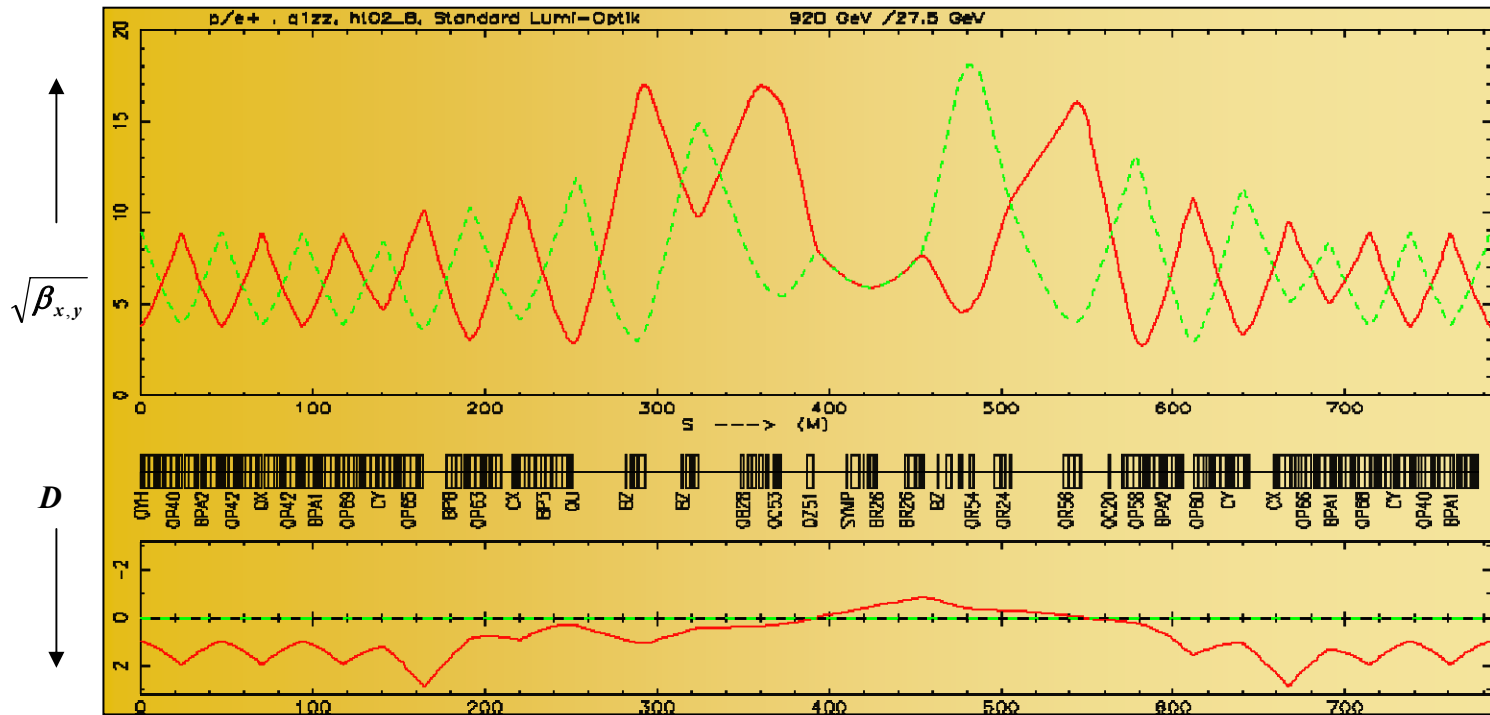


# Lattice Design in Particle Accelerators

## Bernhard Holzer, DESY



**1952: Courant, Livingston, Snyder:**

*Theory of strong focusing in particle beams*

# *Lattice Design: „... how to build a storage ring“*

High energy accelerators → **circular machines**

somewhere in the lattice we need a number of **dipole magnets**,  
that are bending the design orbit to a **closed ring**

Geometry of the ring:

**centrifugal force = Lorentz force**

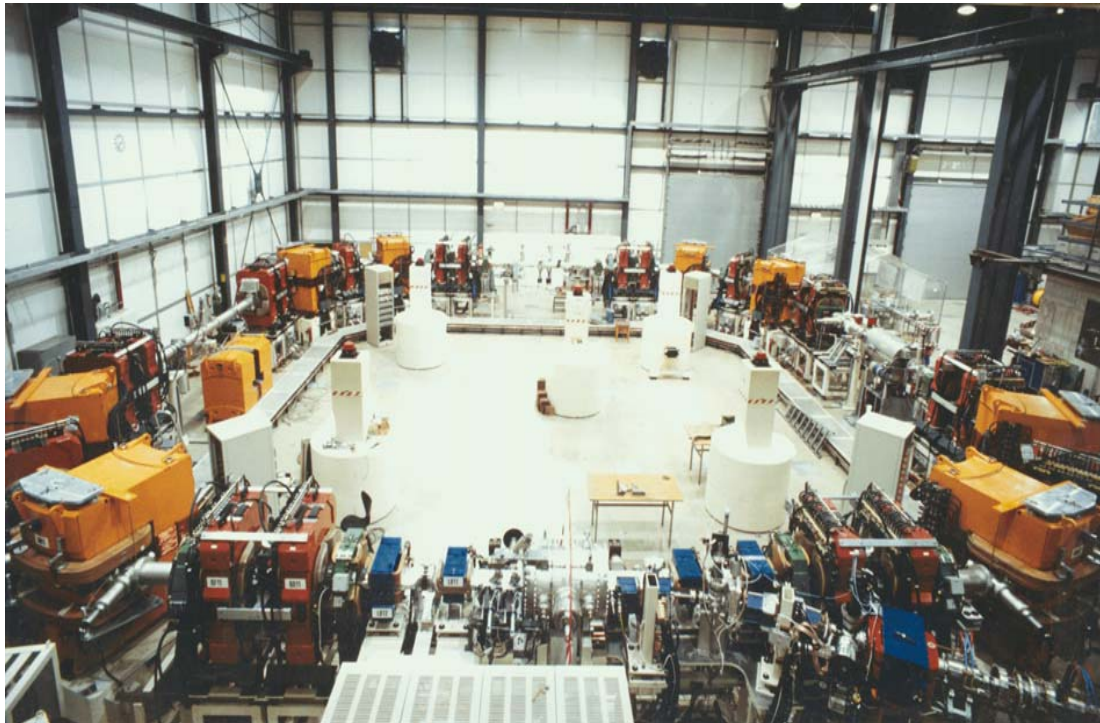
$$e * v * B = \frac{m v^2}{\rho}$$

$$\rightarrow e * B = \frac{m v}{\rho} = p / \rho$$

$$\rightarrow B * \rho = p / e$$

*p = momentum of the particle,*  
*ρ = curvature radius*

*Bρ = beam rigidity*



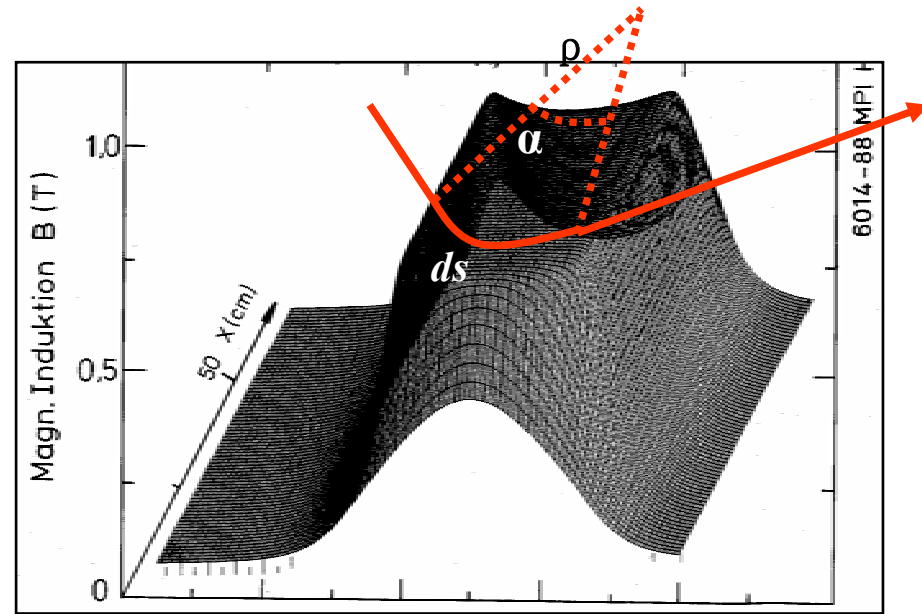
*Example: heavy ion storage ring TSR*  
*8 dipole magnets of equal bending strength*

# Circular Orbit:

„... defining the geometry“

$$\alpha = \frac{ds}{\rho} \approx \frac{dl}{\rho}$$

$$\alpha = \frac{B^* dl}{B^* \rho}$$



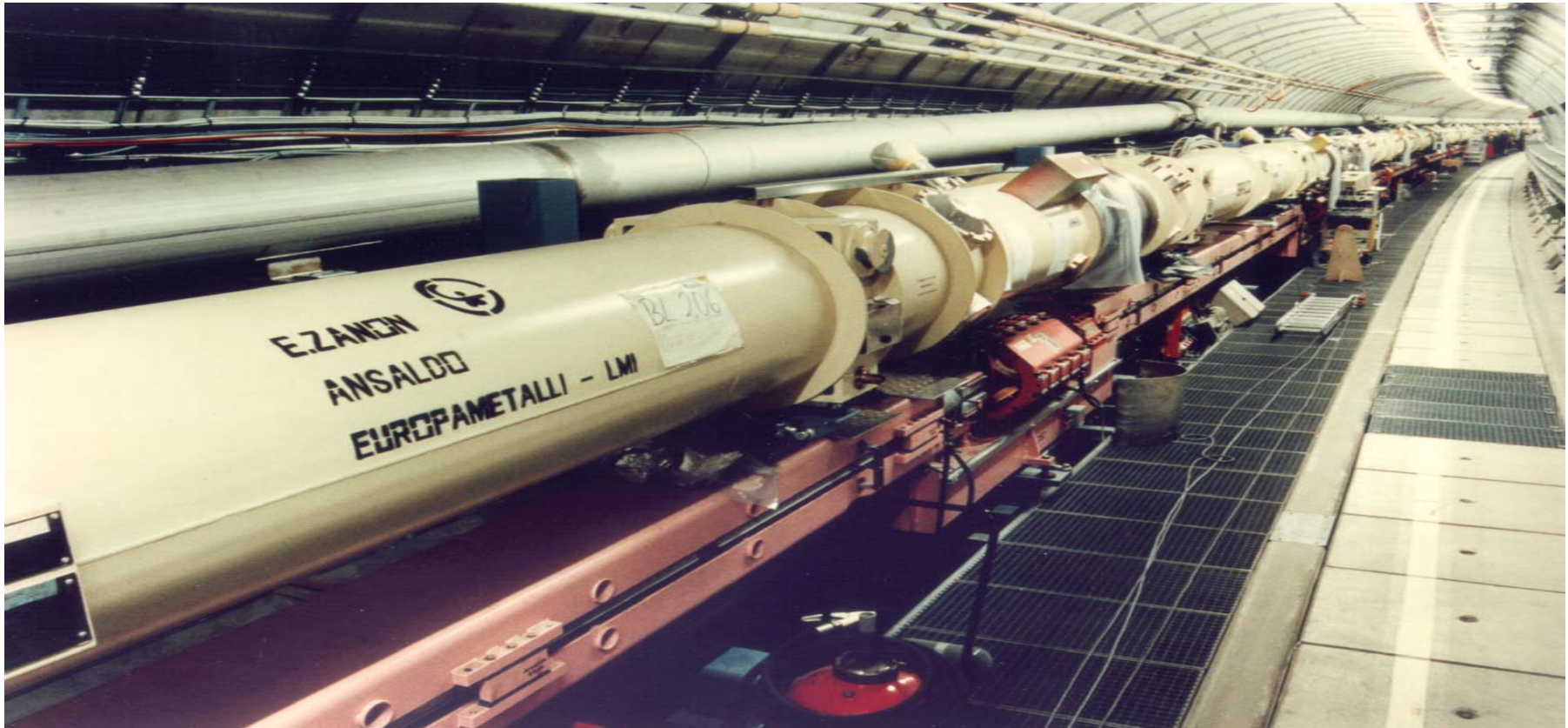
field map of a storage ring dipole magnet

The angle swept out in one revolution must be  $2\pi$ , so

$$\alpha = \frac{\int B dl}{B^* \rho} = 2\pi \quad \rightarrow \quad \int B dl = 2\pi * \frac{p}{q} \quad \dots \text{ for a full circle}$$

*Nota bene:*  $\frac{\Delta B}{B} \approx 10^{-4}$  is usually required !!

## Example HERA:



920 GeV Proton storage ring  
dipole magnets  $N = 416$   
 $l = 8.8\text{m}$   
 $q = +1 e$

$$\int B dl \approx N * l * B = 2\pi p / q$$

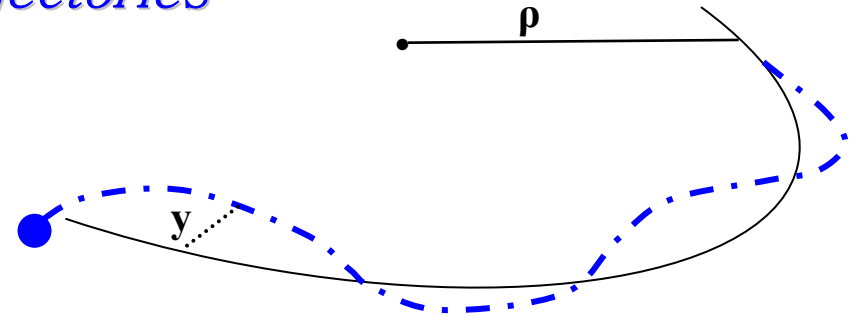
$$B \approx \frac{2\pi * 920 * 10^9 eV}{416 * 3 * 10^8 \frac{m}{s} * 8.8m * e} \approx \underline{\underline{5.15 \text{ Tesla}}}$$

„ Focusing forces † single particle trajectories “

$$y'' + K * y = 0$$

$$K = -k + 1 / \rho^2 \quad \text{hor. plane}$$

$$K = k \quad \text{vert. plane}$$



dipole magnet	$\frac{1}{\rho} = \frac{B}{p/q}$	}
quadrupole magnet	$k = \frac{g}{p/q}$	

Example: HERA Ring:

Bending radius:  $\rho = 580 \text{ m}$

Quadrupole Gradient:  $g = 110 \text{ T/m}$

$$k = 33.64 * 10^{-3} / \text{m}^2$$

$$1/\rho^2 = 2.97 * 10^{-6} / \text{m}^2$$

For estimates in large accelerators *the weak focusing term  $1/\rho^2$  can in general be neglected*

Solution for a focusing magnet

$$y(s) = y_0 * \cos(\sqrt{K} * s) + \frac{y'_0}{\sqrt{K}} * \sin(\sqrt{K} * s)$$

$$y'(s) = -y_0 * \sqrt{K} * \sin(\sqrt{K} * s) + y'_0 * \cos(\sqrt{K} * s)$$

Or written more convenient in matrix form:

$$\begin{pmatrix} y \\ y' \end{pmatrix}_s = M * \begin{pmatrix} y \\ y' \end{pmatrix}_0$$

Hor. **focusing** Quadrupole Magnet

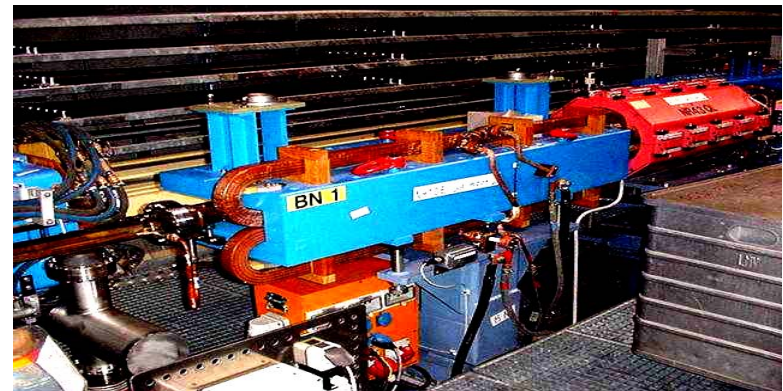
$$M_{QF} = \begin{pmatrix} \cos(\sqrt{K} * l) & \frac{1}{\sqrt{K}} \sin(\sqrt{K} * l) \\ -\sqrt{K} \sin(\sqrt{K} * l) & \cos(\sqrt{K} * l) \end{pmatrix}$$

Hor. **defocusing** Quadrupole Magnet

$$M_{QD} = \begin{pmatrix} \cosh(\sqrt{K} * l) & \frac{1}{\sqrt{K}} \sinh(\sqrt{K} * l) \\ \sqrt{K} \sinh(\sqrt{K} * l) & \cosh(\sqrt{K} * l) \end{pmatrix}$$

Drift space

$$M_{Drift} = \begin{pmatrix} 1 & s \\ 0 & 1 \end{pmatrix}$$



$$M_{lattice} = M_{QF1} * M_{D1} * M_{QD} * M_{D1} * M_{QF2} \dots$$

## VII.) Transfer Matrix $M$

which can be expressed ... for convenience ... in matrix form

$$\begin{pmatrix} x \\ x' \end{pmatrix}_s = M \begin{pmatrix} x \\ x' \end{pmatrix}_0$$

$$M = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} (\cos \psi_s + \alpha_0 \sin \psi_s) & \sqrt{\beta_s \beta_0} \sin \psi_s \\ \frac{(\alpha_0 - \alpha_s) \cos \psi_s - (1 + \alpha_0 \alpha_s) \sin \psi_s}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} (\cos \psi_s - \alpha_s \sin \psi_s) \end{pmatrix}$$

- \* we can calculate *the single particle trajectories* between two locations in the ring, if we know the  $\alpha \beta \gamma$  at these positions.
- \* and nothing but the  $\alpha \beta \gamma$  at these positions.
- \* ... !

# Periodic Lattices

**In the case of periodic lattices** the transfer matrix can be expressed as a function of a set of periodic parameters  $\alpha, \beta, \gamma$

$$M(s) = \begin{pmatrix} \cos \mu + \alpha_s \sin \mu & \beta_s \sin \mu \\ -\gamma_s \sin \mu & \cos(\mu) - \alpha_s \sin \mu \end{pmatrix}$$

$$\mu = \int_s^{s+L} \frac{dt}{\beta(t)}$$

$\mu =$  phase advance per period:

**For stability** of the motion in periodic lattice structures it is required that

$$|\text{trace}(M)| < 2$$

In terms of these new periodic parameters the **solution of the equation of motion** is

$$y(s) = \sqrt{\varepsilon} * \sqrt{\beta(s)} * \cos(\Phi(s) - \delta)$$

$$y'(s) = \frac{-\sqrt{\varepsilon}}{\sqrt{\beta}} * \{\sin(\Phi(s) - \delta) + \alpha \cos(\Phi(s) - \delta)\}$$



## VIII.) Transformation of $\alpha, \beta, \gamma$

consider two positions in the storage ring:  $s_0, s$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_s = M \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

since  $\varepsilon = \text{const}$ :

$$\varepsilon = \beta x'^2 + 2\alpha x x' + \gamma x^2$$

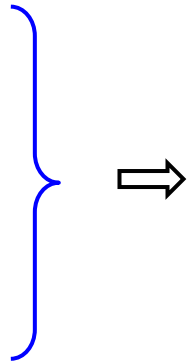
$$\varepsilon = \beta_0 x_0'^2 + 2\alpha_0 x_0 x_0' + \gamma_0 x_0^2$$

express  $x_0, x_0'$  as a function of  $x, x'$ .

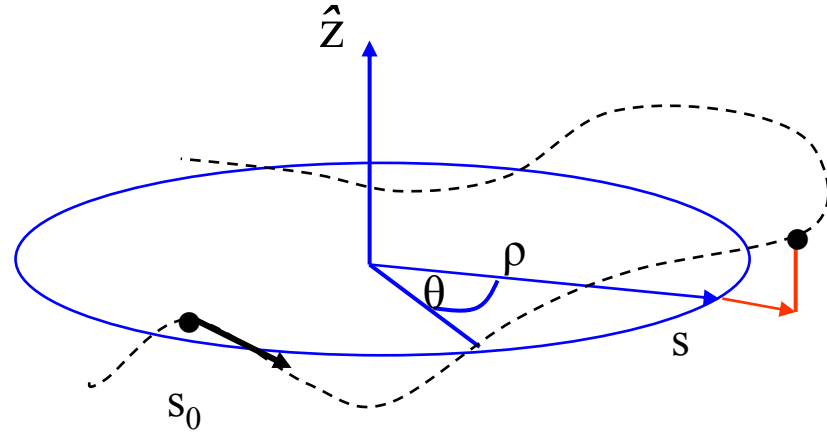
... remember  $W = CS' - SC' = 1$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_0 = M^{-1} \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_s$$

$$M^{-1} = \begin{pmatrix} S' & -S \\ -C' & C \end{pmatrix}$$



$$\begin{aligned} x_0 &= S'x - Sx' \\ x_0' &= -C'x + Cx' \end{aligned}$$



inserting into  $\varepsilon$

$$\varepsilon = \beta x'^2 + 2\alpha x x' + \gamma x^2$$

$$\varepsilon = \beta_0 (Cx' - C'x)^2 + 2\alpha_0 (S'x - Sx')(Cx' - C'x) + \gamma_0 (S'x - Sx')^2$$

sort via  $x, x'$  and compare the coefficients to get ....

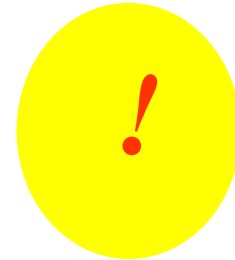
$$\beta(s) = C^2 \beta_0 - 2SC\alpha_0 + S^2 \gamma_0$$

$$\alpha(s) = -CC' \beta_0 + (SC' + S'C)\alpha_0 - SS' \gamma_0$$

$$\gamma(s) = C'^2 \beta_0 - 2S'C'\alpha_0 + S'^2 \gamma_0$$

*in matrix notation:*

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + CS' & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix} \cdot \begin{pmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{pmatrix}$$



- 1.) *this expression is important*
- 2.) *given the twiss parameters  $\alpha$ ,  $\beta$ ,  $\gamma$  at any point in the lattice we can transform them and calculate their values at any other point in the ring.*
- 3.) *the transfer matrix is given by the focusing properties of the lattice elements, the elements of  $M$  are just those that we used to calculate single particle trajectories.*
- 4.) *go back to point 1.)*

The new parameters  $\alpha$ ,  $\beta$ ,  $\gamma$  can be transformed through the lattice via the matrix elements defined above.

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + S'C & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix} * \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

*Question: „ What does that mean ????? “*

... and here starts the **lattice design !!!**

## Most simple example: drift space

$$M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}$$

### particle coordinates

$$\begin{pmatrix} x \\ x' \end{pmatrix}_l = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix} * \begin{pmatrix} x \\ x' \end{pmatrix}_0 \quad \rightarrow \quad \boxed{\begin{aligned} x(l) &= x_0 + l * x_0' \\ x'(l) &= x_0' \end{aligned}}$$

### transformation of twiss parameters:

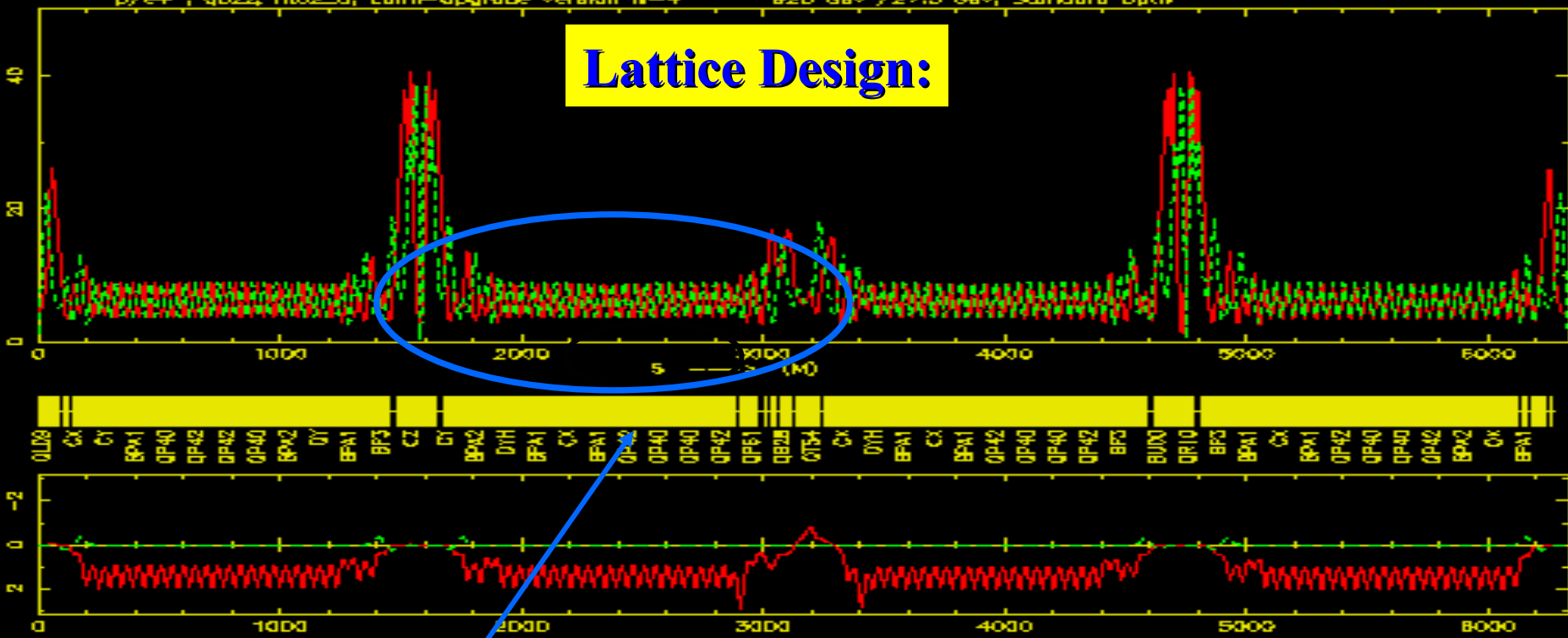
$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_l = \begin{pmatrix} 1 & -2l & l^2 \\ 0 & 1 & -l \\ 0 & 0 & 1 \end{pmatrix} * \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0 \quad \boxed{\beta(s) = \beta_0 - 2l * \alpha_0 + l^2 * \gamma_0}$$

### Stability ...?

$$\text{trace}(M) = 1 + 1 = 2$$

**→ A periodic solution doesn't exist in a lattice built exclusively out of drift spaces.**

## Lattice Design:



**Arc:** regular (periodic) magnet structure:

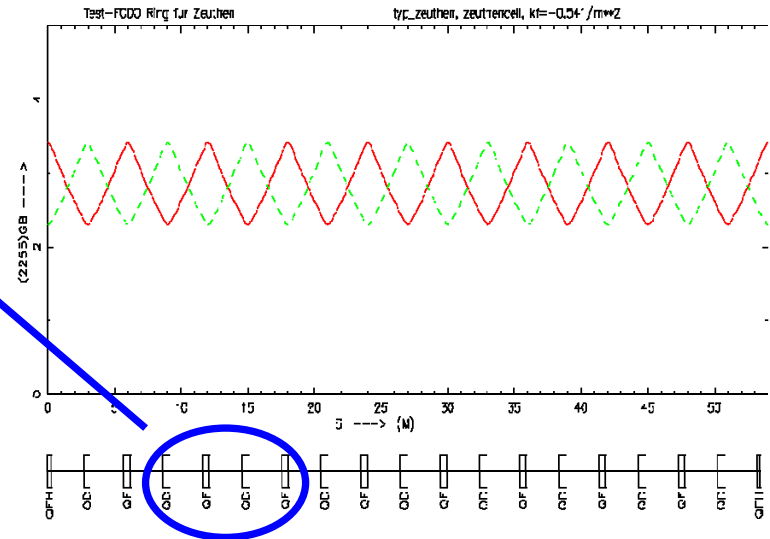
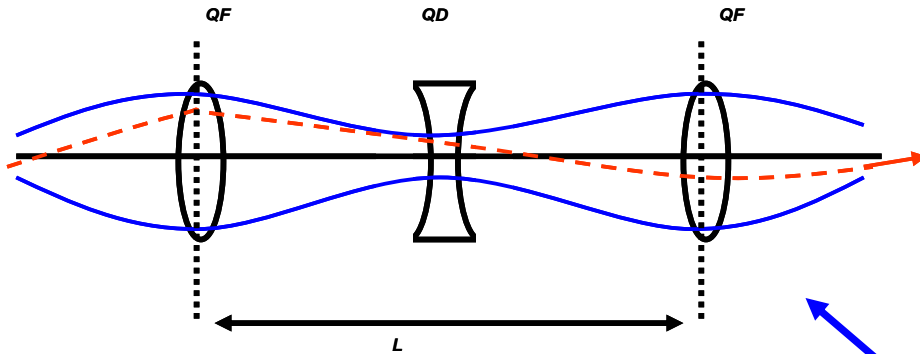
bending magnets  $\rightarrow$  define the energy of the ring  
 main focusing & tune control, chromaticity correction,  
 multipoles for higher order corrections

**Straight sections:** drift spaces for injection, dispersion suppressors,  
 low beta insertions, RF cavities, etc....

... and the high energy experiments if they cannot be avoided

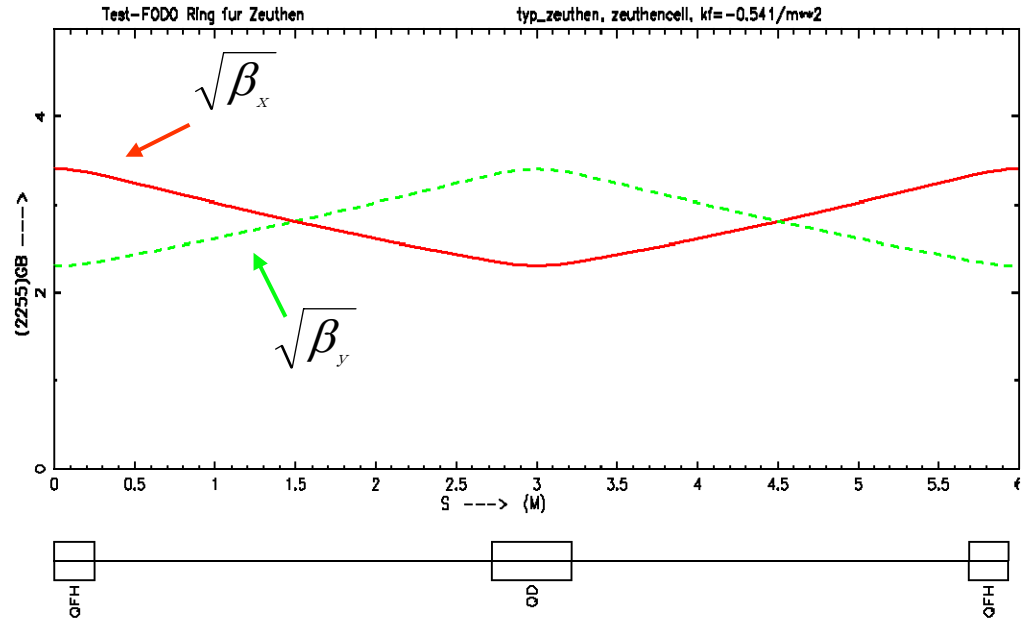
# The FoDo-Lattice

A magnet structure consisting of focusing and defocusing quadrupole lenses in alternating order with **nothing** in between.  
(**Nothing** = elements that can be neglected on first sight: drift, bending magnets, RF structures ... **and especially experiments...**)



Starting point for the calculation: in the middle of a focusing quadrupole  
Phase advance per cell  $\mu = 45^\circ$ ,  
→ calculate the twiss parameters for a periodic solution

# Periodic solution of a FoDo Cell



**Output of the optics program:**

Nr	Type	Length <i>m</i>	Strength <i>1/m2</i>	$\beta_x$ <i>m</i>	$\alpha_x$	$\varphi_x$ <i>1/2π</i>	$\beta_z$ <i>m</i>	$\alpha_z$	$\varphi_z$ <i>1/2π</i>
0	IP	0,000	0,000	11,611	0,000	0,000	5,295	0,000	0,000
1	QFH	0,250	-0,541	11,228	1,514	0,004	5,488	-0,781	0,007
2	QD	3,251	0,541	5,488	-0,781	0,070	11,228	1,514	0,066
3	QFH	6,002	-0,541	11,611	0,000	0,125	5,295	0,000	0,125
4	IP	6,002	0,000	11,611	0,000	0,125	5,295	0,000	0,125

$QX= 0,125 \quad QZ= 0,125$

$0.125 * 2\pi = 45^\circ$

Can we understand, what the optics code is doing?

matrices

$$M_{QF} = \begin{pmatrix} \cos(\sqrt{K} * l_q) & \frac{1}{\sqrt{K}} \sin(\sqrt{K} * l_q) \\ -\sqrt{K} \sin(\sqrt{K} * l_q) & \cos(\sqrt{K} * l_q) \end{pmatrix}, \quad M_{Drift} = \begin{pmatrix} 1 & l \\ 0 & 1_d \end{pmatrix}$$

strength and length of the FoDo elements

$$K = +/- 0.54102 \text{ m}^{-2}$$

$$l_q = 0.5 \text{ m}$$

$$l_d = 2.5 \text{ m}$$

The matrix for the **complete cell** is obtained by multiplication of the element matrices

$$M_{FoDo} = M_{qfh} * M_{ld} * M_{qd} * M_{ld} * M_{qfh}$$

Putting the numbers in and **multiplying out** ...

$$M_{FoDo} = \begin{pmatrix} 0.707 & 8.206 \\ -0.061 & 0.707 \end{pmatrix}$$



# The transfer matrix for 1 period gives us all the information that we need !

1.) is the motion stable?

$$\text{trace}(M_{FoDo}) = 1.415 \rightarrow \underline{\underline{< 2}}$$

2.) Phase advance per cell

$$M(s) = \begin{pmatrix} \cos \mu + \alpha \sin \mu & \beta \sin \mu \\ -\gamma \sin \mu & \cos(\mu) - \alpha \sin \mu \end{pmatrix} \rightarrow \begin{aligned} \cos(\mu) &= \frac{1}{2} * \text{trace}(M) = 0.707 \\ \mu &= \text{arc cos}\left(\frac{1}{2} * \text{trace}(M)\right) = 45^\circ \end{aligned}$$

3.) hor  $\beta$ -function

$$\beta = \frac{M(1,2)}{\sin(\mu)} = 11.611 \text{ m}$$

4.) hor  $\alpha$ -function

$$\alpha = \frac{M(1,1) - \cos(\mu)}{\sin(\mu)} = 0$$

Can we do it a little bit easier ?

We can: ... the „*thin lens approximation*“

Matrix of a focusing quadrupole magnet:

$$M_{QF} = \begin{pmatrix} \cos(\sqrt{K} * l) & \frac{1}{\sqrt{K}} \sin(\sqrt{K} * l) \\ -\sqrt{K} \sin(\sqrt{K} * l) & \cos(\sqrt{K} * l) \end{pmatrix}$$

If the **focal length  $f$**  is much **larger than the length of the quadrupole magnet,**

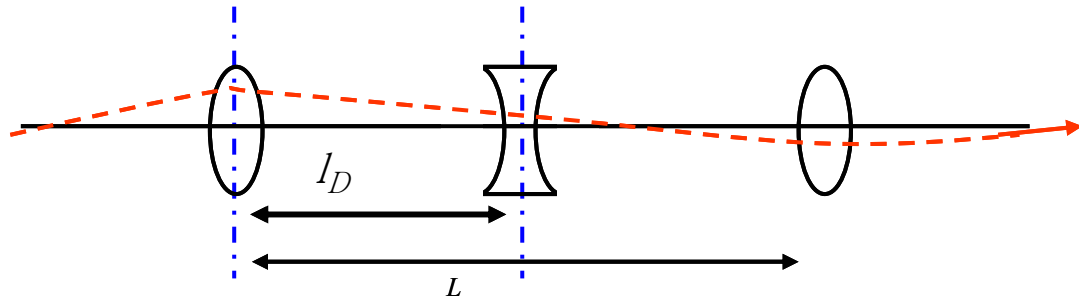
$$f = \frac{1}{kl_q} \gg l_q$$

the transfer matrix can be approximated using

$$kl_q = \text{const}, \quad l_q \rightarrow 0$$

$$M = \begin{pmatrix} 1 & 0 \\ 1/f & 1 \end{pmatrix}$$

## *FoDo in thin lens approximation*



$$l_D = L/2,$$

$$\tilde{f} = 2f$$

***Calculate the matrix for a half cell, starting in the middle of a foc. quadrupole:***

$$M_{halfCell} = M_{QD/2} * M_{ID} * M_{QF/2}$$

$$M_{halfCell} = \begin{pmatrix} 1 & 0 \\ 1/\tilde{f} & 1 \end{pmatrix} * \begin{pmatrix} 1 & l_D \\ 0 & 1 \end{pmatrix} * \begin{pmatrix} 1 & 0 \\ -1/\tilde{f} & 1 \end{pmatrix}$$

*note:  $\tilde{f}$  denotes the focusing strength of half a quadrupole, so  $\tilde{f} = 2f$*

$$M_{halfCell} = \begin{pmatrix} 1 - l_D/\tilde{f} & l_D \\ -l_D/\tilde{f}^2 & 1 + l_D/\tilde{f} \end{pmatrix}$$

*for the second half cell set  $f \rightarrow -f$*

## *FoDo in thin lens approximation*

**Matrix for the complete FoDo cell:**

$$M = \begin{pmatrix} 1 + \frac{l_D}{\tilde{f}} & l_D \\ -\frac{l_D}{\tilde{f}^2} & 1 - \frac{l_D}{\tilde{f}} \end{pmatrix} * \begin{pmatrix} 1 - \frac{l_D}{\tilde{f}} & l_D \\ -\frac{l_D}{\tilde{f}^2} & 1 + \frac{l_D}{\tilde{f}} \end{pmatrix}$$

$$M = \begin{pmatrix} 1 - \frac{2l_D^2}{\tilde{f}^2} & 2l_D \left(1 + \frac{l_D}{\tilde{f}}\right) \\ 2\left(\frac{l_D^2}{\tilde{f}^3} - \frac{l_D}{\tilde{f}^2}\right) & 1 - 2\frac{l_D^2}{\tilde{f}^2} \end{pmatrix}$$

Now we know, that the **phase advance is related to the transfer matrix** by

$$\cos \mu = \frac{1}{2} \text{trace} (M) = \frac{1}{2} * \left(2 - \frac{4l_D^2}{\tilde{f}^2}\right) = 1 - \frac{2l_D^2}{\tilde{f}^2}$$

**After some beer** and with a little bit of trigonometric gymnastics

$$\cos(x) = \cos^2\left(\frac{x}{2}\right) - \sin^2\left(\frac{x}{2}\right) = 1 - 2\sin^2\left(\frac{x}{2}\right)$$

*we can calculate the phase advance as a function of the FoDo parameter ...*

$$\cos(\mu) = 1 - 2 \sin^2(\mu/2) = 1 - \frac{2l_D^2}{\tilde{f}^2}$$

$$\sin(\mu/2) = l_D / \tilde{f} = \frac{L_{Cell}}{2\tilde{f}}$$

$$\sin(\mu/2) = \frac{L_{Cell}}{4f}$$

**Example:**

**45-degree Cell**

$$L_{Cell} = l_{QF} + l_D + l_{QD} + l_D = 0.5m + 2.5m + 0.5m + 2.5m = 6m$$

$$1/f = k * l_Q = 0.5m * 0.541 m^{-2} = 0.27 m^{-1}$$

$$\sin(\mu/2) \approx \frac{L_{Cell}}{4f} = 0.405$$

$$\rightarrow \mu \approx 47.8^\circ$$

$$\rightarrow \beta \approx 11.4m$$

**Remember:**

**Exact calculation yields:**

$$\mu = 45^\circ$$

$$\beta = 11.6m$$

## Stability in a FoDo structure



SPS Lattice

$$M_{\text{FoDo}} = \begin{pmatrix} 1 - \frac{2l_D^2}{\tilde{f}^2} & 2l_D \left(1 + \frac{l_D}{\tilde{f}}\right) \\ 2\left(\frac{l_D^2}{\tilde{f}^3} - \frac{l_D}{\tilde{f}^2}\right) & 1 - 2\frac{l_D^2}{\tilde{f}^2} \end{pmatrix}$$

*Stability requires:*

$$|\text{Trace}(M)| < 2$$

$$|\text{Trace}(M)| = \left| 2 - \frac{4l_d^2}{\tilde{f}^2} \right| < 2$$

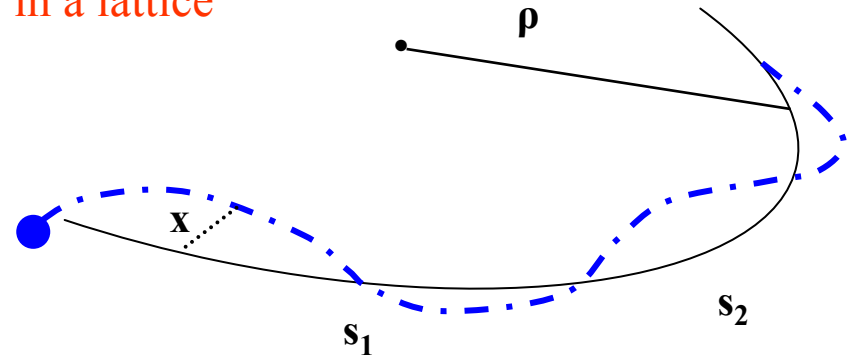
$$\rightarrow f > \frac{L_{\text{cell}}}{4}$$

For stability the focal length has to be larger than a quarter of the cell length !!

# Transformation Matrix in Terms of the Twiss parameters

Transformation of the coordinate vector  $(x, x')$  in a lattice

$$\begin{pmatrix} \mathbf{x}(s) \\ \mathbf{x}'(s) \end{pmatrix} = \mathbf{M}_{s_1, s_2} \begin{pmatrix} \mathbf{x}_0 \\ \mathbf{x}'_0 \end{pmatrix}$$



General solution of the equation of motion

$$\mathbf{x}(s) = \sqrt{\varepsilon * \beta(s)} * \cos(\psi(s) + \varphi)$$

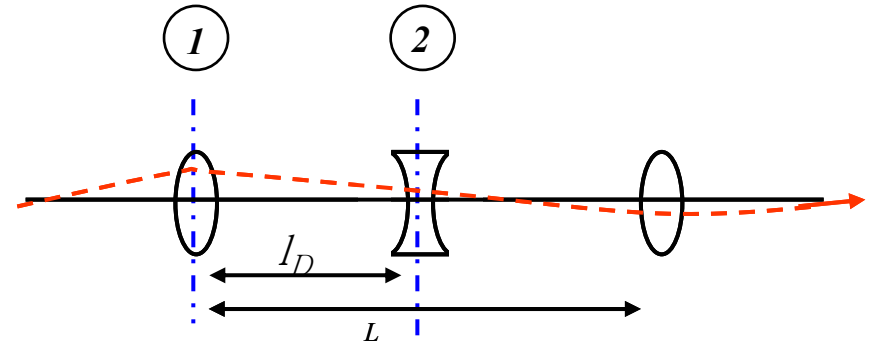
$$\mathbf{x}'(s) = \sqrt{\varepsilon / \beta(s)} * \{ \alpha(s) \cos(\psi(s) + \varphi) + \sin(\psi(s) + \varphi) \}$$

Transformation of the coordinate vector  $(x, x')$  expressed as a function of the twiss parameters

$$\mathbf{M}_{1 \rightarrow 2} = \begin{pmatrix} \sqrt{\frac{\beta_2}{\beta_1}} (\cos \psi_{12} + \alpha_1 \sin \psi_{12}) & \sqrt{\beta_1 \beta_2} \sin \psi_{12} \\ \frac{(\alpha_1 - \alpha_2) \cos \psi_{12} - (1 + \alpha_1 \alpha_2) \sin \psi_{12}}{\sqrt{\beta_1 \beta_2}} & \sqrt{\frac{\beta_1}{\beta_2}} (\cos \psi_{12} - \alpha_2 \sin \psi_{12}) \end{pmatrix}$$

Transfer matrix for half a FoDo cell:

$$M_{\text{halfcell}} = \begin{pmatrix} 1 - l_D / \tilde{f} & l_D \\ -l_D / \tilde{f}^2 & 1 + l_D / \tilde{f} \end{pmatrix}$$



Compare to the twiss parameter form of M

$$M_{1 \rightarrow 2} = \begin{pmatrix} \sqrt{\frac{\beta_2}{\beta_1}} (\cos \psi_{12} + \alpha_1 \sin \psi_{12}) & \sqrt{\beta_1 \beta_2} \sin \psi_{12} \\ \frac{(\alpha_1 - \alpha_2) \cos \psi_{12} - (1 + \alpha_1 \alpha_2) \sin \psi_{12}}{\sqrt{\beta_1 \beta_2}} & \sqrt{\frac{\beta_1}{\beta_2}} (\cos \psi_{12} - \alpha_2 \sin \psi_{12}) \end{pmatrix}$$

In the **middle of a foc (defoc) quadrupole** of the FoDo we always have  $\alpha = 0$ , and the half cell will lead us from  $\beta_{\max}$  to  $\beta_{\min}$

$$M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} = \begin{pmatrix} \sqrt{\frac{\hat{\beta}}{\check{\beta}}} \cos \frac{\mu}{2} & \sqrt{\hat{\beta} \check{\beta}} \sin \frac{\mu}{2} \\ \frac{-1}{\sqrt{\hat{\beta} \check{\beta}}} \sin \frac{\mu}{2} & \sqrt{\frac{\hat{\beta}}{\check{\beta}}} \cos \frac{\mu}{2} \end{pmatrix}$$



Solving for  $\beta_{max}$  and  $\beta_{min}$  and remembering that ....  $\sin \frac{\mu}{2} = \frac{l_D}{\tilde{f}} = \frac{L}{4f}$

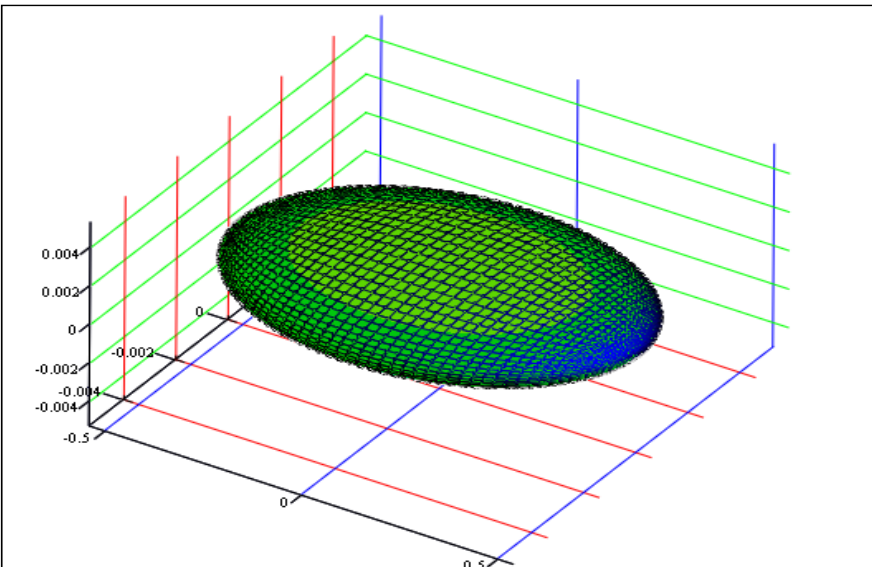
$$\frac{S'}{C} = \frac{\hat{\beta}}{\check{\beta}} = \frac{1+l_D/\tilde{f}}{1-l_D/\tilde{f}} = \frac{1+\sin \frac{\mu}{2}}{1-\sin \frac{\mu}{2}}$$

$$\frac{S}{C'} = \hat{\beta} \check{\beta} = \tilde{f}^2 = \frac{l_D^2}{\sin^2 \frac{\mu}{2}}$$



$$\hat{\beta} = \frac{(1 + \sin \frac{\mu}{2})L}{\sin \mu} \quad !$$

$$\check{\beta} = \frac{(1 - \sin \frac{\mu}{2})L}{\sin \mu} \quad !$$



**The maximum and minimum values of the  $\beta$ -function are solely determined by the phase advance and the length of the cell.**

**Longer cells lead to larger  $\beta$**

*typical shape of a proton bunch in the HERA FoDo Cell*

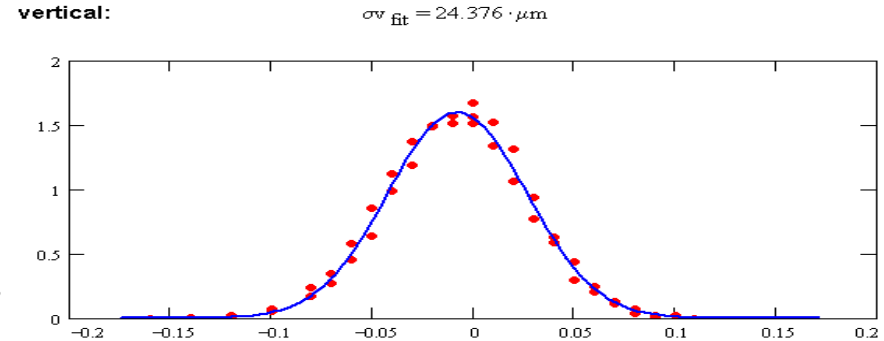
## Beam dimension:

## Optimisation of the FoDo Phase advance:

In both planes a **gaussian particle distribution** is assumed, given by the beam emittance  $\varepsilon$  and the  $\beta$ -function

$$\sigma = \sqrt{\varepsilon\beta}$$

*HERA beam size*

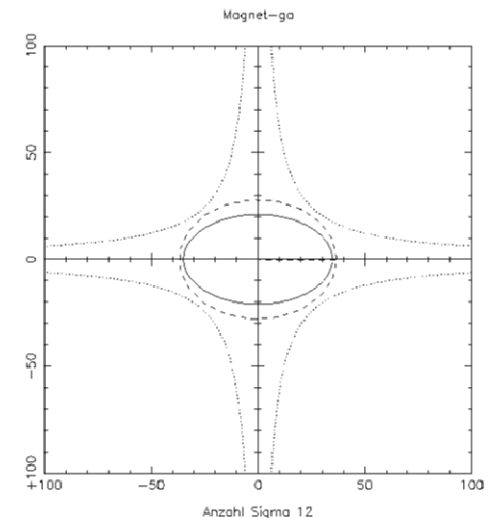


In general **proton beams are „round“** in the sense that

$$\varepsilon_x \approx \varepsilon_y$$

So for highest aperture we have to **minimise the  $\beta$ -function in both planes:**

$$r^2 = \varepsilon_x \beta_x + \varepsilon_y \beta_y$$



*typical beam envelope, vacuum chamber and pole shape in a foc. Quadrupole lens in HERA*

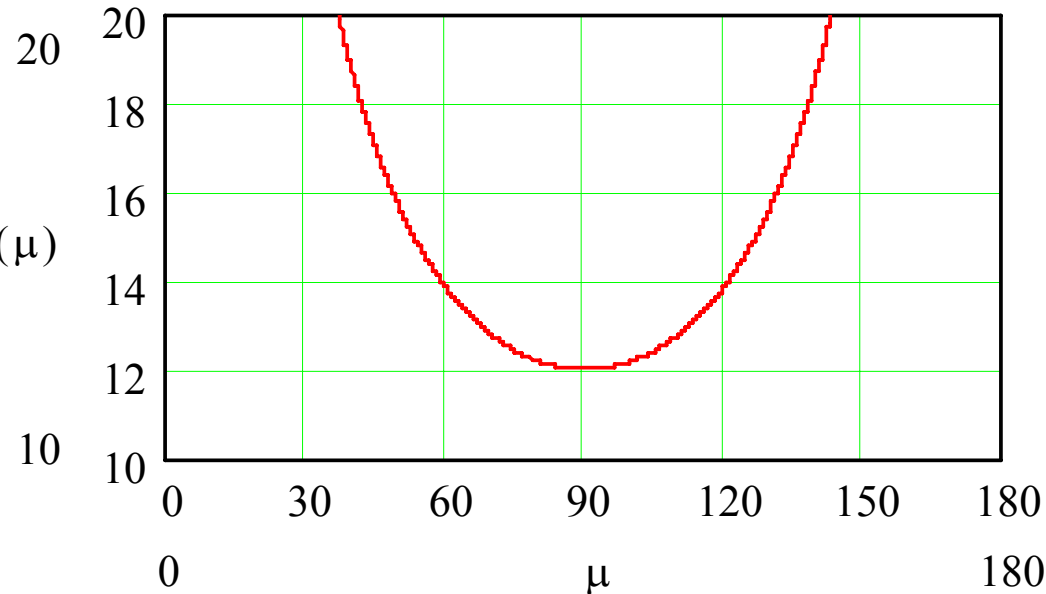
# Optimising the FoDo phase advance

search for the phase advance  $\mu$  that results in a minimum of the sum of the beta's

$$r^2 = \varepsilon_x \beta_x + \varepsilon_y \beta_y$$

$$\hat{\beta} + \check{\beta} = \frac{(1 + \sin \frac{\mu}{2}) * L}{\sin \mu} + \frac{(1 - \sin \frac{\mu}{2}) * L}{\sin \mu}$$

$$\hat{\beta} + \check{\beta} = \frac{2L}{\sin \mu} \quad \frac{d}{d\mu} \left( \frac{2L}{\sin \mu} \right) = 0$$



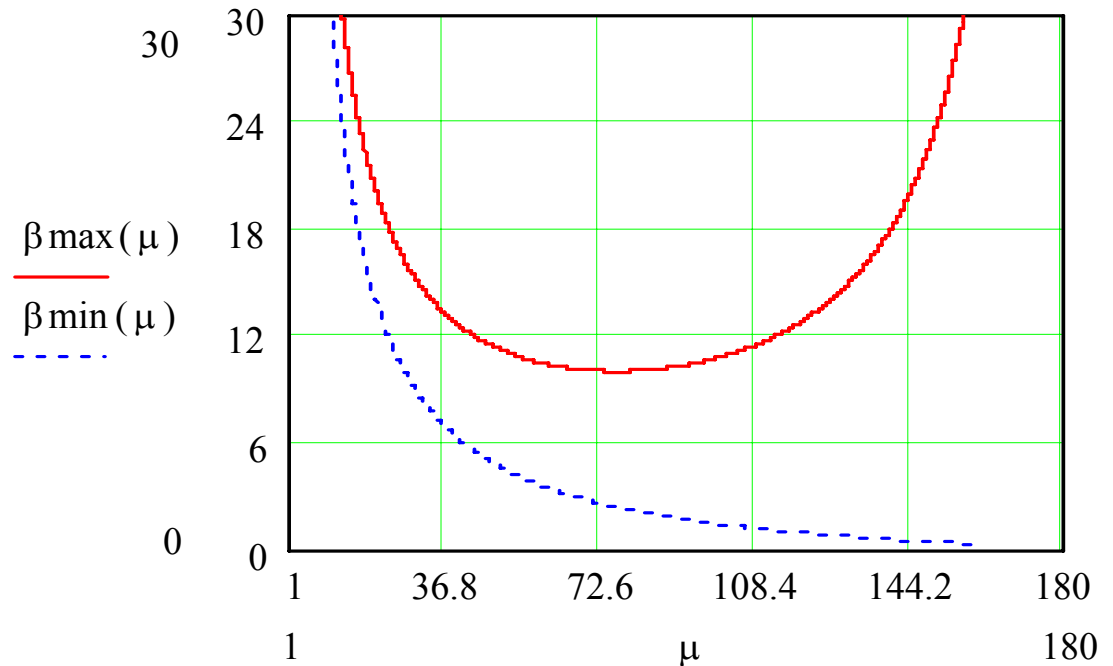
$$\frac{L}{\sin^2 \mu} * \cos \mu = 0 \rightarrow \mu = 90^\circ$$

## Electrons are different

electron beams are usually flat,  $\varepsilon_y \approx 2 - 10 \% \varepsilon_x$   
 $\rightarrow$  optimise only  $\beta_{hor}$

$$\frac{d}{d\mu}(\hat{\beta}) = \frac{d}{d\mu} \frac{L(1 + \sin \frac{\mu}{2})}{\sin \mu} = 0 \rightarrow \mu \approx 76^\circ$$

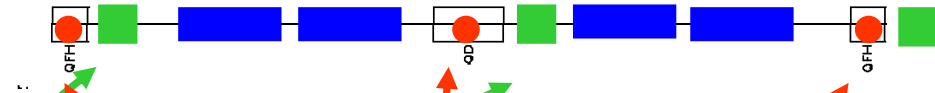
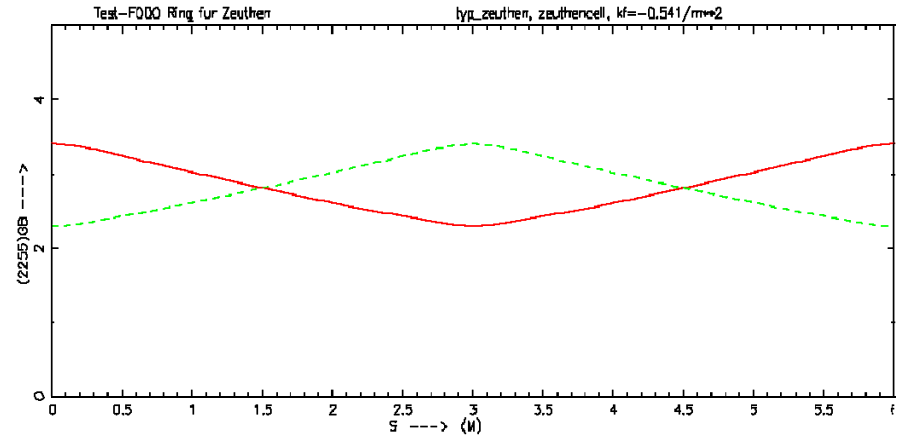
**red curve:**  $\beta_{max}$   
**blue curve:**  $\beta_{min}$   
as a function of the phase advance  $\mu$



# Orbit distortions in a periodic lattice

field error of a dipole/distorted quadrupole

$$\rightarrow \delta(\text{mrad}) = \frac{ds}{\rho} = \frac{\int B ds}{p/e}$$



the particle will follow a new closed trajectory, the distorted orbit:

$$x(s) = \frac{\sqrt{\beta(s)}}{2 \sin(\pi Q)} * \oint \frac{\sqrt{\beta(\tilde{s})}}{\rho(\tilde{s})} \cos(|\psi(\tilde{s}) - \psi(s)| - \pi Q) d\tilde{s}$$

\* the orbit amplitude will be large if the  $\beta$  function at the location of the kick is large  $\beta(\tilde{s})$  indicates the sensitivity of the beam  $\rightarrow$  here orbit correctors should be placed in the lattice

\* the orbit amplitude will be large at places where in the lattice  $\beta(s)$  is large  $\rightarrow$  here beam position monitors should be installed

## *Orbit Correction and Beam Instrumentation in a storage ring*



*Elsa ring, Bonn*

# Resumé:

1.) Dipole strength:

$$\int B ds = N * B_0 * l_{eff} = 2\pi \frac{p}{q}$$

$l_{eff}$  effective magnet length,  $N$  number of magnets

2.) Stability condition:

$$Trace(M) < 2$$

for periodic structures within the lattice / at least for the transfer matrix of the complete circular machine

3.) Transfer matrix for periodic cell

$$M(s) = \begin{pmatrix} \cos \mu + \alpha(s) \sin \mu & \beta(s) \sin \mu \\ -\gamma(s) \sin \mu & \cos(\mu) - \alpha(s) \sin \mu \end{pmatrix}$$

$\alpha, \beta, \gamma$  depend on the position  $s$  in the ring,  $\mu$  (phase advance) is independent of  $s$

4.) Thin lens approximation:

$$M_{QF} = \begin{pmatrix} 1 & 0 \\ \frac{1}{f_Q} & 1 \end{pmatrix} \quad f_Q = \frac{1}{k_Q l_Q}$$

focal length of the quadrupole magnet  $f_Q = 1/(k_Q l_Q) \gg l_Q$

5.) Tune (rough estimate):

$$\mu = \int_s^{s+L} \frac{dt}{\beta(t)}$$

*Tune = phase advance  
in units of  $2\pi$*

$$Q := N * \frac{\mu}{2\pi} = \frac{1}{2\pi} * \oint \frac{ds}{\beta(s)} \approx \frac{1}{2\pi} * \frac{2\pi \bar{R}}{\bar{\beta}} = \bar{R} / \bar{\beta}$$

$\bar{R}$ ,  $\bar{\beta}$  average radius  
and  $\beta$ -function

$$Q \approx \frac{\bar{R}}{\bar{\beta}}$$

6.) Phase advance per FoDo cell

*(thin lens approx)*

$$\sin \frac{\mu}{2} = \frac{L_{Cell}}{4f_Q}$$

**$L_{Cell}$  length of the complete FoDo cell,  $f_Q$  focal length of the quadrupole,  $\mu$  phase advance per cell**

7.) Stability in a FoDo cell

*(thin lens approx)*

$$f_Q > \frac{L_{Cell}}{4}$$

8.) Beta functions in a FoDo cell

*(thin lens approx)*

$$\hat{\beta} = \frac{(1 + \sin \frac{\mu}{2})L_{Cell}}{\sin \mu} \quad \check{\beta} = \frac{(1 - \sin \frac{\mu}{2})L_{Cell}}{\sin \mu}$$

**$L_{Cell}$  length of the complete FoDo cell,  $\mu$  phase advance per cell**



## Conclusion:

- \* *„the arc“ of a storage ring is usually built out of a periodic sequence of single magnet elements eg. FoDo sections*
- \* *a first guess of the main parameters of the beam in the arc is obtained by the settings of the quadrupole lenses in this section*
- \* *we can get an estimate of the beam parameters using a selection of „rules of thumb“*

*Usually the real beam properties will not differ too much from these estimates and we will have a nice storage ring and a beautiful beam and everybody is happy around.*

*And then someone comes and spoils it all by saying something stupid like installing a tiny little piece of detector in our machine ...*

# INSERTIONS



ZEUS