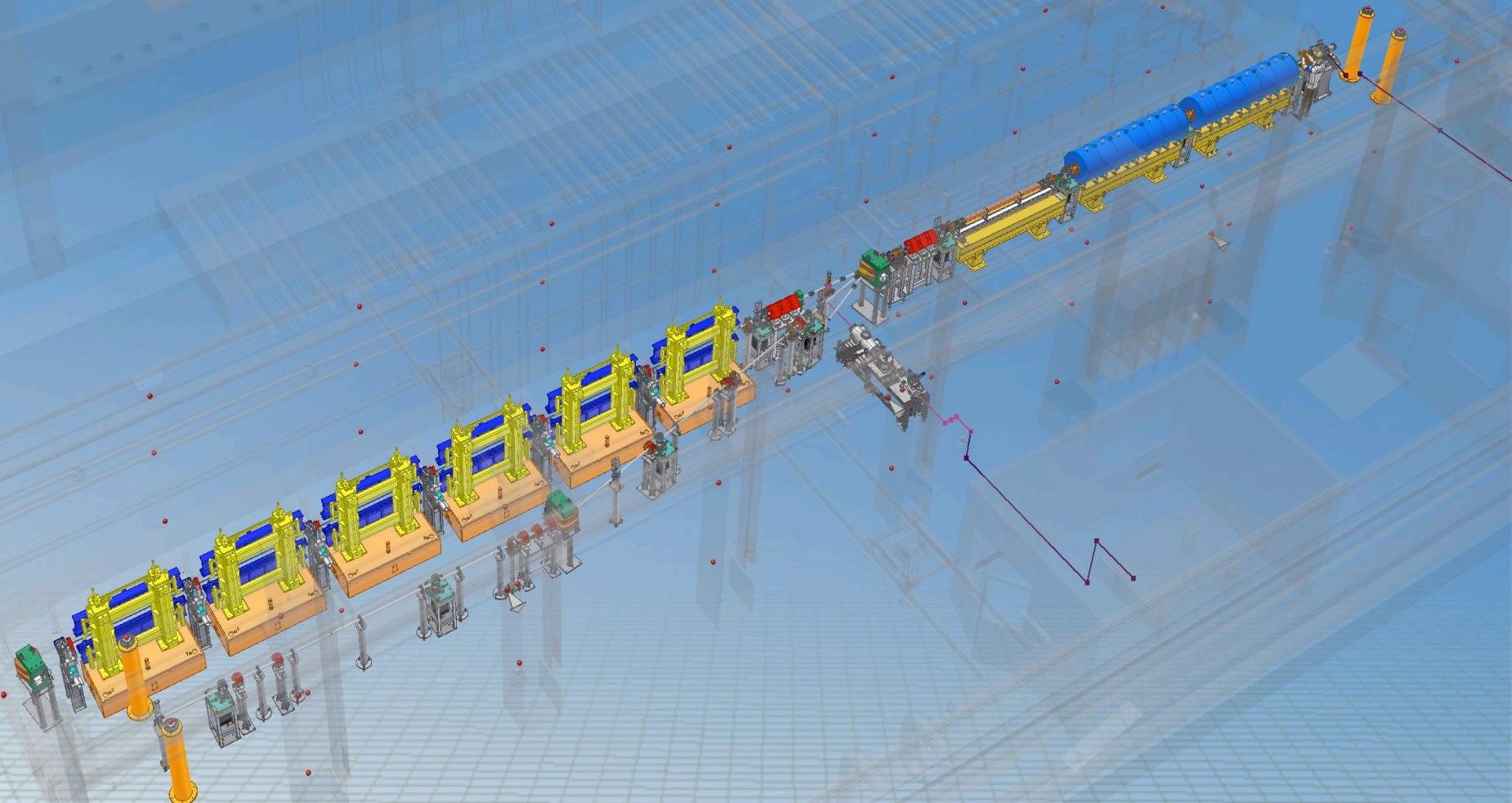


# Linac Driven Free Electron Lasers (III)

Massimo.Ferrario@lnf.infn.it



THE CERN ACCELERATOR SCHOOL



# SASE FEL Electron Beam Requirements: High Brightness $B_n$

$$\lambda_r^{MIN} \propto \sigma_\delta \sqrt{\frac{(1 + K^2/2)}{\gamma B_n K^2}}$$

*energy spread*

*undulator parameter*

*minimum radiation wavelength*

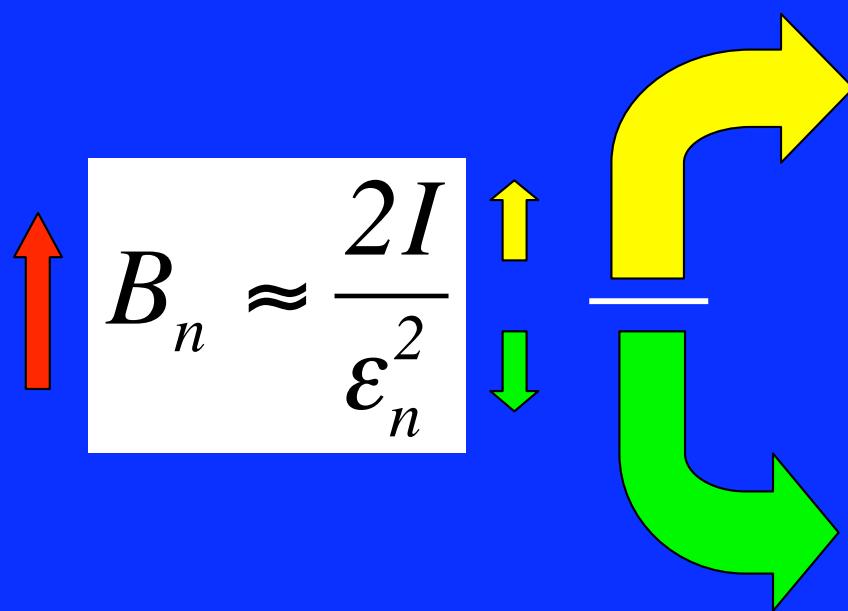
$$B_n = \frac{2I}{\epsilon_n^2}$$

$$L_g \propto \frac{\gamma^{3/2}}{K \sqrt{B_n (1 + K^2/2)}}$$

*gain length*

R. Saldin et al. in *Conceptual Design of a 500 GeV e+e- Linear Collider with Integrated X-ray Laser Facility*, DESY-1997-048

# Short Wavelength SASE FEL Electron Beam Requirement: High Brightness $B_n > 10^{15} \text{ A/m}^2$

$$B_n \approx \frac{2I}{\epsilon_n^2}$$


Bunch compressors  
(RF & magnetic)

Laser Pulse shaping  
Emittance compensation  
Cathode emittance

# The paradox of relativistic bunch compression

Low energy electron bunch injected in a linac:

$$\gamma \approx 1$$

$$L_b = 3\text{mm} = L'_b$$

$$I = 100\text{A}$$



Length contraction?

$$\cancel{\gamma = 1000}$$
$$\cancel{L_b = \frac{L'_b}{\gamma} = 3\mu\text{m}}$$
$$\cancel{I = 100\text{kA}}$$

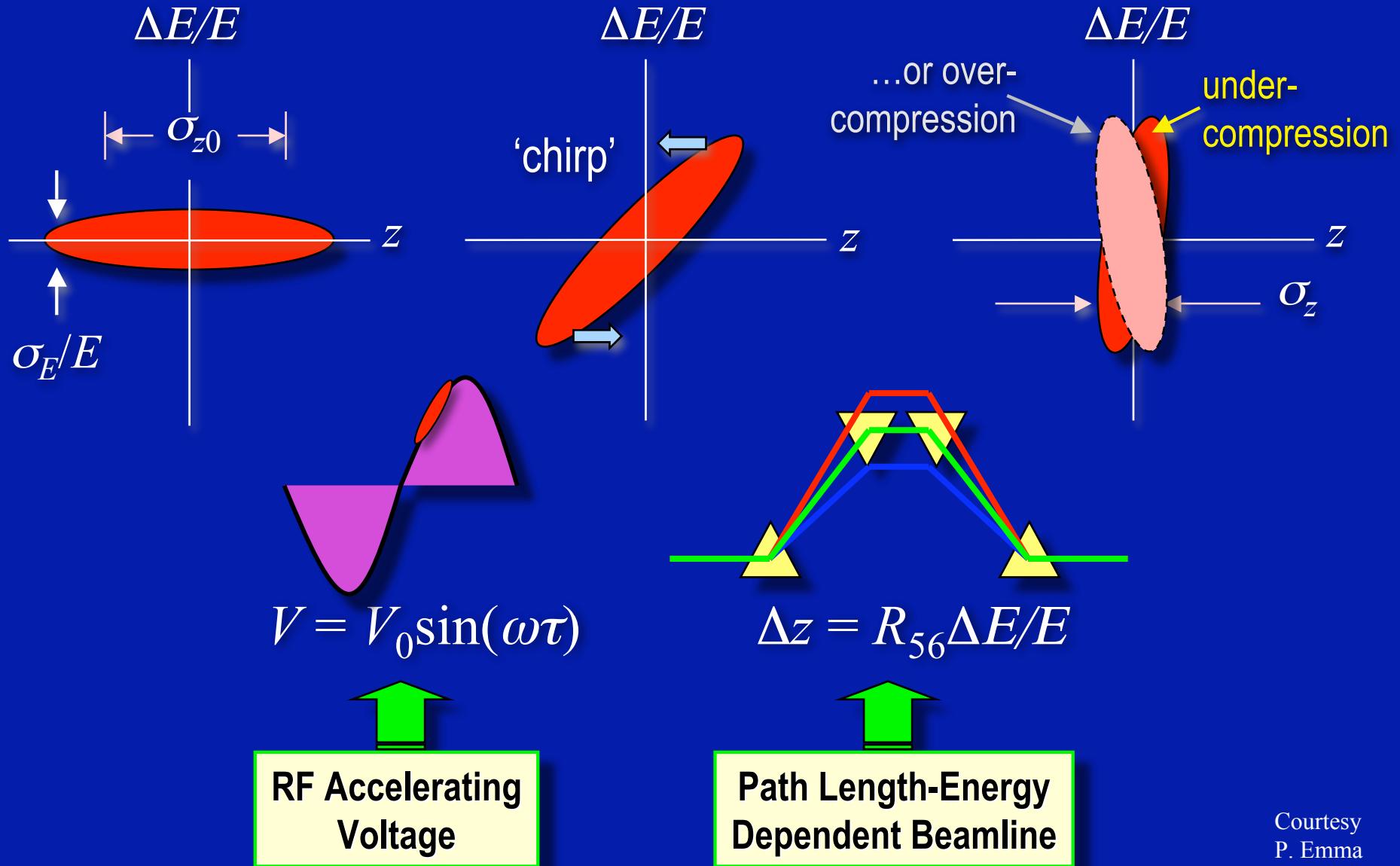
Why do we need a bunch compressor?

$$L''_b = \gamma L_b = 30\text{m}$$
$$L_b = \frac{L''_b}{\gamma} = 3\text{mm}$$
$$I = 100\text{A}$$

# Magnetic compressor (Chicane)



# Magnetic compressor (Chicane)



Courtesy  
P. Emma

# Transfer Matrix including longitudinal phase space

$$\mathbf{R}_{\text{drift}} = \begin{pmatrix} 1 & d \\ 0 & 1 \end{pmatrix}$$

$$\mathbf{R}_{\text{quad}} = \begin{pmatrix} 1 & 0 \\ -1/f & 1 \end{pmatrix}$$

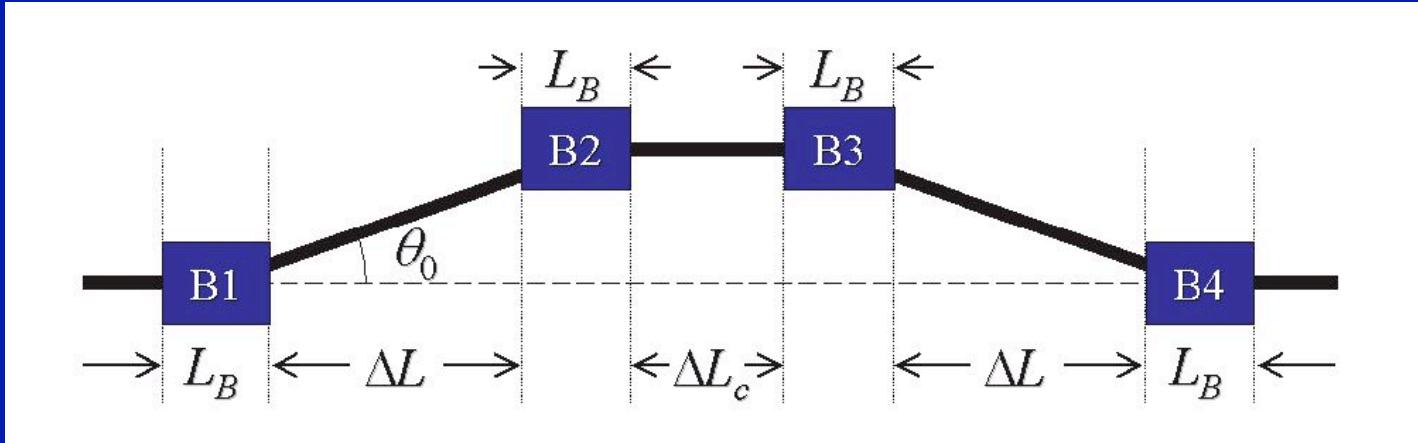
$$\mathbf{R}_{\text{dipole}} = \begin{pmatrix} \cos \theta & \rho \sin \theta \\ -\frac{1}{\rho} \sin \theta & \cos \theta \end{pmatrix}$$

$$\begin{pmatrix} x \\ x' \\ y \\ y' \\ l \\ \delta \end{pmatrix} = \begin{pmatrix} R_{11} & R_{12} & 0 & 0 & 0 & R_{16} \\ R_{21} & R_{22} & 0 & 0 & 0 & R_{26} \\ 0 & 0 & R_{33} & R_{34} & 0 & R_{36} \\ 0 & 0 & R_{43} & R_{44} & 0 & R_{46} \\ R_{51} & R_{52} & R_{53} & R_{54} & R_{55} & R_{56} \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} x_0 \\ x'_0 \\ y_0 \\ y'_0 \\ l_0 \\ \delta_0 \end{pmatrix}$$

$$l_f \approx l_i + R_{56}\delta_i$$

In general, any curved beam line section introduces a path length difference for particles with a relative energy (momentum) deviation  $\delta$ : (with  $\eta$  being the longitudinal dispersion)

$$\Delta S = \eta(\delta)\delta = R_{56}\delta + T_{566}\delta^2 + \dots$$



Path length:

$$S(\vartheta) = \frac{4L_B\vartheta}{\sin\vartheta} + \frac{2\Delta L}{\cos\vartheta} + \Delta L_c$$

Additional Path length:

$$\Delta S(\vartheta) = S(\vartheta) - (4L_B + 2\Delta L + \Delta L_c) \approx \vartheta^2 \left( \frac{2}{3}L_B + \Delta L \right)$$

Expanding  $\vartheta$  in terms of a small relative energy deviation  $\delta$ :

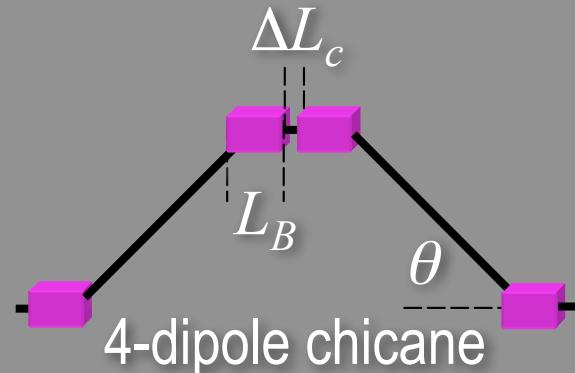
$$\vartheta^2 = \frac{\vartheta_o^2}{(1+\delta)^2} \approx \vartheta_o^2 \left( 1 - 2\delta + 3\delta^2 + \dots \right)$$

we obtain:

$$R_{56} = -2\vartheta_o^2 \left( \frac{2}{3}L_B + \Delta L \right)$$

$$\Delta S = -\frac{R_{56}}{2} \quad T_{566} = -\frac{3}{2}R_{56}$$

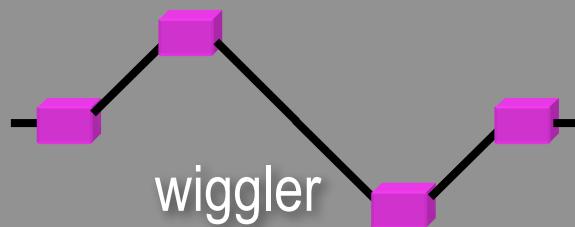
# Types of Compressor



LEUTL,...  
LCLS,  
TTF-BC1,2,  
TESLA-BC1

$$R_{56} \approx -2\theta^2 \left( \frac{L_T}{2} - \frac{4}{3}L_B - \frac{\Delta L_c}{2} \right) < 0$$

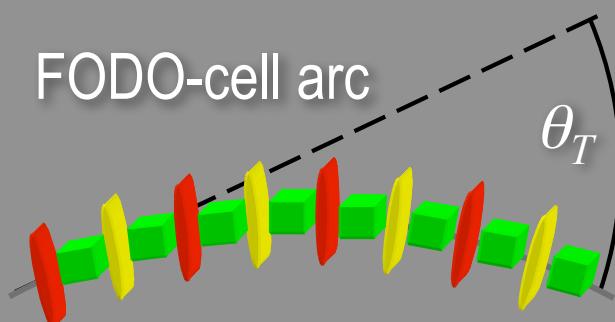
simple, achromatic



TESLA-BC2,3

$$R_{56} \approx -2\theta^2 \left( \frac{L_T}{2} - \frac{4}{3}L_B \right) < 0$$

achromatic



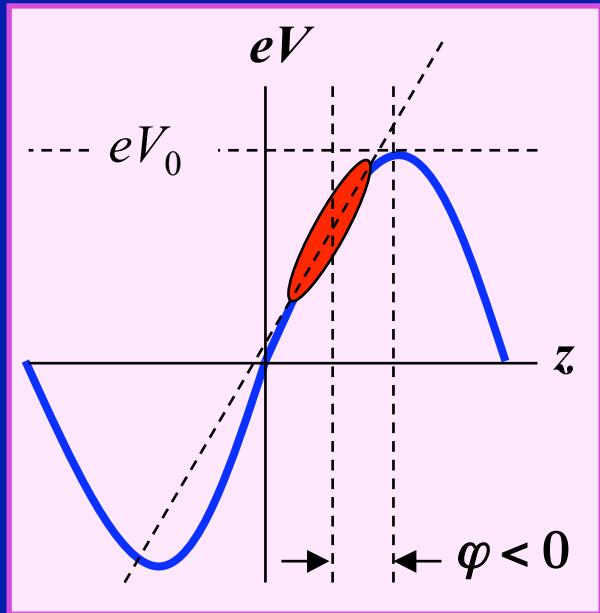
SLC RTL,  
SLC arcs  
NLC BC2

$$R_{56} \approx \frac{\theta_T^2 L_T}{4 N_c^2 \sin^2(\mu_x/2)} > 0$$

reverse sign

But  $T_{566} > 0$  in all cases...

# Single-Stage Bunch Compression



The bunch head is in the  $z < 0$  direction

Energy of a particle after acceleration in a RF linac where  $z$  is the longitudinal position in the bunch:

$$E(z_0) = eV \cos(\phi + kz_0),$$

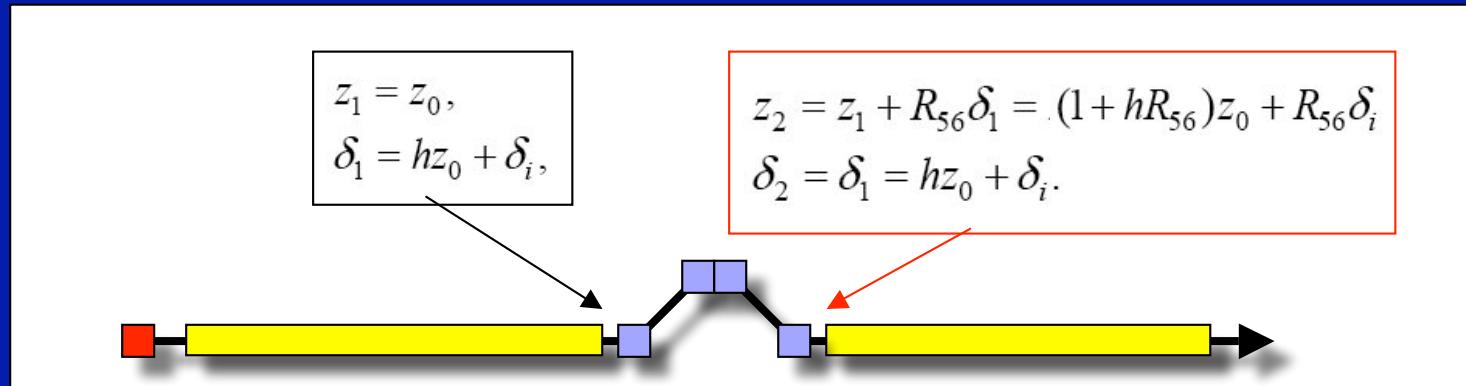
$$E(z_0) = E\left(1 + p' \cdot z_0 + \frac{1}{2} p'' \cdot z_0^2 + \frac{1}{6} p''' \cdot z_0^3 + \mathcal{O}(z_0^4)\right),$$

Defining the Energy Chirp factor  $h$ :

$$h \equiv p' = -\frac{eV}{E} k \sin \phi,$$

The relative **correlated** energy deviation of a particle at a longitudinal position  $z_0$  becomes:

$$\Delta E / E \equiv \delta = h z_0$$



Taking the average over all particles we obtain the final bunch length:

$$\sigma_{z_2} = \sqrt{\langle z_2^2 \rangle} = \sqrt{(1 + hR_{56})^2 \sigma_{z_o}^2 + R_{56}^2 \sigma_{\delta_i}^2}$$

Initial uncorrelated energy spread:  $\sigma_{\delta_i} = \sqrt{\langle \delta_i^2 \rangle}$  Such that:  $\langle z_o \delta_i \rangle = 0$

$\sigma_{\delta}$  in a FEL is extremely small and we can simplify

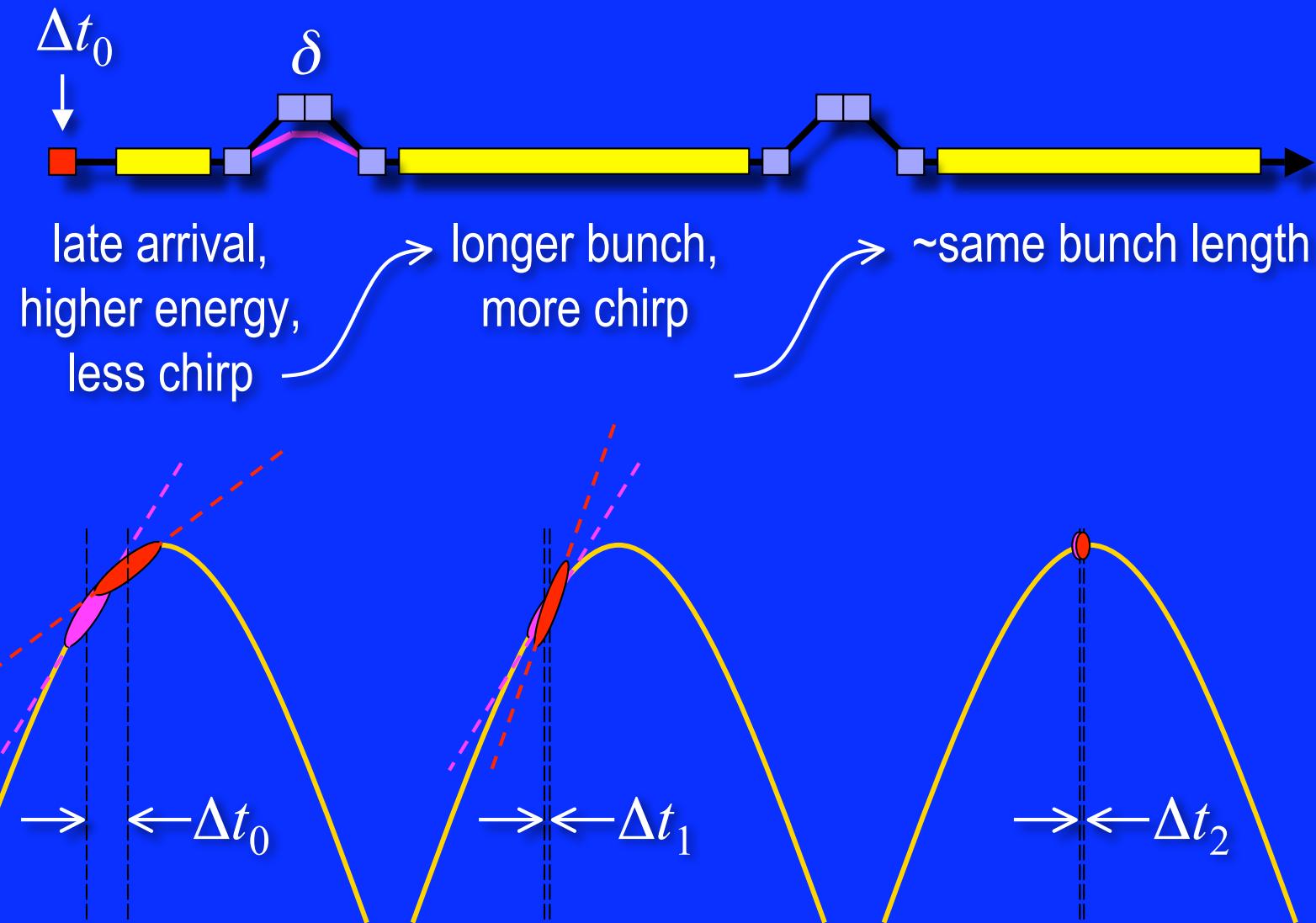
$$\sigma_{z_2} = |1 + hR_{56}| \sigma_{z_o} = \frac{\sigma_{z_o}}{C}$$

Compression factor       $C = \frac{\sigma_{z_o}}{\sigma_{z_2}} \gg 1$

bunch length stability with RF phase jitter...

$$\frac{\Delta \sigma_z}{\sigma_z} \approx - \left( \frac{\sigma_{z_0}}{\sigma_z} \mp 1 \right) \Delta \varphi \cot(\varphi) \Rightarrow \frac{\sigma_{z_0}}{\sigma_z} = 40 : 25\% \text{ jitter / 0.1 psec } @ -15^\circ$$

# Two-Stage Compression Used for Stability



Courtesy  
P. Emma

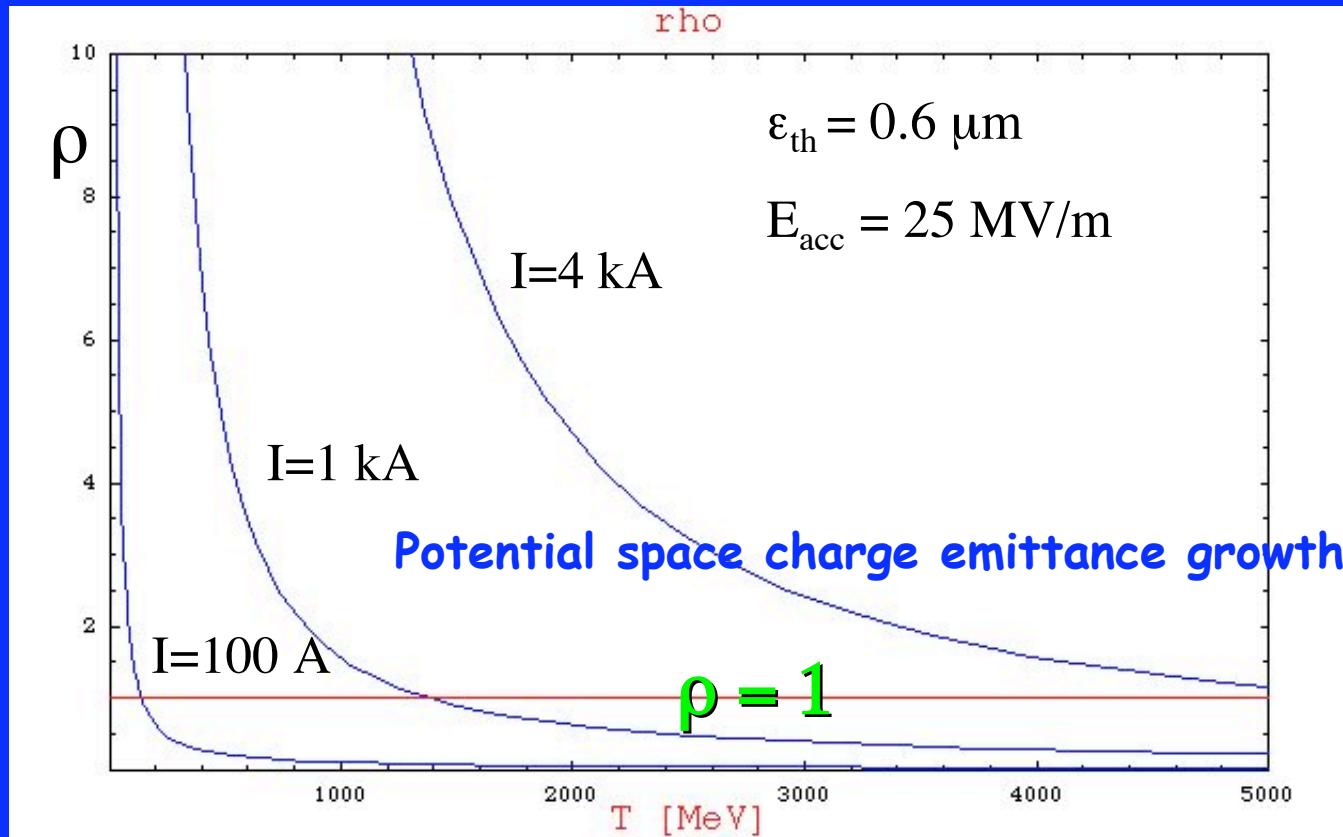
System can be optimized for stability against timing & charge jitter

## Laminarity parameter

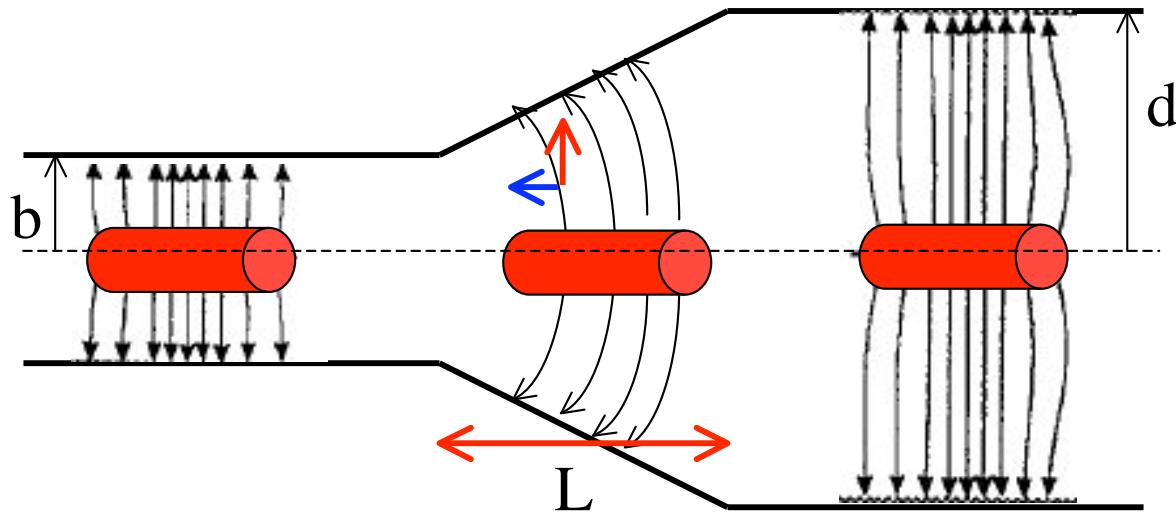
$$\rho = \frac{2I\sigma^2}{\gamma I_A \varepsilon_n^2} = \frac{2I\sigma_q^2}{\gamma I_A \varepsilon_n^2} = \frac{4I^2}{\gamma'^2 I_A^2 \varepsilon_n^2 \gamma^2}$$

## Transition Energy ( $\rho=1$ )

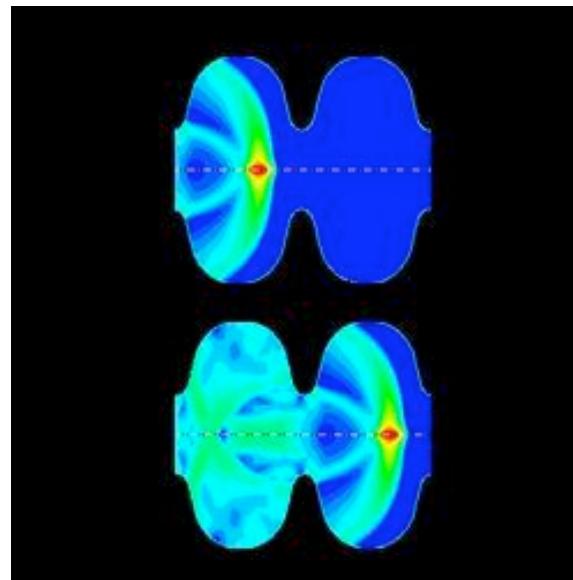
$$\gamma_{tr} = \frac{2I}{\gamma' I_A \varepsilon_n}$$



# Longitudinal Geometric Wakefields



There is a longitudinal  $E_z(r,z)$  field in the transition

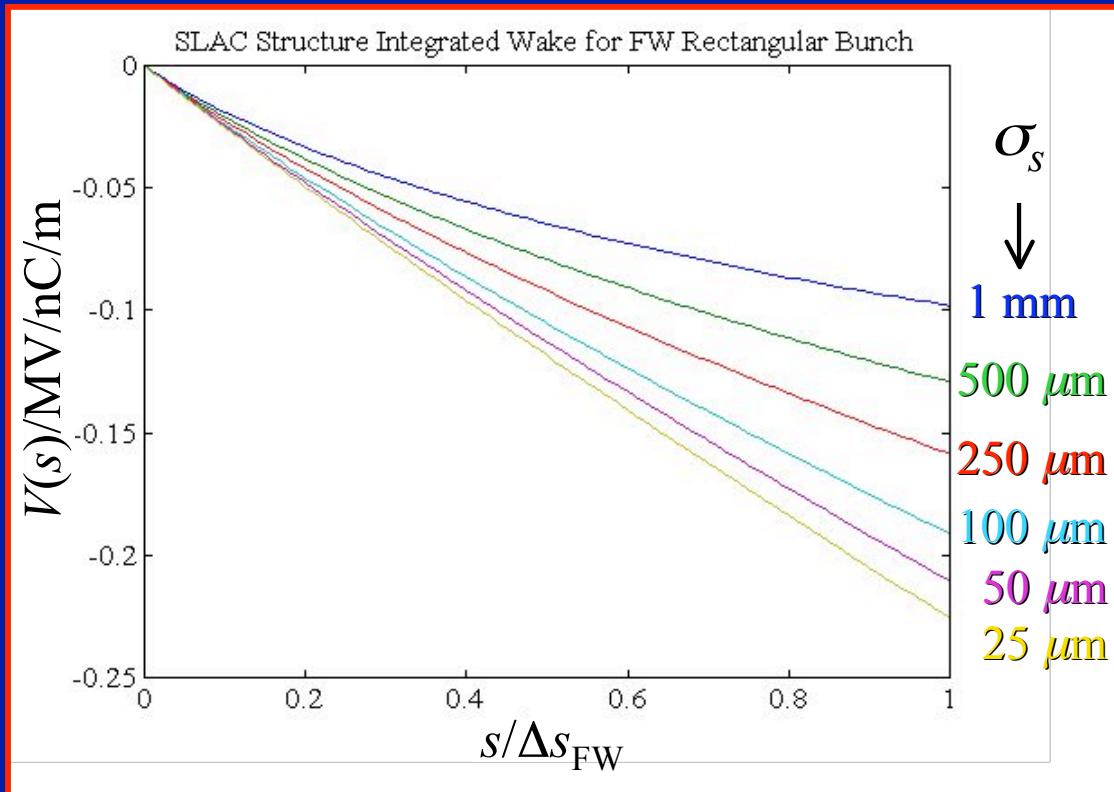


# Longitudinal Geometric Wakefields

Longitudinal point-wake:

$$W(s) \approx \frac{Z_0 c}{\pi a^2} e^{-\sqrt{s/s_0}}$$

K. Bane



**SLAC S-Band:**

$$s_0 \approx 1.32 \text{ mm}$$

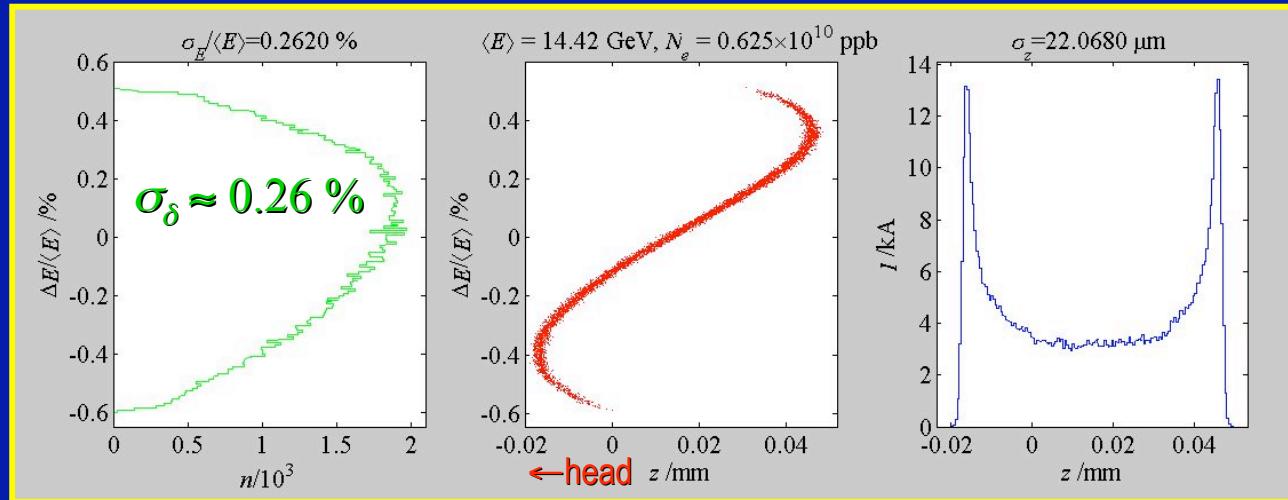
$$a \approx 11.6 \text{ mm}$$

$$s < \sim 6 \text{ mm}$$

Induced voltage along bunch:

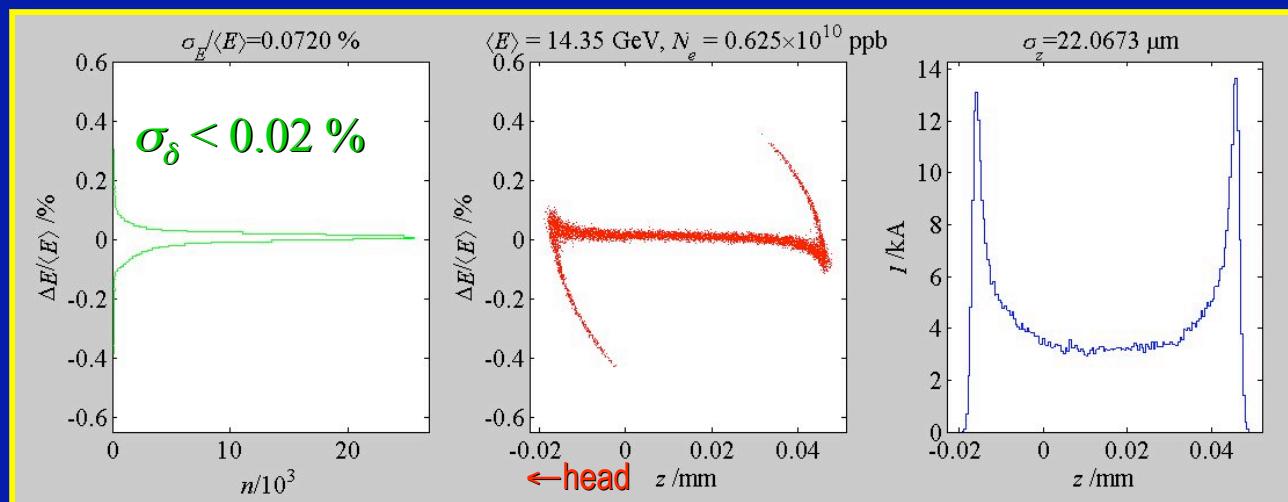
$$V(s) = -NeL \int_{-\infty}^s W(s-s')f(s')ds'$$

# LCLS Example of Wakefield Use



wakefield 'OFF'

end of LCLS linac



wakefield 'ON'

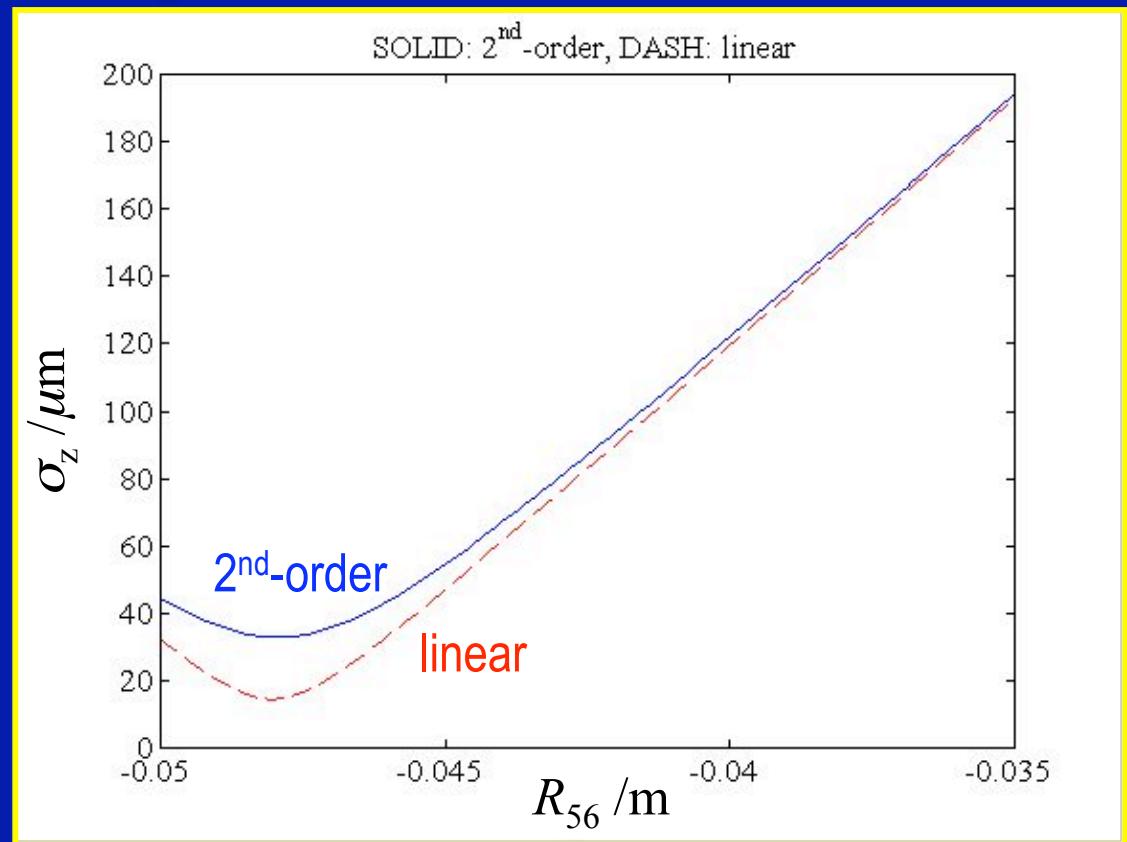
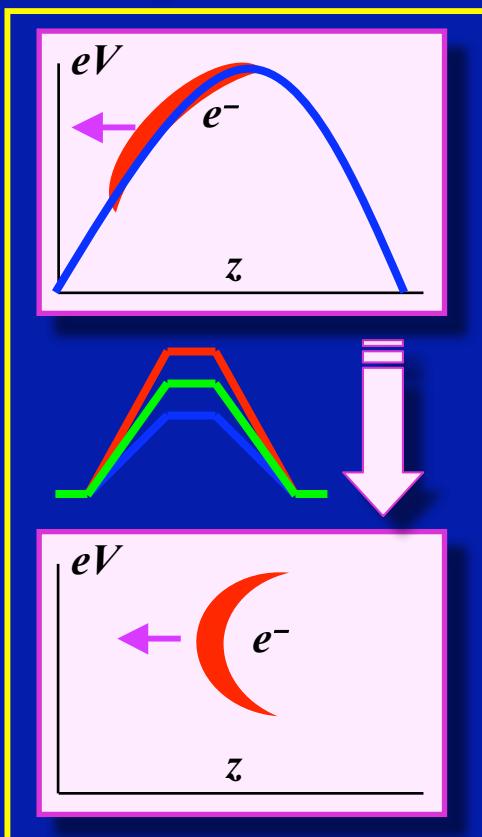
$L \approx 550\text{ m}$ ,  
 $N \approx 6.2 \times 10^9$ ,  
 $\Delta z \approx 75\mu\text{m}$ ,  
 $E = 14\text{ GeV}$

wake-induced  
energy spread

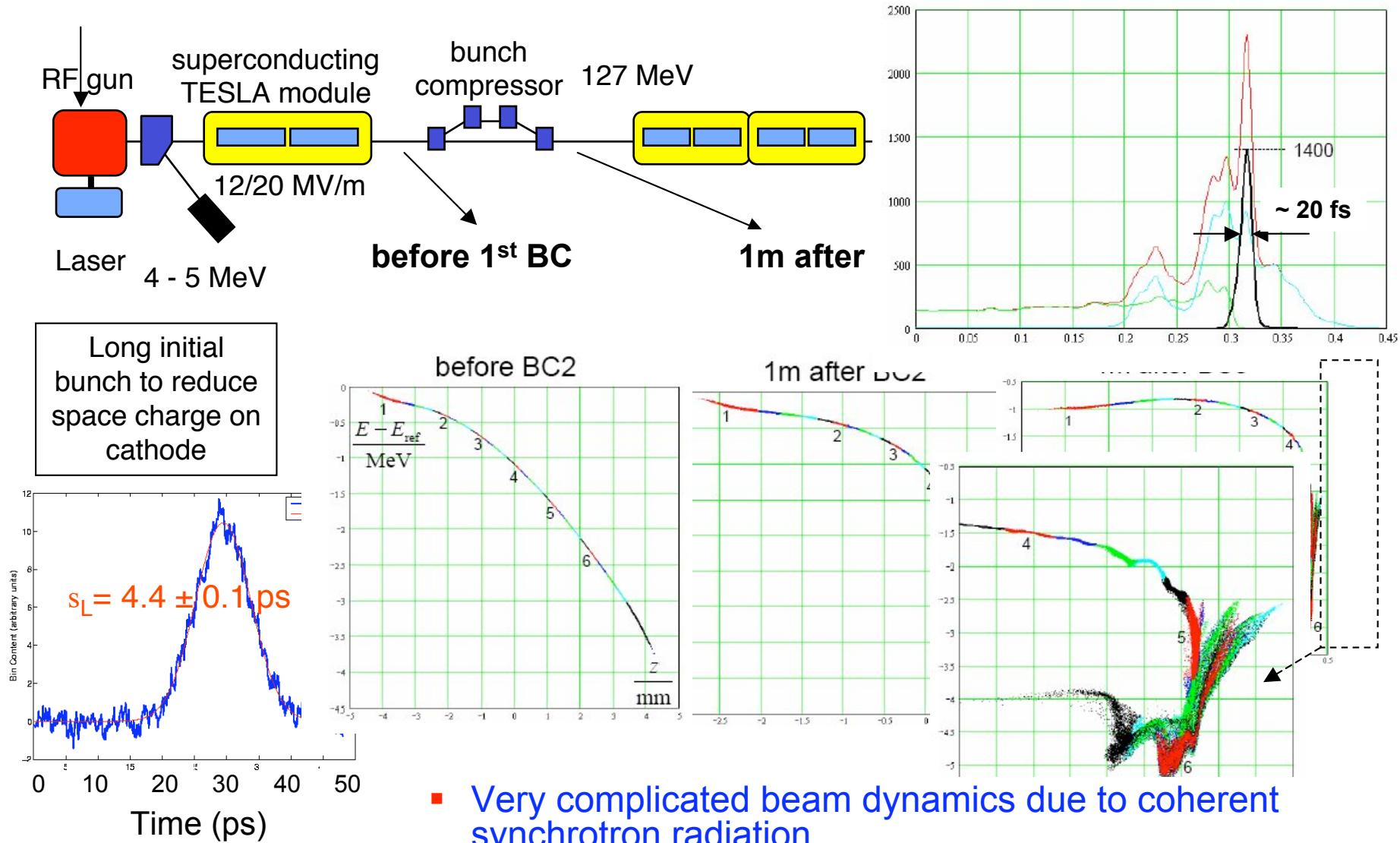
$$\sigma_\delta \approx \frac{2Ne^2cZ_0s_0L}{\pi\sqrt{12}a^2\Delta zE} \left[ 1 - \left( 1 + \sqrt{\Delta z/s_0} \right) e^{-\sqrt{\Delta z/s_0}} \right]$$

for uniform  
distribution

For chicane and accelerating phase, RF curvature and  $T_{566}$  always add, limiting the minimum bunch length ...



# Courtesy Joerg Rossbach (@FLASH)



- Very complicated beam dynamics due to coherent synchrotron radiation
- Difficult access to relevant parameters
- Ultra-short photon pulses created  $\sim 20$  fs FWHM

## RF non linear distortion correction by an harmonic RF section

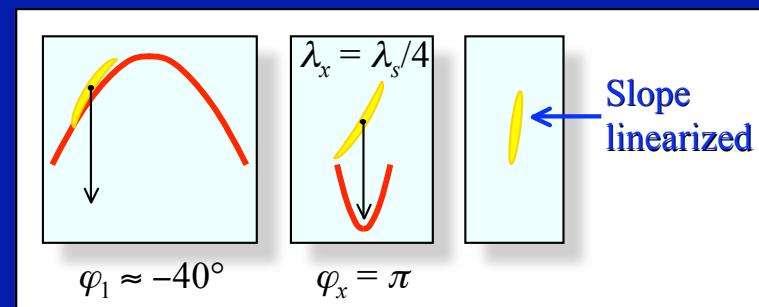
Due to sinusoidal nature of RF voltage

$$V = V_0 \sin(\phi_0) + \Delta\phi V_0 \cos(\phi_0) - \frac{1}{2} \Delta\phi^2 V_0 \sin(\phi_0) + \dots$$

can be corrected by using a higher-harmonic cavity

$$V_h = V_h \sin(\phi_h) + h\Delta\phi V_h \cos(\phi_h) - \frac{1}{2} (h\Delta\phi)^2 V_h \sin(\phi_h) + \dots$$

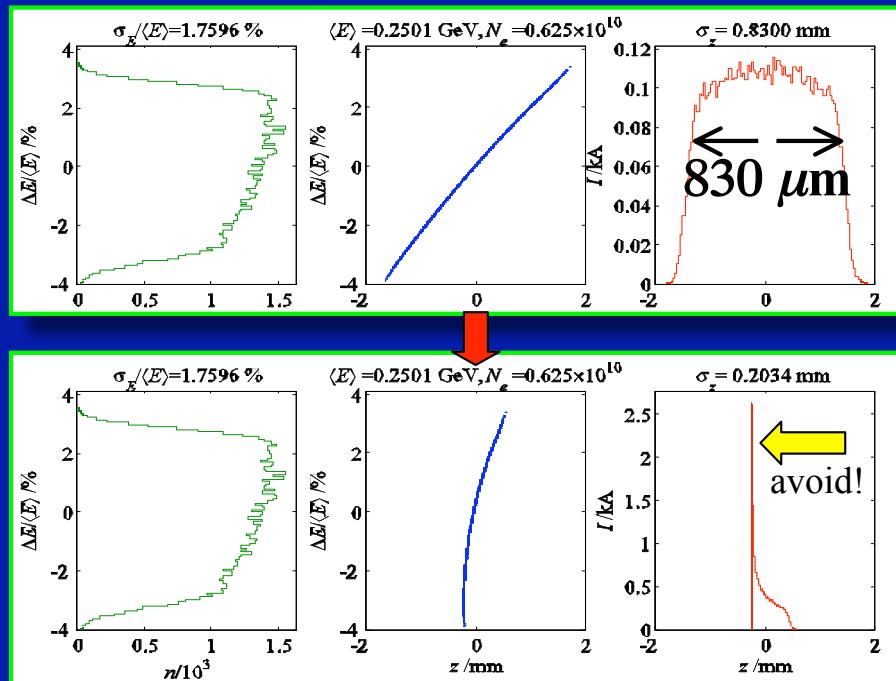
- The second order term in  $V$  can be cancelled by using a decelerating phase  $\phi_h$
- Working on crest ( $\sin(\phi_0)=1$ ) the compensation occurs for  $V_h=V_0/h^2$  and  $\sin(\phi_h) = -1$



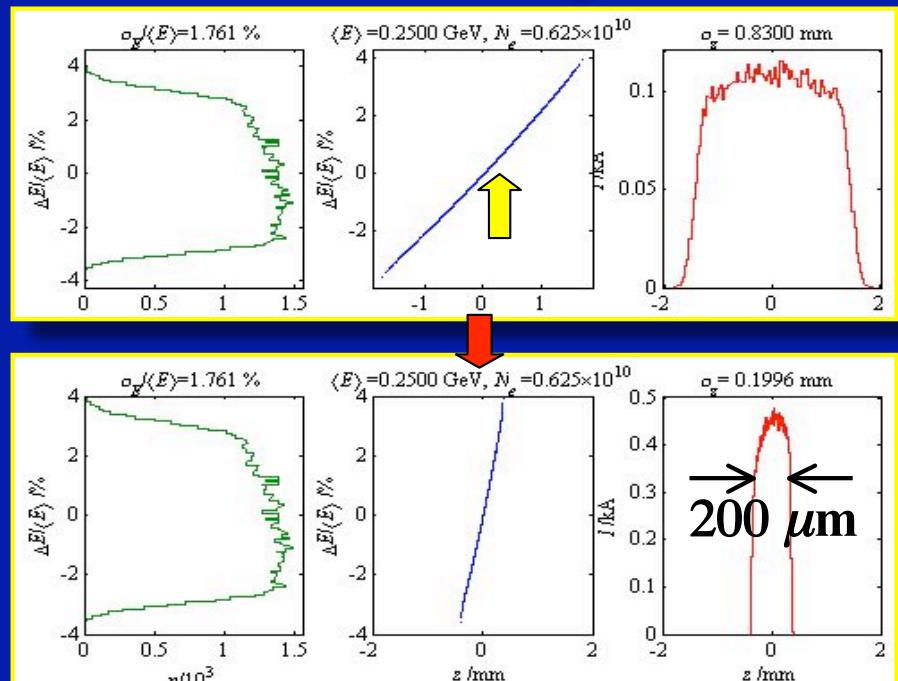
0.5-m X-band section for LCLS (22 MV, 11.4 GHz)

# Harmonic RF used to Linearize Compression

RF curvature and 2<sup>nd</sup>-order compression cause current spikes



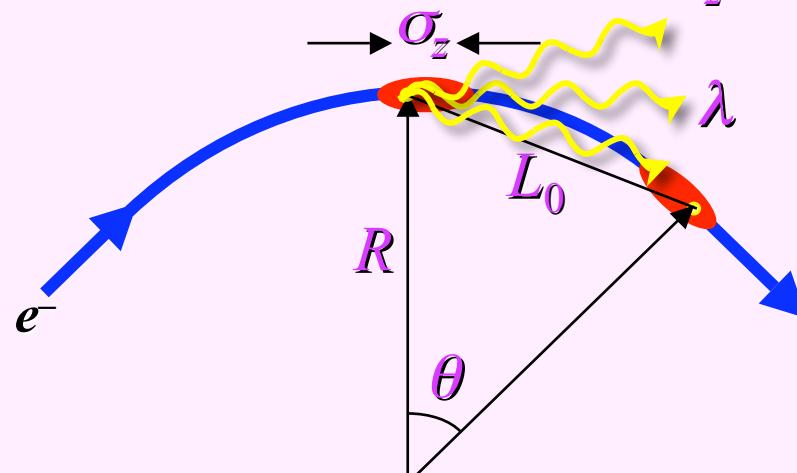
Harmonic RF at decelerating phase corrects 2<sup>nd</sup>-order and allows unchanged z-distribution



# Coherent Synchrotron Radiation (CSR)

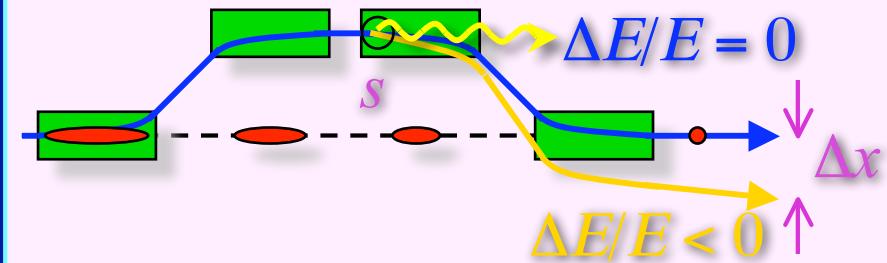
- Powerful radiation generates energy spread in bends
- Energy spread breaks achromatic system
- Causes bend-plane emittance growth (short bunch worse)

coherent radiation for  $\lambda > \sigma_z$



overtaking length:  $L_0 \approx (24\sigma_z R^2)^{1/3}$

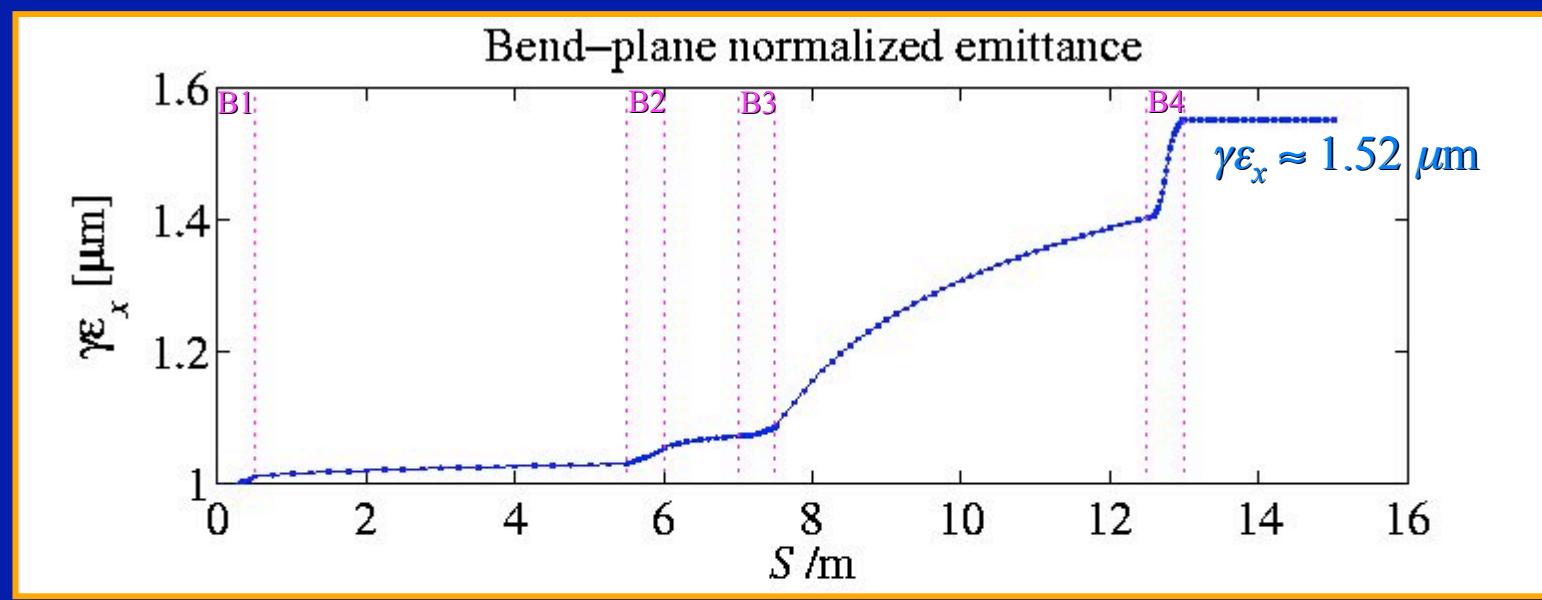
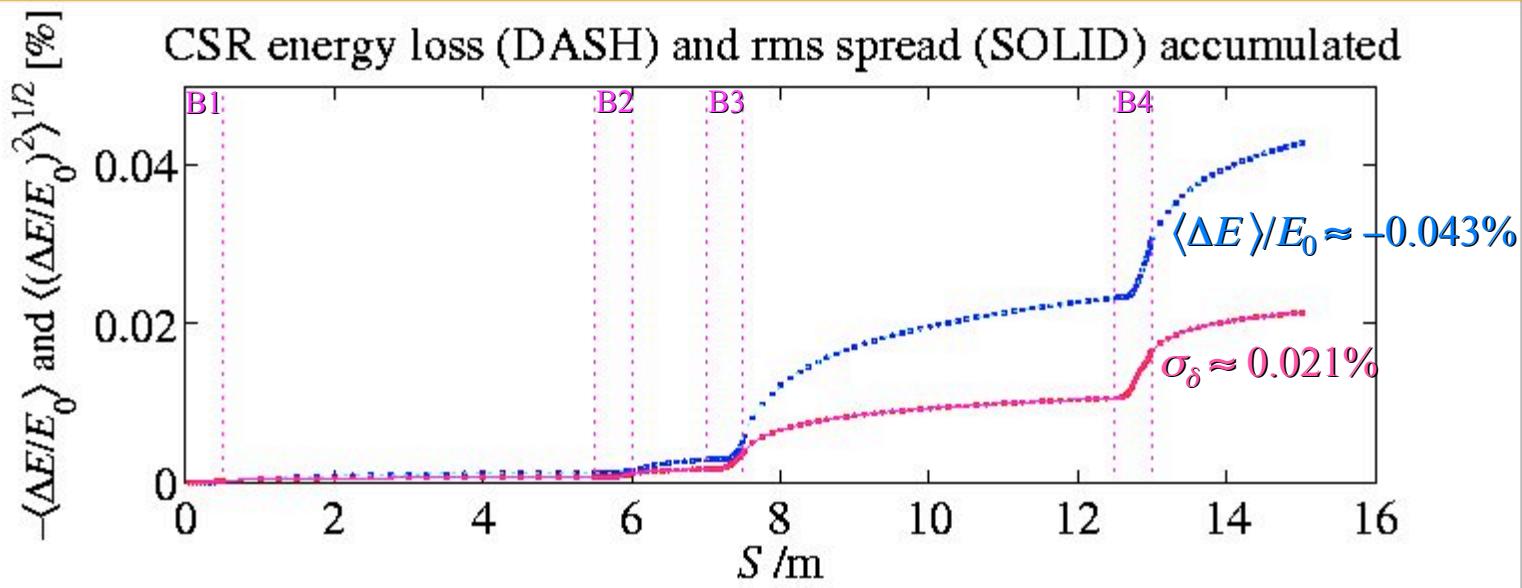
bend-plane emittance growth

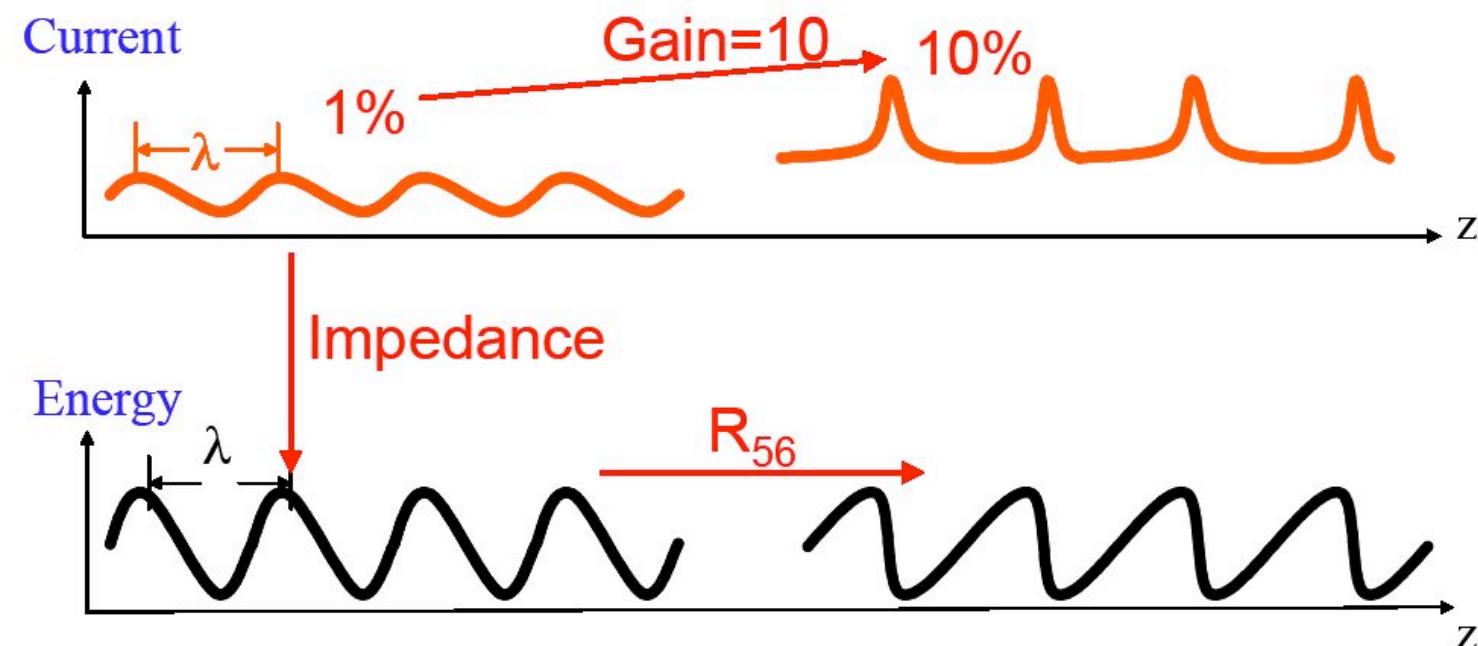


$$\Delta x = R_{16}(s)\Delta E/E$$

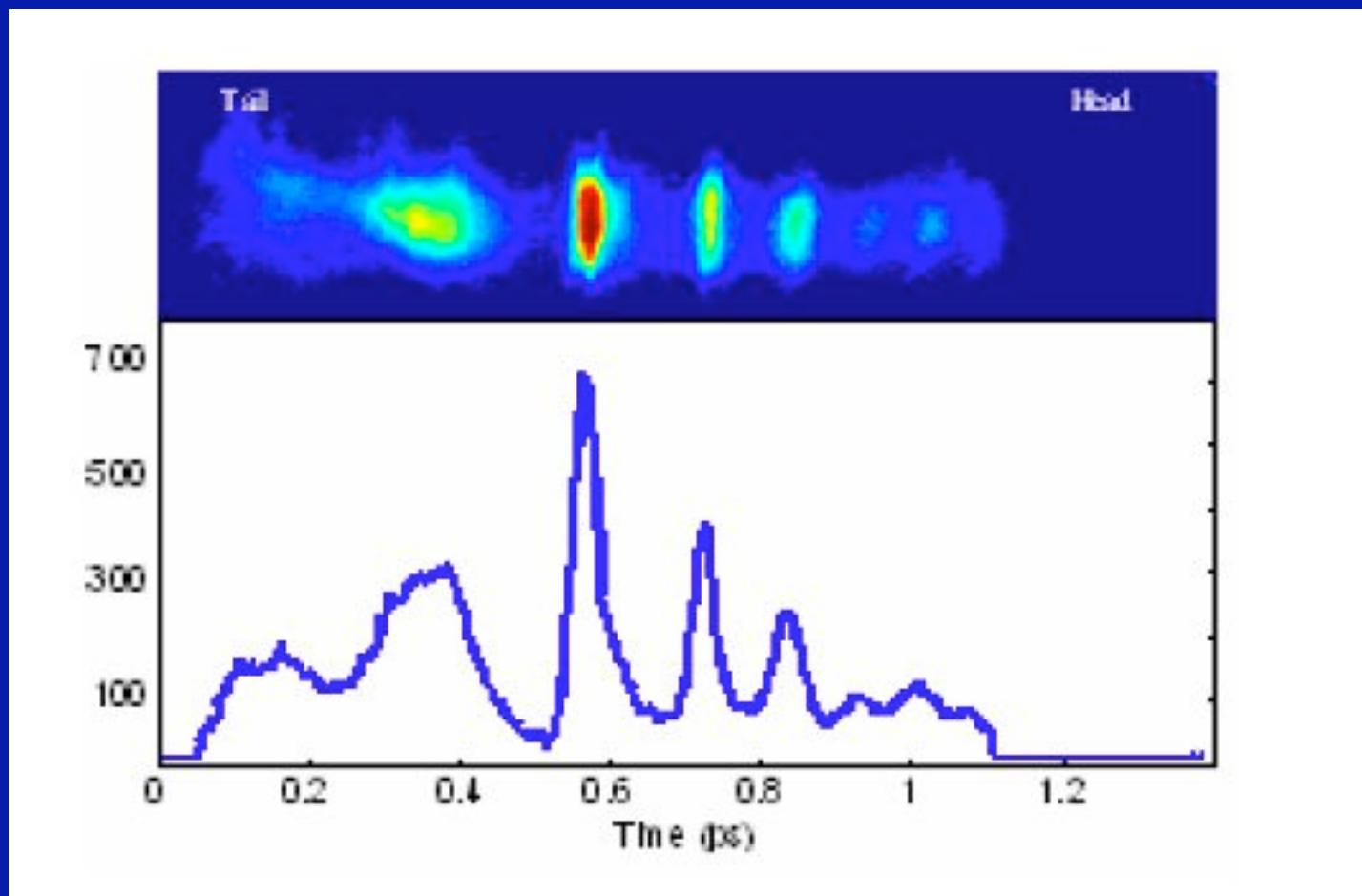
Courtesy  
P. Emma

# Projected Emittance Growth



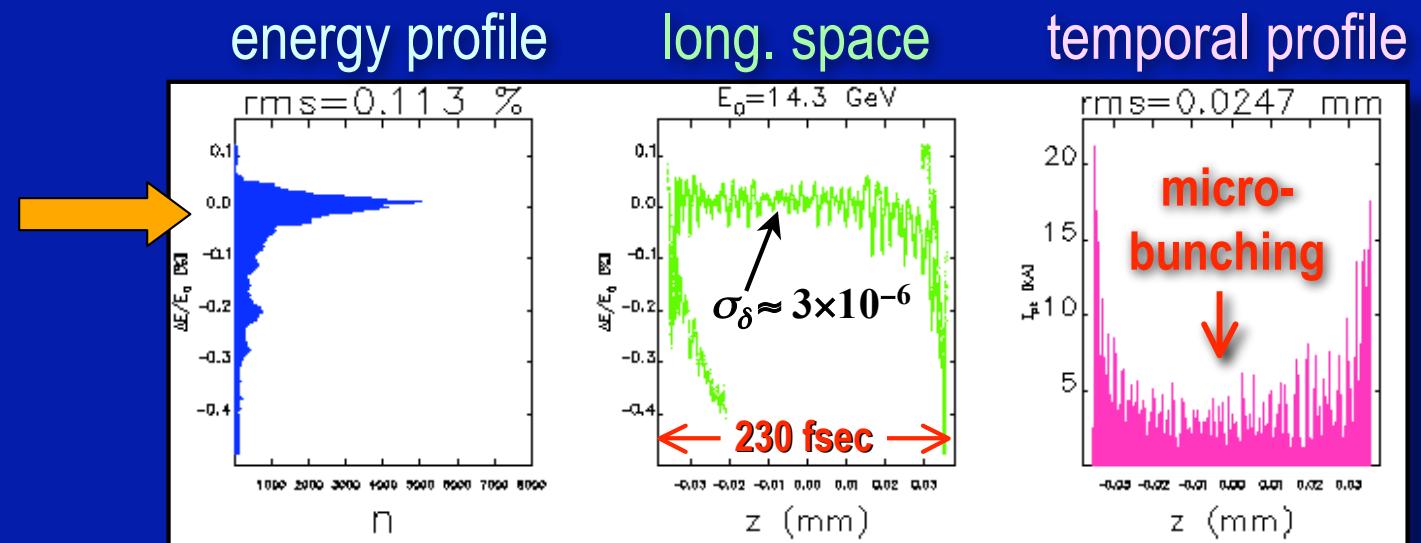


**Figure 1:** An illustration of microbunching instability in a bunch compressor.



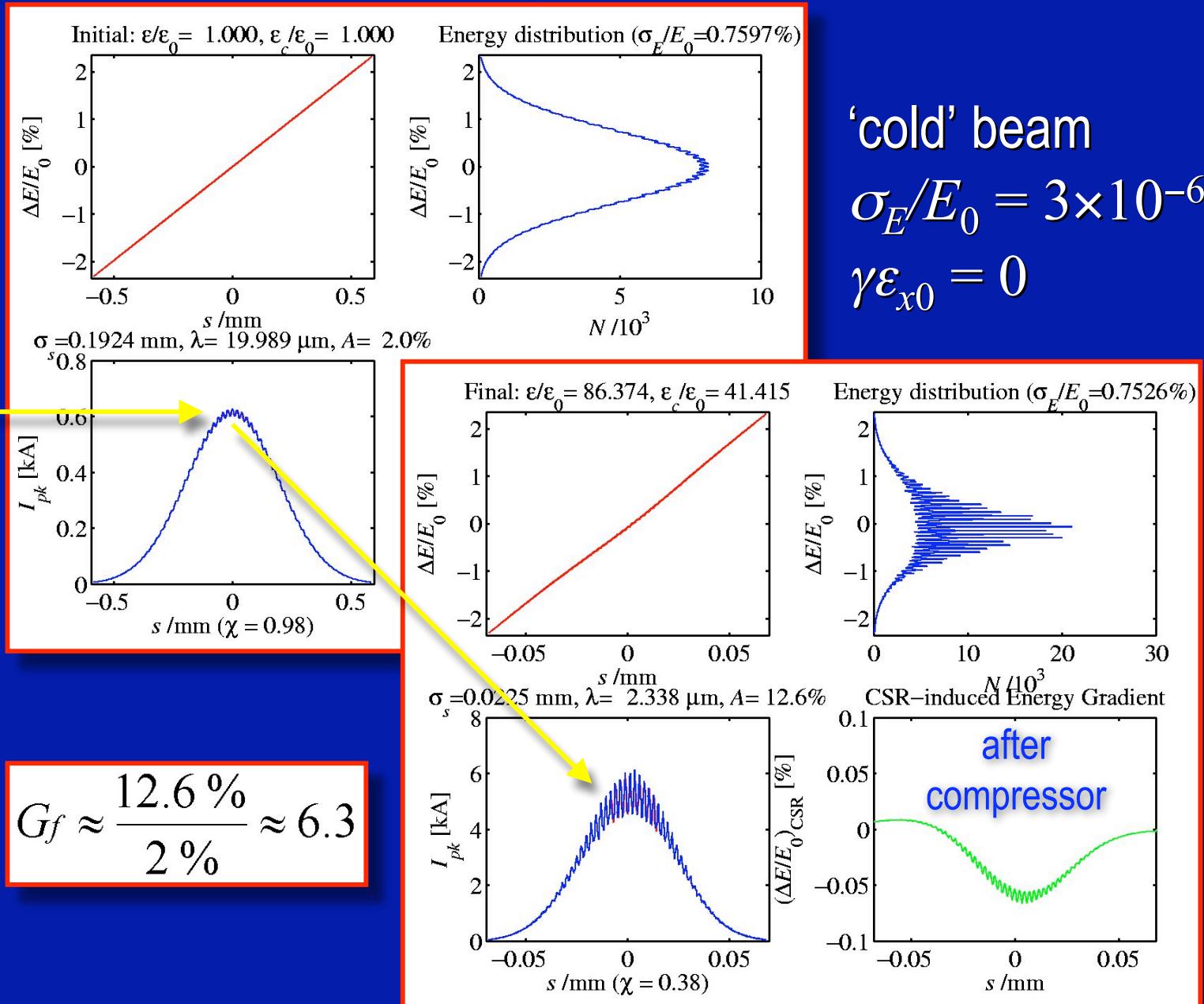
# CSR Microbunching in LCLS

CSR can amplify  
small current  
modulations:



# CSR Microbunching Gain in LCLS BC2

add 2%  
current &  
energy  
modulation



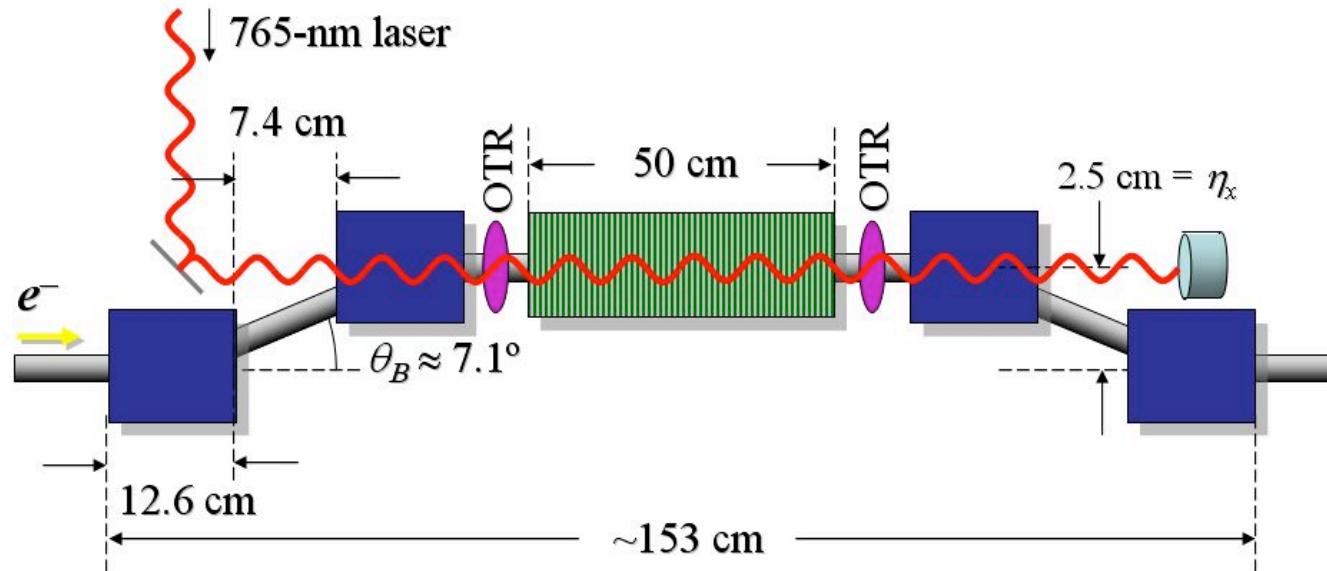
# Laser heater

## Motivation:

- Collective effect: SP/CSR drive micro-bunch instabilities
- Residual energy-spread  $\sim 1\text{-}3\text{keV} \Rightarrow \text{No Landau damping}$
- Energy-spread can be larger for FELs ( $\sigma_E/E < \rho \sim 5\text{e-}4$ )

$\Rightarrow$  increase  $\varepsilon_E \rightarrow 10\text{-}50\text{ keV}$

Example LCLS design



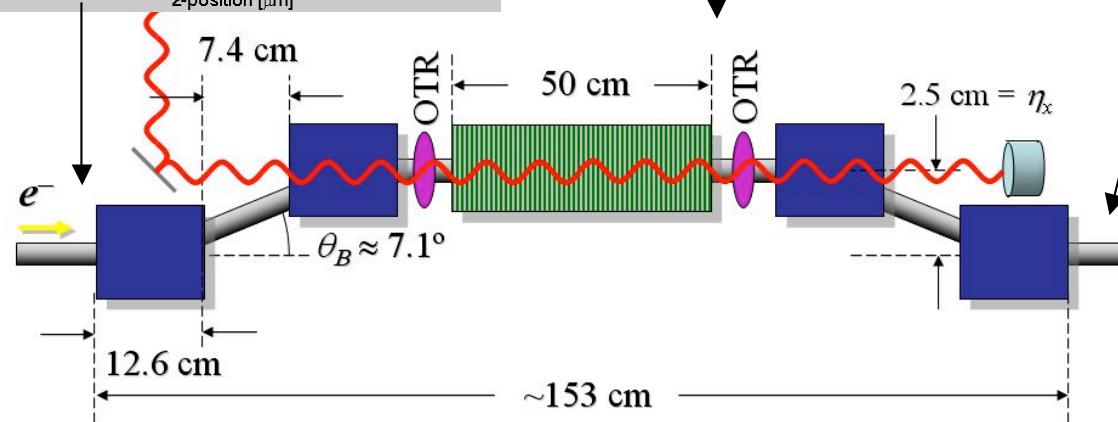
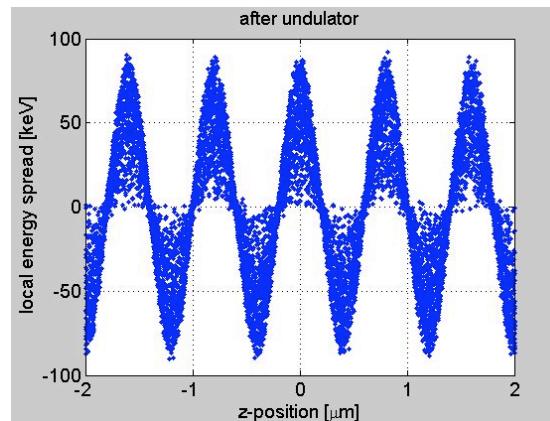
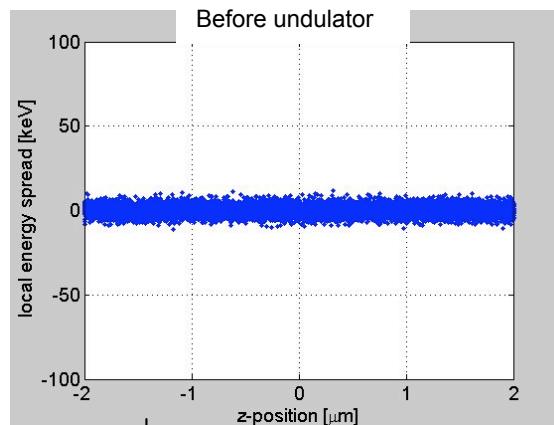
Courtesy H. Schlarb

Z. Huang et al., Phys. Rev. STAB 7, 074401 (2004)  
J. Wu et al., SLAC-PUB-10430

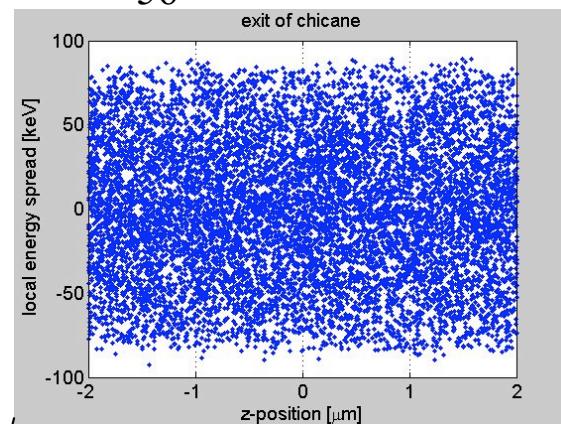
# Laser heater

heating  $\sigma_L \sim 40\text{keV}$

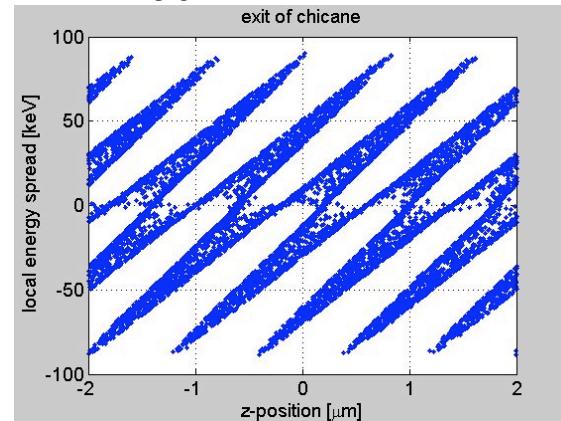
Residual  $\sigma_E \sim 1\text{-}3\text{keV}$

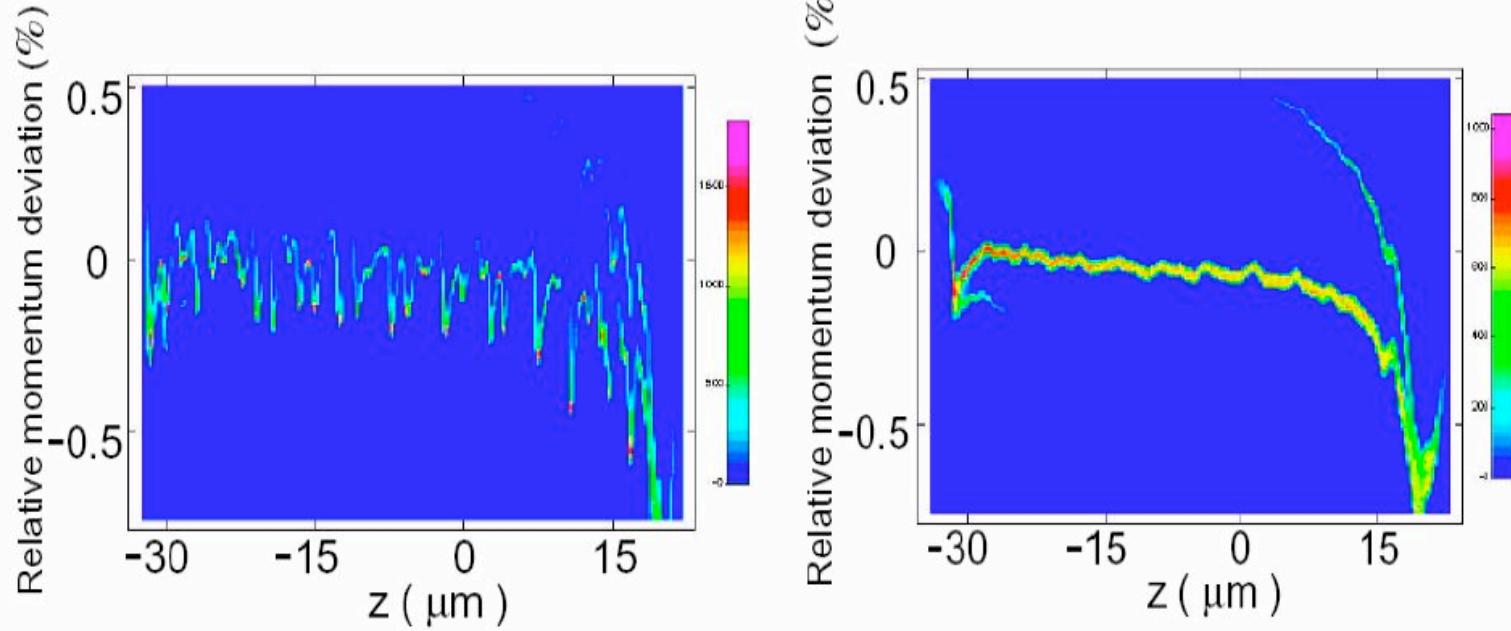


$$R_{56} = -0.024$$



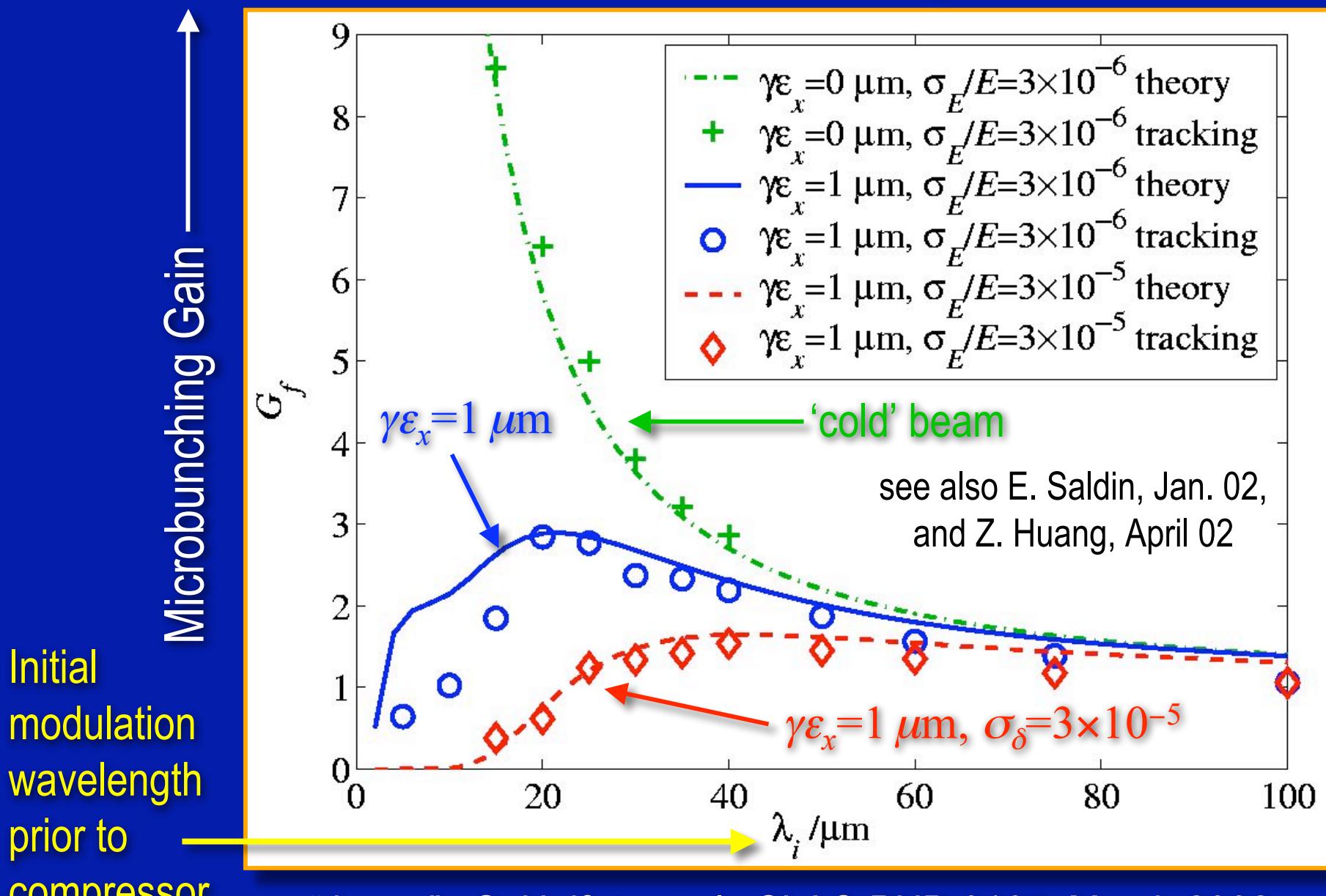
$$R_{56}=0$$



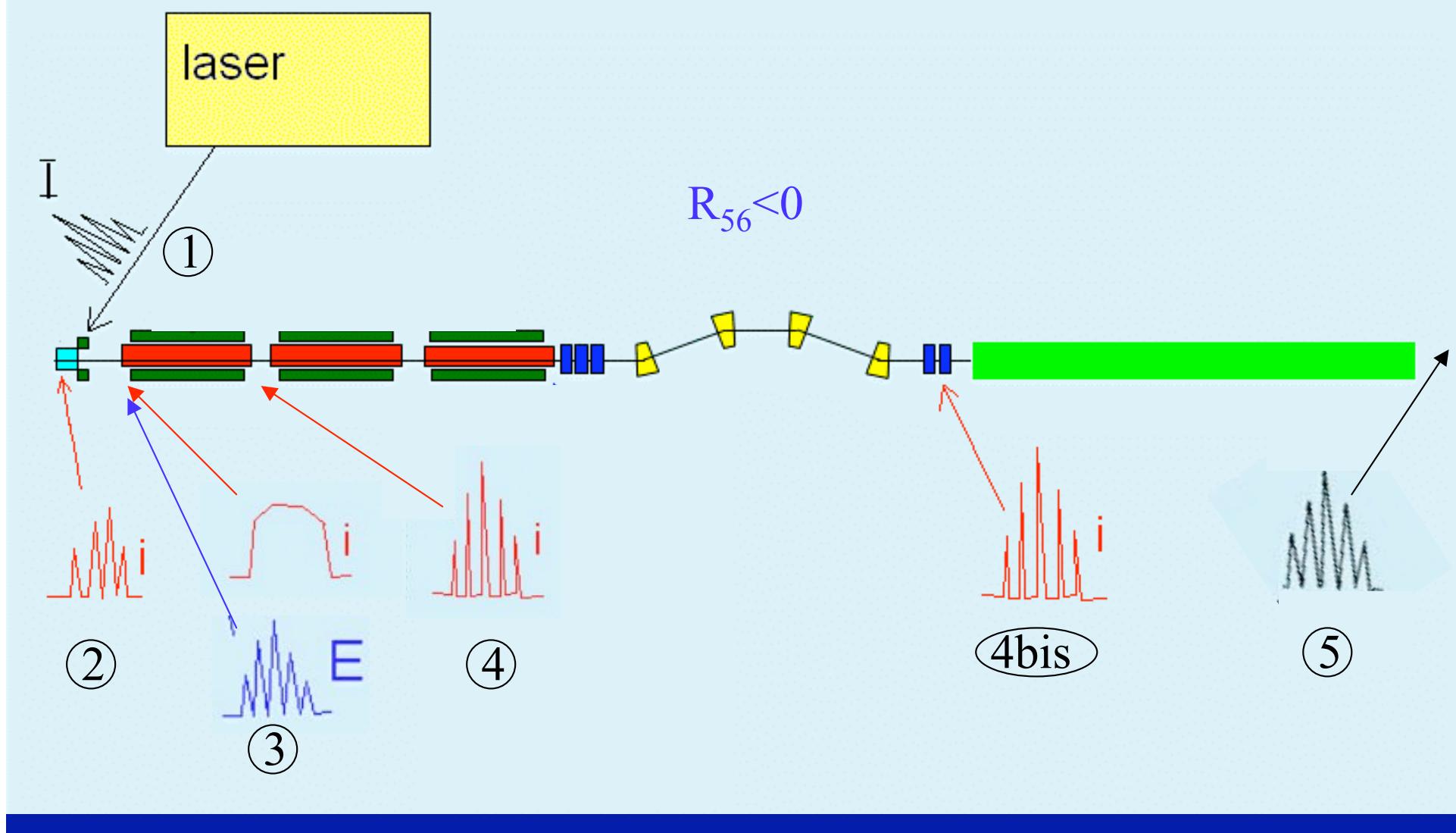


**Figure 5:** Longitudinal phase space distribution at the entrance of the LCLS undulator for an initial  $\pm 8\%$  laser intensity modulation at  $\lambda_0 = 150 \mu\text{m}$  in the start-to-end simulation without the laser-heater (left plot) and with the laser heater (right plot).

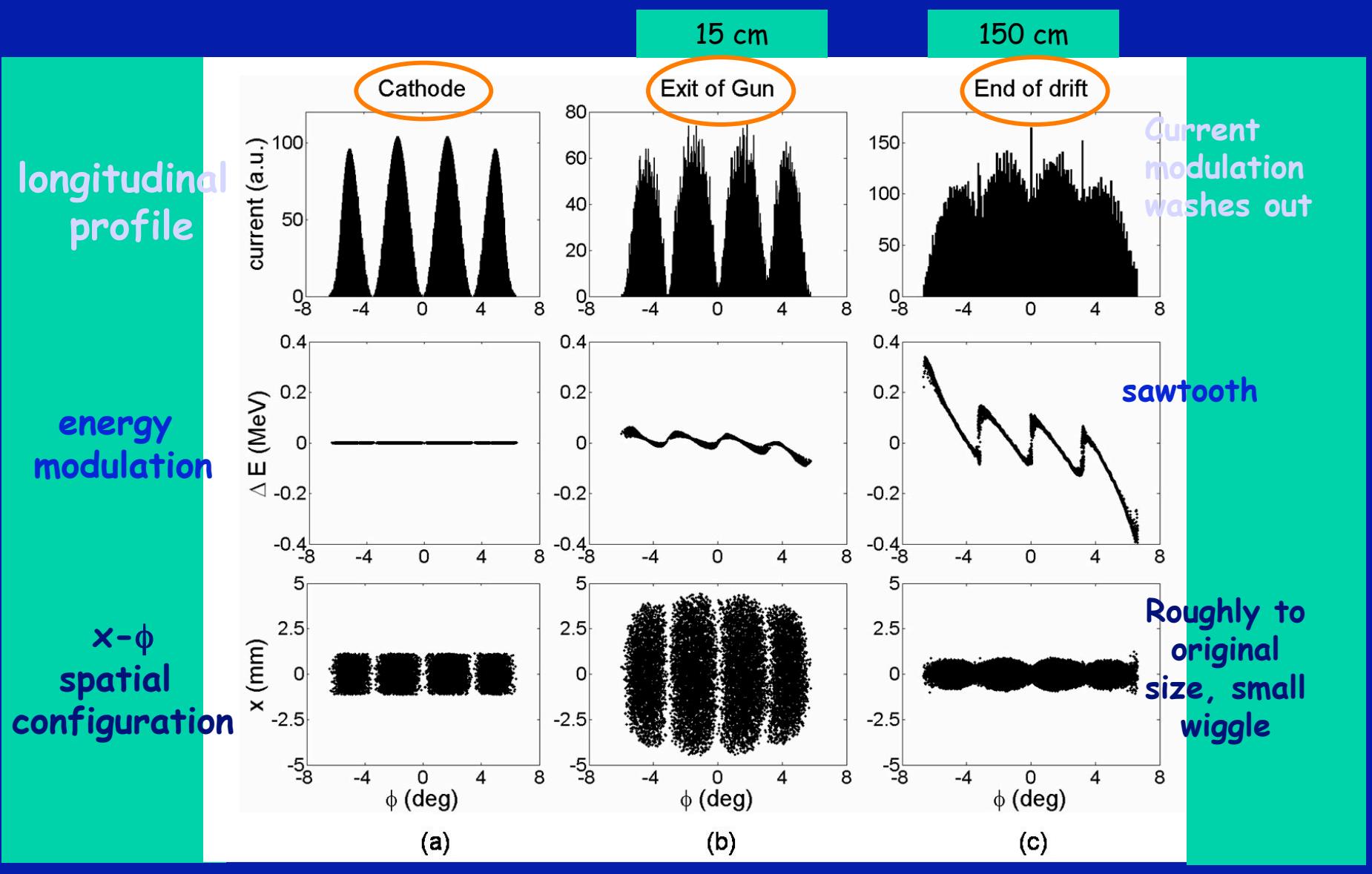
# LCLS BC2 CSR Microbunching Gain vs. $\lambda$



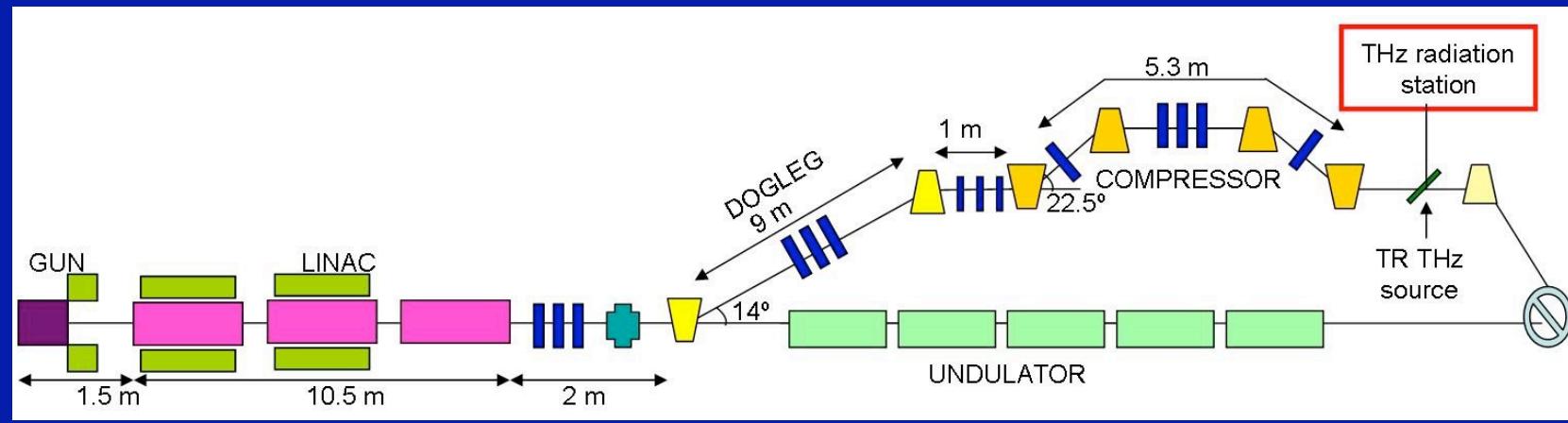
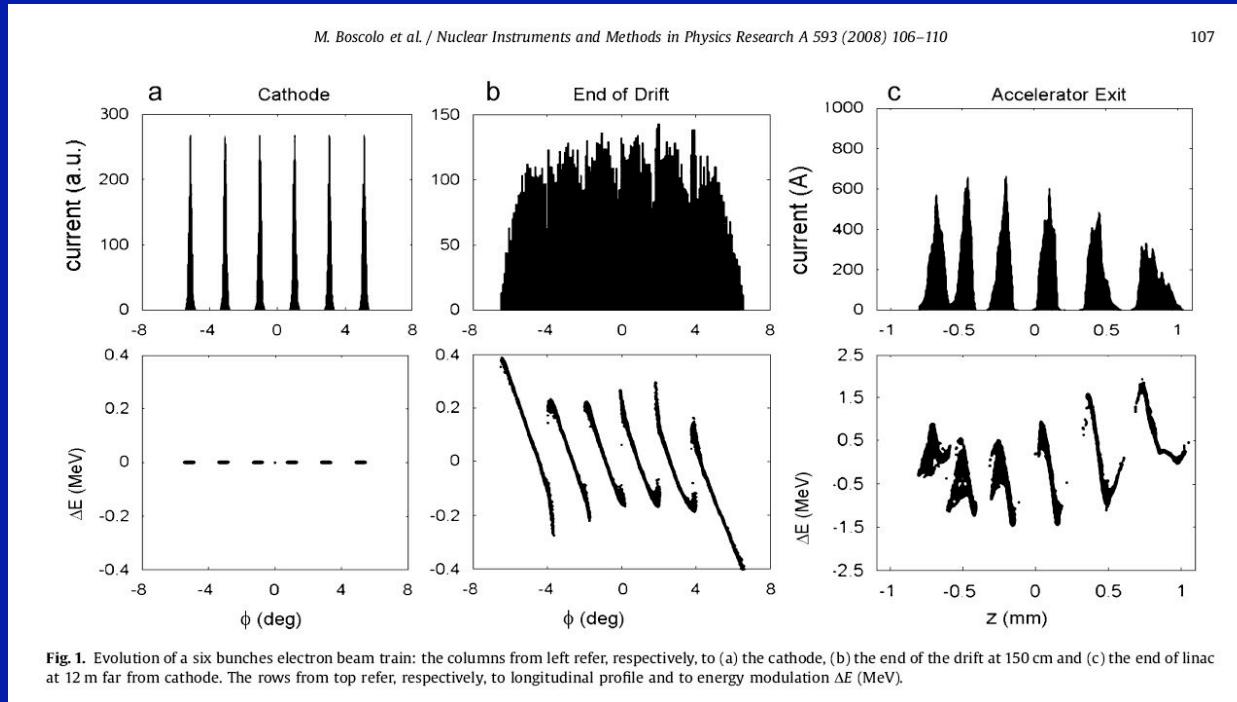
# Laser Comb: a giant microbunch instability



# Example of typical behavior: $N = 4$

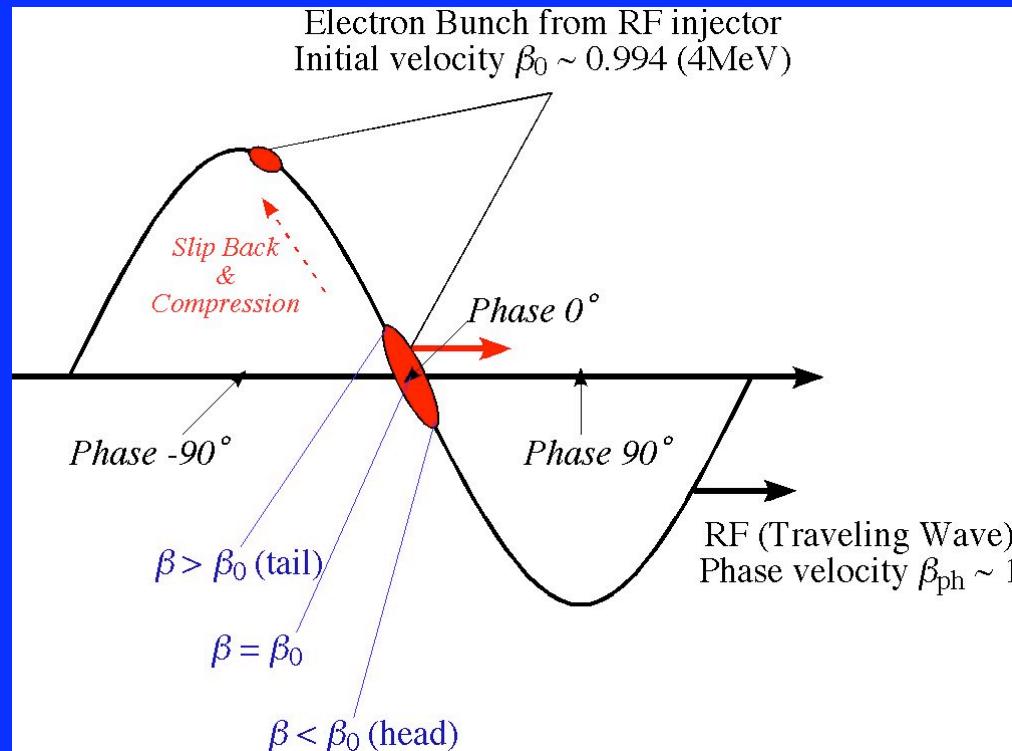


# Laser Comb: a giant microbunch instability

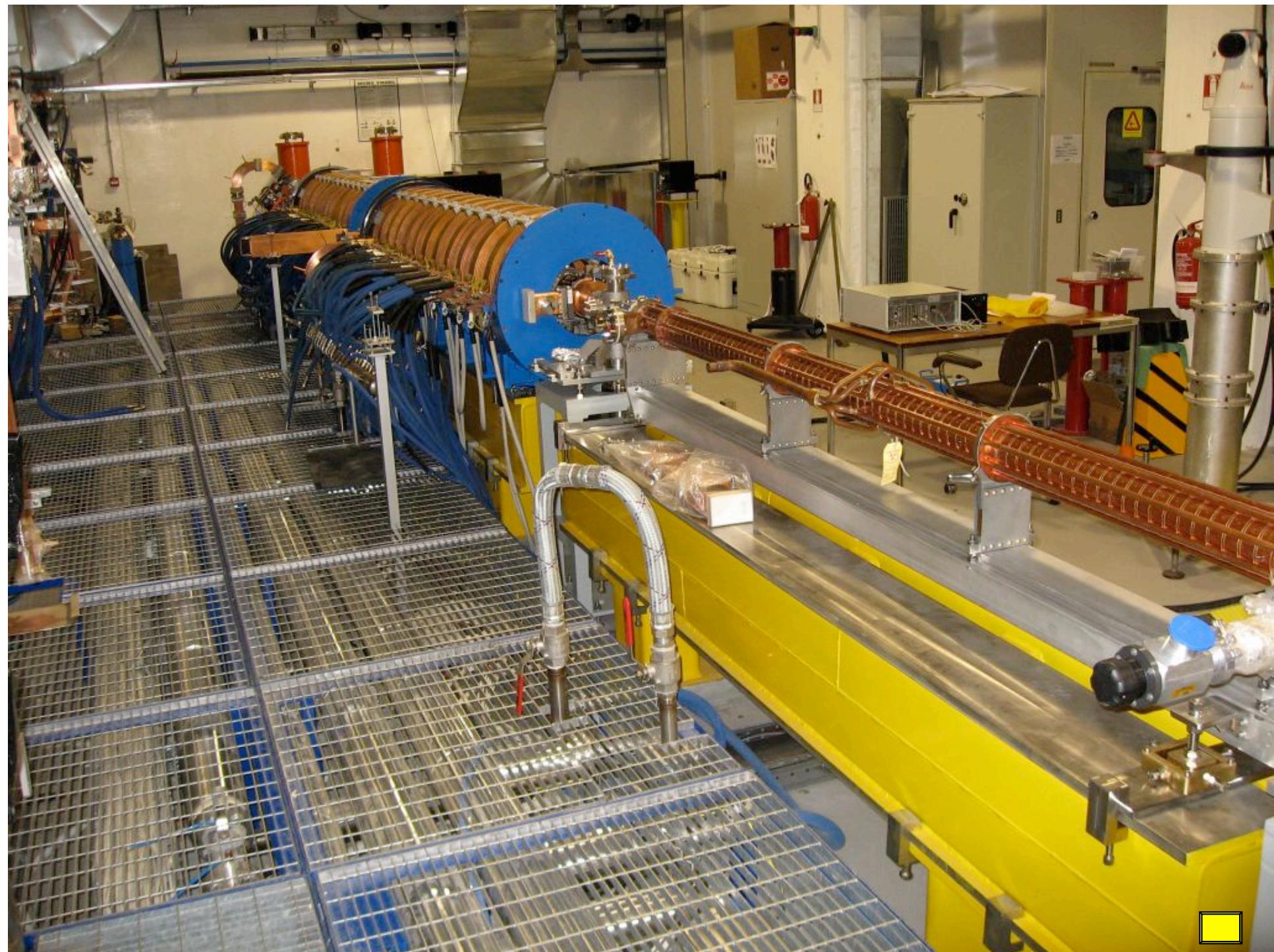


# Velocity bunching concept (RF Compressor)

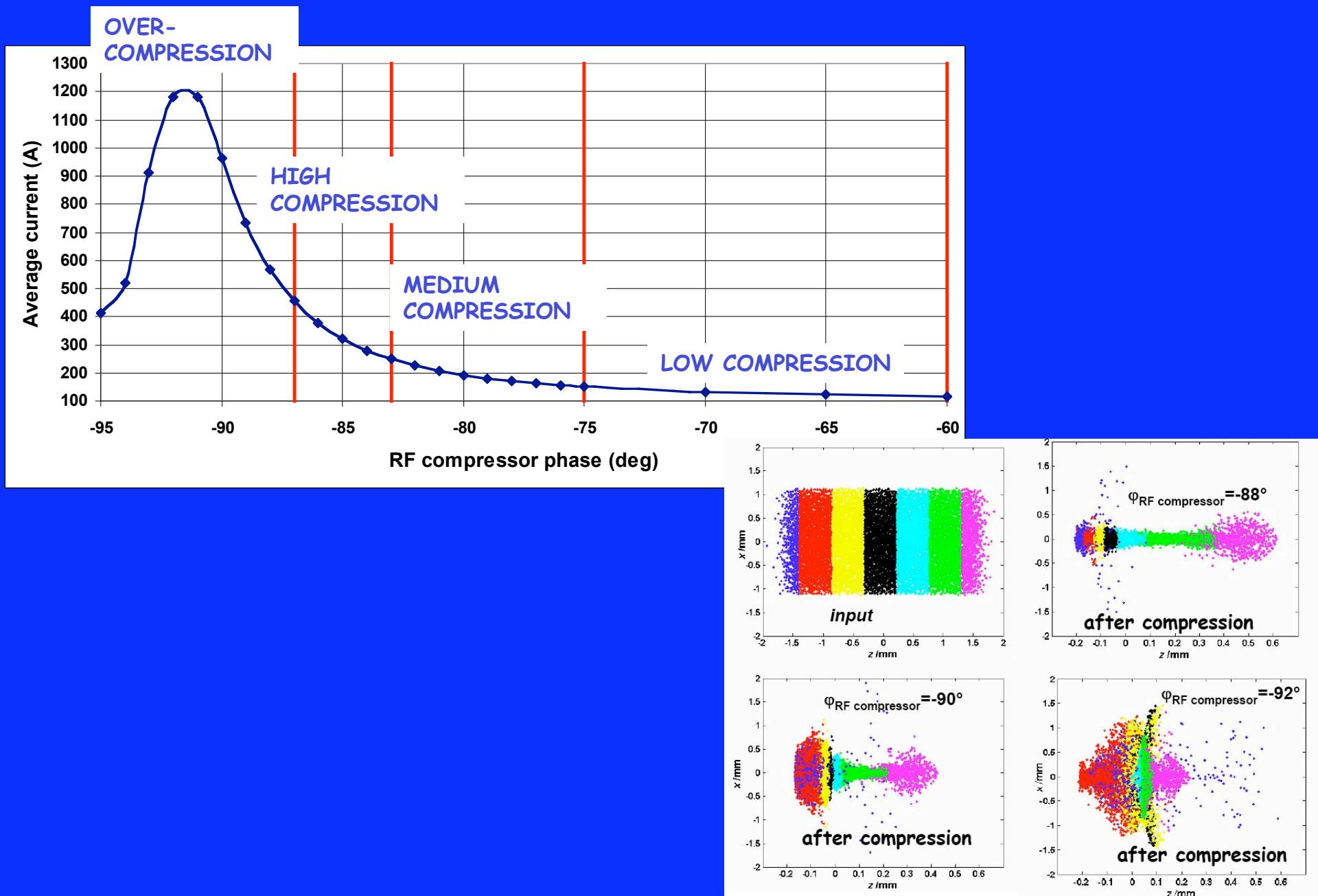
If the beam injected in a long accelerating structure at the crossing field phase and it is slightly slower than the phase velocity of the RF wave , it will slip back to phases where the field is accelerating, but at the same time it will be chirped and compressed.

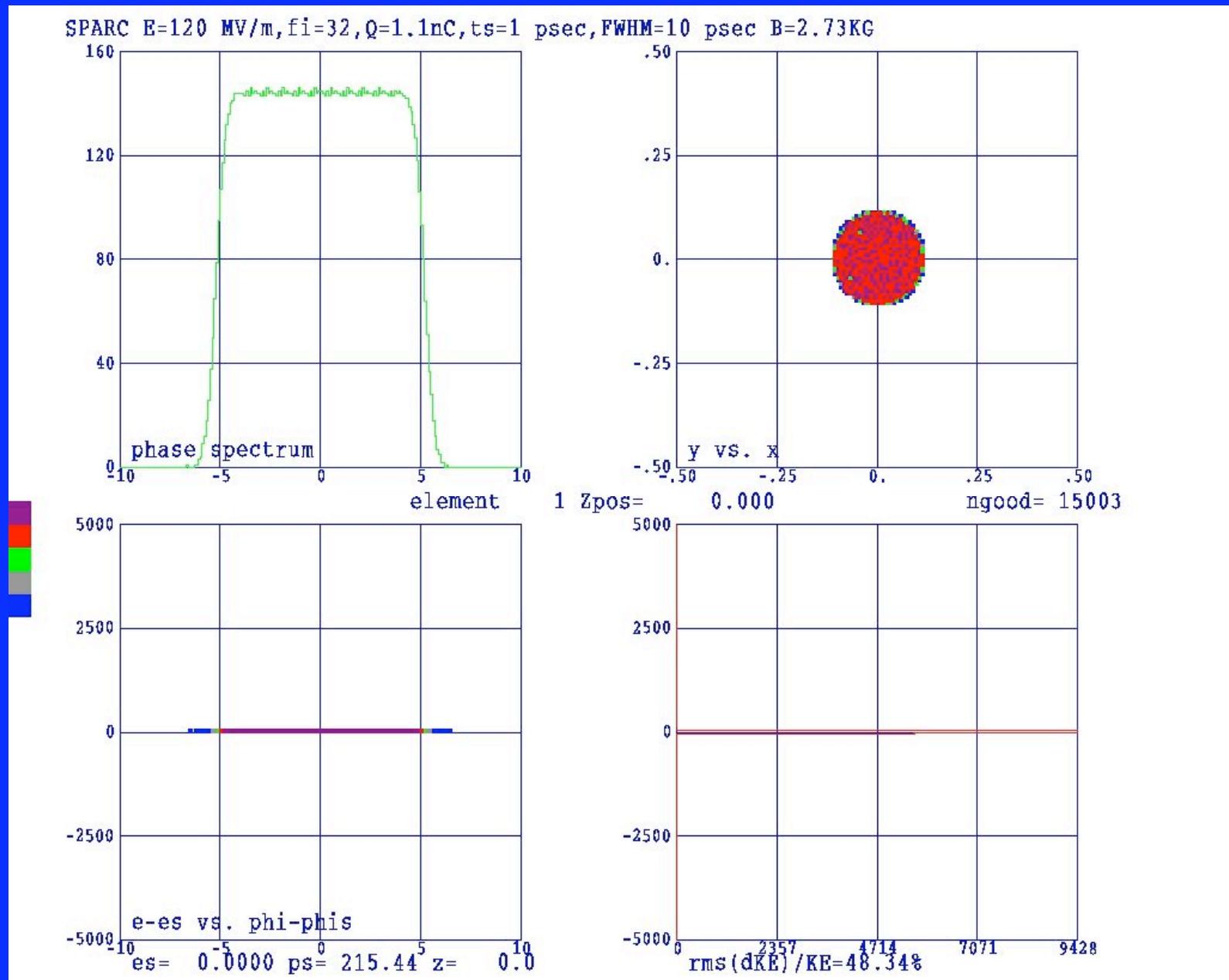


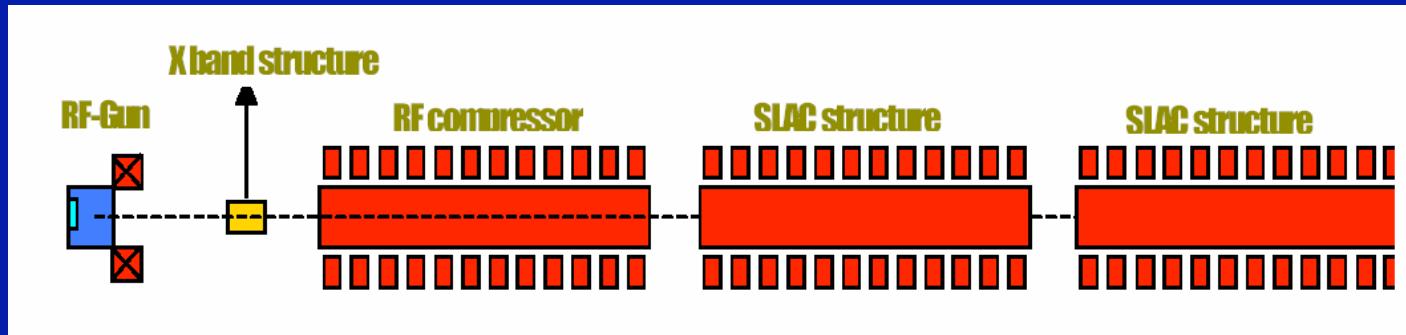
The key point is that compression and acceleration take place at the same time within the same linac section, actually the first section following the gun, that typically accelerates the beam, under these conditions, from a few MeV ( $> 4$ ) up to 25-35 MeV.



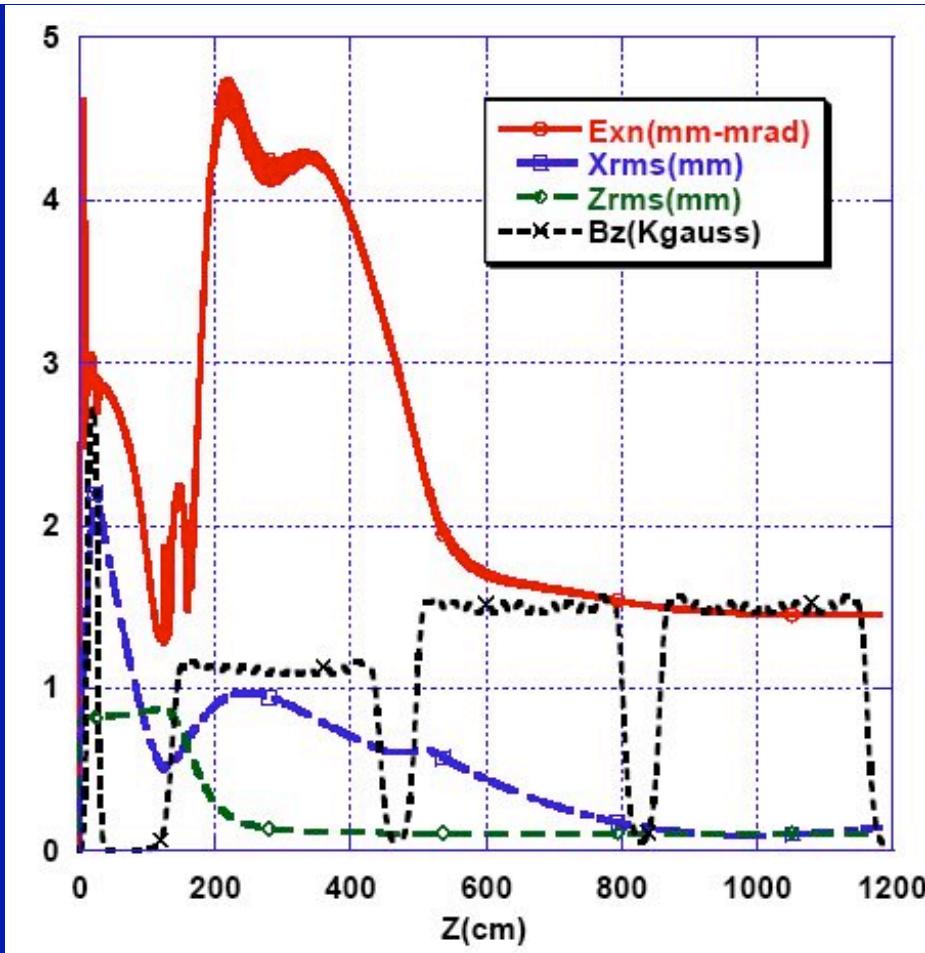
# Average current vs RF compressor phase



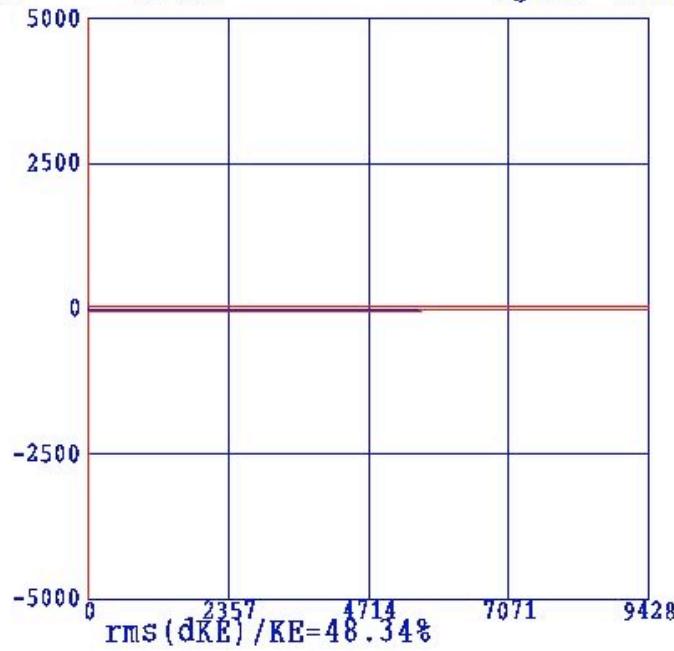
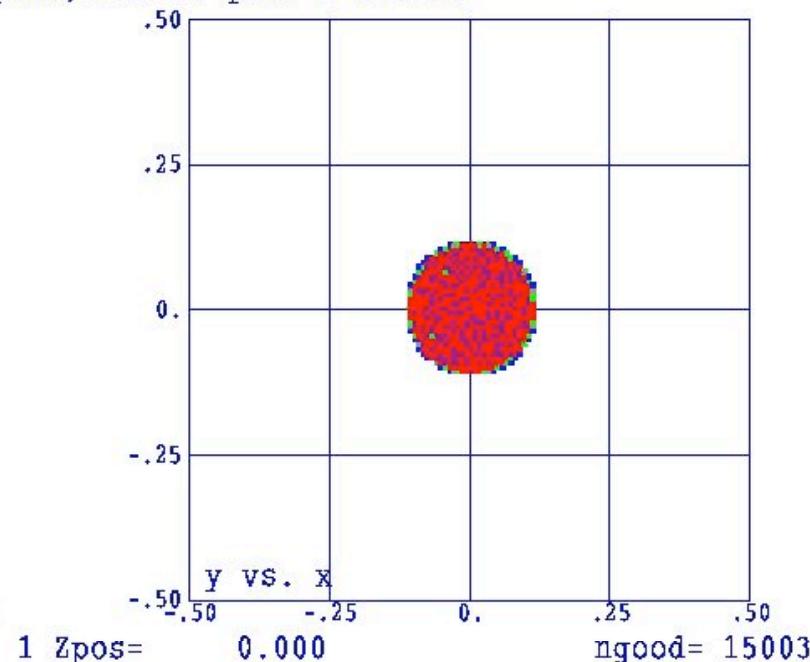
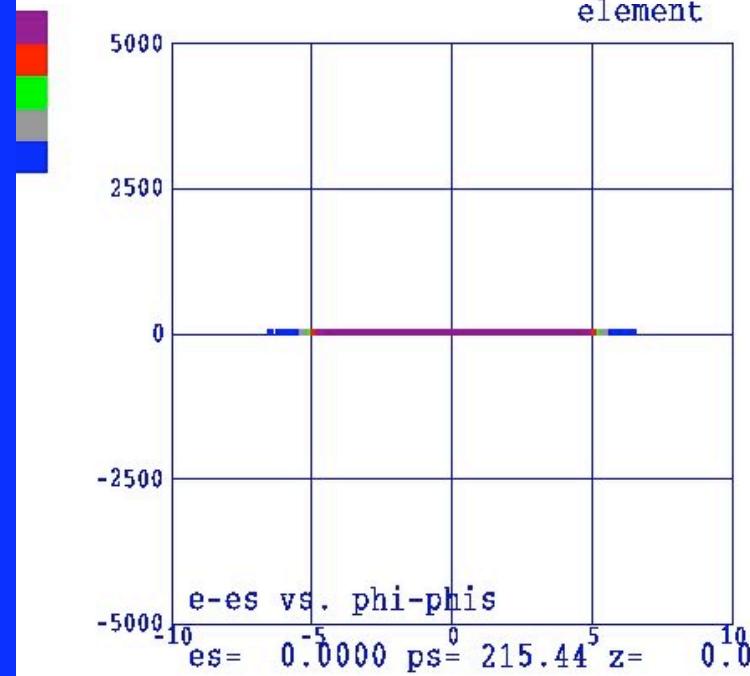
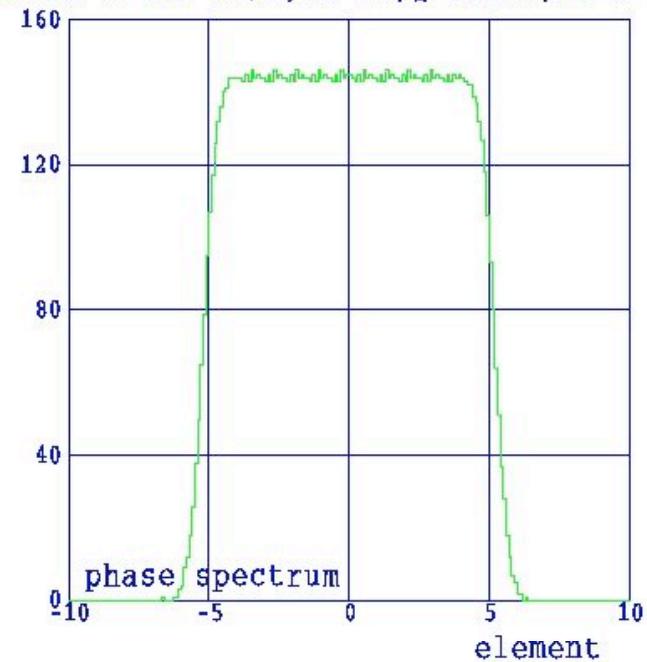




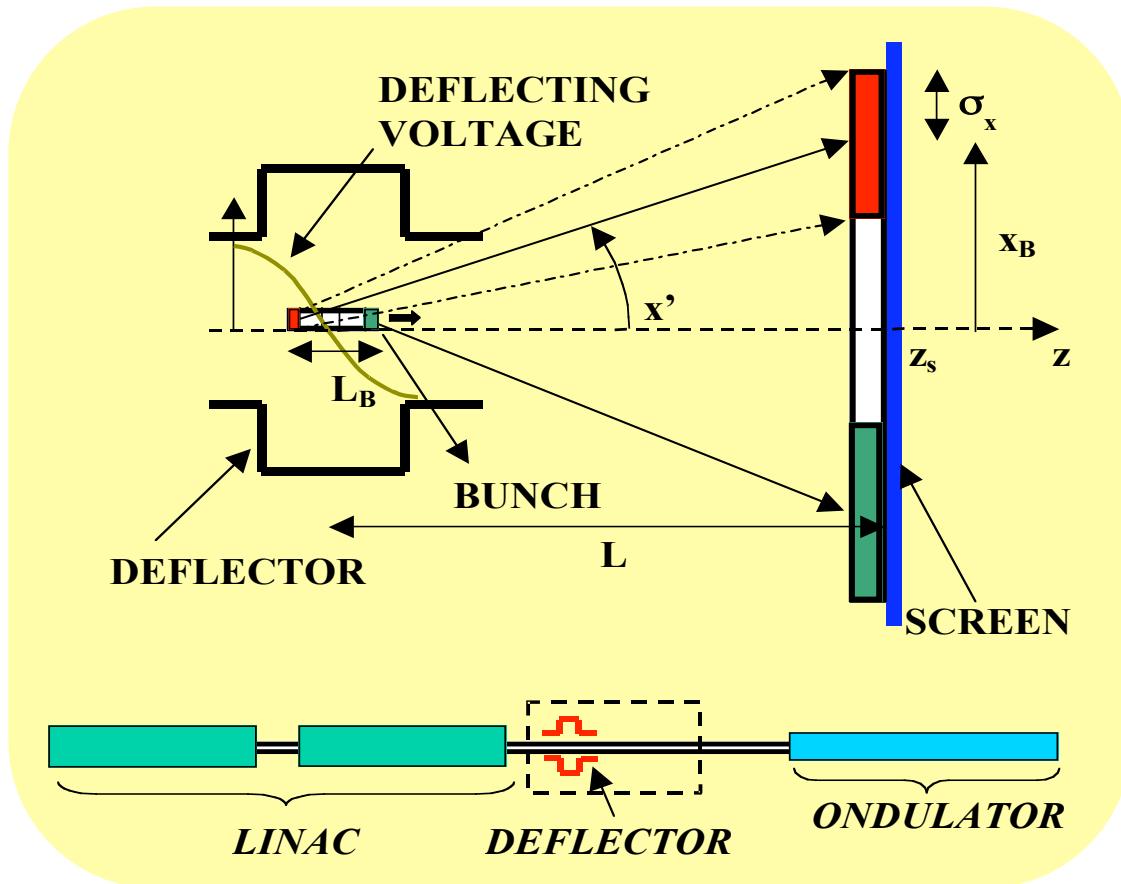
$\langle I \rangle = 860 \text{ A}$   
 $\varepsilon_{nx} = 1.5 \mu\text{m}$



SPARC E=120 MV/m, fi=32, Q=1.1nC, ts=1 psec, FWHM=10 psec B=2.73KG



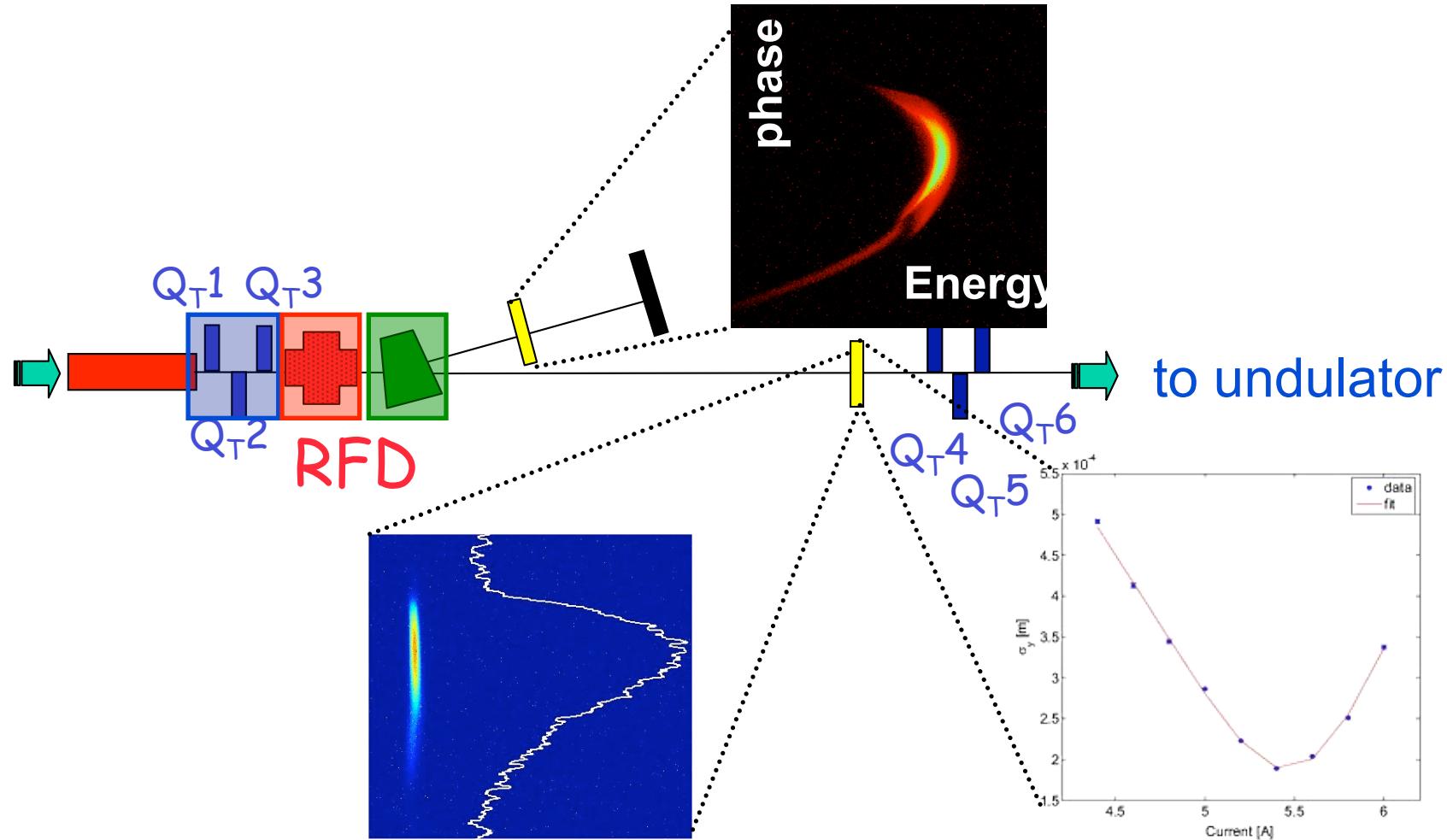
# RF deflector



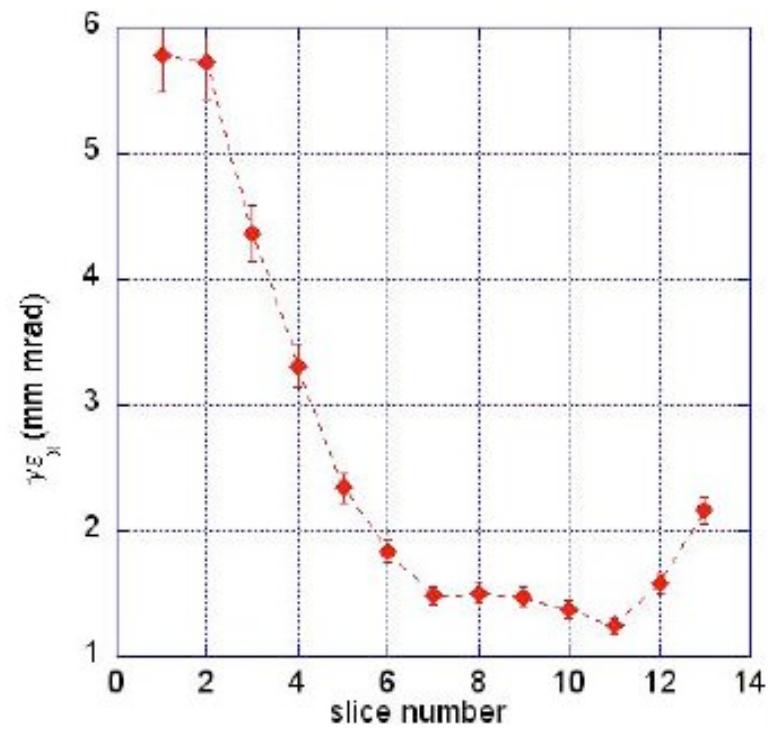
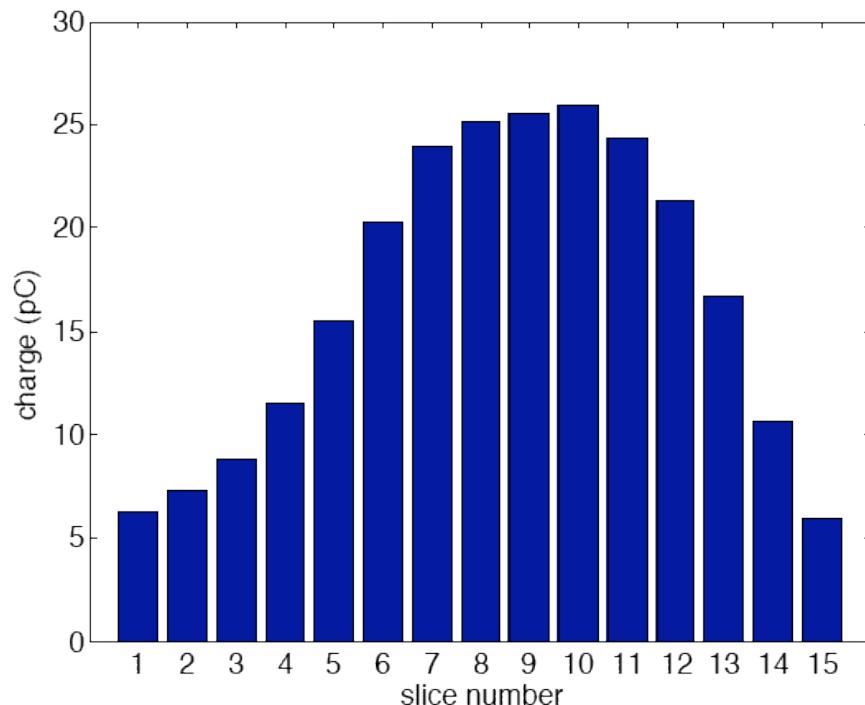
$$x_B = \frac{\pi f_{RF} L L_B V_\perp}{c E / e}$$

$$V_\perp = \frac{\sigma_x c E / e}{\pi f_{RF} L L_{res}}$$

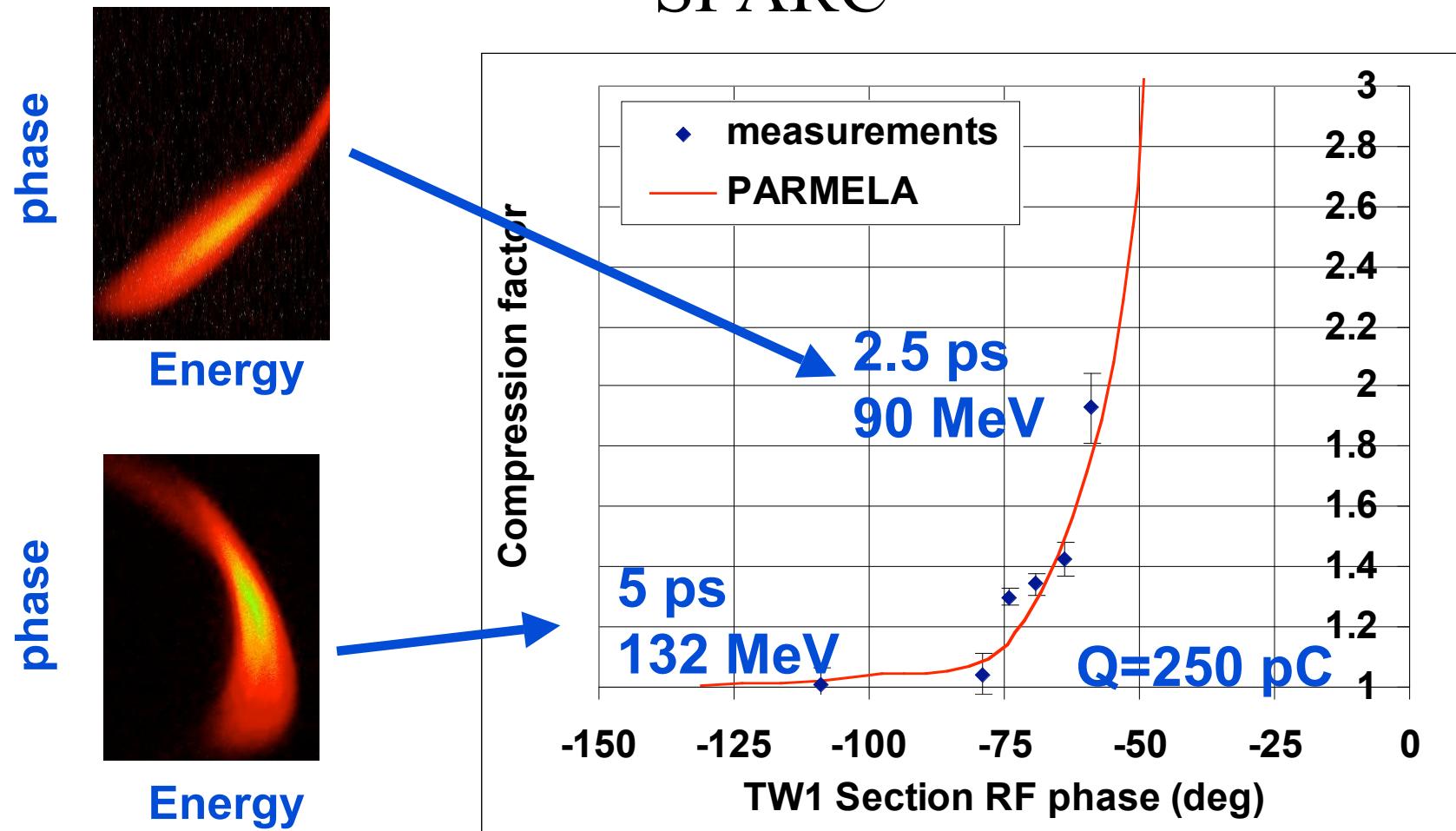
# SPARC Diagnostic Section



# Slice emittance measurements



# Preliminary results for the velocity bunching at SPARC



# Velocity bunching equations

$$\begin{aligned}\frac{d}{dz}(\gamma mc^2) &= eE \sin(kz - \omega t + \varphi_o) \\ \frac{d\gamma}{dz} &= \frac{eE}{mc^2} \sin(kz - \omega t + \varphi_o) \\ \frac{d\gamma}{dz} &= \alpha k \sin(\varphi)\end{aligned}$$

$$\begin{aligned}\frac{d\varphi}{dz} &= \frac{d}{dz}(kz - \omega t + \varphi_o) = \left( k - \omega \frac{dt}{dz} \right) = \left( k - \frac{\omega}{\beta c} \right) \\ &= k \left( 1 - \frac{1}{\beta} \right) = k \left( 1 - \frac{\gamma}{\sqrt{\gamma^2 - 1}} \right)\end{aligned}$$

$$\begin{cases} \frac{d\gamma}{dz} = \alpha k \sin(\varphi) \\ \frac{d\varphi}{dz} = k \left( 1 - \frac{\gamma}{\sqrt{\gamma^2 - 1}} \right) \end{cases}$$

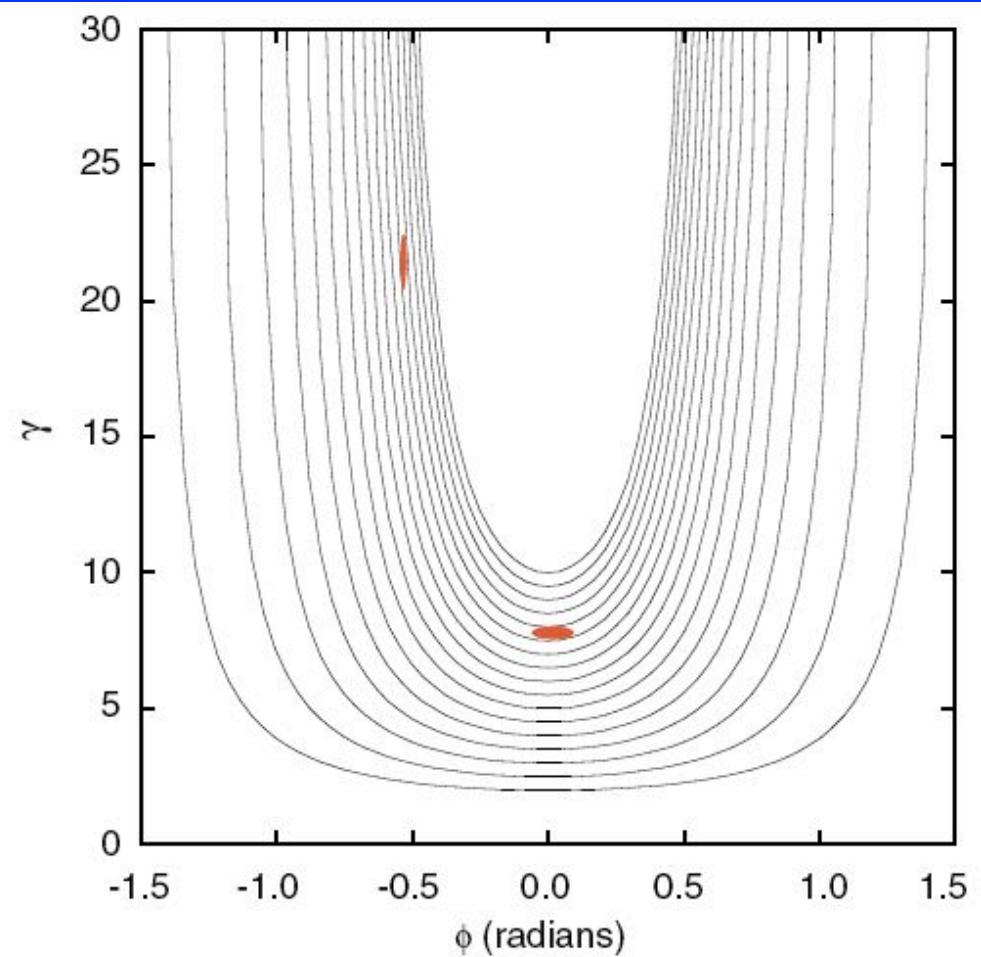
Such a system is solved using the variable separation technique to yield a constant of the motion (total energy):

$$H = \gamma - \sqrt{\gamma^2 - 1} - \alpha \cos(\phi)$$

$$H = \gamma - \sqrt{\gamma^2 - 1} - \alpha \cos(\phi)$$

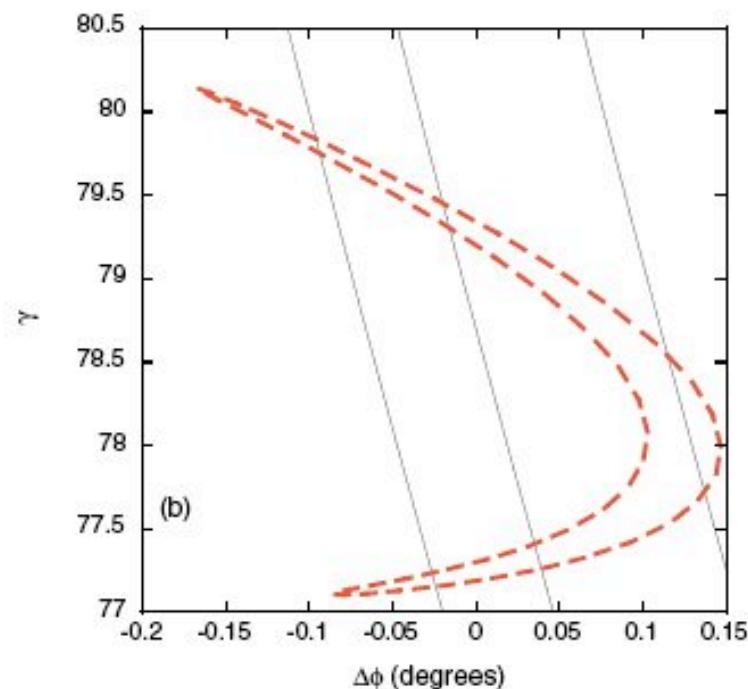
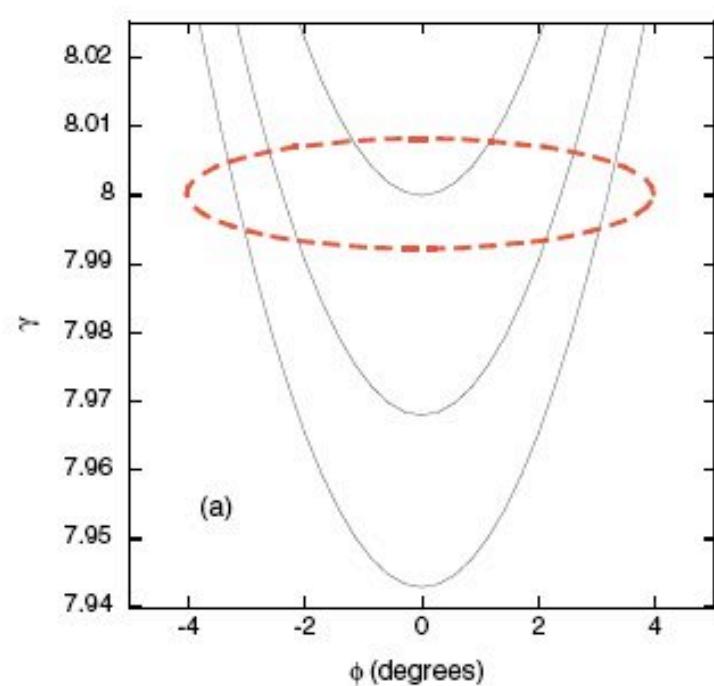
$$H = -\alpha \cos\phi_\infty = \gamma_0 - \sqrt{\gamma_0^2 - 1} - \alpha \cos\phi_0$$

$$\phi_\infty \cong \cos^{-1} \left[ \cos\phi_0 - \frac{1}{2\alpha\gamma_0} \right]$$



## Second order effects

$$\begin{aligned}\Delta\phi_{\infty} = & \frac{\sin\phi_0}{\sin\phi_{\infty}}\Delta\phi_0 + \frac{1}{2\alpha\gamma_0^2\sin\phi_{\infty}}\Delta\gamma_0 \\ & + \frac{1}{2}\left[\frac{\cos\phi_0}{\sin\phi_{\infty}} - \frac{\cos\phi_{\infty}\sin^2\phi_0}{\sin^3\phi_{\infty}}\right](\Delta\phi_0)^2.\end{aligned}$$



**THE END**

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