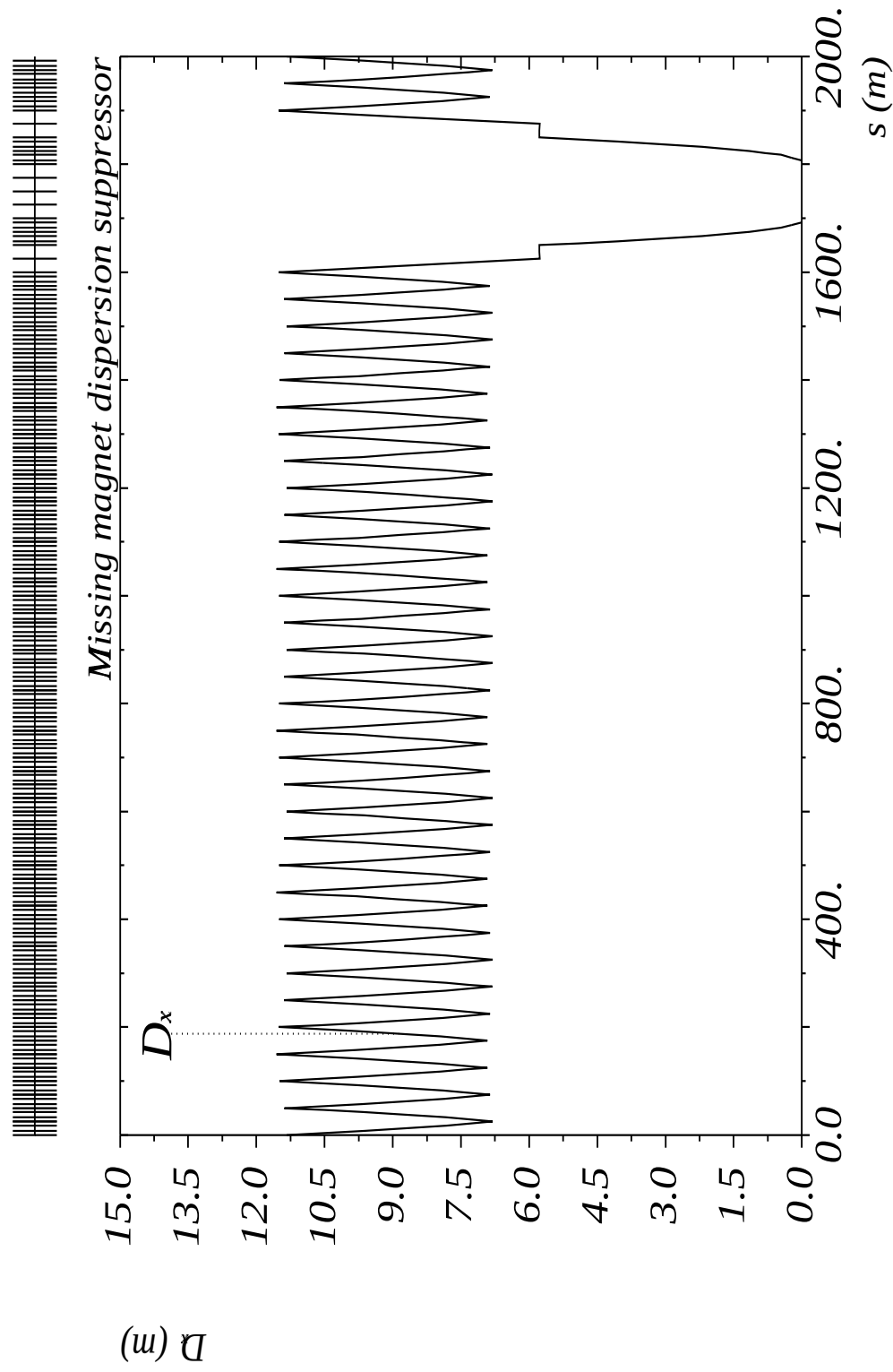
```
match;  
  
vary,name=kq1.1, step=0.00001;  
vary,name=kq2.1, step=0.00001;  
vary,name=kq3.1, step=0.00001;  
vary,name=kq4.1, step=0.00001;  
  
constraint,place=IP,betx= 2.0, alfx=0.0;  
  
endmatch;
```

- The strengths of a small number of additional quadrupoles are varied

# Optical functions (reduced $\beta$ -function)



# Optical functions (reduced dispersion)



# General purpose optics programs

■ Always allow to:

- Compute optical parameters (Twiss functions)
- Match the required properties

■ But also:

- Simulate machine imperfections
- Correct imperfections

→ Example again Methodical Accelerator Design



## (Interlude IV: Course on optics design)

→ Intermediate level CAS 2003 offered a course on optics design

■ Purpose was to develop a realistic accelerator optics

■ Included correction elements, optical matching, dispersion suppressors ...

■ MAD was used for practical implementation

→ The course is available on CD-ROM (on request) or from the web



# Simulation of an accelerator

- Purpose is to imitate the world of a particle or a beam in an accelerator
- Use **local** properties of the machine element to describe its interaction with a particle
- The grand scheme is to derive **global** behaviour



## Evaluation by simulation (1)

- Single particle behaviour
- Usually concerns long term behaviour such as beam loss
- The effect of the accelerator components on a single particle
  - Non-linear elements
  - Machine imperfections
  - External distortions





## Evaluation by simulation (2)

- Multi particle behaviour
  - Usually concerns collective behaviour: coherent motion, emittance increase, damping etc.
    - The effect of the accelerator components on an ensemble of particles (e.g. impedances)
    - Interactions of particles between each other.
- These are usually dictated by the properties of the accelerator (e.g. space charge, beam-beam effects ...)



## Single particle tracking

- The motion of a test particle through the elements of a machine is simulated for a defined number of turns → ”tracking”
- Use appropriate coordinates, start with  $\vec{z}_0$ .
- In each element (or part of the machine), the coordinates are transformed by  $\vec{z}_{n+1} = \mathcal{M} \circ \vec{z}_n$
- $\mathcal{M}$  must be symplectic
- We must distinguish **thick** and **thin** elements



# Tracking through thin elements

■ Thin "magnet": let go length to zero, but keep field integral finite (constant)

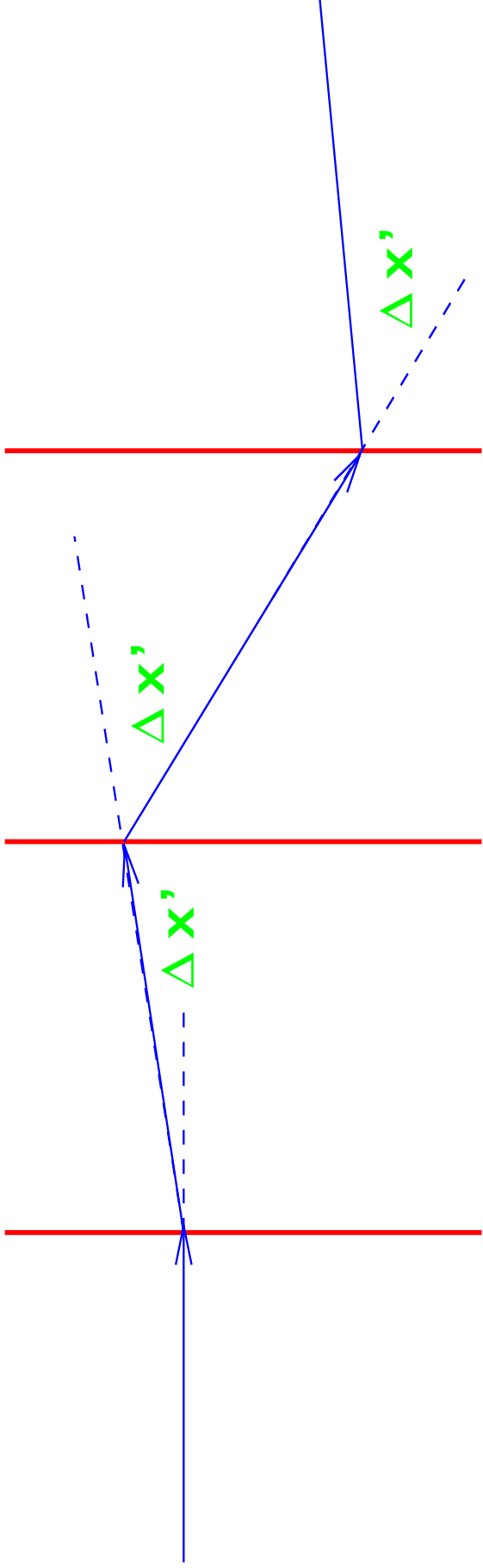
■ No change of amplitudes  $x$  and  $y$

→  $x \rightarrow x$  and  $y \rightarrow y$

■ The momenta  $x'$  and  $y'$  receive an amplitude dependent deflection (kick)

→  $x' \rightarrow x' + \Delta x'$  and  $y' \rightarrow y' + \Delta y'$





- No change of amplitudes  $x$  and  $y$
- The momenta  $x'$  and  $y'$  receive an amplitude dependent deflection (kick)

➡  $x' \rightarrow x' + \Delta x'$  and  $y' \rightarrow y' + \Delta y'$



## Tracking through thin elements

- So-called kick-codes (thin lens tracking)
- Always symplectic ! (homework)
- Usually rather fast on computers
- A "thick" element can be sliced into several thin elements



## Analysis tools

- Fourier analysis, diffusion coefficients, chaos detection ...
- Phase space plots (simple example):
  - Start with a "particle" with initial coordinates  $x$  and  $x'$  at a position  $s_0$
  - Pass through the One-Turn-Map (for position  $s_0$  !)
  - Plot the new  $x$  and  $x'$  coordinates at position  $s_0$  after every turn



## A simple example

Linear transformation plus a constant deflection  
(i.e. orbit kick from displaced quadrupole)

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{n+1} = \begin{pmatrix} \cos(\mu) & \sin(\mu) \\ -\sin(\mu) & \cos(\mu) \end{pmatrix}_{s_0} \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_n + \begin{pmatrix} 0 \\ b \end{pmatrix}$$

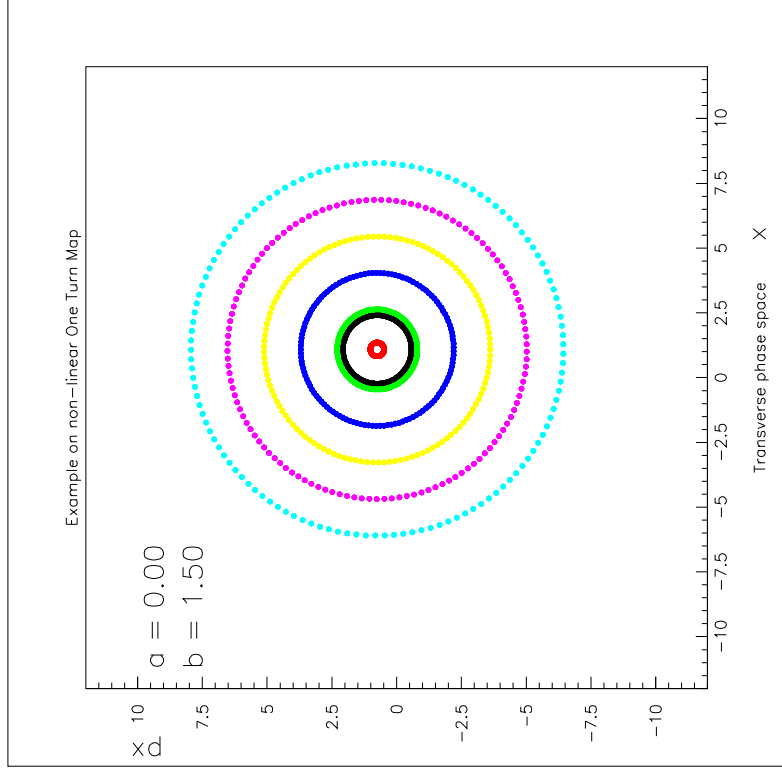
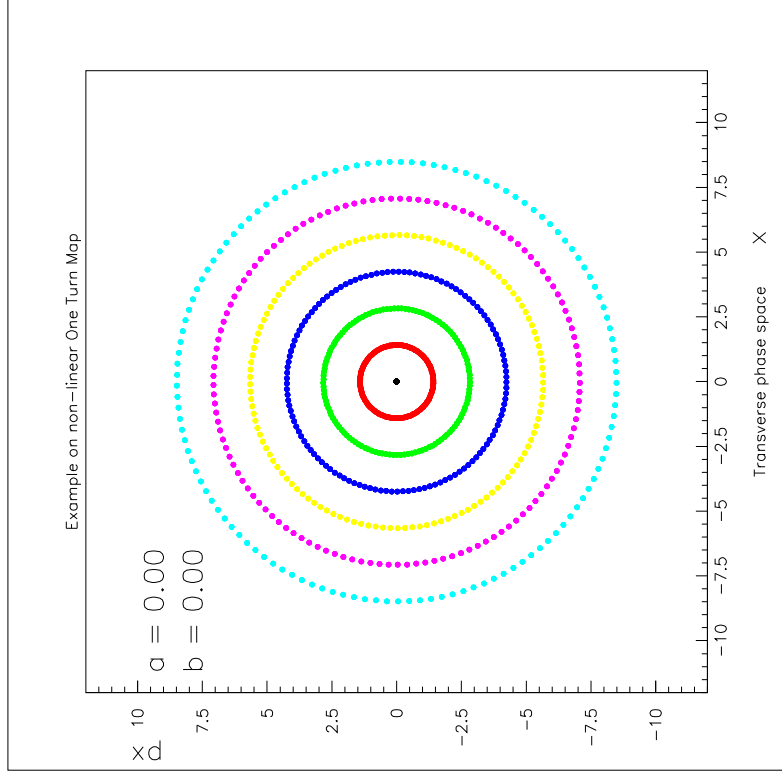
$$\mu = 2\pi Q_x = 2\pi \cdot 0.19,$$

constant  $b$  is a free parameter

→ Find the fixed point(s) (closed orbit)



# A simple example ..



Start at different amplitudes and ”observe”  $x$  and  $x'$  at position  $s_0$



## A (still) simple example

Linear transformation plus a quadratic non-linearity (e.g. **thin**) sextupole) plus a constant deflection

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{n+1} = \begin{pmatrix} \cos(\mu) & \sin(\mu) \\ -\sin(\mu) & \cos(\mu) \end{pmatrix}_{s_0} \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_n + \begin{pmatrix} 0 \\ ax^2 \end{pmatrix} + \begin{pmatrix} 0 \\ b \end{pmatrix}$$

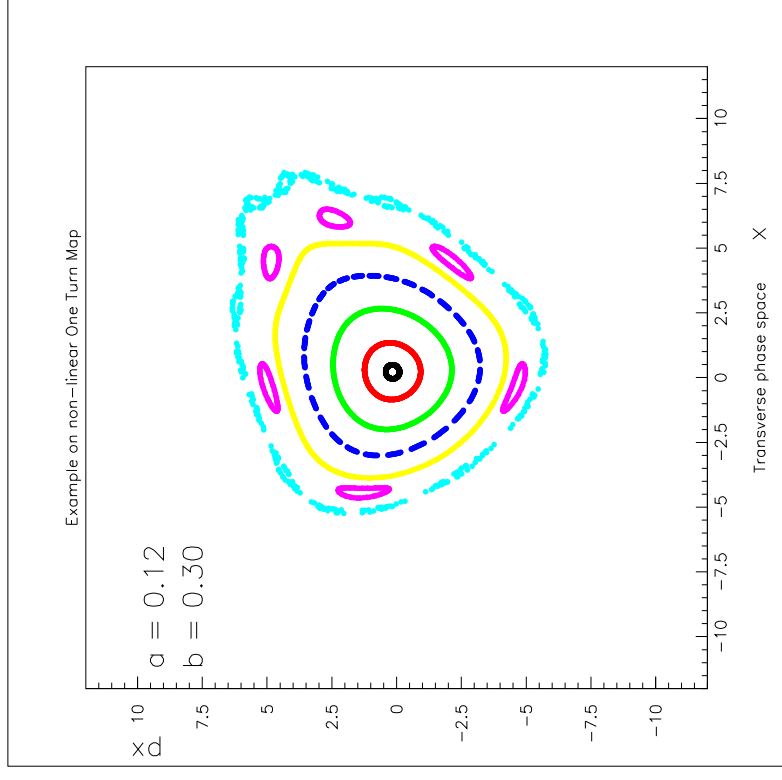
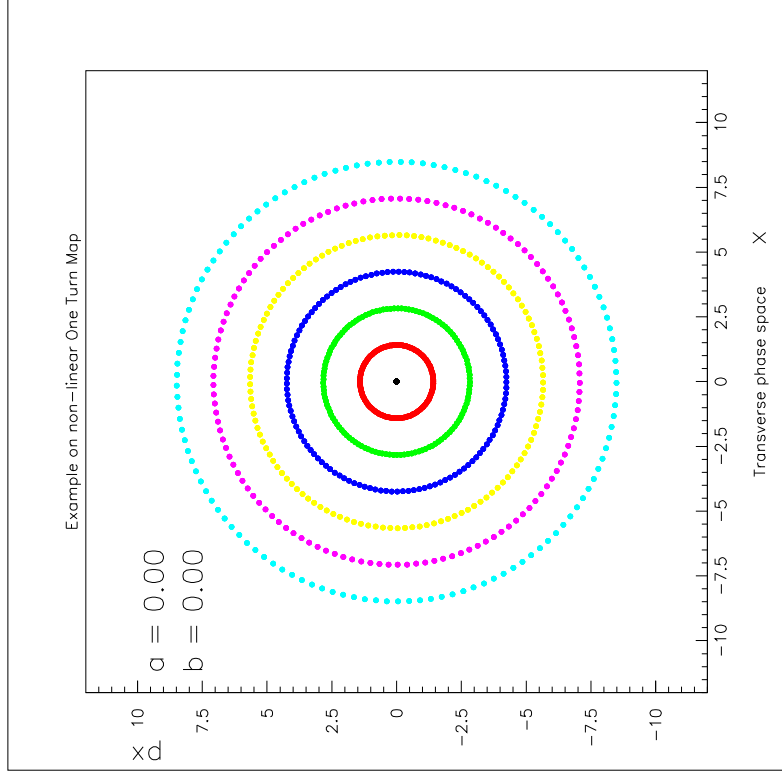
$$\mu = 2\pi Q_x = 2\pi \cdot 0.19,$$

constants **a** and **b** are free parameters

➡ Find the fixed points (how many do you see ?)



# A (still) simple example ..



- Motion at different amplitudes distorted
- Stability region reduced by non-linear effect

# Tracking through thick elements

- Real magnets are NOT thin !
- Consequence: they are NOT linear elements (also not dipoles, quadrupoles ..)
- Especially important for ”small” machines (e.g. large deflections, fringe fields etc.)
- Constructing a MAP for a thick element is more involved



## MAPS for thick elements

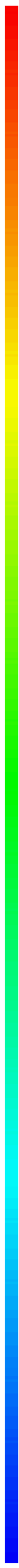
- Non-linear, i.e. not matrices (even for quadrupoles)
- Need integration of equation of motion
- Special techniques have been developed, some keywords:
  - Lie transforms
  - Symplectic integration
  - Differential Algebra ...
- In the end: we get again a One-Turn-Map



# Single particle dynamics in a nutshell

or: things are simpler than you thought

- Try to compute a (one turn) MAP
- It contains everything
- Its analysis will tell you what you need to know
- It doesn't matter how you got it !
- Use the Lorentz force (or equivalent) for the construction of maps (no need to "apply" accelerator physics concepts !)



## You can derive:

- Tunes (we already did)
- Betatron functions (we already did)
- Stability borders, dynamic aperture
- Detuning with amplitudes
- Fixpoints, closed orbit, resonance strength
- ... and much more !

Try to construct a global, time dependent  
Hamiltonian to get all that !



You do **not** get:

- Rules of thumb for simple calculations
- ”Handy” formulae
- Scaling laws for estimates (indirectly)



## Complications: light particles

- Light particles ( $e^-$ ,  $e^+$  etc.) emit synchrotron radiation and motion is damped
  - ➔ Stochastic component
  - ➔ No symplecticity, no invariants (but equilibrium parameters, e.g. emittance)
- Synchrotron motion must be simulated
- Computation of damping properties





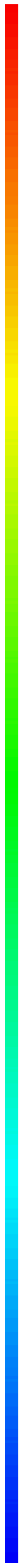
# Simulation of multi particle effects

- Often requires the simulation of a **beam**:  
simulate many ( $10^4$  or more) particles simultaneously and study their behaviour:
  - Beam shape (density distribution)
  - Centre of mass motion of all particles
- Fields generated by the beam need to be computed
- Advanced algorithms for field calculation have been developed and are used.



# Complications: many particles

- Particles have different amplitudes
- Particles have different tunes
- Particles have different momenta !
- Definition of emittance becomes more complicated



# Strategy for multi-particle simulations (1)

- Generate and simulate many particles  
( $10^4 - 10^5$ ) simultaneously
- Every particle interacts with the machine  
elements individually
- The whole ensemble interacts with the machine  
elements
- Every particle interacts with other particles !
- ➡ Feed back into motion of individual particles



## Strategy for multi-particle simulations (2)

- All particles must be treated in parallel
- For realistic LHC:  $10^7$  to  $10^8$  particles to simulate
- Already for storage requires  $\approx 10$  Gb memory
- Parallel processing needed for reasonable computing time
- Often requires (intelligent) simplifications



# Simulation of interactions with environment

This means: interaction of the individual particles  
**and** the whole beam with:

- Machine elements (e.g. magnets, RF, ...)
- Wake fields
- Impedances
- Electron cloud
- Intercepting elements (e.g. collimators, ...)

→ Strategies have changed with fast computers ...



# Simulation of interactions with itself

Particles inside a beam interact with other particles from the same beam:

- Space charge effects
- Intra-beam scattering
- Multi-bunch effects



# Simulation of interactions with other beams

## So-called beam-beam effects

- Other beam acts like a (very) non-linear lens
- Incoherent beam-beam effects (on each individual particle)
- Coherent beam-beam effects (on ensemble of particles)
- Requires the knowledge of fields generated by the other beam



# Matrix formulation (linear models)

- One-Turn-Maps can be written for two bunches or two beams (e.g. 1 and 2)
- ➡ Additional elements couple two beams

$$\begin{pmatrix} x_1 \\ x'_1 \\ x_2 \\ x'_2 \end{pmatrix}_{n+1} = \begin{pmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{pmatrix} \circ \begin{pmatrix} x_1 \\ x'_1 \\ x_2 \\ x'_2 \end{pmatrix}_n$$

- ➡ Allows computation of eigenmodes, eigenfrequencies etc.





## Field computation

- Some simulations require the computation of fields (or forces) produced by a beam from Poisson equation (here 2-dimensional):

$$\Delta V = -4\pi \cdot \rho(x, y)$$

- The density of the beam is  $\rho(x, y)$
- For simple distributions (Gaussian, uniform ...)  
can be solved analytically
- In general (i.e. in the interesting cases !) it is  
done numerically

## Some basic methods

**Particle - particle methods:** compute field between each particle pair and add up (unpractical for large number of particles, sometimes used in celestial mechanics)

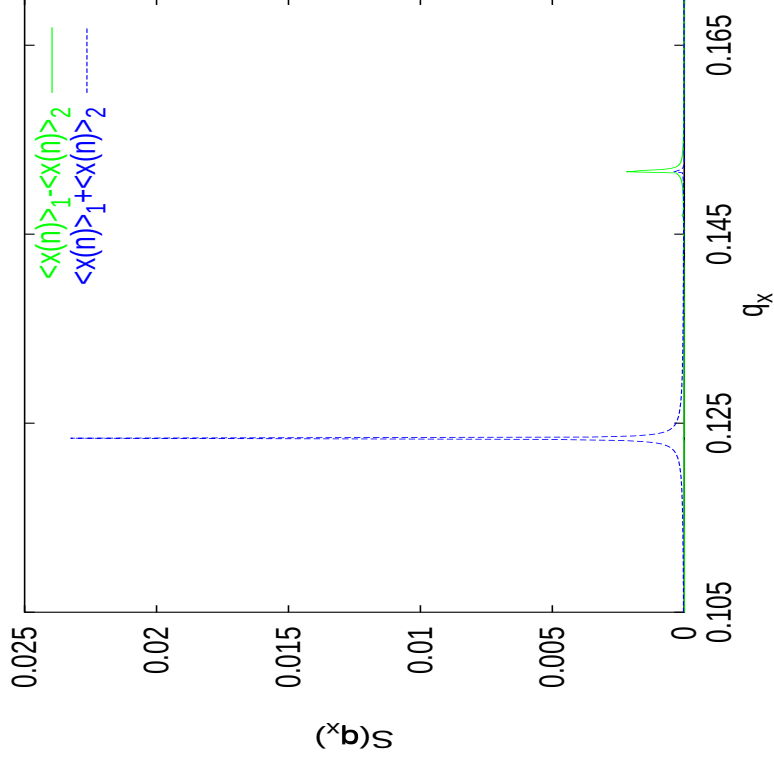
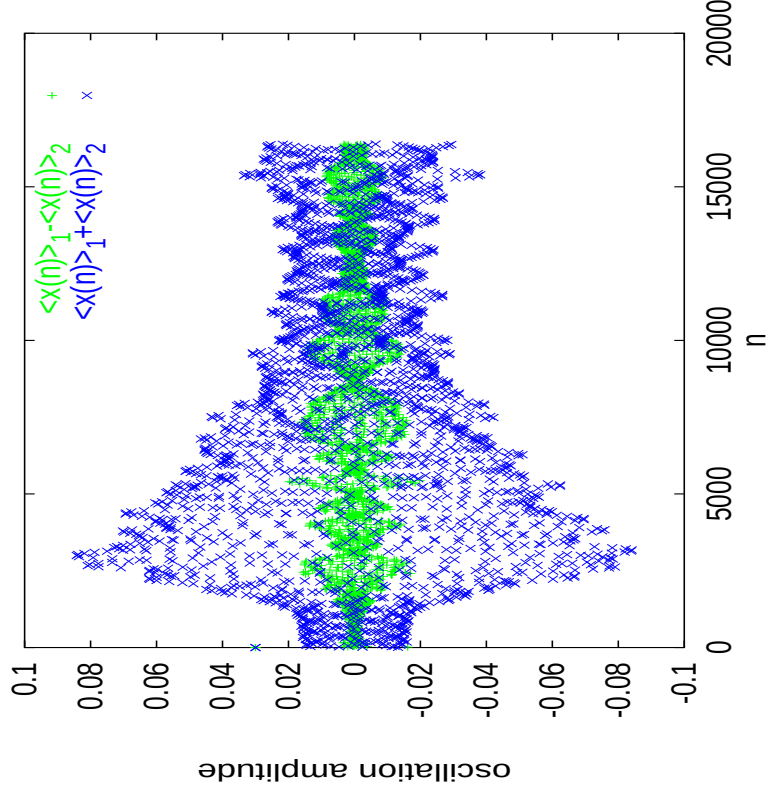
**Particle - mesh methods:** distribute particles on a mesh (grid) and solve the Poisson equation for discrete points

**Multipole methods:** develop potentials/fields as multipole expansion

→ Choice depends on application and parameters

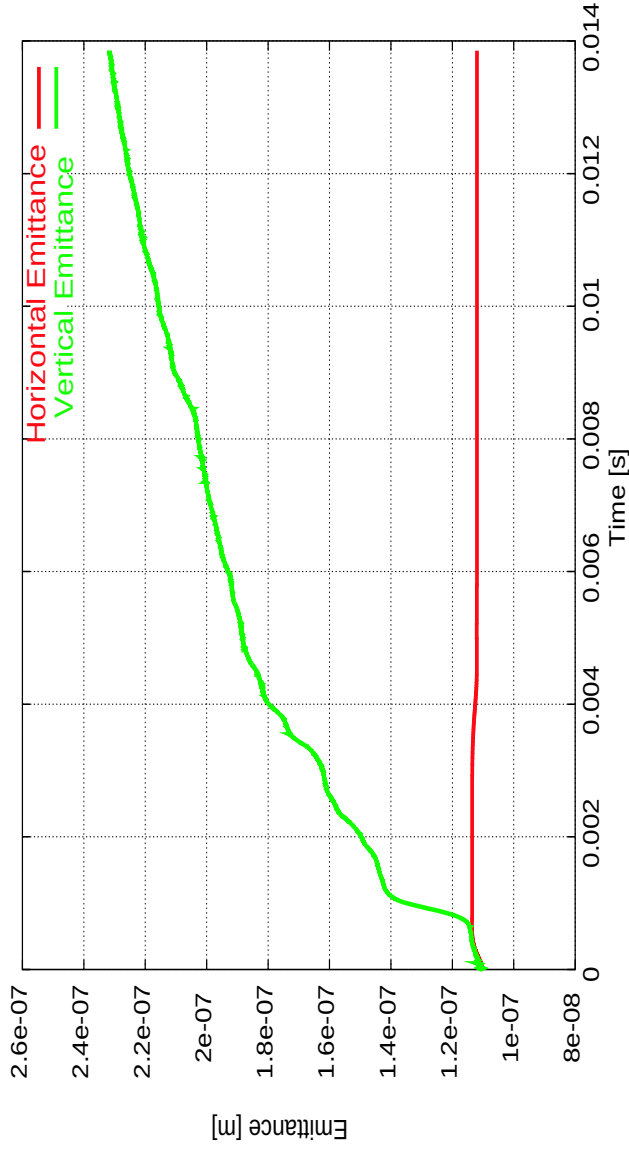


# Example: Centre of mass motion as function of time



➡ From beam-beam simulations: Bunch oscillations and frequency spectrum

## Example: Beam size as function of time



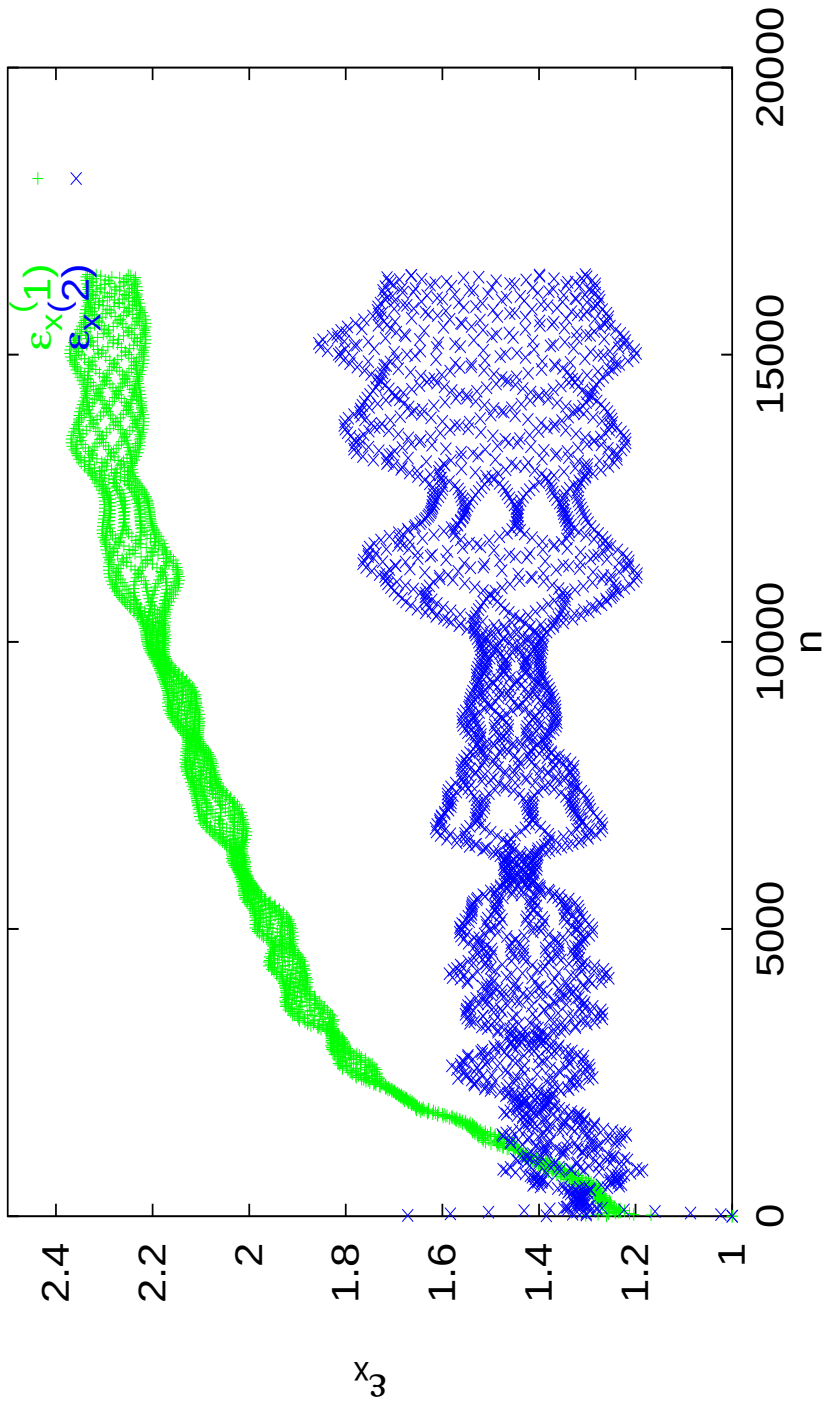
➡ From electron-cloud simulation (courtesy: E. Benedetto)

## Alternatives

- Sometimes multi-particle simulations are too time consuming
- Numerical solution of the Vlasov-equation
  - E.g. finite difference methods
  - Intermediate level school



## Example: Beam size as function of time



→ Beam-beam simulation: numerical solution of Vlasov equation gives evolution of beam sizes

## (Personal) Comments on simulations:

- Here I gave only a selective overview of what can be done
- Techniques and tools in dedicated schools and courses (some in Intermediate CAS Course)
- What can be done has changed a lot in the last decade
- It is easy to write a program !
- Analysis and interpretation is usually the difficult part



# Control and operation

■ Basic aim: optimize performance

As operator or accelerator physicist:

■ Provide and improve model of machine

■ Measure and interpret beam parameters

■ Correct and control beam parameters

■ Conduct machine experiments





# Control and operation of an accelerator

Basic problem: measure and control beam parameters

- Control (orbit, chromaticities ..) depend on machine model which may be incomplete
  - Feedback from measurements improves the model and simulations
  - Should use the same strategies and methods as during design (Remember: matching !)
- May be an iterative process



# Control and operation of an accelerator

- Very similar to simulation or design of a machine except:
  - ➔ Interface to hardware and control (e.g. power converters)
  - ➔ Beam instrumentation !
  - ➔ Communication (networks, etc.)
  - ➔ Issues such as: timing, alarms, interlocks,
- Treated in dedicated workshops and schools

