

# Lattice Design in Particle Accelerators

Bernhard Holzer, DESY

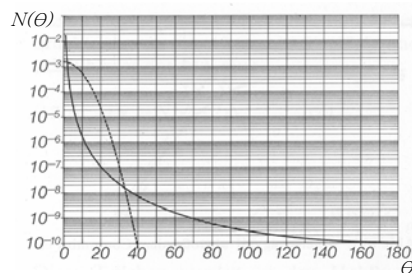
## Historical note:

... Particle acceleration where **lattice design is not needed**

$$N(\theta) = \frac{N_i n t Z^2 e^4}{(8\pi\epsilon_0)^2 r^2 K^2} * \frac{1}{\sin^4(\theta/2)}$$

Rutherford Scattering, 1906

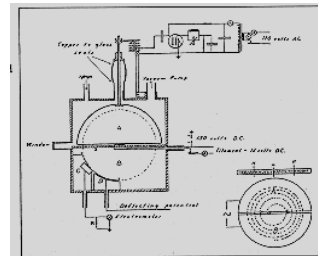
Using radioactive particle sources:  
 $\alpha$ -particles of some MeV energy



## Historical note:

II.) The „infancy of particle accelerators“

- 1923 Betatron,
- 1928 Cockroft-Walton Generator,
- 1929 Cyclotron
- 1932 Van de Graaf Generator, etc

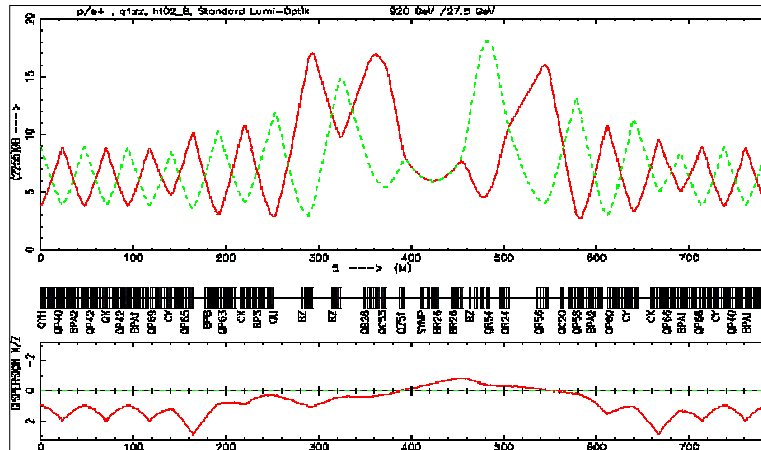


*Diagram of the first cyclotron  
by Lawrence and Livingstone*



*12 MV-Tandem van de Graaf  
Accelerator*

1952: Courant, Livingston, Snyder: Theory of strong focusing in particle beams → Ted Wilson in this school



**Lattice design:** design and optimisation of the principle elements of an accelerator ... *the lattice cells*

### Lattice Design: Prerequisites

~~... I will start very easy ... and slowly the topic will become more and more difficult~~ ... interesting

Lorentz Force:

$$\vec{F} = q * (\vec{E} + \vec{v} \times \vec{B})$$

neglecting electrical fields:

$$\vec{F} = q * (\vec{v} \times \vec{B})$$

High energy accelerators → circular machines

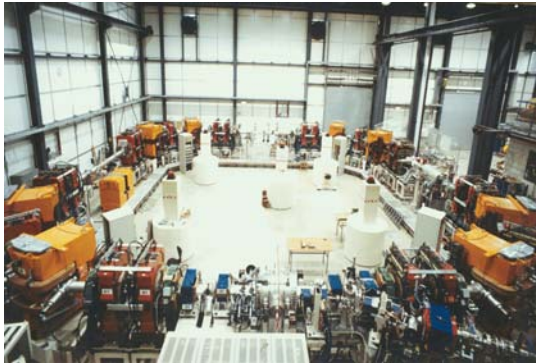
somewhere in the lattice we need a number of dipole magnets, that are bending the design orbit to a closed ring

In a constant external magnetic field the particle trajectory will be a part of a circle and ...

... the centrifugal force will be equal to the Lorentz force

$$e \cdot v \cdot B = \frac{mV^2}{\rho} \quad \rightarrow \quad e \cdot B = \frac{mV}{\rho} = p/\rho$$

$$\rightarrow \quad B \cdot \rho = p/e$$



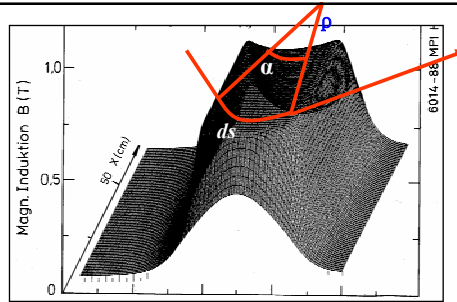
$p$  = momentum of the particle,  
 $\rho$  = curvature radius

$B \cdot \rho$  is called the “beam rigidity”

*Example: Heavy Ion Storage Ring: TSR  
 8 dipole magnets of equal bending strength*

### Circular Orbit:

$$\alpha = \frac{ds}{\rho} \approx \frac{dl}{\rho} \quad \alpha = \frac{B \cdot dl}{B \cdot \rho}$$



*field map of a storage ring dipole magnet*

The angle swept out in one revolution must be  $2\pi$ , so

$$\alpha = \frac{\int B dl}{B \cdot \rho} = 2\pi \quad \dots \text{ for a full circle} \quad \rightarrow \quad \int B dl = 2\pi \cdot \frac{p}{q}$$

### Example HERA:

920 GeV Proton storage ring

number of dipole magnets  $N = 416$

$l = 8.8\text{m}$

$q = +1e$

$$\int B dl \approx N \cdot l \cdot B = 2\pi p / q$$

$$B \approx \frac{2\pi \cdot 920 \cdot 10^9 \text{ eV}}{416 \cdot 3 \cdot 10^8 \frac{\text{m}}{\text{s}} \cdot 8.8\text{m} \cdot e} \approx \underline{\underline{5.15 \text{ Tesla}}}$$

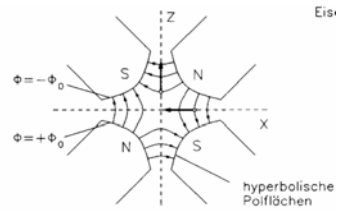
## Focusing forces and particle trajectories:

Magnetic field in a quadrupole magnet

$$B_x = -g * z, \quad B_z = -g * x$$

leads to a linear restoring force on the particle.

Relating the fields to their optical effect: normalise to the particles momentum:



$$\text{dipole magnet: } \frac{1}{\rho} = \frac{B}{p/e}$$

$$\text{quadrupole lens: } k = \frac{g}{p/e} \quad \text{focal length: } f := \frac{1}{k * l}$$

Under the influence of the focusing and defocusing forces the differential equation of the particles trajectory can be developed:

$$x'' + K * x = 0 \quad K = -k + 1/\rho^2 \quad \text{hor. plane}$$

$$K = k \quad \text{vert. plane}$$

Example:

HERA Ring: Circumference:

Circumference:  $C_0 = 6335 \text{ m}$   
 Bending radius:  $\rho = 580 \text{ m}$   
 Quadrupol Gradient:  $G = 110 \text{ T/m}$

$$\rightarrow k = 33.64 * 10^{-3} / \text{m}^2$$

$$\rightarrow 1/\rho^2 = 2.97 * 10^{-6} / \text{m}^2$$



the two storage rings  
of the HERA collider



For estimates in large accelerators the weak focusing term  $1/\rho^2$  can in general be neglected ...

### Single particle trajectories:

#### Equation of motion

$$y'' + K(s) * y = 0$$

$$y(s) = y_0 * \cos(\sqrt{|K|} * s) + \frac{y'_0}{\sqrt{|K|}} * \sin(\sqrt{|K|} * s)$$

$$y'(s) = -y_0 * \sqrt{|K|} * \sin(\sqrt{|K|} * s) + y'_0 * \cos(\sqrt{|K|} * s)$$

Or written more convenient in matrix form:

$$\begin{pmatrix} y \\ y' \end{pmatrix}_s = M * \begin{pmatrix} y \\ y' \end{pmatrix}_0$$

#### Matrices of lattice elements

**Hor. focusing** Quadrupole Magnet

$$M_{QF} = \begin{pmatrix} \cos(\sqrt{|K|} * l) & \frac{1}{\sqrt{|K|}} \sin(\sqrt{|K|} * l) \\ -\sqrt{|K|} \sin(\sqrt{|K|} * l) & \cos(\sqrt{|K|} * l) \end{pmatrix}$$

**Hor. defocusing** Quadrupole Magnet

$$M_{QD} = \begin{pmatrix} \cosh(\sqrt{|K|} * l) & \frac{1}{\sqrt{|K|}} \sinh(\sqrt{|K|} * l) \\ \sqrt{|K|} \sinh(\sqrt{|K|} * l) & \cosh(\sqrt{|K|} * l) \end{pmatrix}$$

**Drift space**

$$M_{Drift} = \begin{pmatrix} 1 & s \\ 0 & 1 \end{pmatrix}$$

### Periodic Lattices:

In the case of periodic lattices the transfer matrix can be expressed as a function of a set of periodic parameters  $\alpha, \beta, \gamma$

$$M(s) = \begin{pmatrix} \cos \mu + \alpha_s \sin \mu & \beta_s \sin \mu \\ -\gamma_s \sin \mu & \cos(\mu) - \alpha_s \sin \mu \end{pmatrix} \quad \mu = \int_s^{s+L} \frac{dt}{\beta(t)}$$

$\mu =$  phase advance per period.

For stability of the motion in periodic lattice structures it is required that

$$|\text{trace}(M)| < 2$$

In terms of these new periodic parameters the solution of the equation of motion is

$$y(s) = \sqrt{\epsilon} * \sqrt{\beta(s)} * \cos(\Phi(s) - \delta)$$

$$y'(s) = \frac{-\sqrt{\epsilon}}{\sqrt{\beta}} * \{ \sin(\Phi(s) - \delta) + \alpha \cos(\Phi(s) - \delta) \}$$

The new parameters  $\alpha, \beta, \gamma$  can be transformed through the lattice via the matrix elements defined above.

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC'+S'C & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix} * \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

Question: What does that mean ????

... and here starts the **lattice design !!!**

Question: What does that mean ????

Most simple example: drift space  $M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}$

particle coordinates  $\begin{pmatrix} x \\ x' \end{pmatrix}_l = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix} * \begin{pmatrix} x \\ x' \end{pmatrix}_0 \quad \begin{matrix} \rightarrow x(l) = x_0 + l * x'_0 \\ \rightarrow x'(l) = x'_0 \end{matrix}$

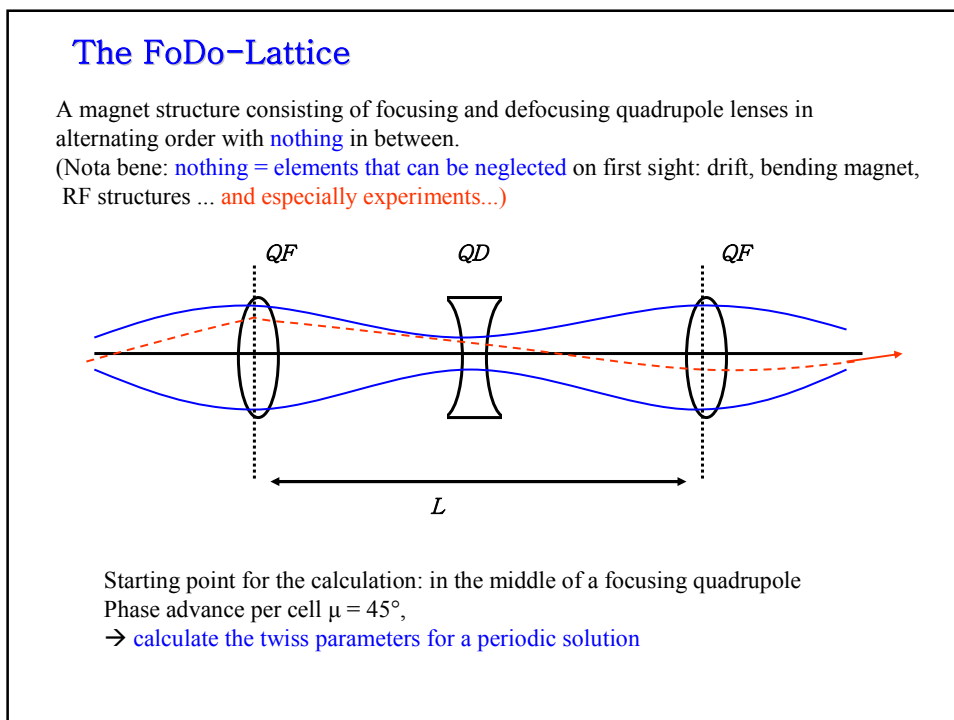
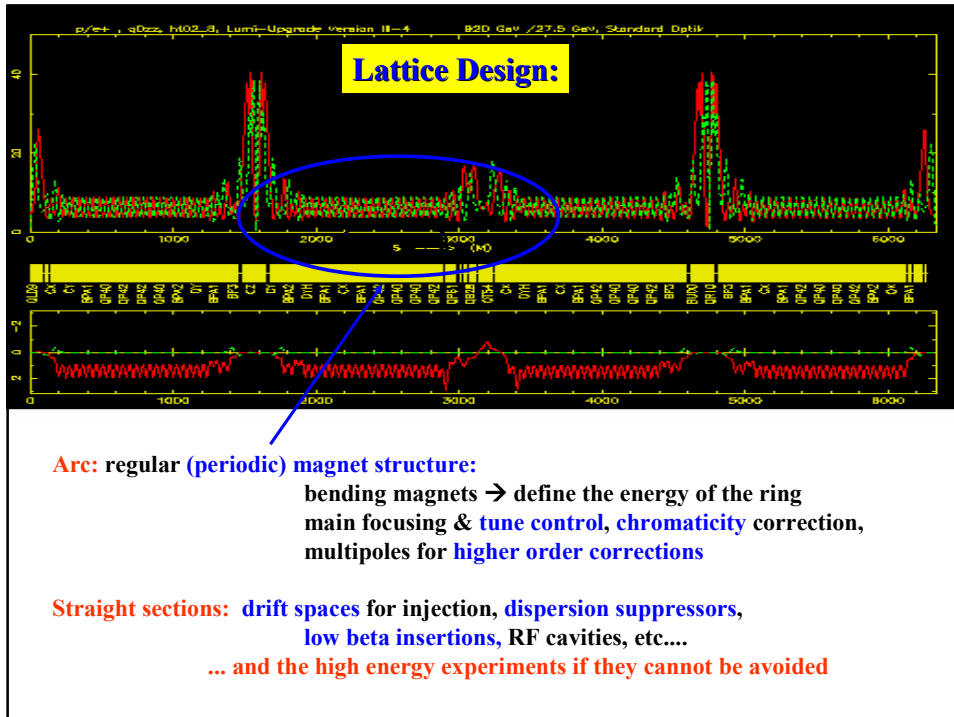
transformation of twiss parameters:

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_l = \begin{pmatrix} 1 & -2l & l^2 \\ 0 & 1 & -l \\ 0 & 0 & 1 \end{pmatrix} * \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0 \quad \beta(s) = \beta_0 - 2l * \alpha_0 + l^2 * \gamma_0$$

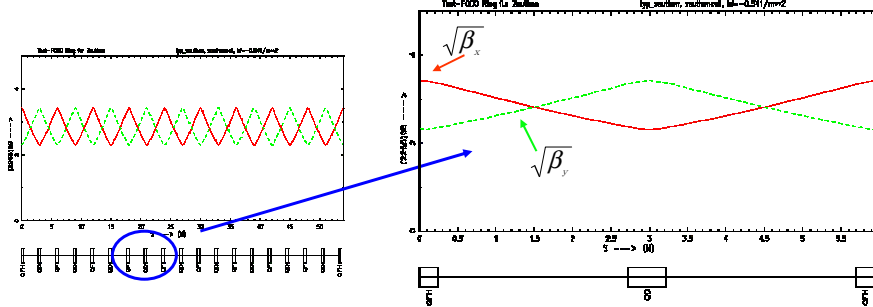
Stability ...?

$$|\text{trace}(M)| = 1 + 1 = 2$$

→ A periodic solution doesn't exist in a magnetic lattice built exclusively of drift spaces.



## Periodic solution of a FoDo Cell



Output of the optics program:

NR	TYP	LENGTH	STRENGTH	BETAX	ALFAX	PHIX	BETAZ	ALFAZ	PHIZ
0	IP	0	0.00E+00	11.611		0	5.295	0	0
1	QFH	0.25	-5.41E-01	11.228	1.514	0.0035	5.488	-0.78	0.007
2	QD	3.251	5.41E-01	5.4883	-0.781	0.0699	11.23	1.514	0.066
3	QFH	6.002	-5.41E-01	11.611		0.125	5.295	0	0.125
4	IP	6.002	0.00E+00	11.611		0.125	5.295	0	0.125

QX= 0.125 QZ= 0.125

$$0.125 * 2\pi = 45^\circ$$

... Can we understand, what the optics code is doing?

The action of a magnet on the beam is given by the transfer matrix:

$$M_{QF} = \begin{pmatrix} \cos(\sqrt{|K|} * l) & \frac{1}{\sqrt{|K|}} \sin(\sqrt{|K|} * l) \\ -\sqrt{|K|} \sin(\sqrt{|K|} * l) & \cos(\sqrt{|K|} * l) \end{pmatrix}$$

Input: strength and length of the FoDo elements

$$K = +/- 0.54102 \text{ m}^{-2}$$

$$lq = 0.5 \text{ m}$$

$$ld = 2.5 \text{ m}$$

$$M_{Drift} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}$$

The matrix for the complete cell is obtained by multiplication of the element matrices

$$M_{FoDo} = M_{QFH} * M_{LD} * M_{QD} * M_{LD} * M_{QFH}$$

Putting the numbers in and multiplying out ...

$$M_{FoDo} = \begin{pmatrix} 0.707 & 8.206 \\ -0.061 & 0.707 \end{pmatrix}$$



The transfer matrix for 1 period gives us all the information that we need !

1.) is the motion stable?  $|\text{trace}(M_{\text{FoDo}})| = 1.415 \rightarrow \underline{\underline{< 2}}$

2.) Phase advance per cell

$$M(s) = \begin{pmatrix} \cos\mu + \alpha \sin\mu & \beta \sin\mu \\ -\gamma \sin\mu & \cos\mu - \alpha \sin\mu \end{pmatrix} \rightarrow \begin{aligned} \cos(\mu) &= \frac{1}{2} * \text{trace}(M) = 0.707 \\ \mu &= \arccos\left(\frac{1}{2} * \text{trace}(M)\right) = \underline{\underline{45^\circ}} \end{aligned}$$

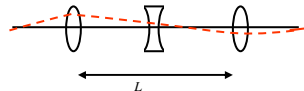
3.) hor  $\beta$ -function

$$\beta = \frac{M(1,2)}{\sin(\mu)} = \underline{\underline{11.611 \text{ m}}}$$

4.) hor  $\alpha$ -function

$$\alpha = \frac{M(1,1) - \cos(\mu)}{\sin(\mu)} = \underline{\underline{0}}$$

Some pearls of wisdom about lattice cells:



1.) think first ...

- \* a **first estimate** of the FoDo parameters can and should be done before we run our optics codes.
- \* we can learn a lot without doing too many too sophisticated calculations
- \* the optic codes will never tell us whether a lattice cell is **technically feasible**
- \* at the very beginning **we have to define parameters** that lead at least to a stable periodic solution

2.) some rules of „thumb“... to start with: the tune Q

phase advance per cell (i.e. )period:

$$\mu = \int_s^{s+L} \frac{dt}{\beta(t)}$$

Tune := phase advance of the machine in units of  $2\pi$

$$Q := N * \frac{\mu}{2\pi} = \frac{1}{2\pi} * \oint \frac{ds}{\beta(s)}$$

$$\rightarrow Q \approx \frac{1}{2\pi} * \frac{2\pi\bar{R}}{\bar{\beta}} = \bar{R}/\bar{\beta}$$

The tune is roughly given by the mean bending radius of the circular accelerator divided by the mean  $\beta$ -function

3.) can we do it a little bit easier ?

We can: the thin lens approximation

Matrix of a focusing quadrupole magnet: 
$$M_{QF} = \begin{pmatrix} \cos(\sqrt{|K|} * l) & \frac{1}{\sqrt{|K|}} \sin(\sqrt{|K|} * l) \\ -\sqrt{|K|} \sin(\sqrt{|K|} * l) & \cos(\sqrt{|K|} * l) \end{pmatrix}$$

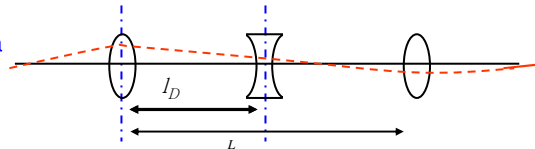
If the focal length  $f$  is much larger than the length of the quadrupole magnet,

$$f = 1/kl_Q \gg l_Q$$

the transfer matrix can be approximated using  $kl_Q = \text{const}, l_Q \rightarrow 0$

$$M = \begin{pmatrix} 1 & 0 \\ 1/f & 1 \end{pmatrix}$$

FoDo in thin lens approximation



Calculate the matrix for a half cell, starting in the middle of a foc. quadrupole:

$$M_{\text{halfCell}} = M_{QD/2} M_{ID} M_{QF/2}$$

$$M_{\text{halfCell}} = \begin{pmatrix} 1 & 0 \\ 1/\tilde{f} & 1 \end{pmatrix} * \begin{pmatrix} 1 & l_D \\ 0 & 1 \end{pmatrix} * \begin{pmatrix} 1 & 0 \\ -1/\tilde{f} & 1 \end{pmatrix}$$

$l_D$  indicates the length of the drift which is now just half the cell length

$$l_D = L/2$$

and starting at the middle of a quadrupole the focal length of the half quad is

$$\tilde{f} = 2f$$

$$M_{\text{halfCell}} = \begin{pmatrix} 1 - l_D/\tilde{f} & l_D \\ -l_D/\tilde{f}^2 & 1 + l_D/\tilde{f} \end{pmatrix}$$

For the second half cell set  $f \rightarrow -f$

### FoDo in thin lens approximation

Matrix for the **complete FoDo cell**:

$$M = \begin{pmatrix} 1 + \frac{l_D}{\tilde{f}} & l_D \\ -\frac{l_D}{\tilde{f}^2} & 1 - \frac{l_D}{\tilde{f}} \end{pmatrix} * \begin{pmatrix} 1 - \frac{l_D}{\tilde{f}} & l_D \\ -\frac{l_D}{\tilde{f}^2} & 1 + \frac{l_D}{\tilde{f}} \end{pmatrix}$$

Multiplying out we get ...

$$M = \begin{pmatrix} 1 - \frac{2l_D^2}{\tilde{f}^2} & 2l_D(1 + \frac{l_D}{\tilde{f}}) \\ 2(\frac{l_D^2}{\tilde{f}^3} - \frac{l_D}{\tilde{f}^2}) & 1 - 2\frac{l_D^2}{\tilde{f}^2} \end{pmatrix}$$

Now we know, that the **phase advance is related to the transfer matrix** by

$$\cos \mu = \frac{1}{2} \text{trace}(M) = \frac{1}{2} * (2 - \frac{4l_D^2}{\tilde{f}^2}) = 1 - \frac{2l_D^2}{\tilde{f}^2}$$

**After some beer** and with a little bit of trigonometric gymnastics

$$\cos(x) = \cos^2(x/2) - \sin^2(x/2) = 1 - 2\sin^2(x/2)$$

We can calculate the phase advance as a function of the FoDo parameter

$$\cos(\mu) = 1 - 2\sin^2(\mu/2) = 1 - \frac{2l_D^2}{\tilde{f}^2}$$

$$|\sin(\mu/2)| = l_D / \tilde{f} = \frac{L_{\text{Cell}}}{2\tilde{f}}$$

$$|\sin(\mu/2)| = \frac{L_{\text{Cell}}}{4f}$$

**Example: 45-degree Cell**

$$L_{\text{Cell}} = l_{\text{QF}} + l_D + l_{\text{QD}} + l_D = 0.5\text{m} + 2.5\text{m} + 0.5\text{m} + 2.5\text{m} = 6\text{m}$$

$$1/f = k * l_Q = 0.5\text{m} * 0.541 \text{ m}^{-2} = 0.27 \text{ m}^{-1}$$

$$\sin(\mu/2) \approx \frac{L_{\text{Cell}}}{4f} = 0.405$$

$$\rightarrow \mu \approx 47.8^\circ$$

$$\rightarrow \beta \approx 11.4 \text{ m}$$

**Remember:**  
Exact calculation yields:

$$\mu = 45^\circ$$

$$\beta = 11.6 \text{ m}$$

### Stability in a FoDo structure

transfer matrix for the complete cell

$$M = \begin{pmatrix} 1 - \frac{2l_D^2}{f^2} & 2l_D(1 + \frac{l_D}{f}) \\ 2(\frac{l_D^2}{f^3} - \frac{l_D}{f^2}) & 1 - 2\frac{l_D^2}{f^2} \end{pmatrix}$$

Stability requires:  $|\text{trace}(M)| < 2$        $|\text{trace}(M)| = \left| 2 - \frac{4l_D^2}{f^2} \right| < 2$



SPS Lattice

$$\rightarrow f > \frac{L_{\text{cell}}}{4}$$

For stability the focal length has to be larger than a quarter of the cell length !!

### Transformation matrix in terms of the Twiss parameters

[en detail](#)

Transformation of the coordinate vector  $(x, x')$  in a magnet

$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = M \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} \quad M_{QF} = \begin{pmatrix} \cos(\sqrt{|K|} * l) & \frac{1}{\sqrt{|K|}} \sin(\sqrt{|K|} * l) \\ -\sqrt{|K|} \sin(\sqrt{|K|} * l) & \cos(\sqrt{|K|} * l) \end{pmatrix}$$

General solution of the equation of motion

$$x(s) = \sqrt{\epsilon * \beta(s)} * \cos(\phi(s) + \varphi)$$

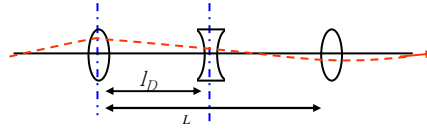
$$x'(s) = -\sqrt{\epsilon / \beta(s)} * \{ \alpha(s) \cos(\phi(s) + \varphi) + \sin(\phi(s) + \varphi) \}$$

Transformation of the coordinate vector  $(x, x')$  expressed as a function of the twiss parameters

$$M_{0 \rightarrow s} = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} (\cos \phi + \alpha_s \sin \phi) & \sqrt{\beta_s \beta_0} \sin \phi \\ \frac{(\alpha_0 - \alpha_s) \cos \phi - (1 + \alpha_0 \alpha_s) \sin \phi}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} (\cos \phi - \alpha_s \sin \phi) \end{pmatrix}$$

Transfer matrix for half a FoDo cell:

$$M_{\text{halfCell}} = \begin{pmatrix} 1 - l_D/\tilde{f} & l_D \\ -l_D/\tilde{f}^2 & 1 + l_D/\tilde{f} \end{pmatrix}$$



Compare to the twiss parameter form of M where  $\Phi$  denotes the phase advance through the half cell

$$M = \begin{pmatrix} \sqrt{\frac{\beta}{\beta_0}}(\cos \phi + \alpha \sin \phi) & \sqrt{\beta\beta_0} \sin \phi \\ \frac{(\alpha_0 - \alpha) \cos \phi - (1 + \alpha_0 \alpha) \sin \phi}{\sqrt{\beta\beta_0}} & \sqrt{\frac{\beta_0}{\beta}}(\cos \phi - \alpha \sin \phi) \end{pmatrix}$$

In the middle of a foc (defoc) quadrupole of the FoDo we always have  $\alpha=0$ , and the half cell will lead us from  $\beta_{\max}$  to  $\beta_{\min}$

$$M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} = \begin{pmatrix} \sqrt{\frac{\beta}{\beta_0}} \cos \phi & \sqrt{\beta\beta_0} \sin \phi \\ \frac{-1}{\sqrt{\beta\beta_0}} \sin \phi & \sqrt{\frac{\beta_0}{\beta}} \cos \phi \end{pmatrix}$$

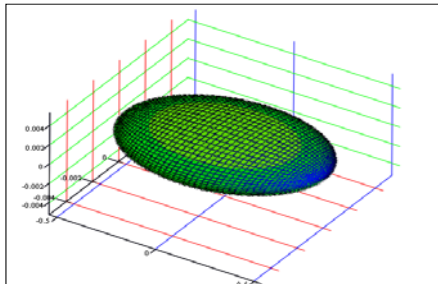
Solving for  $\beta_{\max}$  and  $\beta_{\min}$  and remembering that ....

$$\left| \sin \frac{\mu}{2} \right| = \frac{l_D}{\tilde{f}} = \frac{L}{4f}$$

$$\left. \begin{aligned} \frac{S'}{C} = \frac{\hat{\beta}}{\check{\beta}} = \frac{1+l_D/\tilde{f}}{1-l_D/\tilde{f}} = \frac{1+\sin \frac{\mu}{2}}{1-\sin \frac{\mu}{2}} \\ \frac{S}{C'} = \hat{\beta} \check{\beta} = \tilde{f}^2 = \frac{l_D^2}{\sin^2 \frac{\mu}{2}} \end{aligned} \right\} \rightarrow$$

$$\hat{\beta} = \frac{(1 + \sin \frac{\mu}{2})L}{\sin \mu} \quad !$$

$$\check{\beta} = \frac{(1 - \sin \frac{\mu}{2})L}{\sin \mu} \quad !$$



(Z, X, Y)

The maximum and minimum values of the  $\beta$ -function are solely determined by the phase advance and the length of the cell.

Longer cells lead to larger  $\beta$

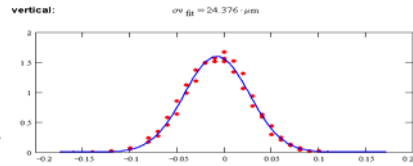
typical shape of a proton bunch in the HERA FoDo Cell

### Optimisation of the FoDo Phase advance: Beam dimension

In both planes a **gaussian particle distribution** is assumed given by the beam emittance  $\epsilon$  and the  $\beta$ -function

$$\sigma = \sqrt{\epsilon\beta}$$

*measured beam size at the HERA IP*

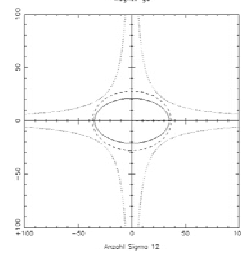


In general **proton beams are „round“** in the sense that

$$\epsilon_x \approx \epsilon_y$$

So for highest aperture we have to minimise the  $\beta$ -function in both planes:

$$r^2 = \epsilon_x \beta_x + \epsilon_y \beta_y$$



*typical beam envelope, vacuum chamber and pole shape in a foc. Quadrupole lens in HERA*

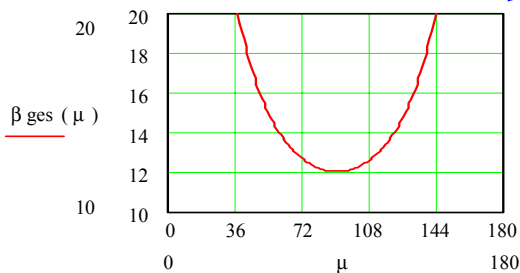
### Optimising the FoDo phase advance

$$r^2 = \epsilon_x \beta_x + \epsilon_y \beta_y$$

search for the phase advance  $\mu$  that results in a minimum of the sum of the beta's

$$\hat{\beta} + \check{\beta} = \frac{(1 + \sin \frac{\mu}{2}) * L}{\sin \mu} + \frac{(1 - \sin \frac{\mu}{2}) * L}{\sin \mu}$$

$$\hat{\beta} + \check{\beta} = \frac{2L}{\sin \mu} \quad \frac{d}{d\mu} \left( \frac{2L}{\sin \mu} \right) = 0$$

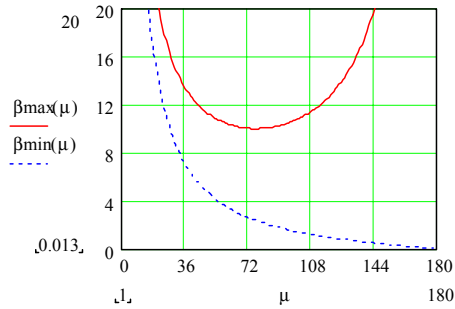


$$\frac{L}{\sin^2 \mu} * \cos \mu = 0 \rightarrow \underline{\underline{\mu = 90^\circ}}$$

Nota bene: electron beams are typically flat,  $\varepsilon_y \approx 2 \dots 10 \% \varepsilon_x$   
 → optimise only  $\beta_{hor}$

$$\frac{d}{d\mu}(\beta) = \frac{d}{d\mu} \frac{L(1 + \sin \frac{\mu}{2})}{\sin \mu} = 0 \rightarrow \mu \approx 76^\circ$$

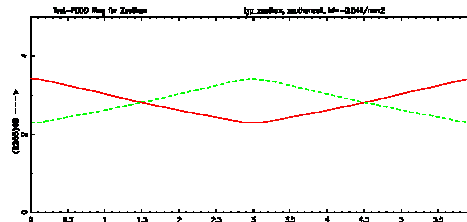
red curve:  $\beta_{max}$   
 blue curve:  $\beta_{min}$   
 as a function of the phase advance  $\mu$



### Orbit distortions in a periodic lattice

field error of a dipole/distorted quadrupole

$$\rightarrow \delta(\text{mrad}) = \frac{ds}{\rho} = \frac{\int B ds}{p/e}$$



the particle will follow a new closed trajectory: the distorted orbit:

$$x(s) = \frac{\sqrt{\beta(s)}}{2 \sin \pi Q} \int \frac{\sqrt{\beta(\tilde{s})}}{\rho(\tilde{s})} \cos(|\phi(\tilde{s}) - \phi(s)| - \pi Q) d\tilde{s}$$

- \* the orbit amplitude will be large if the  $\beta$  function at the location of the kick is large  
 $\beta(\tilde{s})$  indicates the sensitivity of the beam → here orbit correctors should be placed in the lattice
- \* the orbit amplitude will be large at places where in the lattice  $\beta(s)$  is large → here beam position monitors should be installed

## Chromaticity in the FoDo Lattice

**Definition**  $\Delta Q = \xi * \frac{\Delta p}{p}$

The **chromaticity** describes an **optical error of quadrupole lenses**: For a given magnetic field, i.e. gradient particles with **smaller momentum will feel a stronger focusing force** and vice versa.

For small momentum errors  $\Delta p/p$  the focusing parameter  $k$  can be written as

$$k(p) = \frac{g}{p/e} = g * \frac{e}{p_0 + \Delta p}$$

$$k(p) \approx \frac{e}{p_0} (1 - \frac{\Delta p}{p}) * g = k_0 + \Delta k \quad \rightarrow \quad \Delta k = -k_0 \frac{\Delta p}{p}$$

This describes a **quadrupole error that leads to a tune shift** of ...

$$\Delta Q = \frac{1}{4\pi} \int \Delta k \beta(s) ds = \frac{-1}{4\pi} \frac{\Delta p}{p} \int k_0 \beta(s) ds$$

$\xi$  contribution in the lattice  $\xi = -\frac{1}{4\pi} \int \beta(s) * k(s) ds$

## Chromaticity in the FoDo Lattice

$$\xi = -\frac{1}{4\pi} \int \beta(s) * k(s) ds$$

$$\xi \approx -\frac{1}{4\pi} N * \frac{\beta - \beta^v}{f_Q} = -\frac{1}{4\pi} N * \frac{1}{f_Q} * \left\{ \frac{L(1 + \sin \frac{\mu}{2}) - L(1 - \sin \frac{\mu}{2})}{\sin \mu} \right\}$$

using some **trigonometric transformations** ...  $\xi$  can be expressed in a very simple form:

$$\xi = -\frac{1}{4\pi} N \frac{1}{f_Q} \frac{2L \sin \frac{\mu}{2}}{\sin \mu} = -\frac{1}{4\pi} N \frac{1}{f_Q} \frac{L \sin \frac{\mu}{2}}{f_Q \sin \frac{\mu}{2} \cos \frac{\mu}{2}}$$

remember ...  
 $\sin x = 2 \sin \frac{x}{2} \cos \frac{x}{2}$

$$\xi_{cell} = -\frac{1}{4\pi} \frac{1}{f_Q} \frac{L \tan \frac{\mu}{2}}{f_Q \sin \frac{\mu}{2}}$$

putting ...  $\sin \frac{\mu}{2} = \frac{L}{4f_Q}$

Contribution of one FoDo Cell to the chromaticity of the ring:

$$\xi_{cell} = -\frac{1}{\pi} * \tan \frac{\mu}{2}$$



## Resumé

1.) Dipole strength:  $\int B ds = N * B_0 * l_{eff} = 2\pi \frac{p}{q}$

$l_{eff}$  effective magnet length, N number of magnets

2.) Stability condition:  $|Trace(M)| < 2$

for periodic structures within the lattice / at least for the transfer matrix of the complete circular machine

3.) Transfer matrix for periodic cell  $M(s) = \begin{pmatrix} \cos \mu + \alpha(s) \sin \mu & \beta(s) \sin \mu \\ -\gamma(s) \sin \mu & \cos(\mu) - \alpha(s) \sin \mu \end{pmatrix}$

$\alpha, \beta, \gamma$  depend on the position  $s$  in the ring,  $\mu$  (phase advance) is independent of  $s$

4.) Thin lens approximation:  $M_{QF} = \begin{pmatrix} 1 & 0 \\ \frac{1}{f_Q} & 1 \end{pmatrix} \quad f_Q = \frac{1}{k_Q l_Q}$

focal length of the quadrupole magnet  $f_Q = 1/(k_Q l_Q) \gg l_Q$

5.) Tune (rough estimate):  $Q \approx \frac{\bar{R}}{\bar{\beta}}$

$\bar{R}, \bar{\beta}$  average values of radius and  $\beta$ -function

6.) Phase advance per FoDo cell  $\left| \sin \frac{\mu}{2} \right| = \frac{L_{Cell}}{4f_Q}$   
(thin lens approx)

$L_{Cell}$  length of the complete FoDo cell,  $f_Q$  focal length of the quadrupole,  $\mu$  phase advance per cell

7.) Stability in a FoDo cell  $f_Q > \frac{L_{Cell}}{4}$   
(thin lens approx)

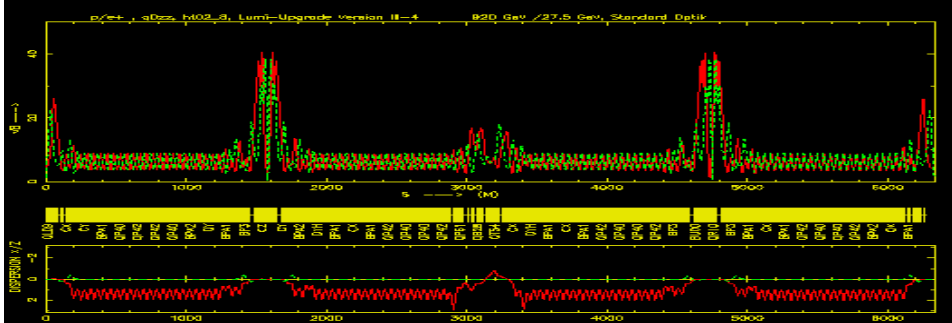
8.) Beta functions in a FoDo cell  $\hat{\beta} = \frac{(1 + \sin \frac{\mu}{2}) L_{Cell}}{\sin \mu} \quad \check{\beta} = \frac{(1 - \sin \frac{\mu}{2}) L_{Cell}}{\sin \mu}$   
(thin lens approx)

$L_{Cell}$  length of the complete FoDo cell,  $\mu$  phase advance per cell

**Resumé** periodic section („the arc“ in a large accelerator):

- parameters of the lattice cell defined by 2 quadrupole strengths (sometimes even only by one if in series)
- for a given tune (phase advance) the twiss parameters are fixed et vice versa.
- tune adjustments, variations of cell lengths, matching of twiss parameters creation of symmetry points in the lattice ...

.... need more degrees of freedom, i.e. additional free quadrupole lenses, varying drift lengths etc.



## APPENDIX

### Single particle trajectories:

$$y'' + K * y = 0$$

The differential equation for the particle movement can be solved by the Ansatz ...

$$y = a_1 * \cos(\omega * s) + a_2 * \sin(\omega * s)$$

$$y' = -a_1 \omega * \sin(\omega * s) + a_2 \omega * \cos(\omega * s)$$

$$y'' = -a_1 \omega^2 * \cos(\omega * s) - a_2 \omega^2 * \sin(\omega * s) \\ = -\omega^2 * y$$

$$\rightarrow K = \omega^2, \quad \omega = \sqrt{K}$$

So we get for the equation of motion in a storage ring

$$y(s) = a_1 * \cos(\sqrt{K} * s) + a_2 * \sin(\sqrt{K} * s)$$

### Equation of motion

$$y(s) = a_1 * \cos(\sqrt{K} * s) + a_2 * \sin(\sqrt{K} * s)$$

The parameters  $a_1$  and  $a_2$  refer to the individual particle and are determined by boundary conditions.

$$y(0) = y_o \quad \rightarrow a_1 = y_o$$

$$y'(0) = y_o' \quad \rightarrow a_2 = \frac{y_o'}{\sqrt{K}}$$

resulting in

$$y(s) = y_o * \cos(\sqrt{K} * s) + \frac{y_o'}{\sqrt{K}} * \sin(\sqrt{K} * s)$$

$$y'(s) = -y_o * \sqrt{K} * \sin(\sqrt{K} * s) + y_o' * \cos(\sqrt{K} * s)$$

Or written more convenient in matrix form:

$$\begin{pmatrix} y \\ y' \end{pmatrix}_s = M * \begin{pmatrix} y \\ y' \end{pmatrix}_o, \quad M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix}$$

### Matrices of lattice elements

$$M_{\text{qr}} = \begin{pmatrix} \cos(\sqrt{K} * l) & \frac{1}{\sqrt{K}} \sin(\sqrt{K} * l) \\ -\sqrt{K} \sin(\sqrt{K} * l) & \cos(\sqrt{K} * l) \end{pmatrix} \quad \text{Hor. focusing} \\ \text{Quadrupole Magnet}$$

$$M_{\text{qb}} = \begin{pmatrix} \cosh(\sqrt{K} * l) & \frac{1}{\sqrt{K}} \sinh(\sqrt{K} * l) \\ \sqrt{K} \sinh(\sqrt{K} * l) & \cosh(\sqrt{K} * l) \end{pmatrix} \quad \text{Hor. defocusing} \\ \text{Quadrupole Magnet}$$



$$M_{\text{Drift}} = \begin{pmatrix} 1 & s \\ 0 & 1 \end{pmatrix} \quad \text{Drift space}$$

$$K = -k + \frac{1}{\rho^2} \quad \text{in horizontal plane}$$

$$K = k \quad \text{in vertical plane}$$

### Transformation of the principal trajectories in terms of the Twiss parameters

General solution of the equation of motion

$$(1) \quad \begin{aligned} x(s) &= \sqrt{\varepsilon * \beta(s)} * \cos(\phi(s) + \varphi) \\ x'(s) &= -\sqrt{\varepsilon/\beta(s)} * \{\alpha(s) \cos(\phi(s) + \varphi) + \sin(\phi(s) + \varphi)\} \end{aligned}$$

Using theorems of trigonometric functions

$$\sin(a+b) = \sin(a) \cos(b) + \cos(a) \sin(b) \dots$$

$$(2) \quad \begin{aligned} x(s) &= \sqrt{\varepsilon * \beta(s)} * \{\cos \phi(s) \cos(\varphi) - \sin \phi(s) \sin(\varphi)\} \\ x'(s) &= -\sqrt{\varepsilon/\beta(s)} * \{\alpha(s) \cos \phi(s) \cos(\varphi) - \alpha(s) \sin \phi(s) \sin(\varphi) + \\ &\quad + \sin \phi(s) \cos(\varphi) + \cos \phi(s) \sin(\varphi)\} \end{aligned}$$

Set initial conditions:  $x(0)=x_0, x'(0)=x'_0,$

$$\beta(0)=\beta_0, \alpha(0)=\alpha_0, \Phi(0)=0$$

$$(3) \quad \cos \phi = \frac{x_0}{\sqrt{\varepsilon \beta_0}} \quad \sin \phi = \frac{-1}{\sqrt{\varepsilon}} \left( x'_0 \sqrt{\beta_0} + \frac{\alpha_0 x_0}{\sqrt{\beta_0}} \right)$$

Inserting in (1)  $x(s) = \sqrt{\frac{\beta(s)}{\beta_0}} \{ \cos \phi(s) + \alpha_0 \sin \phi(s) \} x_0 + \sqrt{\beta(s)\beta_0} \sin \phi(s) x'_0$

$$x'(s) = \sqrt{\frac{1}{\beta(s)\beta_0}} \{ (\alpha_0 - \alpha(s)) \cos \phi(s) - (1 + \alpha_0 \alpha(s)) \sin \phi(s) \} x_0 \\ + \sqrt{\frac{\beta_0}{\beta(s)}} \{ \cos \phi(s) - \alpha(s) \sin \phi(s) \} x'_0$$

So again we have got a matrix that transforms the orbit vector  $(x_0, x'_0)$  into  $(x(s), x'(s))$

$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = M \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$

$$M = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} (\cos \phi + \alpha_s \sin \phi) & \sqrt{\beta_s \beta_0} \sin \phi \\ \frac{(\alpha_0 - \alpha_s) \cos \phi - (1 + \alpha_0 \alpha_s) \sin \phi}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} (\cos \phi - \alpha_s \sin \phi) \end{pmatrix}$$