

# Intensity Measurements

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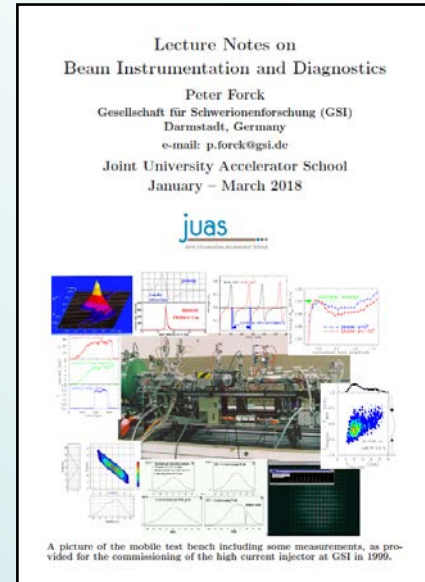
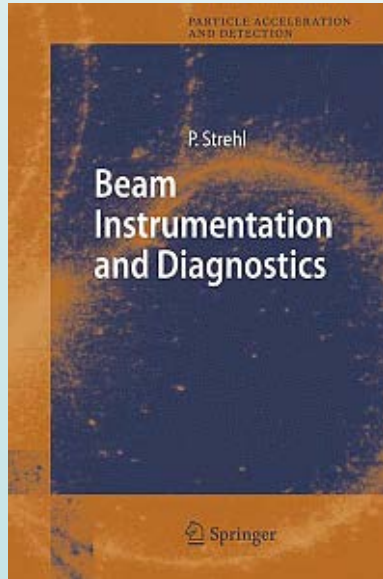
# Outline

- Classification of intensity/current measurement devices
- Beam destructive/scattering monitors:
  - Stopping the Beam, e.g. Faraday cups
  - Interaction of the beam with matter, e.g. ionization chambers
- Non-destructive current monitors → current transformers (ac, dc)
- Conclusion and Acknowledgements

# Introduction

- Literature:

[https://indico.cern.ch/event/683638/contributions/2801669/attachments/1563566/2540684/juas\\_script.pdf](https://indico.cern.ch/event/683638/contributions/2801669/attachments/1563566/2540684/juas_script.pdf)



- See: <http://cas.web.cern.ch/cas/CAS%20Welcome/Previous%20Schools.htm>
  - *Beam Diagnostics* from U. Raich, CERN in CAS, *Small Accelerators*, 2005
  - *CERN Accelerator School on Beam Diagnostics*, 2008, Talk of J.-C. Denard
- .... and much more sources as e.g. [www.jacow.org](http://www.jacow.org)!

# Introduction

Beam diagnostic devices are necessary as *“the eyes of the operator”* to the accelerator for:

- Observation and Logging
- Measuring feedback on parameter setting/tuning
- Searching for errors in the machine, e.g. a temperature drift effect, a short in a coil, etc.

The different beam diagnostics systems can be classified in three groups:

- I. Non-destructive diagnostic systems that will work online during experiments and in all other cases.
- II. Destructive measurement devices that will be used for the daily checks of the machine and the beam stability, and in addition for machine tuning and solving simpler machine problems.
- III. Special devices that will be necessary during the commissioning and in case of serious machine problems.

# Beam Intensity/Current Measurement

## Definitions:

- The **Intensity** is the power transferred per unit area, where the area is measured on the plane perpendicular to the direction of propagation of the energy.
- An **electric current** is a flow of electric charge (in accelerators mostly electrons, protons and ions).

## The **beam intensity/current** is the basic quantity of the beam:

- It is the first check of the accelerator functionality.
- It has to be determined in an absolute manner.
- It is important for transmission measurement and to prevent for beam losses.



# Beam Intensity/Current Measurement

Different devices are used:

➤ **Faraday cups (beam is stopped):**

- Measurement of the beam's **electrical charges**.
- They are destructive.
- For “low” energies only.
- Low currents can be determined.

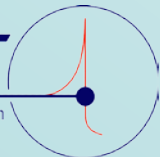
➤ **Particle detectors (beam is scattered):**

- Measurement of the particle's **energy loss** in matter.
- Examples are scintillators, ionization chambers, secondary e<sup>-</sup> emission monitors, ...
- Used for low currents at high energies e.g. for slow extraction.

➤ **Transformers (beam is not disturbed):**

- Measurement of the beam's **magnetic field**.
- They are non-destructive and can measure ac- and dc-beams
- No dependence on beam energy.
- They have (normally) a limited detection threshold ( $\sim \mu\text{A}$ ).

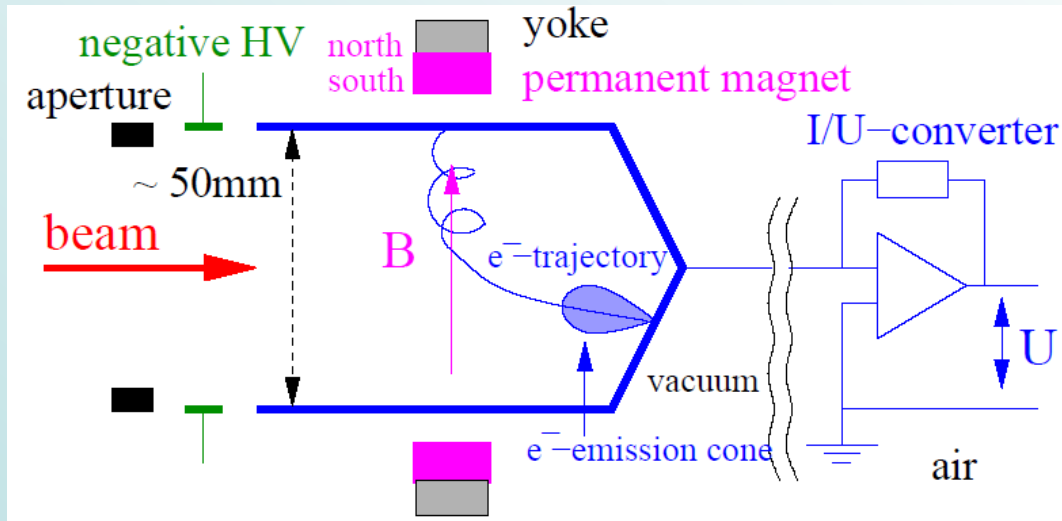
# Faraday Cups



# Faraday Cups for Beam Charge Measurement

The beam particles are collected inside a metal cup  
⇒ The beam's charge is recorded as a function of time.

The cup is moved in the beam pass → destructive device!



Currents **down to 10 pA** with bandwidth of 100 Hz!

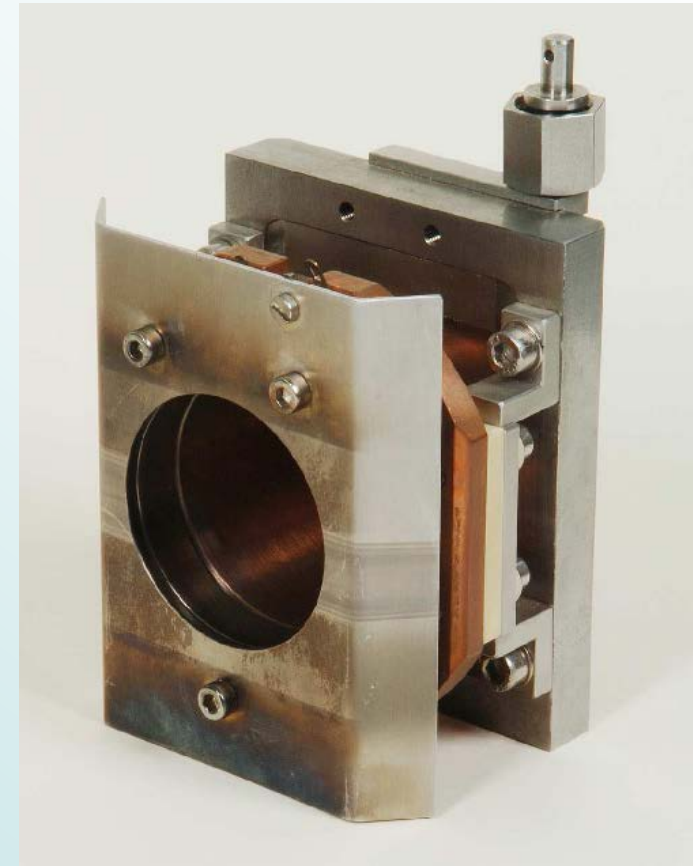
## Magnetic field:

To prevent for secondary electrons leaving the cup

*And / Or*

## Electric field:

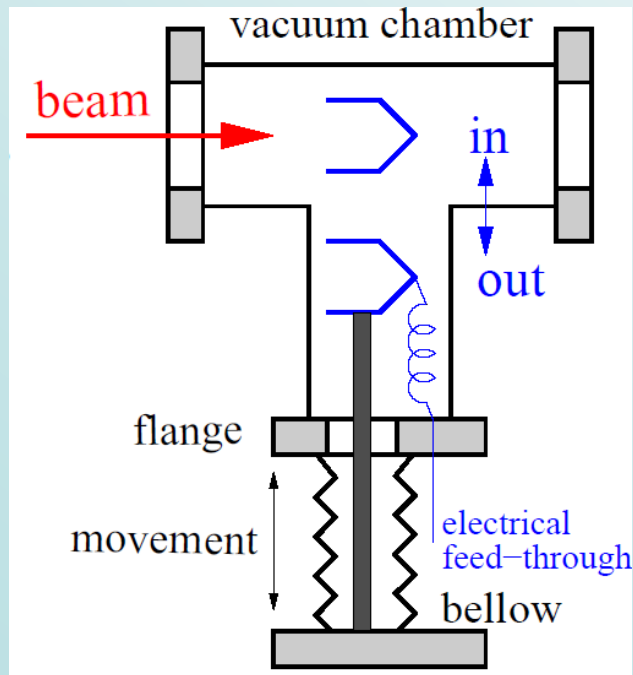
Potential barrier at the cup entrance





# Realizations of Faraday Cups

The Faraday Cup is moved into the beam pipe using an air-pressured actuator.



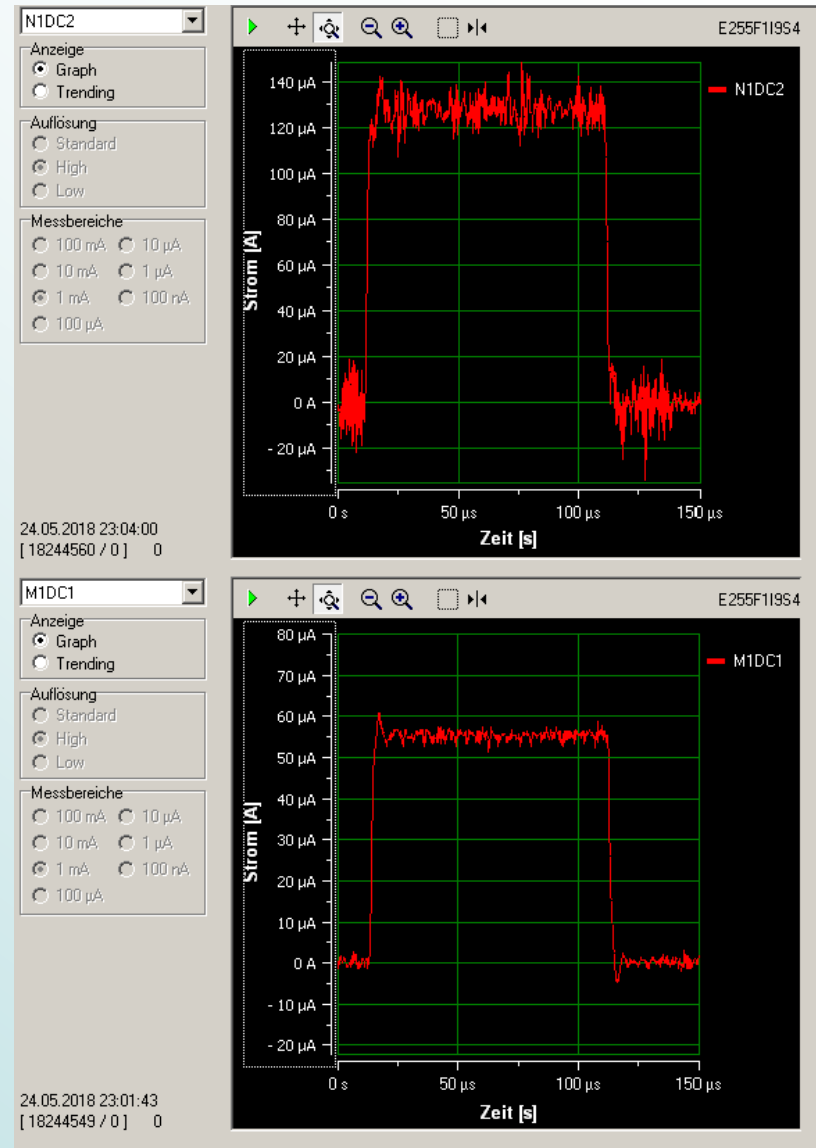
Example from HIT – uncooled FC for the MEBT section

# Realizations of Faraday Cups

Example measurements with Faraday cups shown on the previous slide (HIT):

Carbon beam ( $^{12}\text{C}^{4+}$ ) with 8 keV/u from an ECR ion source after the chopper directly in front of the RFQ

Carbon beam ( $^{12}\text{C}^{6+}$ ) with 7 MeV/u after the Linac (RFQ and IH-DTL) and the foil stripper



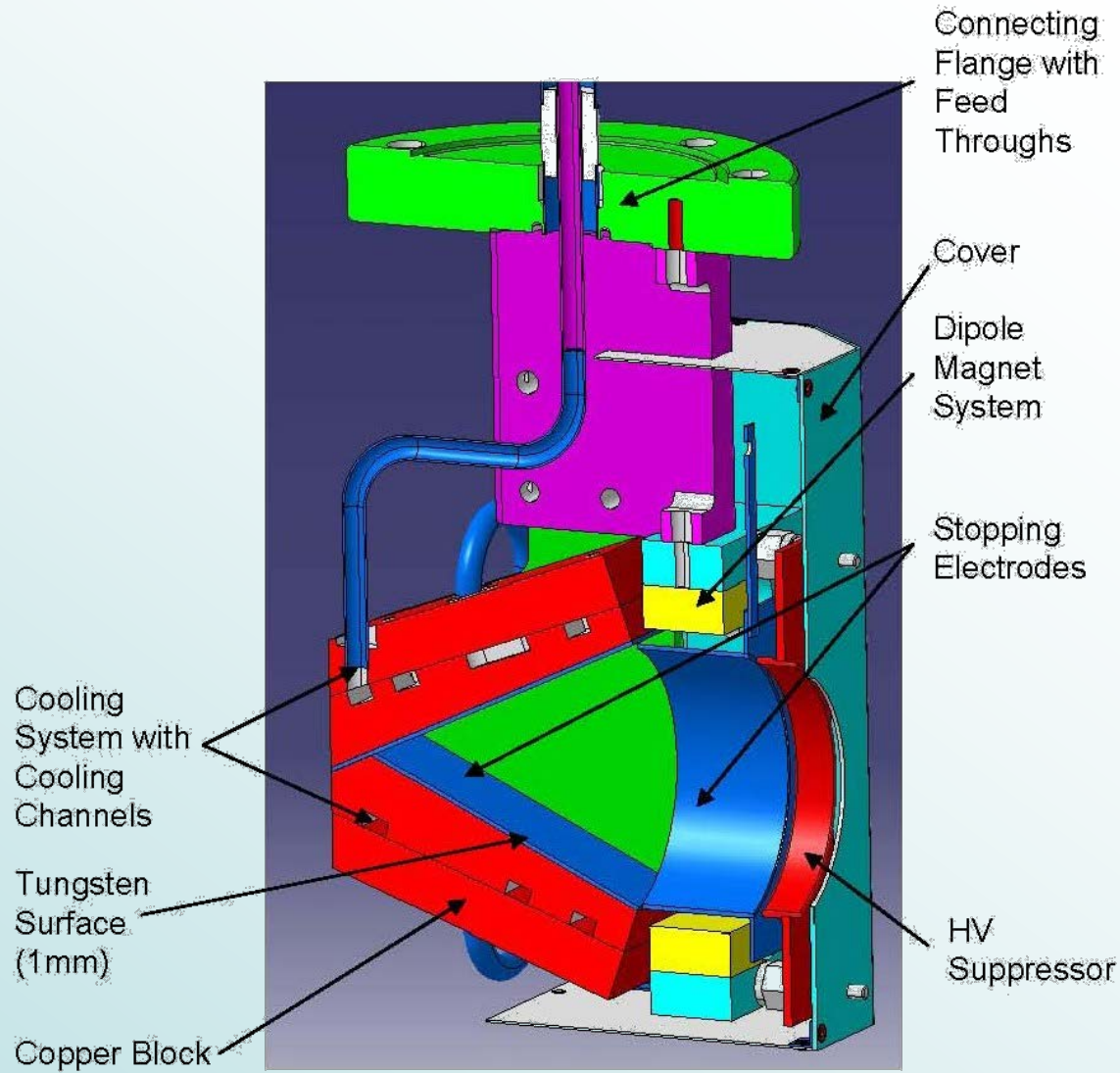
# Realizations of Faraday Cups

## High Power Version

needed e.g. for beams from ECR Ion Sources  
(**up to 20 mA** overall  
DC current possible) at  
low energies (**keV/u**)

→ very small  
penetration depth of  
only **some ten nm!**

Material with very high  
melting point needed,  
e.g. Tungsten or  
Tantalum with cone  
shape





# Realizations of Faraday Cups

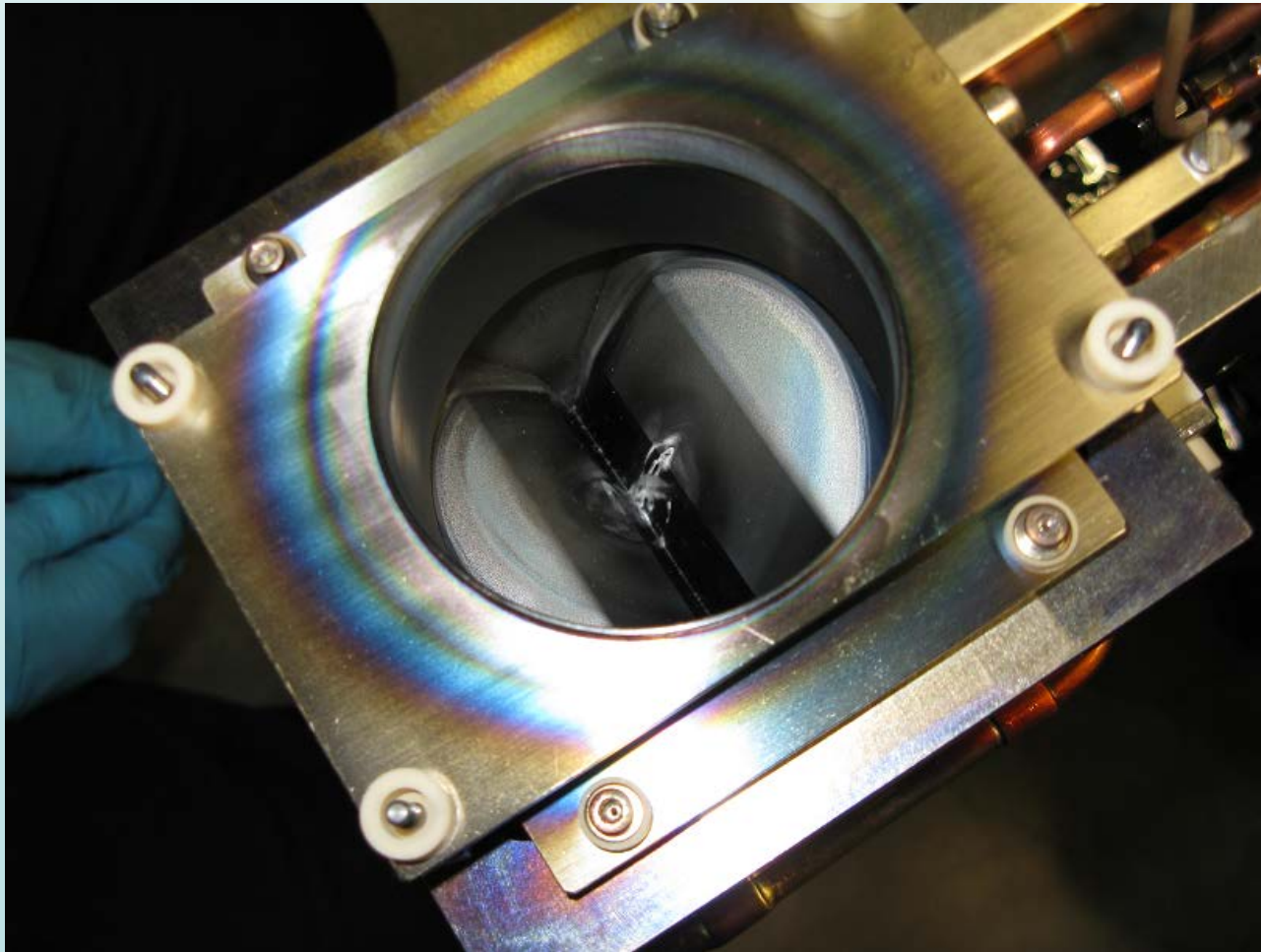
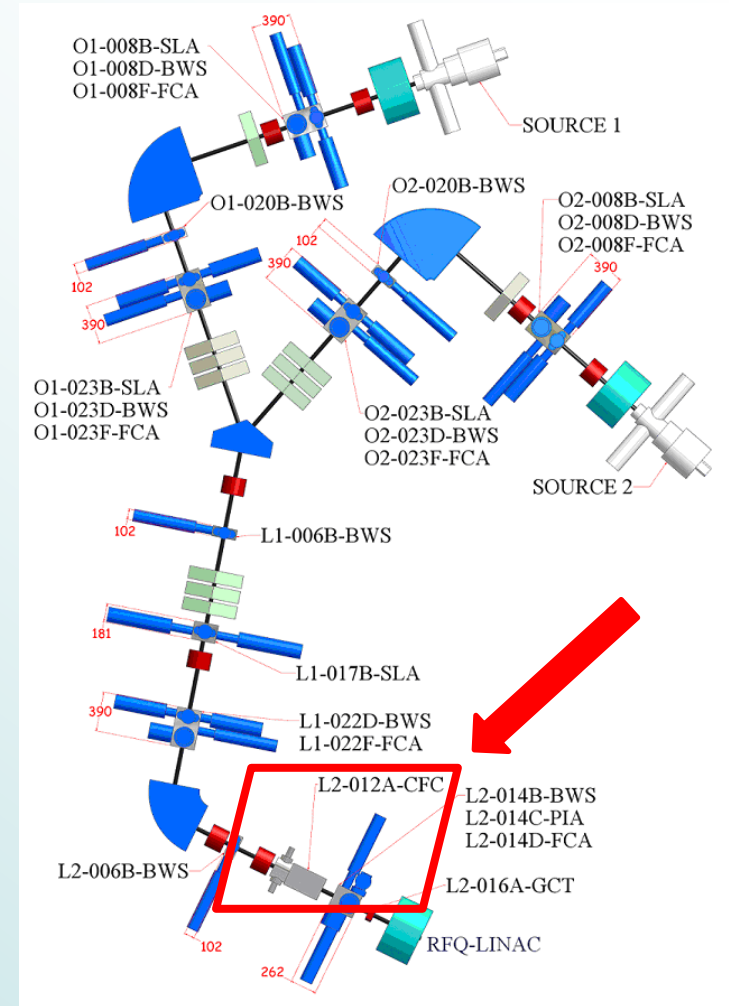
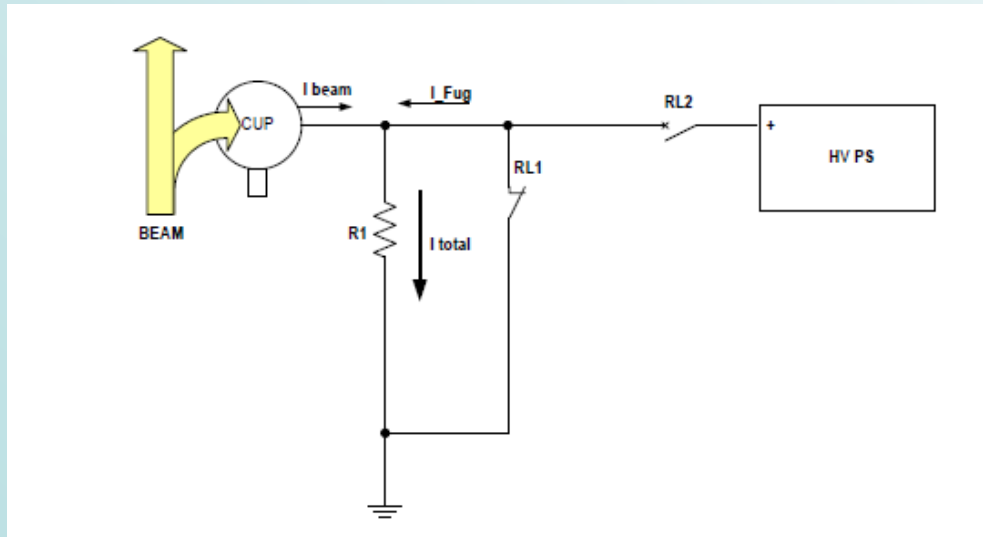


Photo of a used **Faraday cup** at the HIT LEBT, mounted closely behind the ECR ion sources, showing the **funnel-shaped geometry** → Obvious influences of **heating** and **sputtering** can be seen.

# A “non-interceptive” Faraday Cup

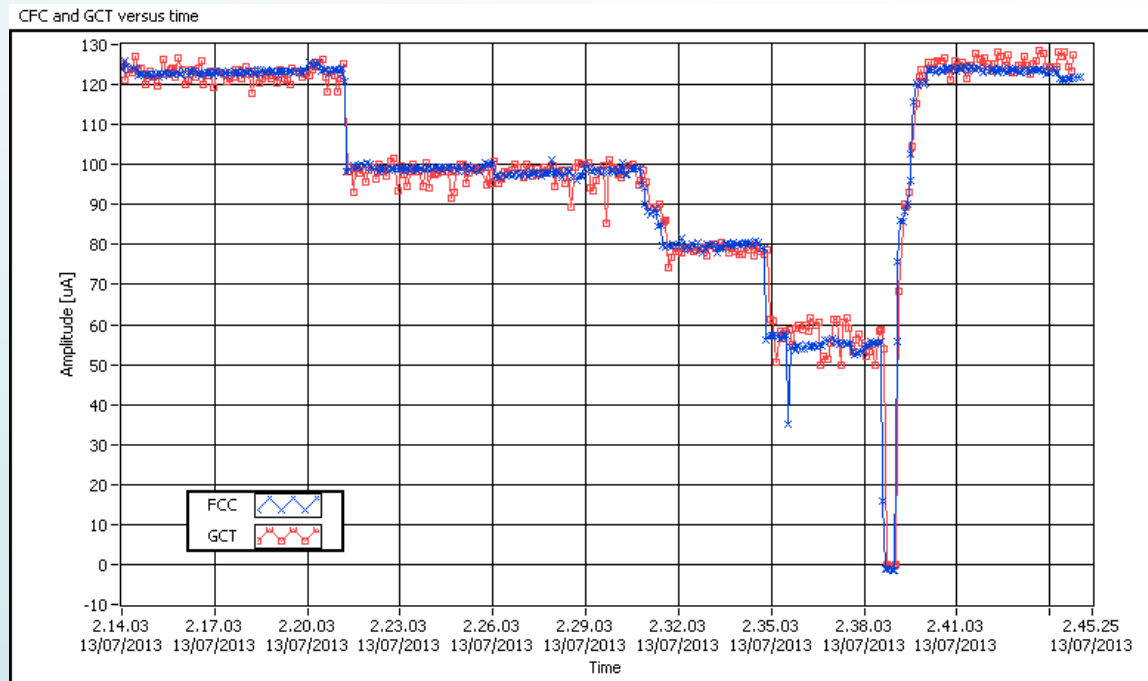
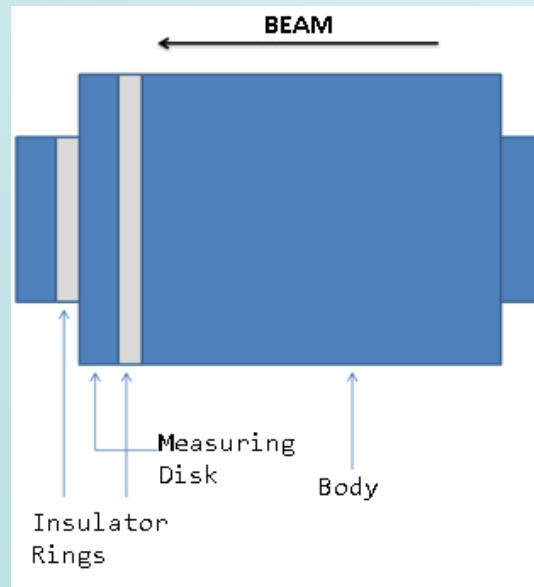
A **Chopper faraday Cup (CFC)** was designed and is presently in use on the CNAO machine. It **measures the chopped beam**, namely the beam (8keV/u energy) deviated by the Chopper deflector (installed at the end of the LEBT line) towards the vacuum chamber wall.



CNAO Low Energy Beam Transfer (LEBT) line



# A “non-interceptive” Faraday Cup



Current intensity vs. acquisition time for carbon ion beam: comparison of CFC and AC Current Transformer (at the entrance of the Linac) performances. [By courtesy of CNAO]

# Faraday Cups for High Energy Beams

Bethe Bloch formula: 
$$-\frac{dE}{dx} = 4\pi N_A r_e m_e c^2 \cdot \frac{Z_t}{A_t} \rho_t \cdot \frac{Z_p^2}{\beta^2} \left( \ln \frac{2m_e c^2 \gamma^2 \beta^2}{I} - \beta^2 \right)$$

Range: 
$$R = \int_0^{E_{\max}} \left( \frac{dE}{dx} \right)^{-1} dE$$

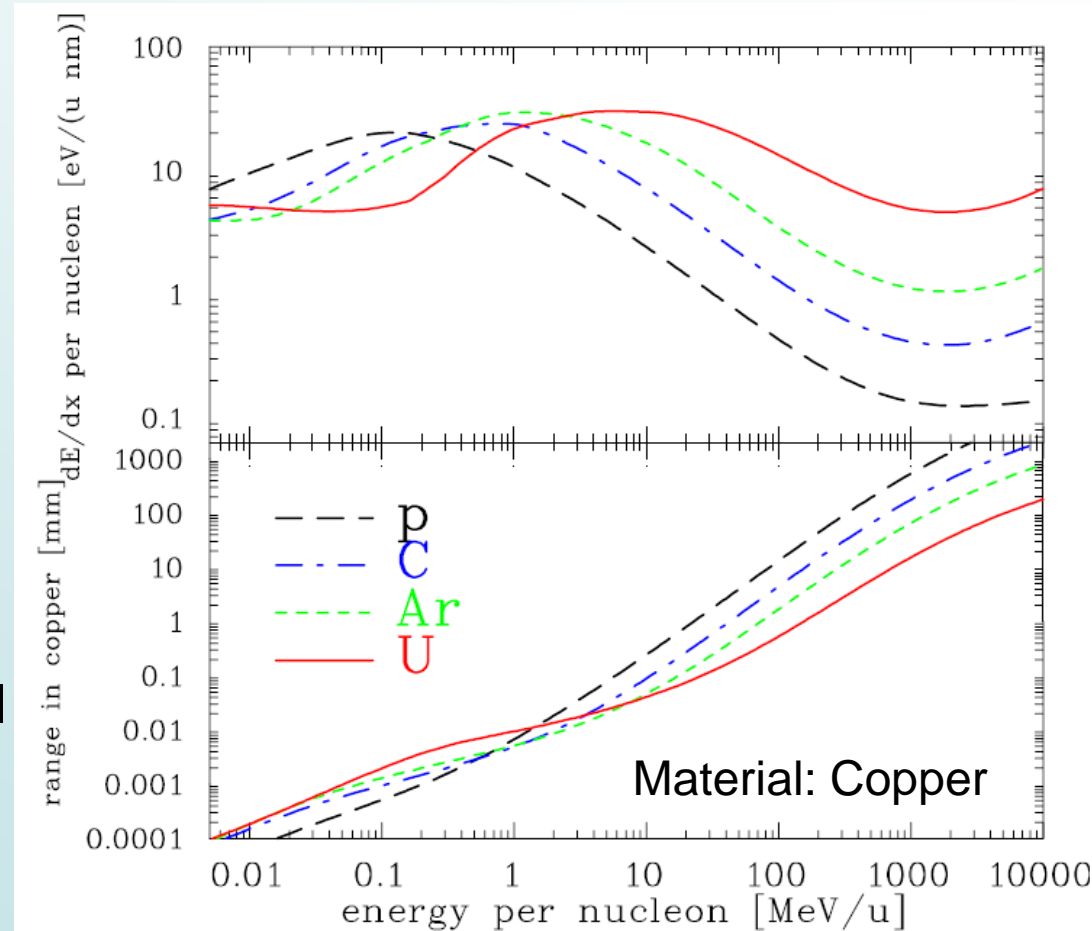
with approx. scaling  $R \propto E_{\max}^{1.75}$

→ Faraday Cups for **ion beams**

only for

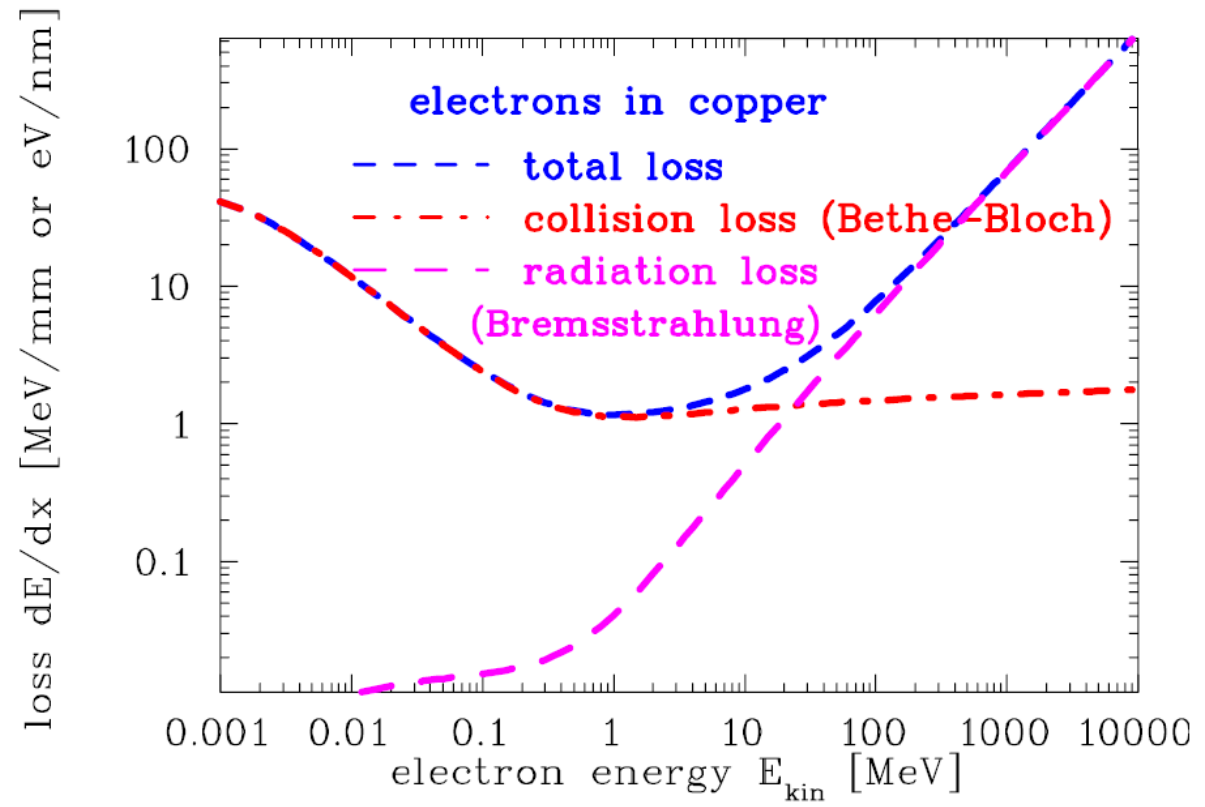
$E_{kin} < 100 \text{ MeV/u}$  with  $R < 10 \text{ mm}$ !

For higher energies more material is necessary (mechanics!), but nuclear reactions and fragments must be taken into account!



# Faraday Cups for High Energy Beams

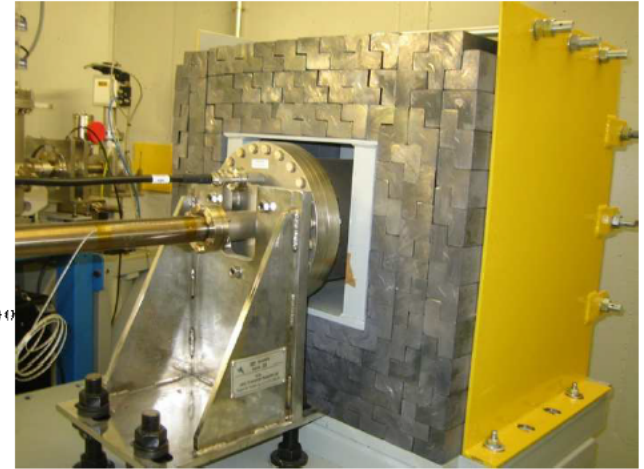
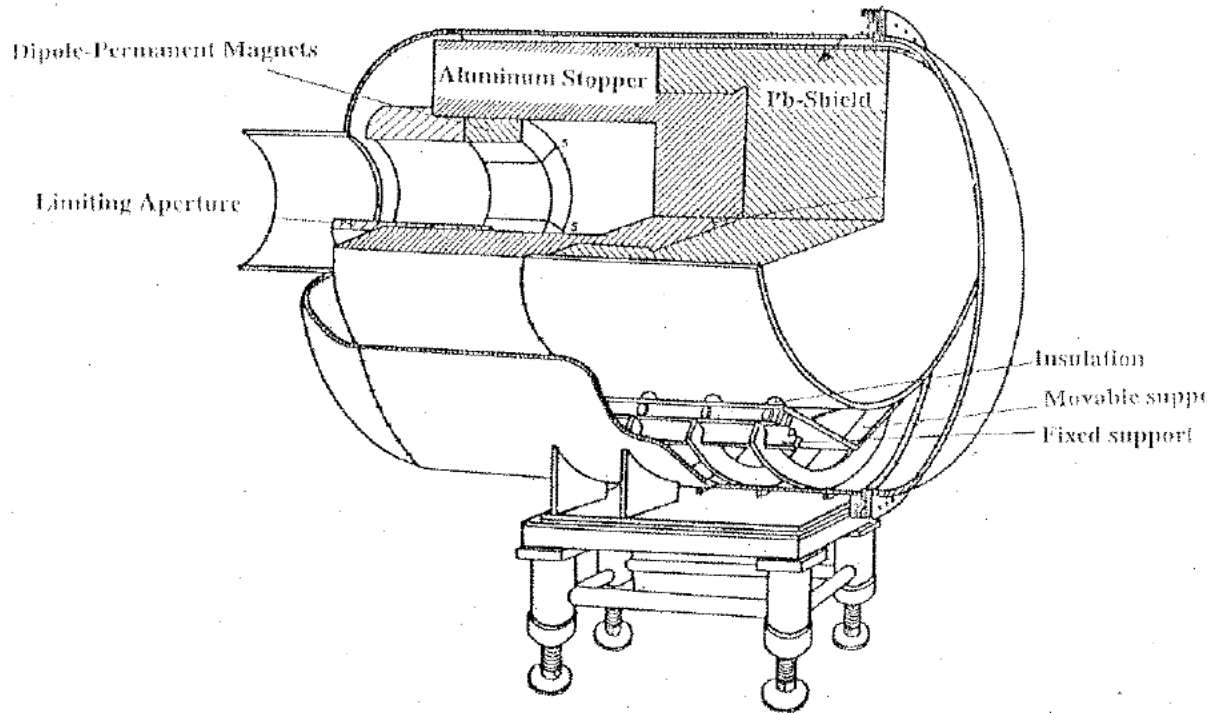
The stopping of **electrons** in matter differs from protons and ions → here the sum of the two relevant processes of collisional loss  $dE/dx_{\text{col}}$  (modified Bethe-Bloch formula for electrons) and radiation loss  $dE/dx_{\text{rad}}$  have to be added.



In addition: Electrons have much larger lateral straggling than ions and also the longitudinal straggling is larger resulting in a wider range distribution, thus Faraday cups for stopping electrons are seldom used at electron accelerators.

# Faraday Cups for High Energy Beams

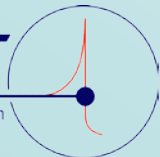
Example of a Faraday cup for 60 MeV Electrons



Left: A drawing of a Faraday cup used for **60 MeV electrons**.

Right: The installation of a Faraday cup used as a beam dump at ALBA, Barcelona.

# Particle Counters





# Particle Counters

- Used for **low current measurements of high-energetic particles** e.g. for slow extracted proton and ion beams from synchrotrons for atomic or nuclear physics experiments.
- Overview of the typical dynamic range of detectors:
  - For an ion rate below  $10^6 \text{ s}^{-1}$ , the individual particles can be counted by **scintillators**.
  - For the medium range from about  $10^4$  to  $10^9 \text{ s}^{-1}$  the energy loss in a gas is measured by an **ionization chamber (IC)**.
  - For the higher range from about  $10^8 \text{ s}^{-1}$  the emission of secondary electrons from a metal surface forced by the primary ion's energy loss is determined by **secondary electron monitors (SEM)**.

# Scintillation Counters

Plastic Scintillator i.e. organic fluorescence molecules in a plastic matrix

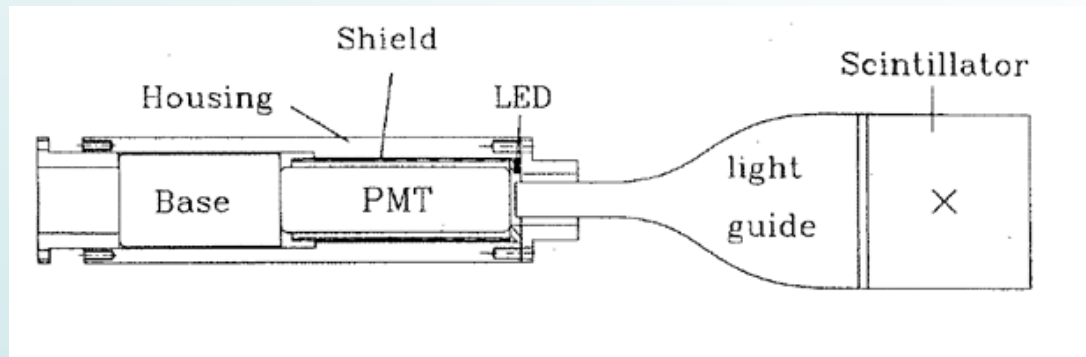
**Advantage:** easily machinable, cheap, blue wave length, fast decay time

**Disadvantage:** not radiation hard

Particle counting: PMT → discriminator → scaler → computer

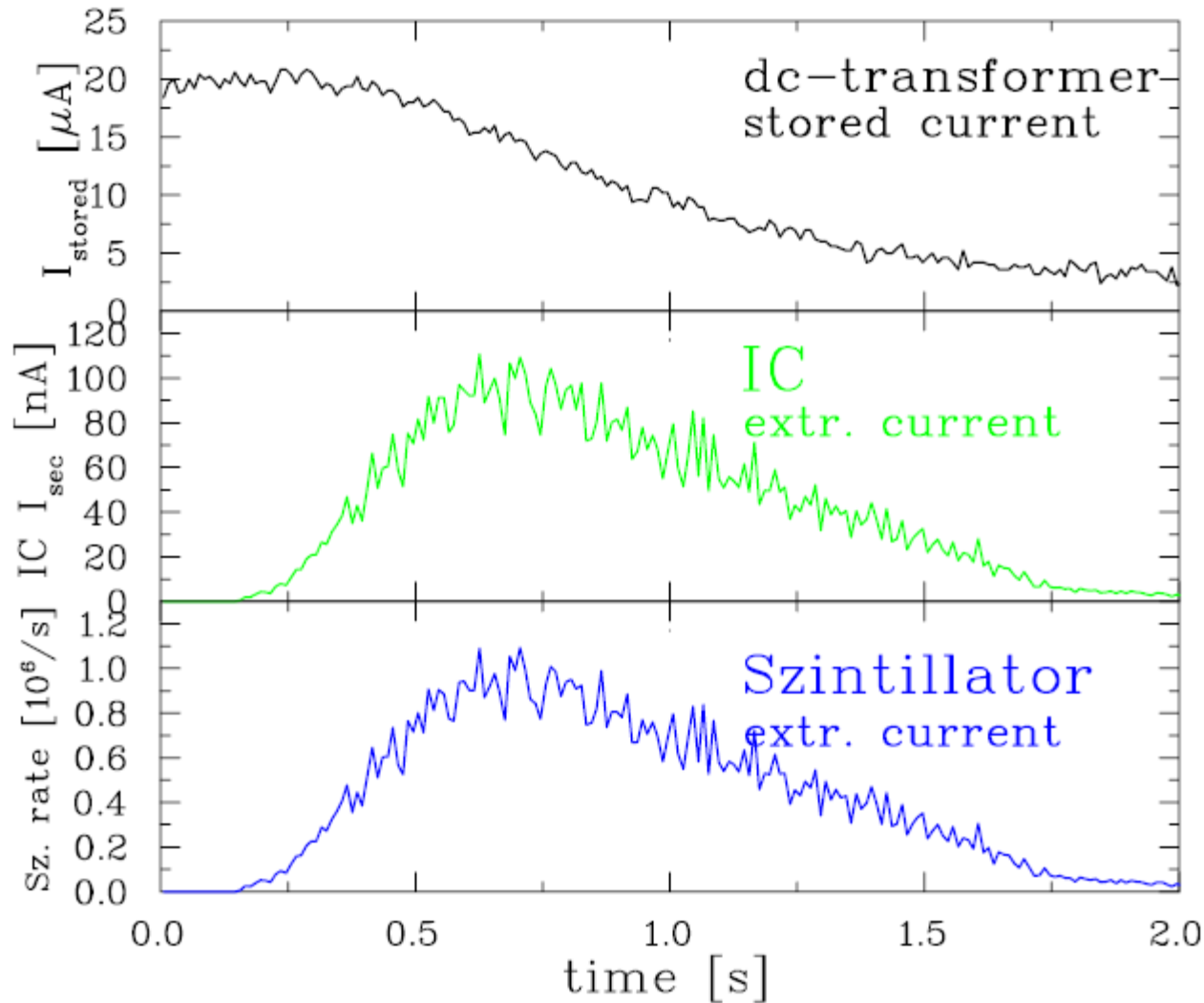


Example from HIT (HEBT section)

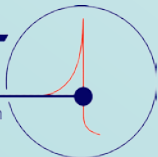


Active Area:	75×75 mm <sup>2</sup>
Thickness:	3 mm
Scintillation material:	BC400
Measurement rate:	<10 <sup>6</sup> Particles/s

# Scintillation Counters



Example of extracted beam (250 MeV/u  $^{208}\text{Pb}^{67+}$ ) from GSI's SIS18 Heavy Ion Synchrotron showing the maximum dynamics of **Scintillation Counters**  $\rightarrow$  for higher currents the use of **Ionization Chambers** is necessary.



# Ionization Chambers

Energy loss in matter (mainly gases) → electronic stopping:

Bethe Bloch-  
Equation:

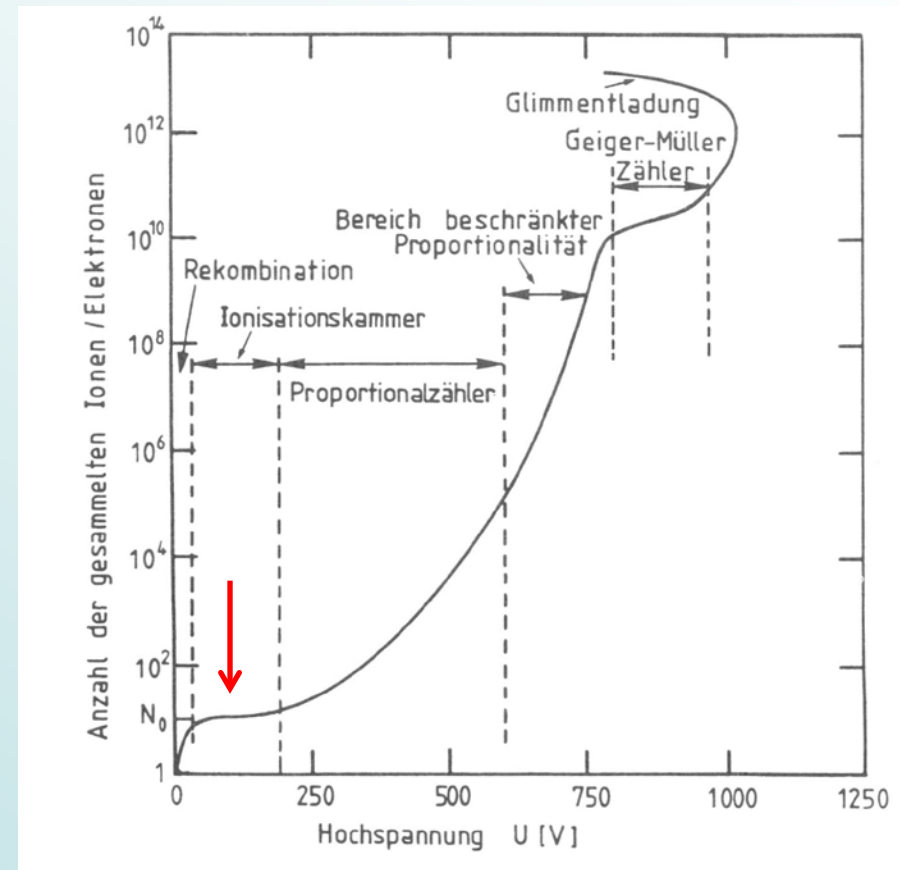
$$-\frac{dE}{dx} = 4\pi N_A r_e^2 m_e c^2 \cdot \frac{Z_t}{A_t} \rho \left( \frac{Z_p^2}{\beta^2} \right) \left[ \ln \frac{2m_e c^2 \gamma^2 \beta^2}{I} - \beta^2 \right]$$

Target:

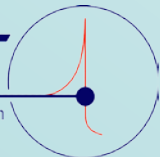
Charge & Mass ( $Z_t$ ,  $A_t$ ), Density ( $\rho$ ),  
Ionization Potential ( $I$ )

Projectile:

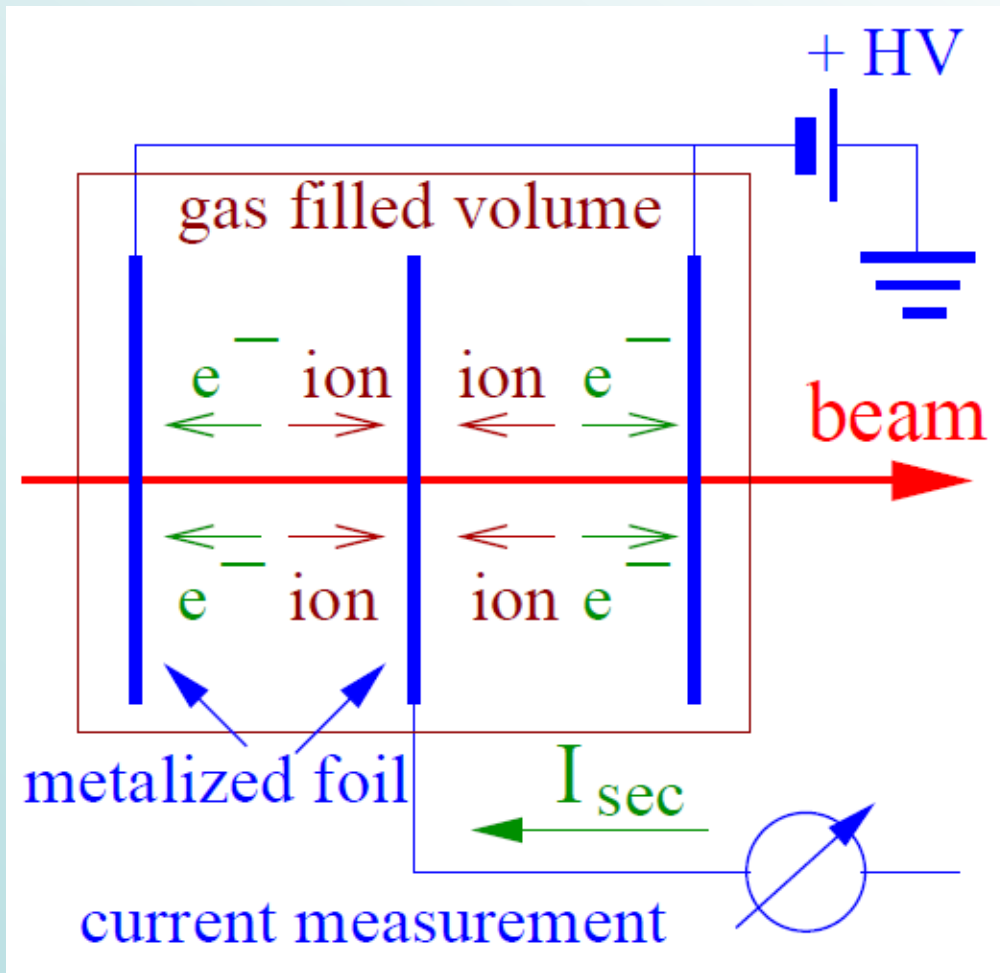
effective charge ( $Z_p$ ), Velocity ( $\gamma$ ,  $\beta$ )



Operating ranges of gas detectors



# Ionization Chambers



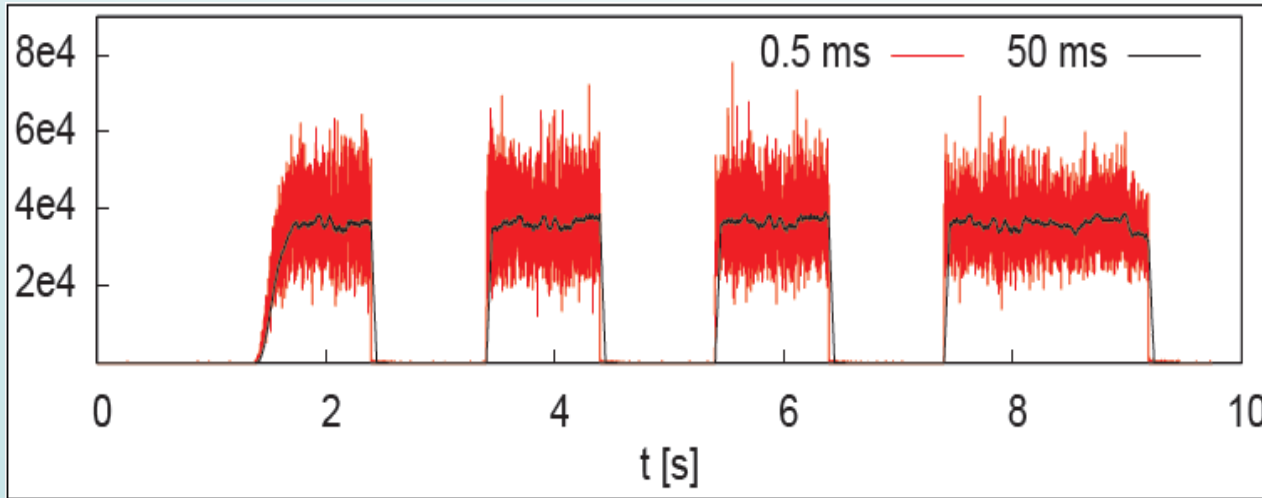
$$I_{sec} = \frac{1}{W} \cdot \frac{dE}{dx} \Delta x \cdot I_{beam}$$

Choice of output signal strength  
vs. response velocity

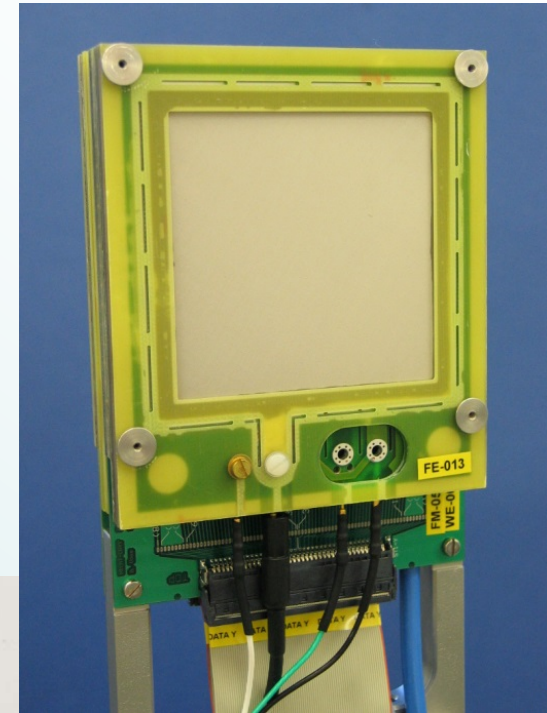
Gas	W-value [eV]
H <sub>2</sub>	36.4
He	42.7
N <sub>2</sub>	36.4
O <sub>2</sub>	32.2
Ar	26.3
CH <sub>4</sub>	29.1
CO <sub>2</sub>	33.0



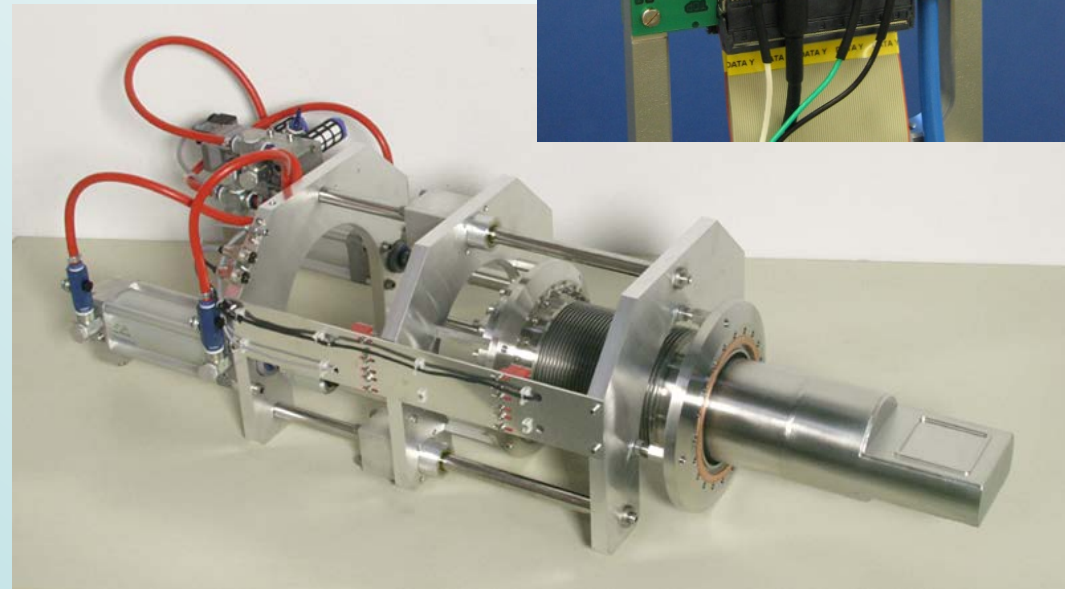
# Ionization Chambers



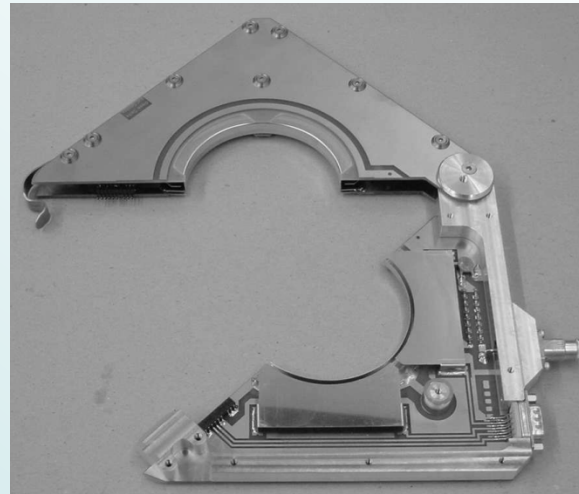
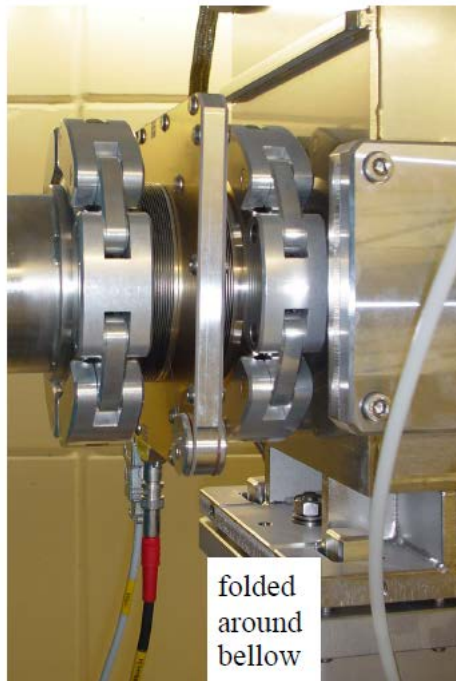
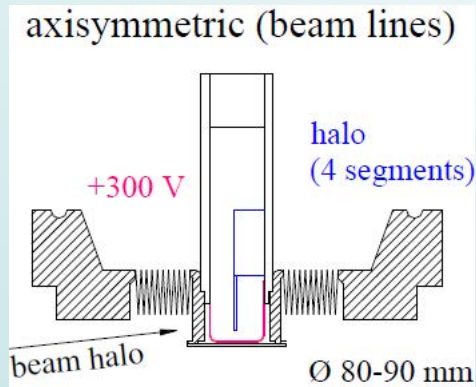
Intensity of extracted beam from HIT synchrotron („spill” with pauses)



IC detector (upper right):  
70x70 mm<sup>2</sup> active area,  $\Delta x=3$  mm,  
with Ar/CO<sub>2</sub> gas mixture;  
air-pressured actuator with  
stainless steel windows (50  $\mu$ m)

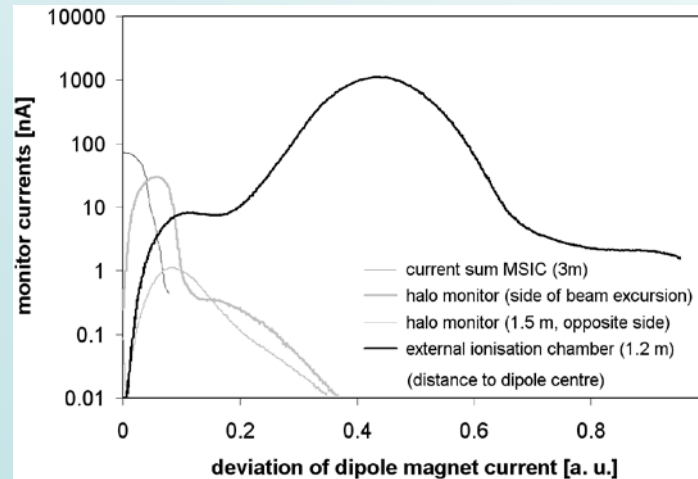


# Ionization Chambers



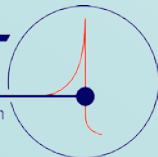
Ionization chambers as **halo monitors** around the beam pipe for **online monitoring of beam displacements**

[By courtesy of PSI]



Signal levels of several monitors when the beam is steered far off-axis

Beam current: 1.4 nA  
Beam energy: 230 MeV

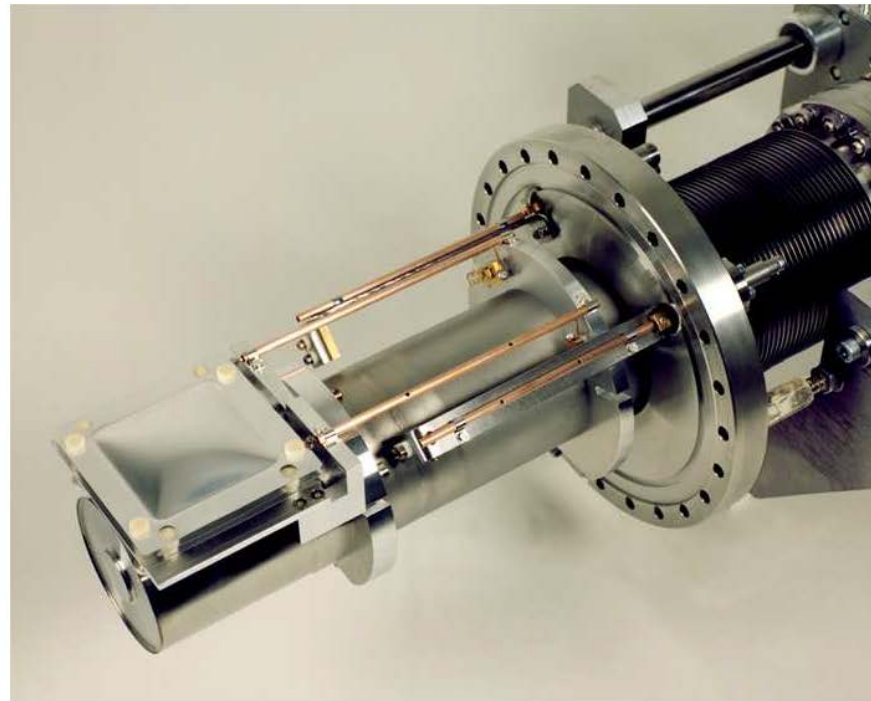
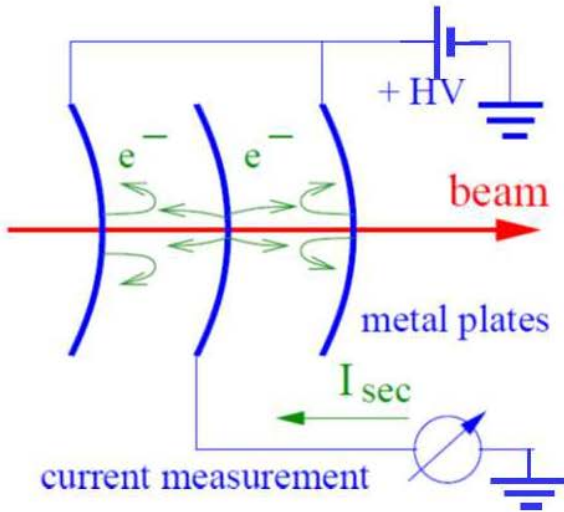


# Secondary Electron Monitors (SEM)

The secondary emission current depends on the energy loss at the surface  $dE/pdx$ , it is given by the Sternglass formula:

$$I_{sec} = Y \cdot dE/pdx \cdot I_{beam}$$

with  $Y$  being the yield factor describing the amount of secondary emission per unit of energy loss at the surface.



Left: **Scheme of a SEM**

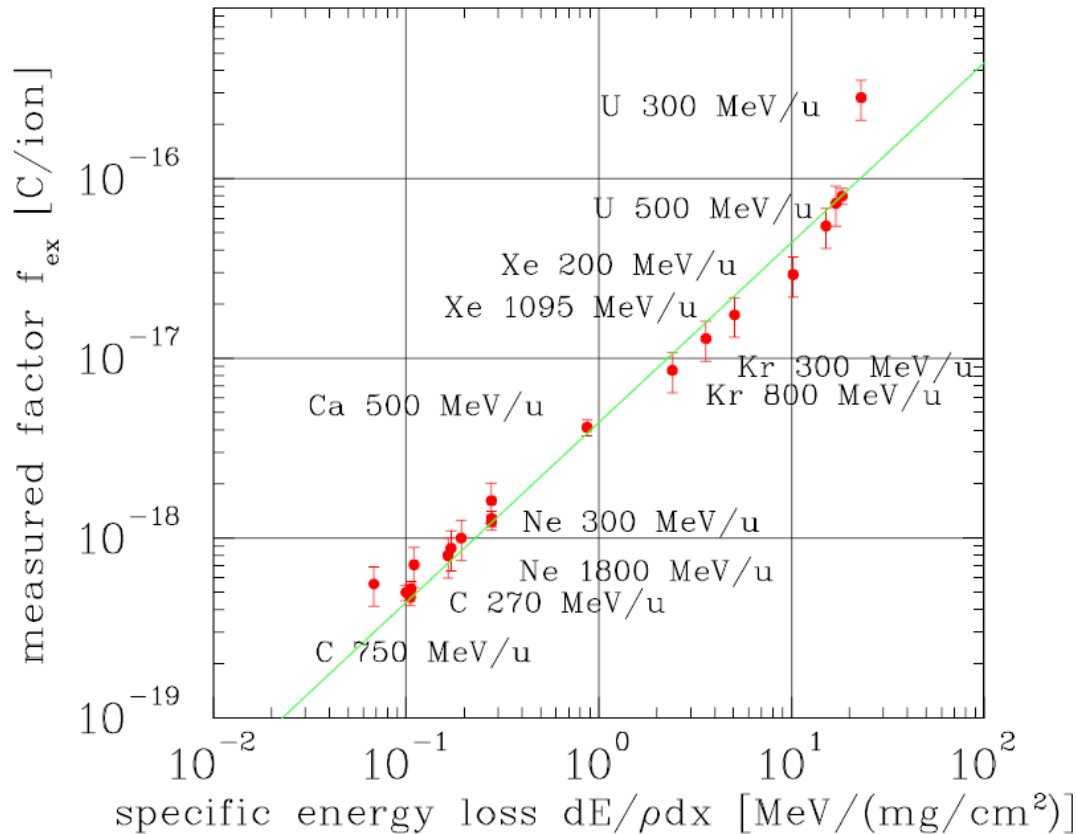
made of three metal foils.

Right: **Photo of the SEM** part

made of 3 Al foils with thickness of 100  $\mu\text{m}$  used for slow extraction meas. at GSI



# Secondary Electron Monitors (SEM)



**Calibration curve of a SEM**  
with 3 Al foils – the yield factor value was fitted to

$$Y = 27.4 \text{ e}^-/(\text{MeV}/\text{mg}/\text{cm}^2)$$

for various slowly extracted ions from the GSI synchrotron.

Value may depend on surface properties, e.g. material production and cleaning method.

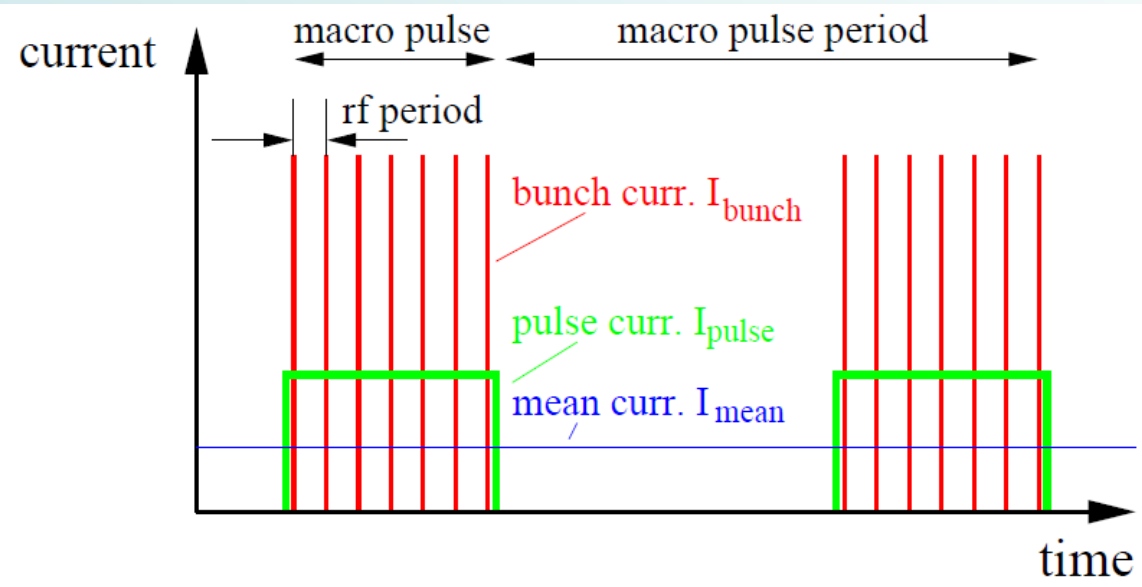
The emission yield  $Y$  might change with irradiation, caused by modifications of the surface. A degradation by a factor of two was measured after  $10^{18}$  protons/cm<sup>2</sup> (beam of 450 GeV at CERN SPS) → Ti-foils show a much lower sensitivity to radiation.

# Current Transformers



# Current Measurement – Pulsed Beams

Pulsed LINACs and cyclotrons used for injection to synchrotrons with  $t_{pulse} \approx 100 \mu s$ :

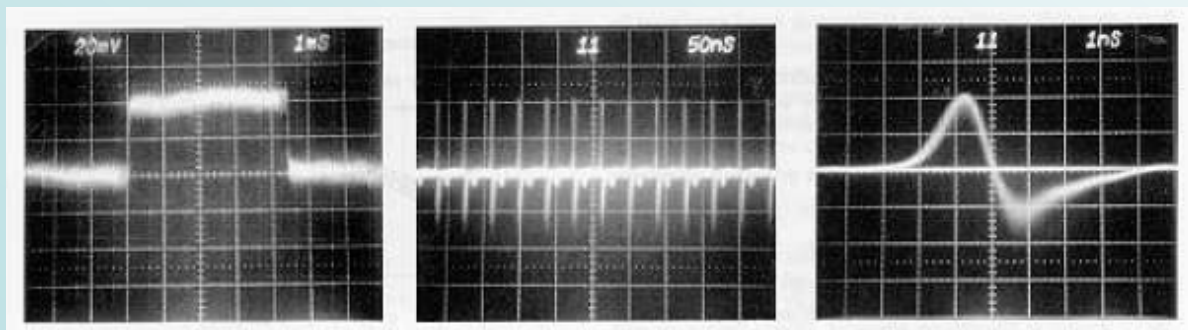


**One distinguish between:**

- Mean current  $I_{mean}$ 
  - long time average in [A]
- Pulse current  $I_{pulse}$ 
  - during the macro pulse in [A]
- Bunch current  $I_{bunch}$ 
  - during the bunch in [C/bunch]
  - or [particles/bunch]

**Remark:** ECR ion sources:  
→ no bunch structure / DC

**Example:**  
Pulse and bunch structure at GSI LINAC



# Magnetic field of the beam and the ideal transformer

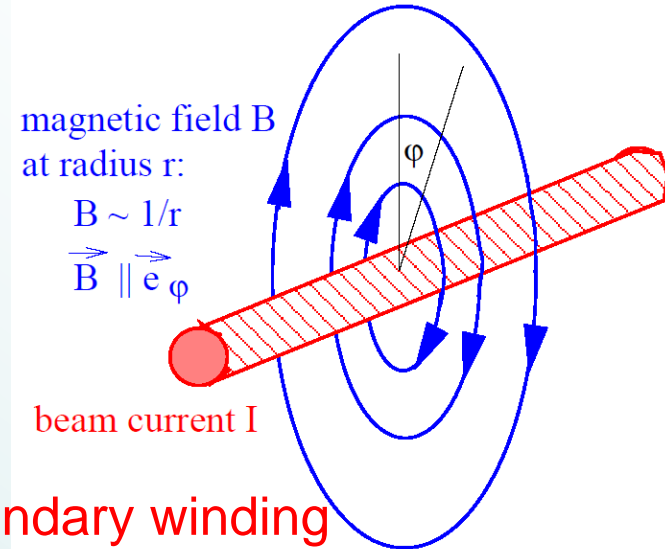
- Beam current of  $N$  charges with velocity  $\beta$ :

$$I_{beam} = qe \cdot \frac{N}{t} = qe \cdot \beta c \cdot \frac{N}{l}$$

- Cylindrical symmetry → only azimuthal component

$$\vec{B} = \mu_0 \frac{I_{beam}}{2\pi r} \cdot \vec{e}_\varphi$$

(Example: 1  $\mu$ A,  $r = 10$ cm → 2 pT)



**Idea: Beam as primary winding and sense by secondary winding**

⇒ Loaded current transformer

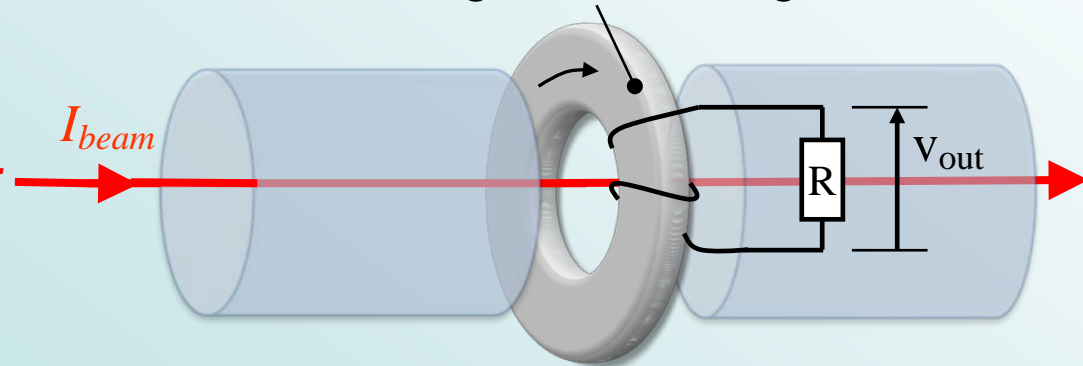
$$I_1/I_2 = N_2/N_1 \rightarrow I_{sec} = 1/N \cdot I_{beam}$$

- Inductance of a torus of  $\mu_r$

$$L = \frac{\mu_0 \mu_r}{2\pi} \cdot l N^2 \cdot \ln \frac{r_{out}}{r_{in}}$$

- Goal of Torus: Large inductance  $L$  **and** guiding of field lines.

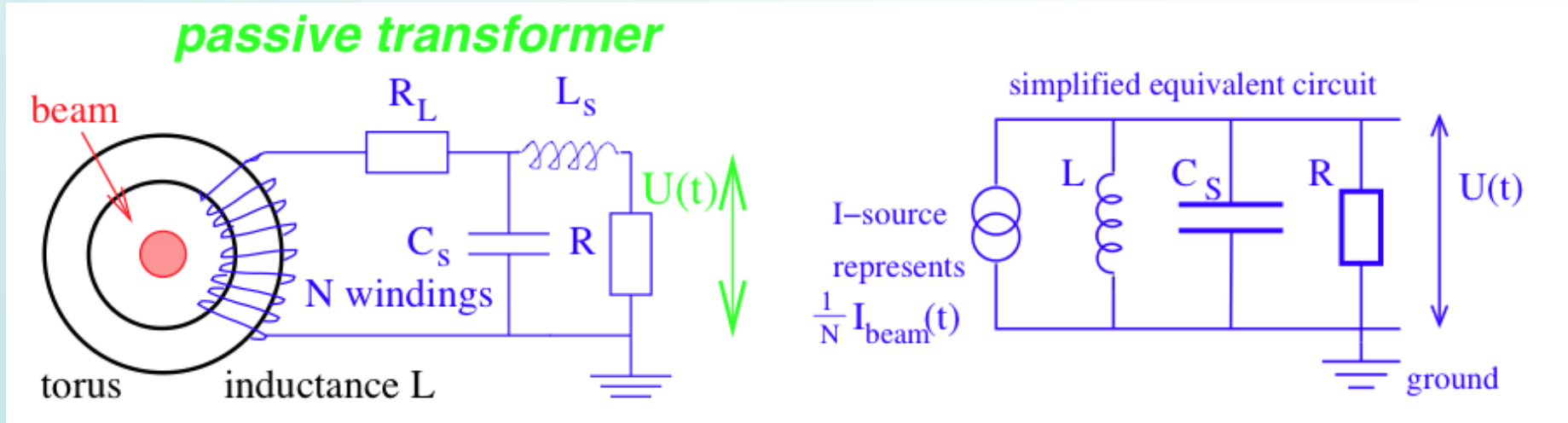
Torus to guide the magnetic field



Definition:  $U = L \cdot dl/dt$

# Passive Transformer / Fast Current Transformer (FCT)

Simplified electrical circuit of a passively loaded transformer:



A voltage is measured:  $U = R \cdot I_{sec} = R/N \cdot I_{beam} \equiv S \cdot I_{beam}$

with **S sensitivity [V/A]**, equivalent to transfer function or transfer impedance **Z**.

Equivalent circuit is used for analysis of sensitivity and bandwidth

(disregarding the loss resistivity  $R_L$ )

# Passive Transformer: Rise and Droop Time

## Time domain description:

Droop time:  $t_{droop} = 1/3f_{low} = L/R$

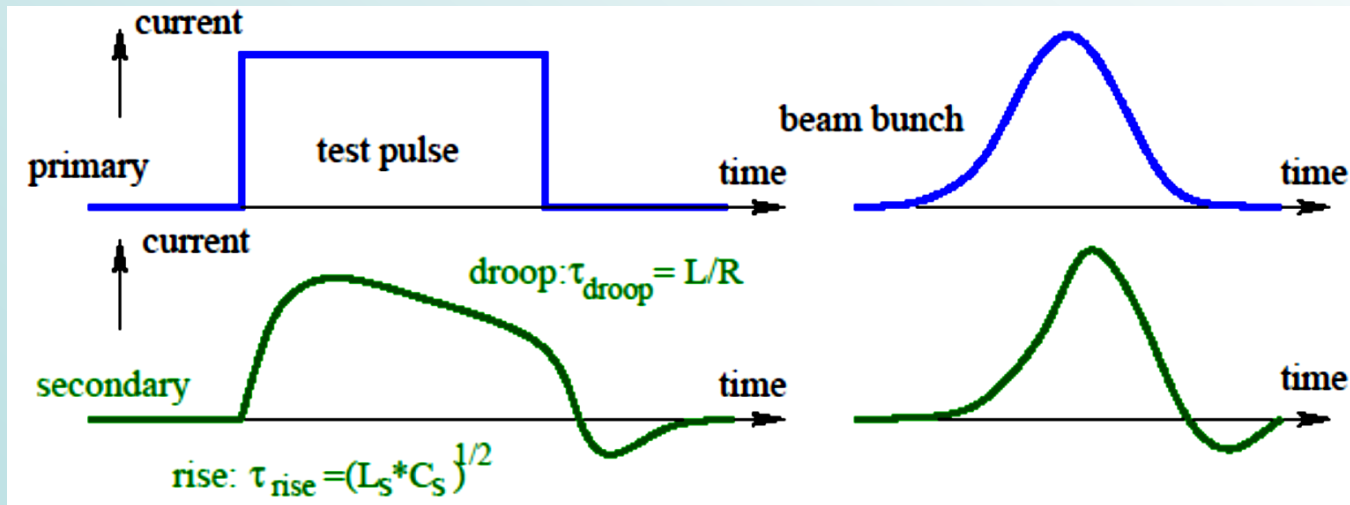
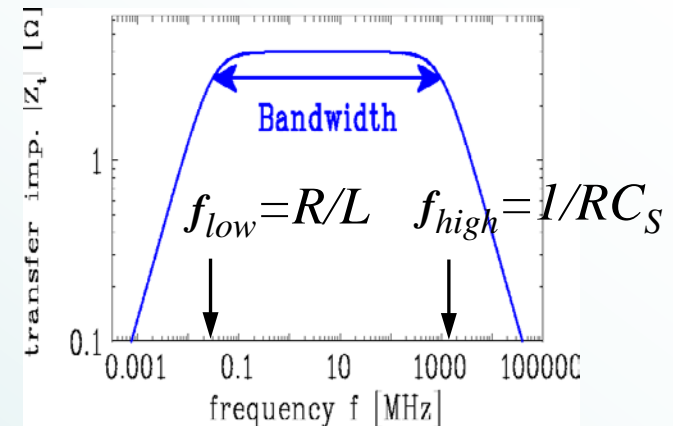
Rise time:  $t_{rise} = 1/3f_{high} = 1/RC_S$  (ideal without cables)

Rise time:  $t_{rise} = 1/3f_{high} = \sqrt{L_S C_S}$  (with cables)

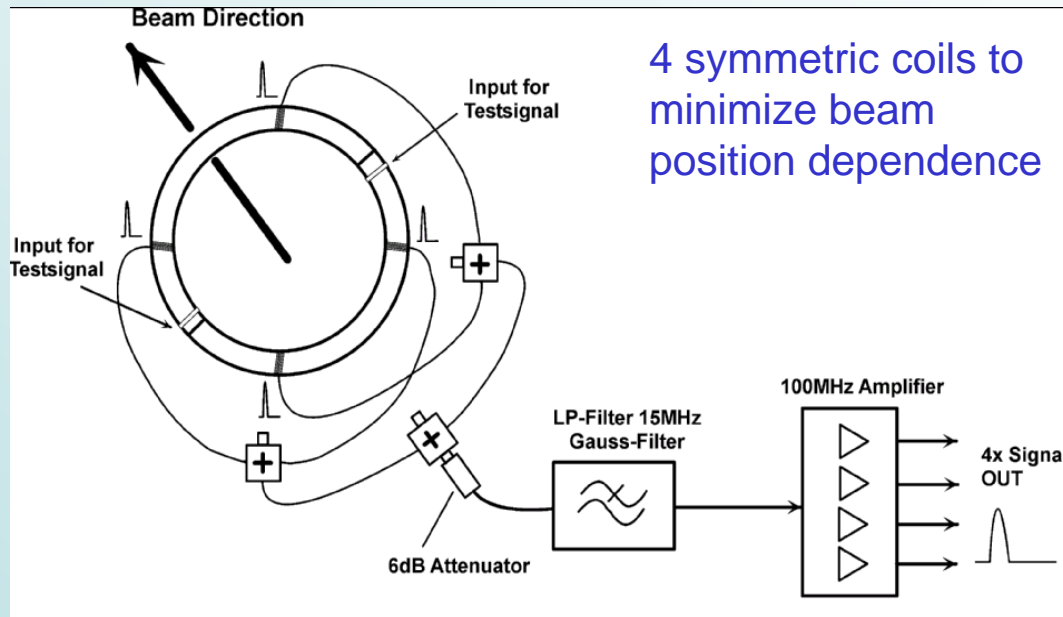
$R_L$ : loss resistivity,  $R$ : for measuring.

For the working region the voltage output is

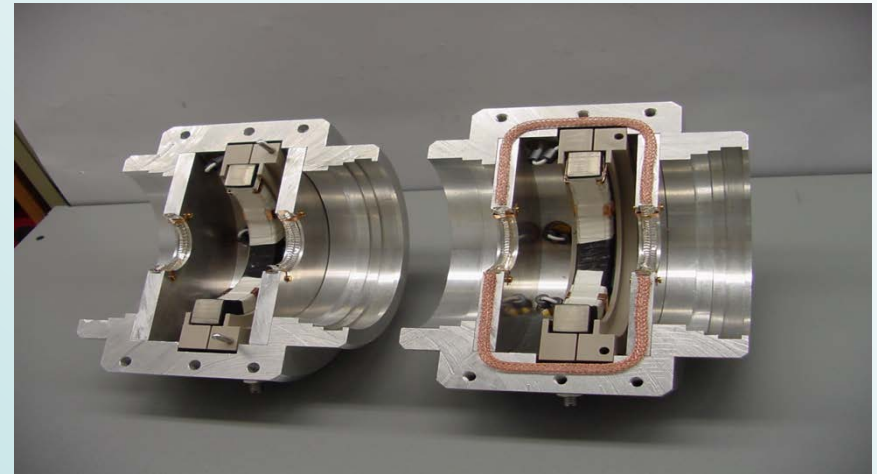
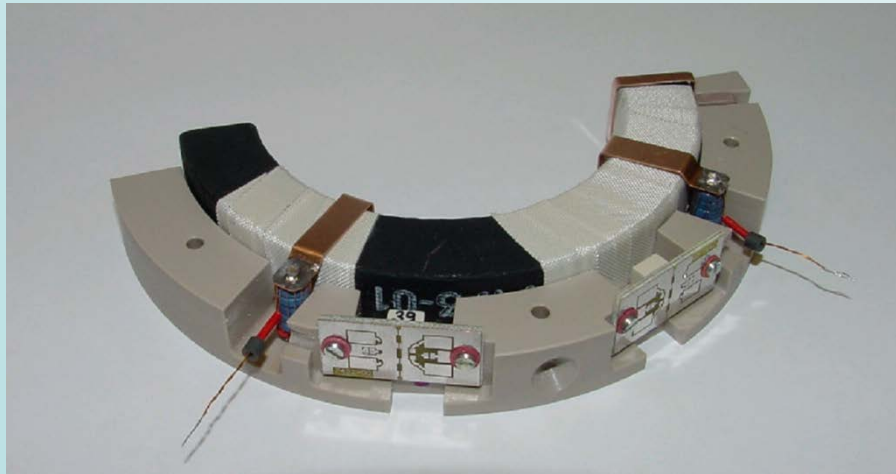
$$U(t) = \frac{R}{N} \cdot e^{-t/\tau_{droop}} \cdot I_{beam}$$



# Passive Transformer / Fast Current Transformer (FCT)



Standard Beam Current Monitors for XFEL and FLASH II (with split core for easier mounting)

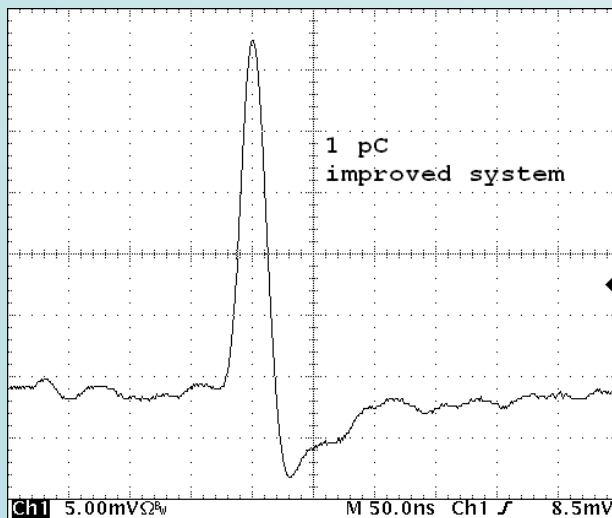
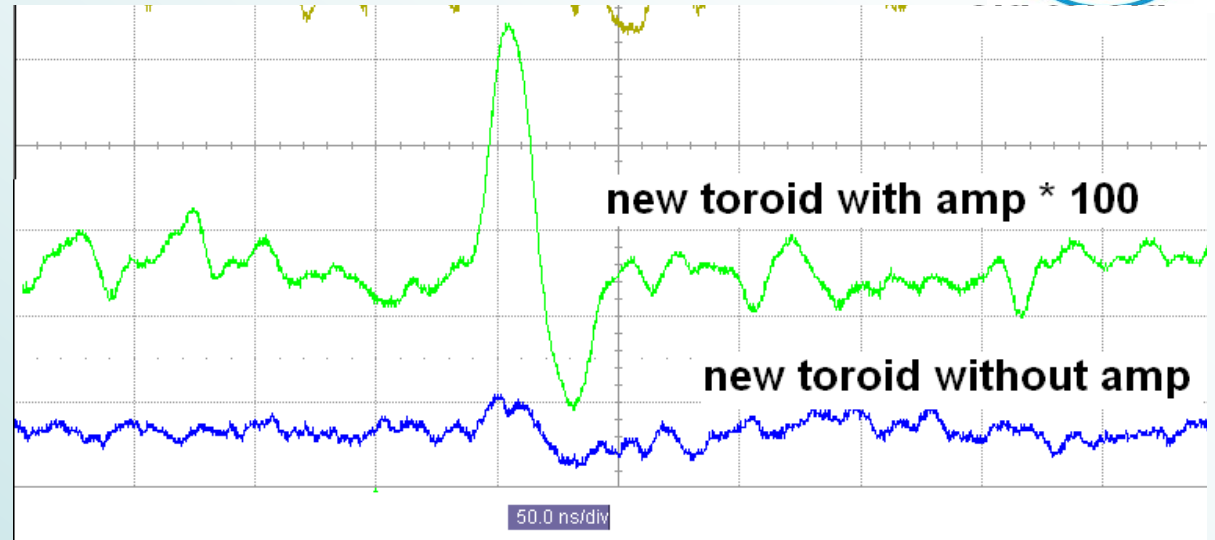
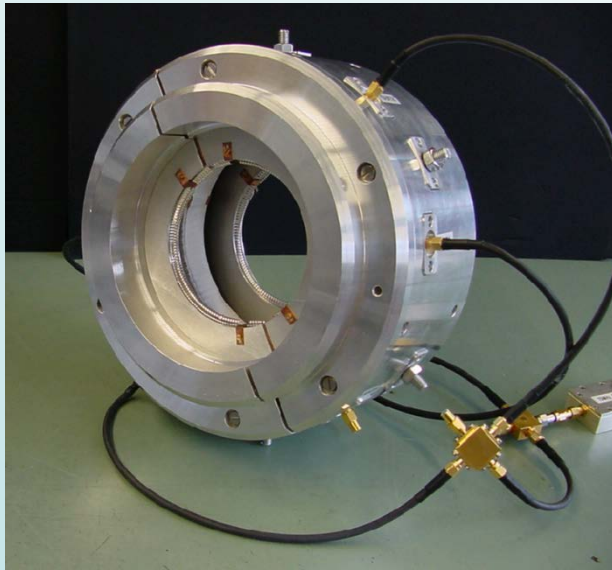




# Passive Transformer / Fast Current Transformer (FCT)



Complete FCT setup



Left: Measurement in the lab → achieved resolution of **< 0.02 pC RMS**

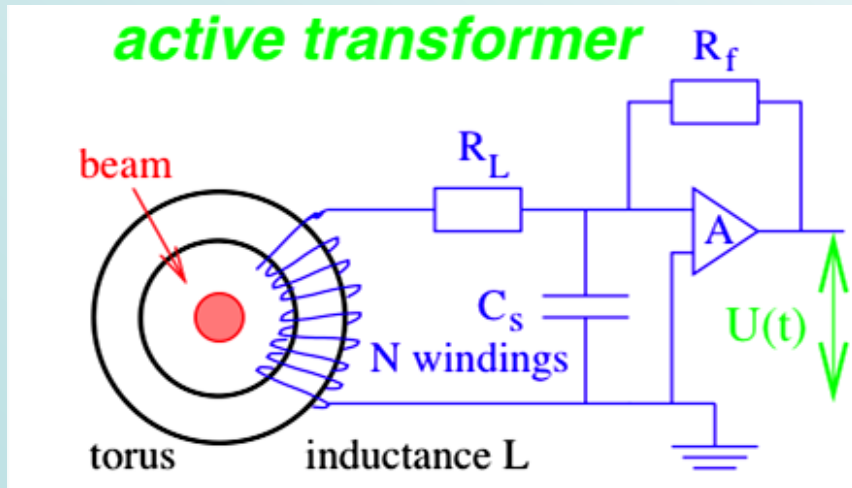
Above: Operation in FLASH with 8 pC bunches, estimated resolution **~ 0.6pC RMS** (BW=20MHz, non-averaged).

# “Active” Transformer with longer Droop Time

An Active Transformer or Alternating Current Transformer **ACT** uses a trans-impedance amplifier (I/U converter) to a  $R \approx 0 \Omega$  load impedance i.e. a current sink + compensation feedback

⇒ longer droop time  $t_{droop}$

Application: measurement of longer pulses with  $t > 10 \mu s$  e.g. at LINACs



The input resistor is for an op-amp:

$$R_f/A \ll R_L$$

$$\Rightarrow t_{droop} = L/(R_f/A + R_L) \approx L/R_L$$

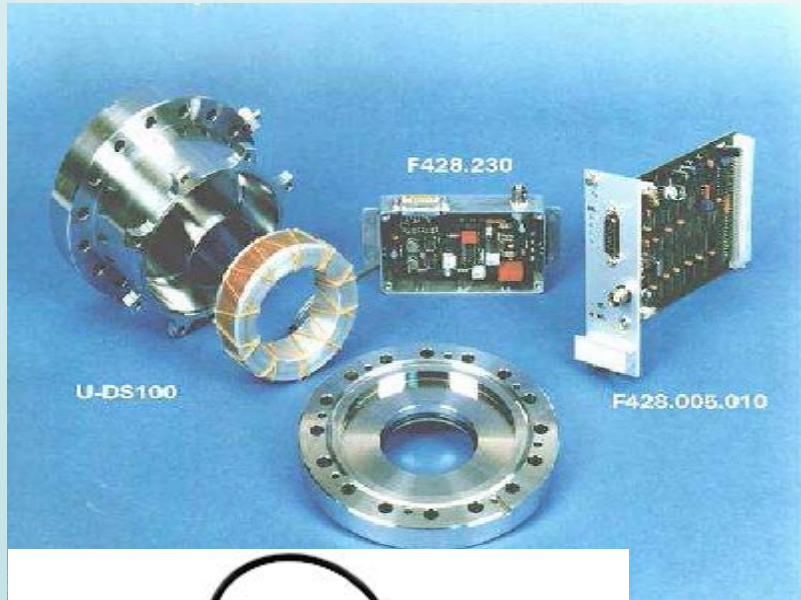
Droop time constant can be up to 1 s!

The feedback resistor is also used for range switching.

→ An additional active feedback loop is used to compensate the droop.

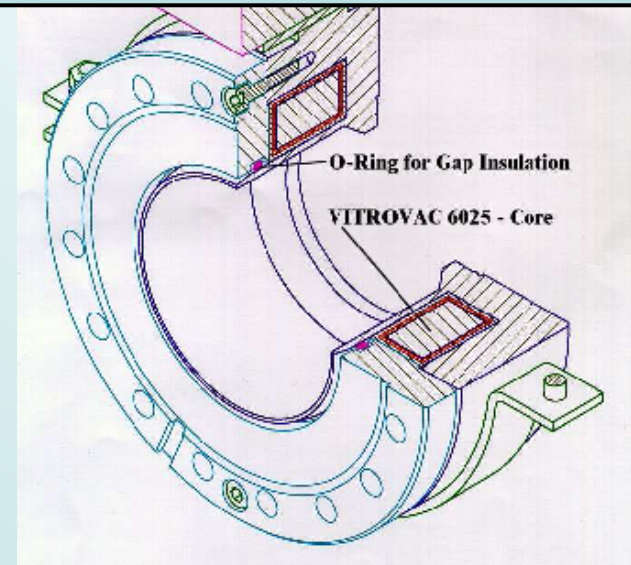
# “Active” Transformer Realization

Active transformer system used at GSI Linacs and for the HIT and CNAO injectors



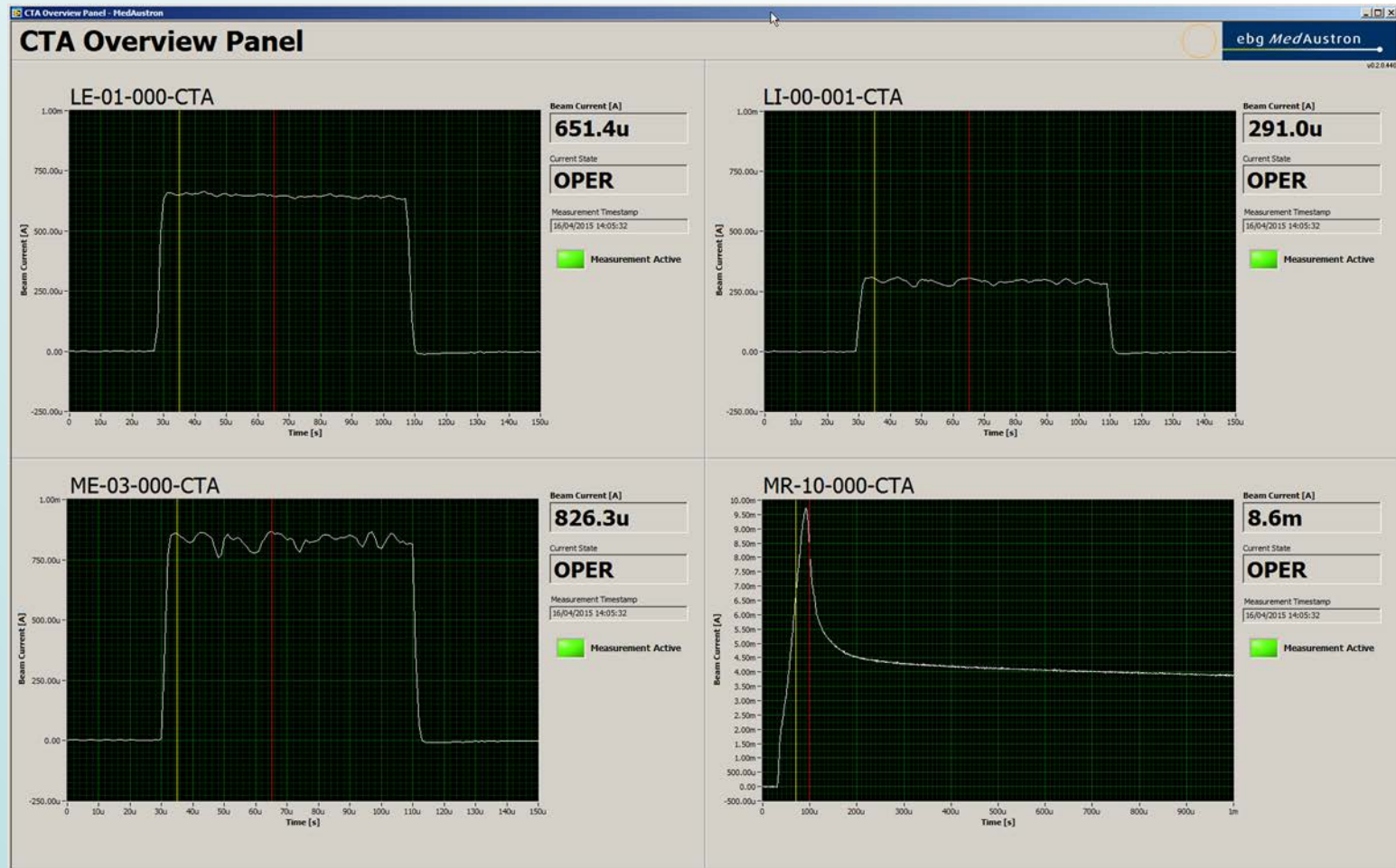
System offered by Bergoz, used at MedAustron, MIT and SHPIC (Shanghai)

Torus inner radius	$r_i=30$ mm
Torus outer radius	$r_o=45$ mm
Core thickness	$l=25$ mm
Core material	Vitrovac 6025 $(\text{CoFe})_{70\%}(\text{MoSiB})_{30\%}$
Core permeability	$\mu_r=10^5$
Number of windings	2x10 crossed
Max. sensitivity	$10^6$ V/A
Beam current range	10 $\mu\text{A}$ to 100 mA
Bandwidth	1 MHz
Droop rms resolution	0.5 % for 5 ms 0.2 $\mu\text{A}$ for full bw





# “Active” Transformer Measurements



MedAustron: ACCT overview panel during commissioning

# Current Measurement of DC beams

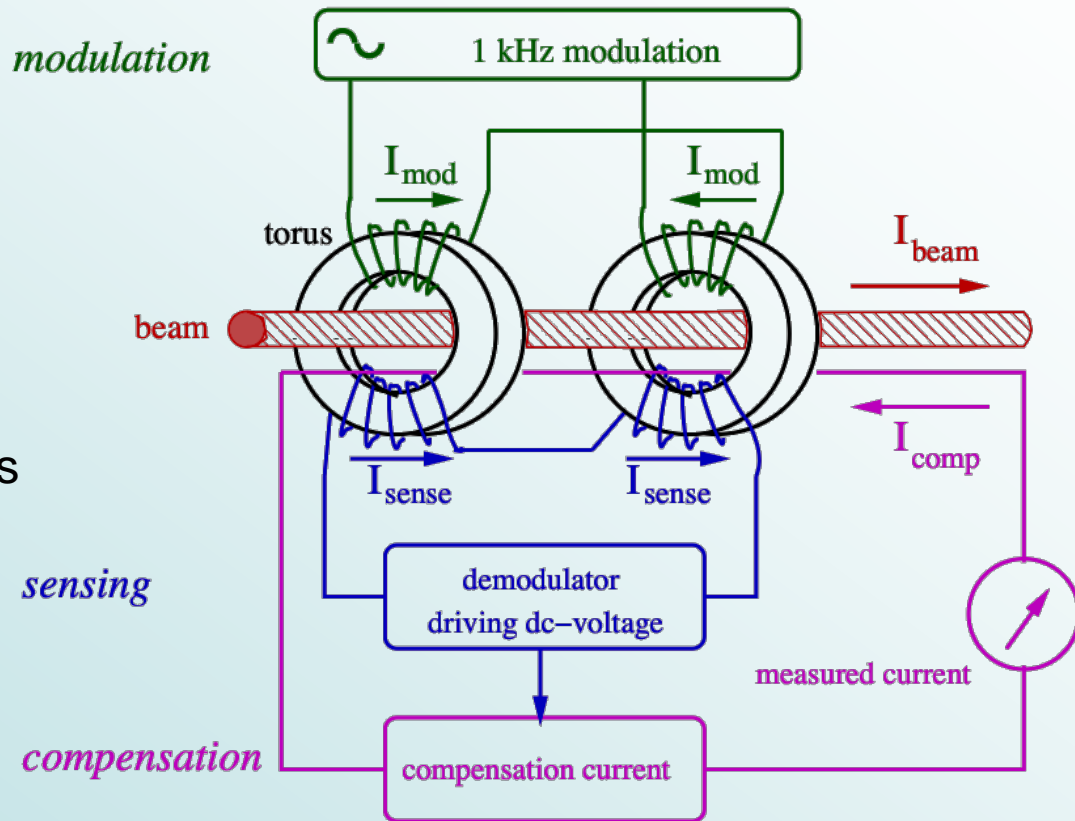
- The current transformer discussed above sees only **B-flux changes**.
- For measuring DC beams non-destructively the DC Current Transformer (DCCT) is the solution – method: look at the magnetic saturation of two tori.

➤ **Modulation** of the primary windings forces both tori into saturation twice per cycle.

➤ **Sense windings** measure the modulation signal and cancel each other.

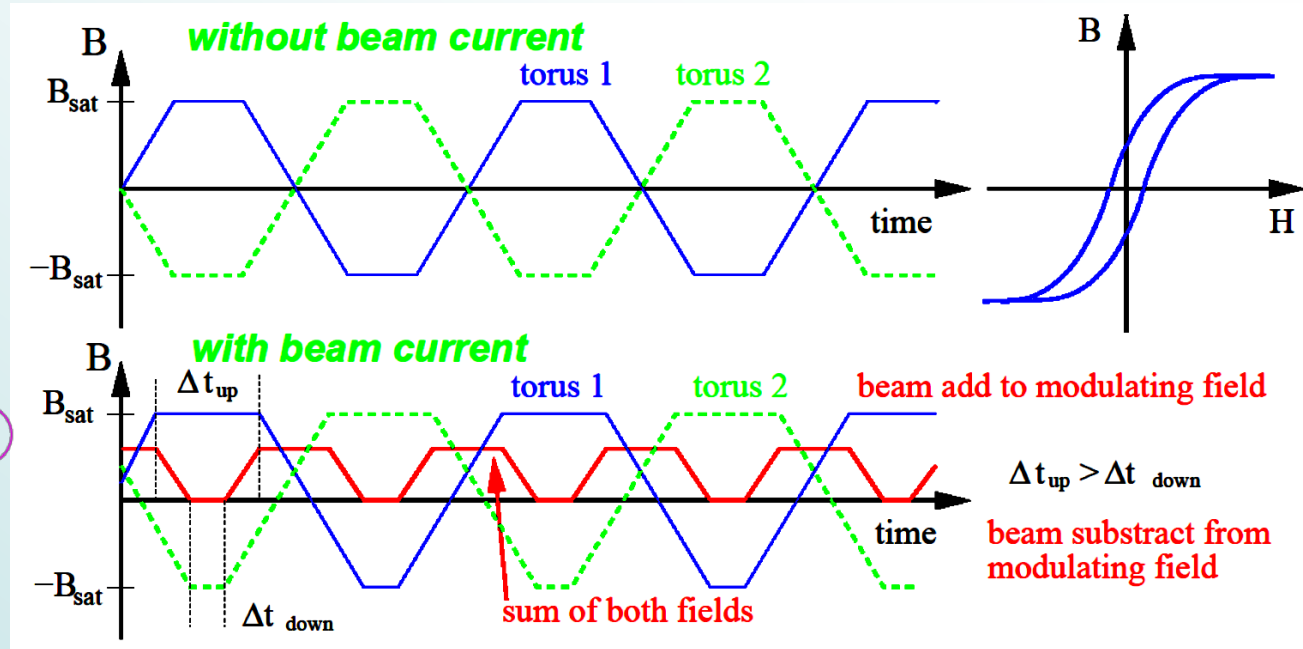
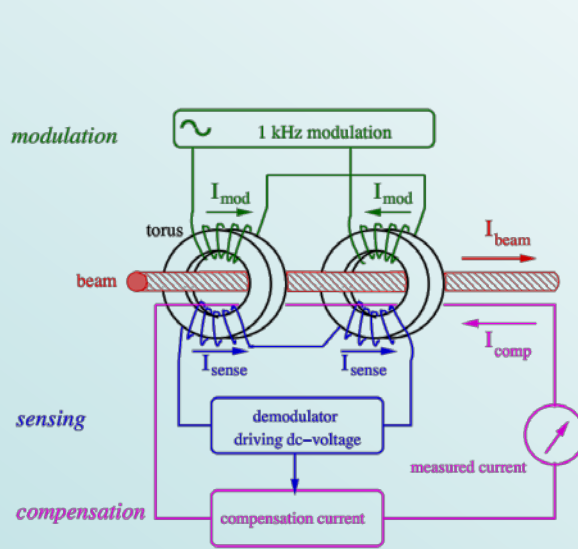
➤ But with the  $I_{beam}$ , the saturation is shifted and  $I_{sense}$  is not zero

➤ **Compensation current** adjustable until  $I_{sense}$  is zero once again.





# DCCT Function Schematics



- **Modulation without beam:** typically about 1 kHz to saturation → **no** net flux
- **Modulation with beam:** saturation is reached at different times, → net flux
- **Net flux:** double frequency than modulation,
- **Feedback:** Current fed to compensation winding for larger sensitivity
- **Two magnetic cores:** Must be very similar.

# DCCT Realizations

Example: The DCCT at GSI synchrotron (designed 1990 at GSI):

Core radii	$r_i = 135 \text{ mm}, r_o = 145 \text{ mm}$
Core thickness	10 mm
Core material	Vitrovac 6025: $(\text{CoFe})_{70\%}(\text{MoSiB})_{30\%}$
Core permeability	$\mu_r \simeq 10^5$
Saturation $B_{sat}$	$\simeq 0.6 \text{ T}$
Isolating cap	$\text{Al}_2\text{O}_3$
Number of windings	16 for modulation and sensing 12 for feedback
Ranges for beam current	300 $\mu\text{A}$ to 1 A
Resolution	2 $\mu\text{A}$
Bandwidth	dc to 20 kHz
rise time	20 $\mu\text{s}$
Offset compensation	$\pm 2.5 \mu\text{A}$ in auto mode < 15 $\mu\text{A}/\text{day}$ in free run
temperature coeff.	1.5 $\mu\text{A}/^\circ\text{C}$



Commercial product specification (Bergoz NPCT):

Most parameters: comparable the GSI-model  
 Temperature coeff. 0.5  $\mu\text{A}/^\circ\text{C}$   
 Resolution several  $\mu\text{A}$  (b.w. dependent)



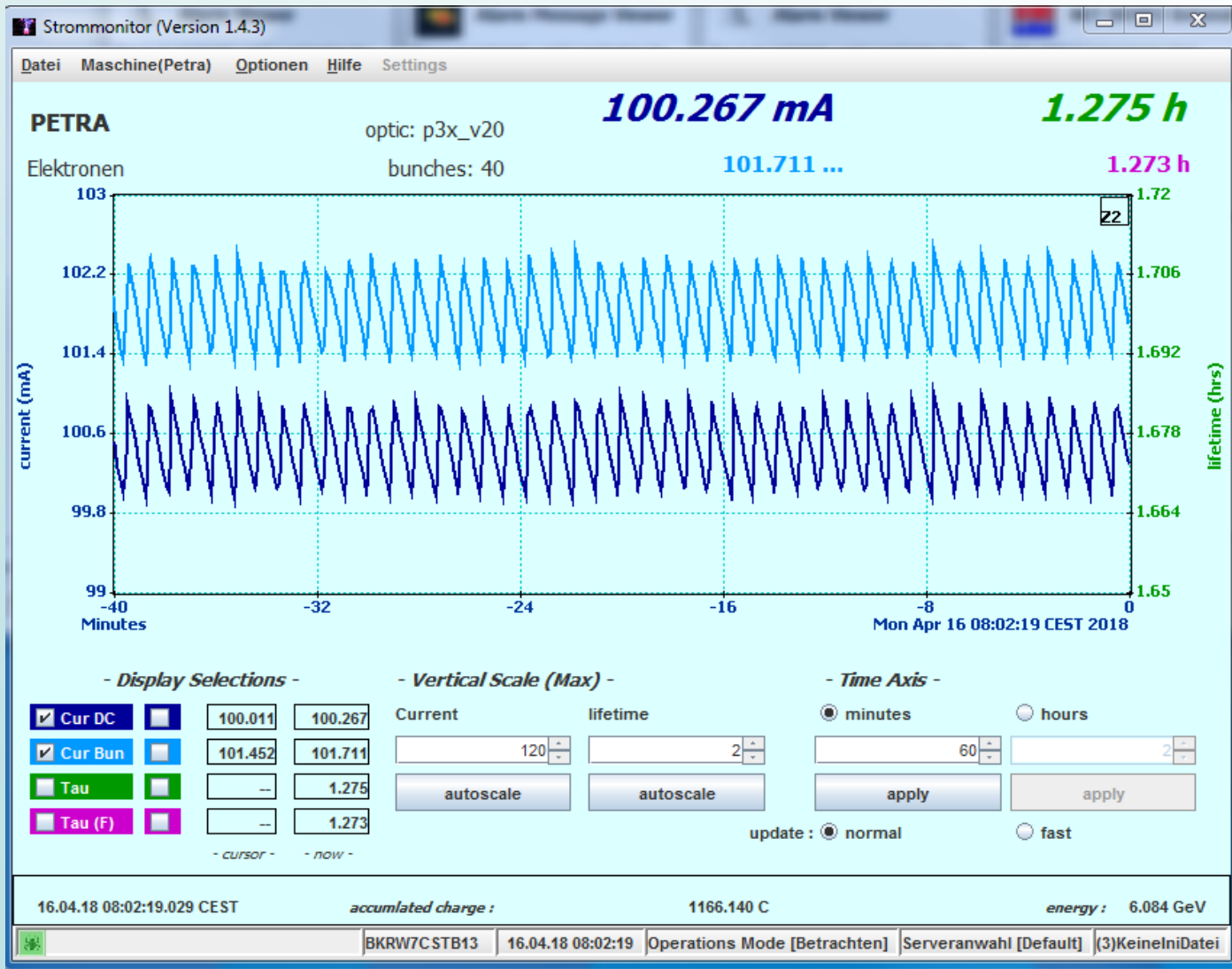
In-flange NPCT with 96-mm aperture

# AC/DC Beam Current Measurement

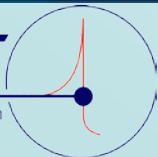


**Example:**  
Injection and acceleration at the HIT facility

# DC Beam Current Measurement

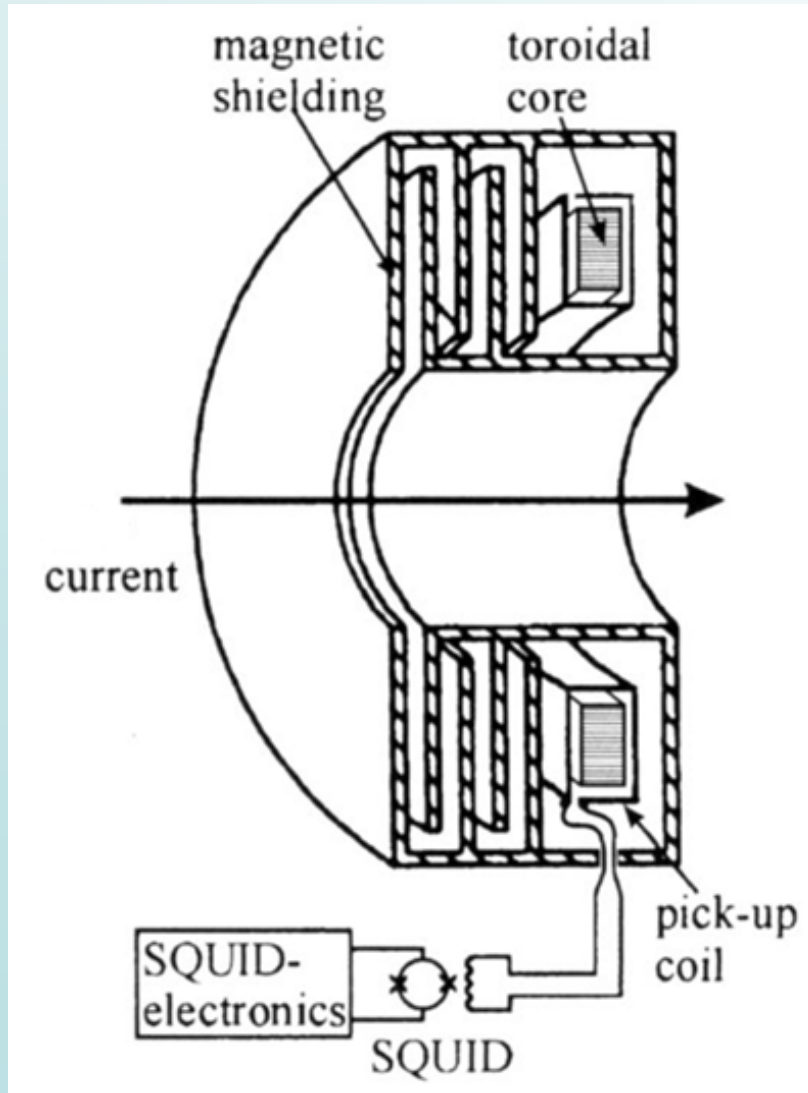


Top-Up  
Operation  
at PETRA  
synchrotron  
(upper  
trace →  
Bergoz  
PCT)





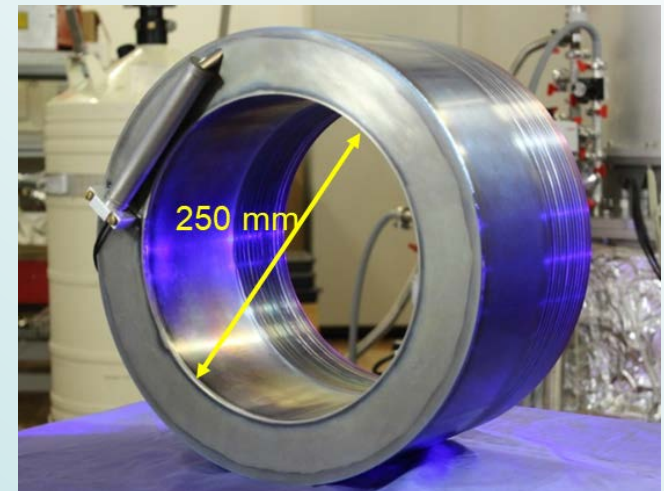
# The CCC – a “nA dc transformer”



Non-destructive measurement device for low intensity beams (between 1 nA and 10  $\mu$ A)

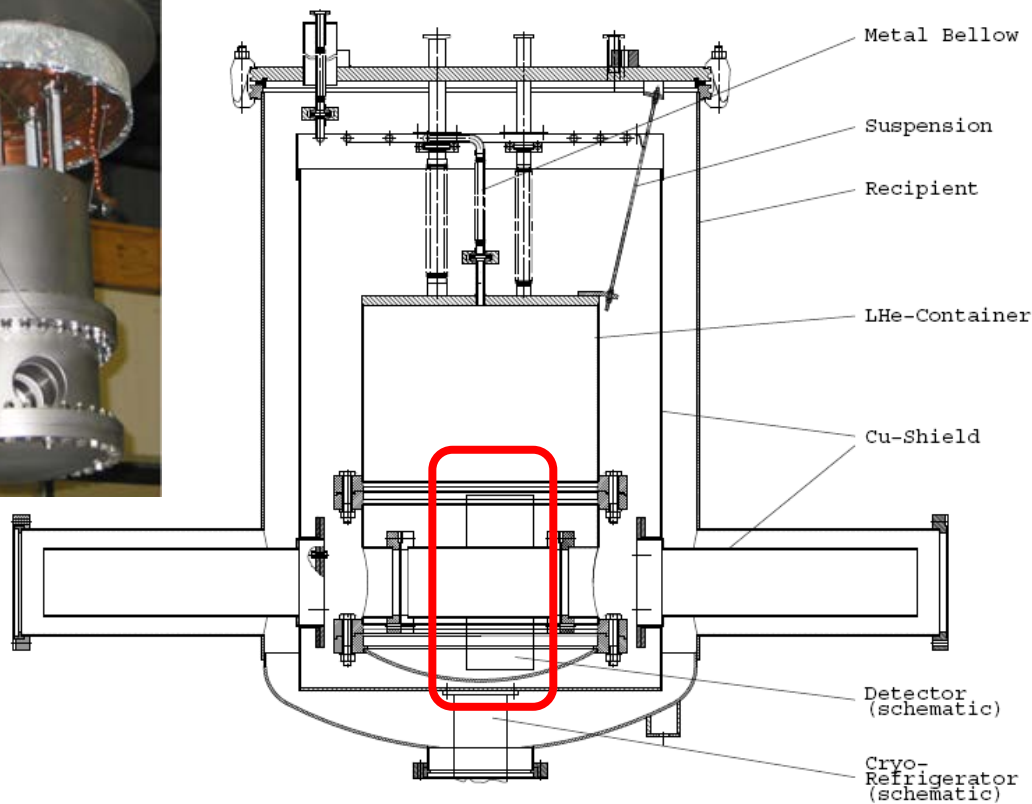
Cryogenic Current Comparator: Precise measurement of azimuthal magnetic field (fT-range) using DC-SQUIDS

Toroid version for FAIR with big bore (from GSI)

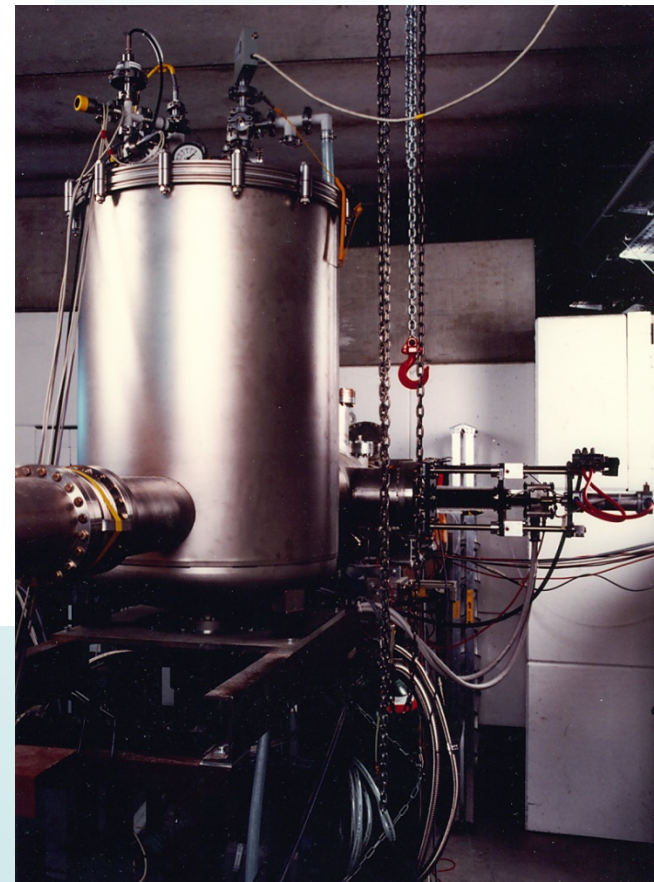




# The CCC – a “nA dc transformer”

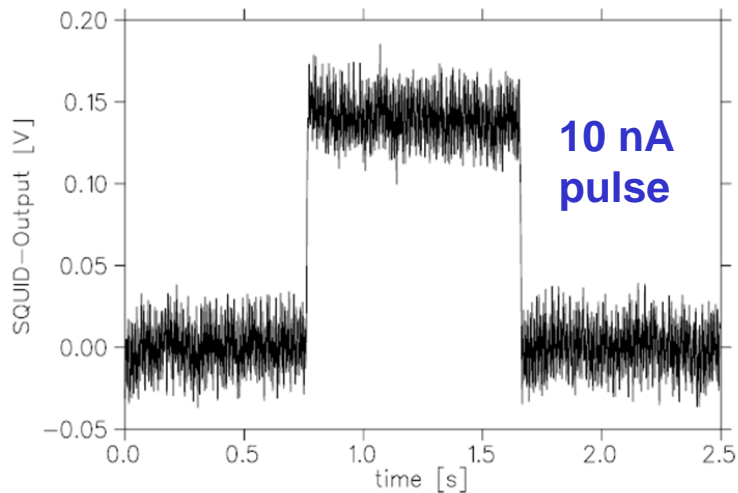


Schematic Setup of a CCC device including cryostat



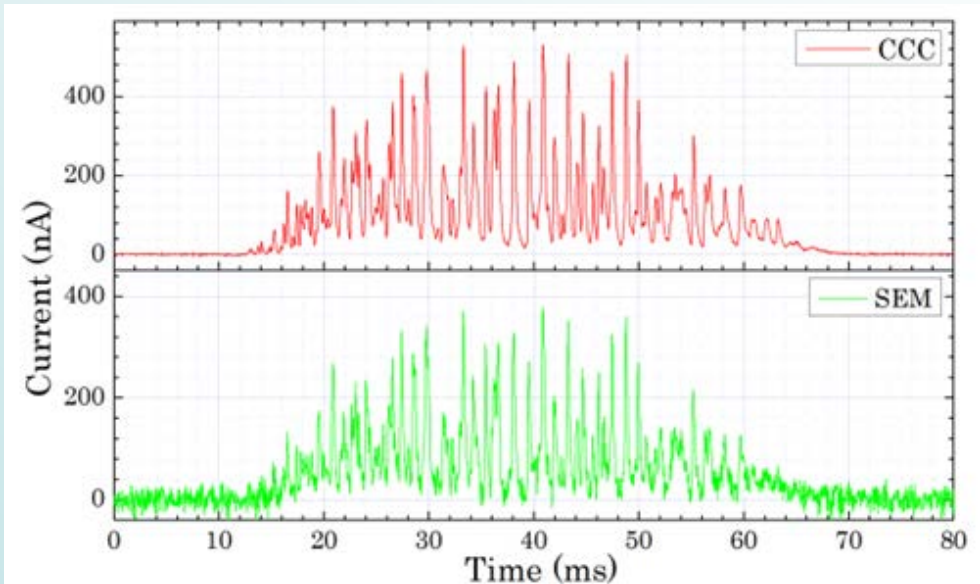
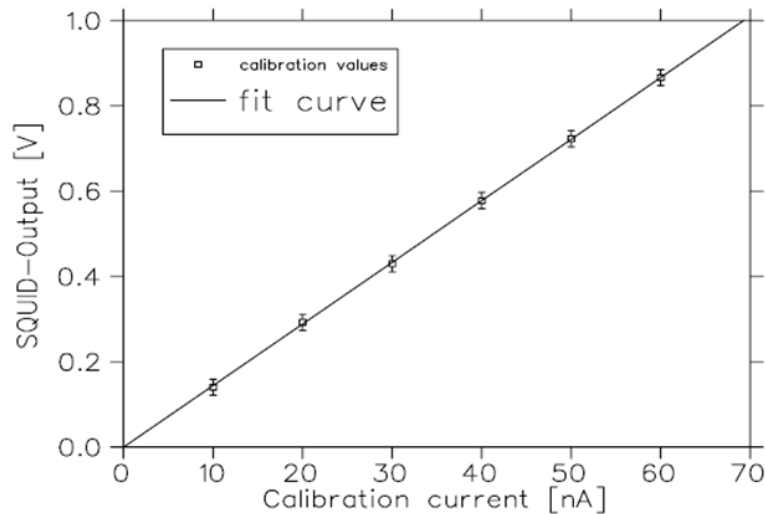
CCC measurement device in a GSI beamline behind SIS18 synchrotron (in front of a beam dump)

# The CCC – a “nA dc transformer”

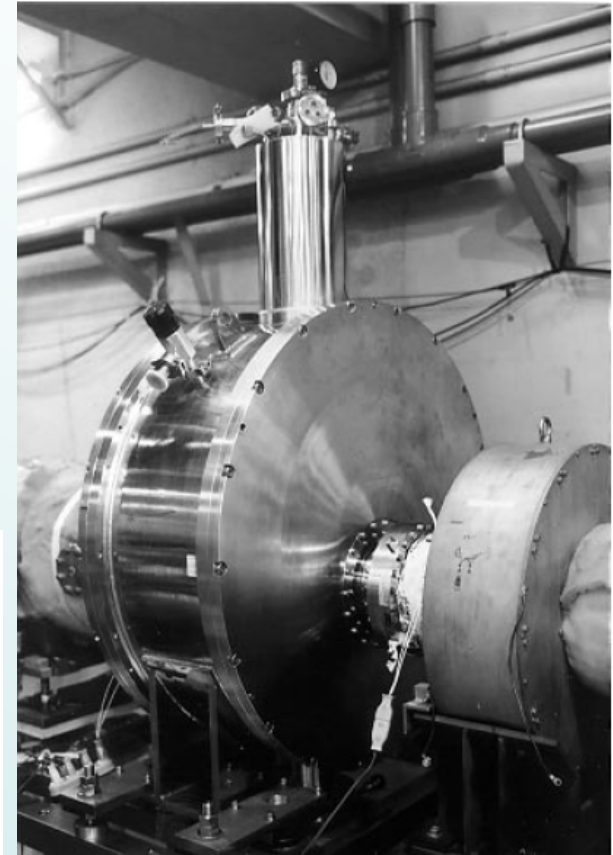
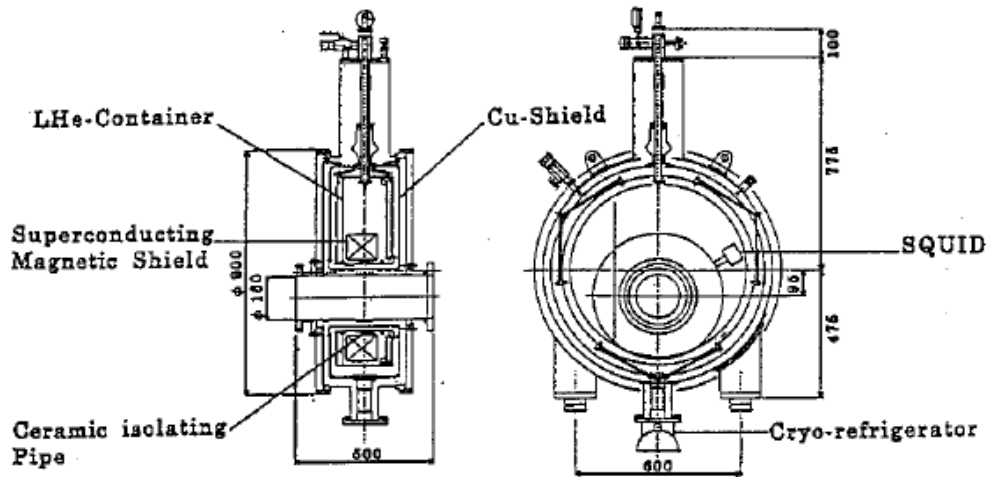


Left: CCC calibration data;  
current resolution:  $60 \text{ pA}/\sqrt{\text{Hz}}$

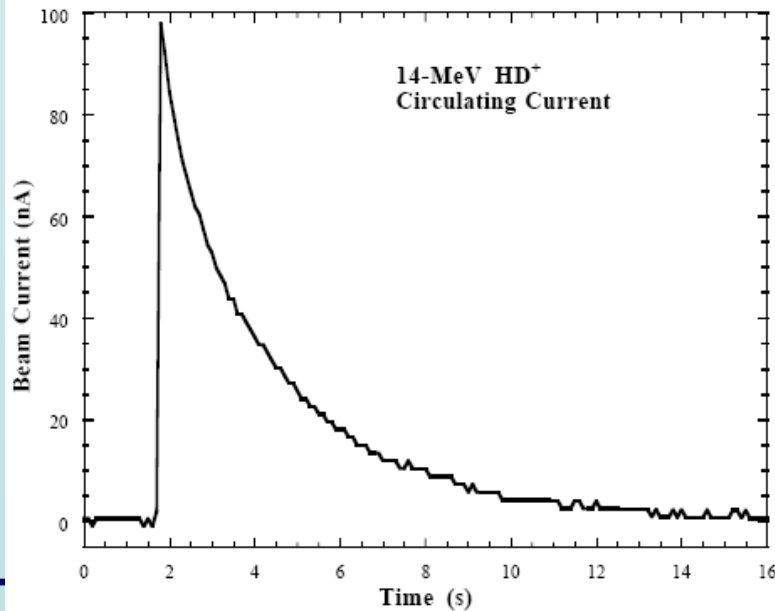
Below: Slowly extracted beam,  
600 MeV/u  $\text{Ni}^{26+}$ ; upper trace:  
CCC, lower trace: SEM signal



# The CCC – a “nA dc transformer”



University  
of Tokyo,  
TARN-II  
storage  
ring



Lifetime measurements  
on stored molecules  
(HD<sup>+</sup>, 14 MeV)



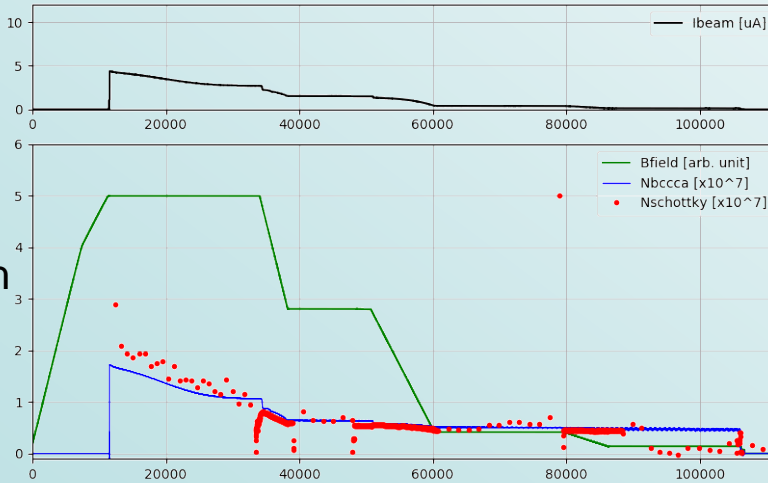
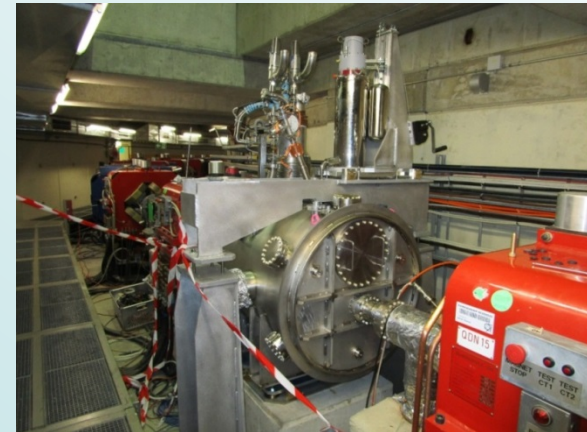
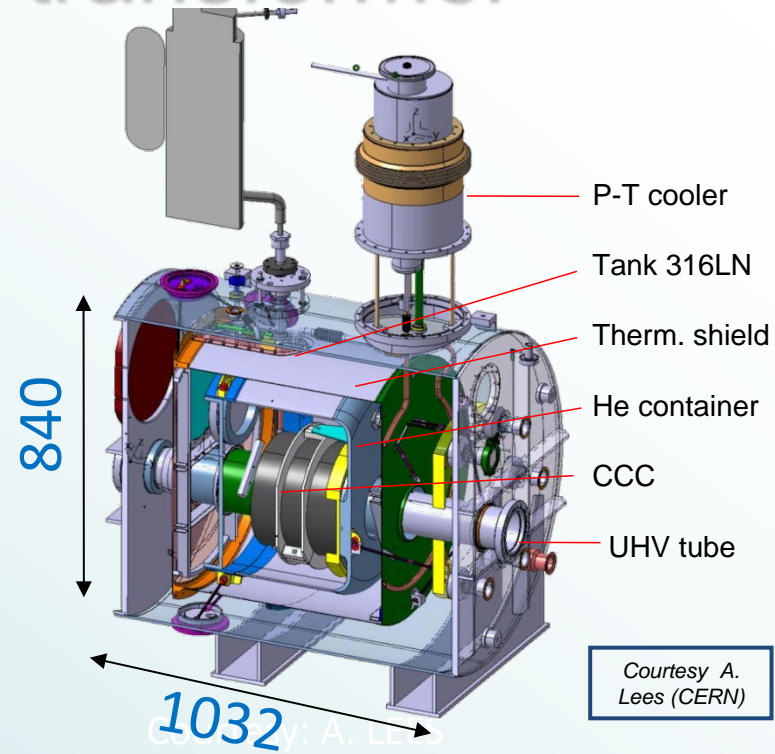
# The CCC – a “nA dc transformer”

## Installation at CERN-AD

### Requirements:

- Intensity measurement alternative to Schottky
- Current resolution: 10 nA,  
intensity resolution:  $5 \times 10^5$  pbar
- Bandwidth DC - 1 kHz

(Collaboration between CERN, FSU/HIJ/IPHT Jena, TU DA and GSI since 2014)



AD cycle measured with Schottky PU and CCC

	3.5 GeV/c	2.0 GeV/c	300 MeV/c	100 MeV/c R	100MeV/c E
Schottky vistar	7.3861e+06	5.3801e+06	4.4613e+06	4.4324e+06	n.a.
Schottky plot	7.3861e+06	5.3801e+06	4.4613e+06	4.4324e+06	-1.0000e+00
BCCA plot	8.5654e+06	5.6582e+06	4.9809e+06	4.7068e+06	4.4330e+06
Ratio	+13.8%	+4.9%	+10.4%	+5.8%	+100.0%



# Conclusion and Acknowledgements

- Beam Instrumentation is the “**the eyes of the operator**” to the behavior of the accelerator, thus **robustness** and **reliability** of beam diagnostic devices is mandatory, especially for the **work horses like ac/dc beam transformers** described in this talk.
- Current measurement devices need **excellent maintenance**, e.g. **calibration** to always guarantee reliable measurement results within the specifications.
- Nowadays a **strong link to the accelerator control system** is a must for beam instrumentation to filter and post-work the raw signal and to present the measurement data in the control room, fill longtime archives for later data evaluation, etc.



# Conclusion and Acknowledgements

*Many thanks to all colleagues from **HIT, MedAustron, CNAO, PSI, ALBA, DESY, CERN, Bergoz, Univ. of Tokyo** and **GSI/FAIR** – especially to Peter Forck – for their advice and giving me interesting example measurements and photos of beam instrumentation from their facilities!*



***Thank you for your attention!***

