

# Coils & wires to Measure Magnets

## Cern Accelerator School on Magnets

Brugge

16 – 25 June 2009

*L. Walckiers - Cern*

# Outline

- **Measure  $B_y(\mathbf{x})$  with coils**
  - Flip coils for strength**
  - Coils displaced along horizontal plane**
  - Static coils in pulsed fields**
    - example : system to measure CNAO dipoles**
- **B Train generation in PS reference magnet**
- **Single Stretched Wire [SSW]**
  - Dipole strength & field direction**
  - Quadrupole axis**
  - Quadrupole strength : sag & wire magnetisation**
  - Vibrating wire for axis search**

# Flip coils to measure magnet strength

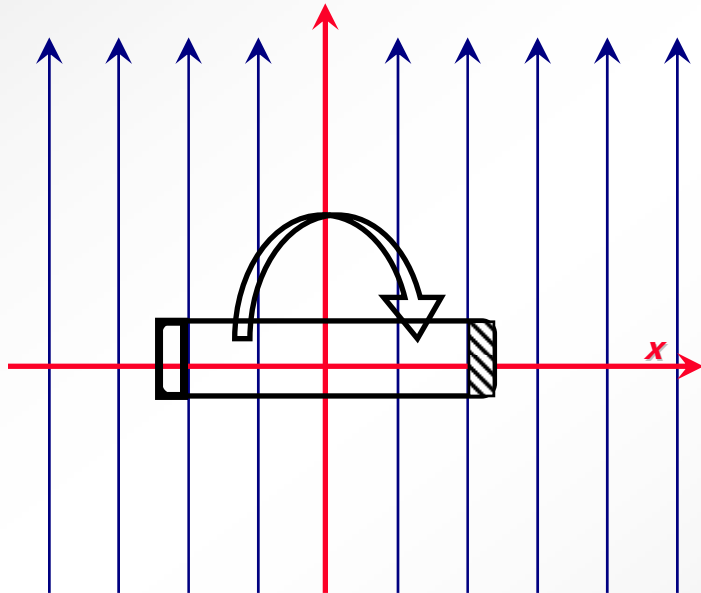
➤ Advantage : measure the whole particle trajectory in one signal.  
Particles (most often) see integrated fields

➤ Most important

Dipole :  $\int B dl(I)$  or Transfer Function =  $\int B dl / I$  [T·m/kA]

Quadr :  $\int G dl(I)$  or Transfer Function =  $\int G dl / I$  [T/kA]

$$\Psi(\pi) - \Psi(0) = 2 \cdot \int_0^L B_y(x) \cdot dl \quad \text{Integrators measure Flux differences}$$



Coil must be longer than the magnet

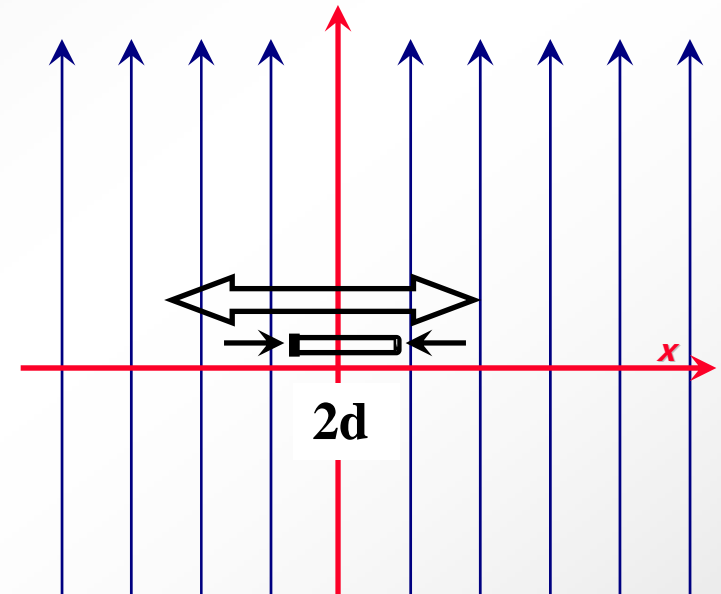
- Rule of thumb : should extend outside by 2.5 \* aperture
- perform  $B(z)$  scanning with Hall plate
- full 3D calculation

# Measure Field Quality by lateral displacement

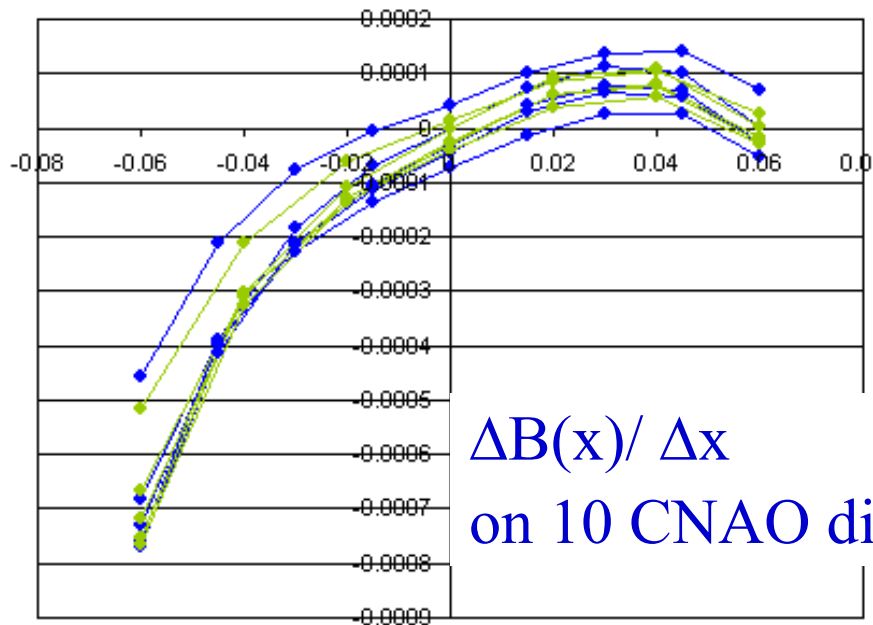
Coil with

- 1 turn (or very small winding section)
- small width  $2d \ll \Delta B(x) / \Delta x$
- (2D case i.e. per unit length)

$$\frac{\Delta B_y(x)}{\Delta x} = \frac{\Psi(x + \delta) - \Psi(x)}{2d}$$



Limitation for  
this simple coil :  
no sensitivity



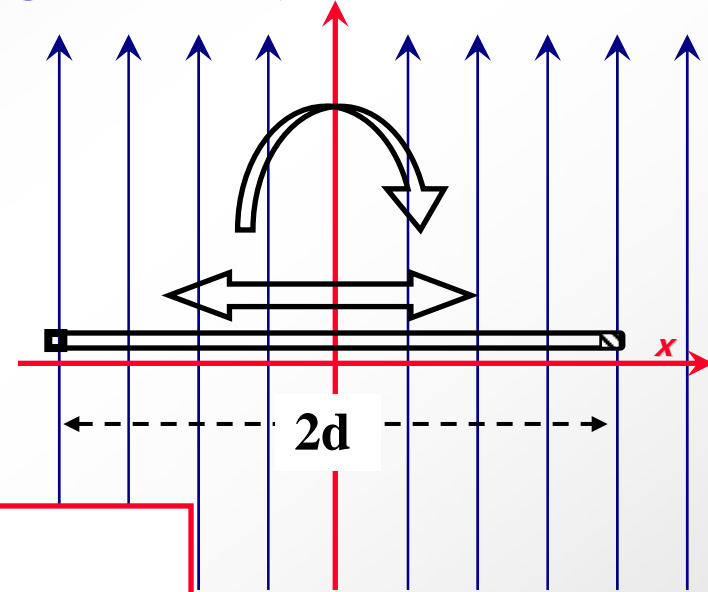
# The coil picks-up a large surface

Coil with 1 turn (or very small winding section)

$$B_y(x) = B_1 + B_2 \cdot x + B_3 \cdot x^2 + \dots$$

Coil going from  $[x - d]$  to  $[x + d]$

$$\Psi(x) = B_1 \cdot 2d + B_2 \cdot 2dx + B_3 \cdot (6x^2d + 2d^3)$$



The sextupole enters for flip of half turn

$$\Psi(\pi, x = 0) - \Psi(0, x = 0) = 2 \cdot (2d \cdot B_1 + 2d^3 \cdot B_3)$$

Displacement: harmonics enter with different & varying sensitivity

$$\Psi(x + \delta) - \Psi(x) = 2d\delta \cdot B_2 + 6d \cdot (2x\delta + \delta^2) \cdot B_3 + \dots$$

**What is measured is not  $B_1$  at coil center**

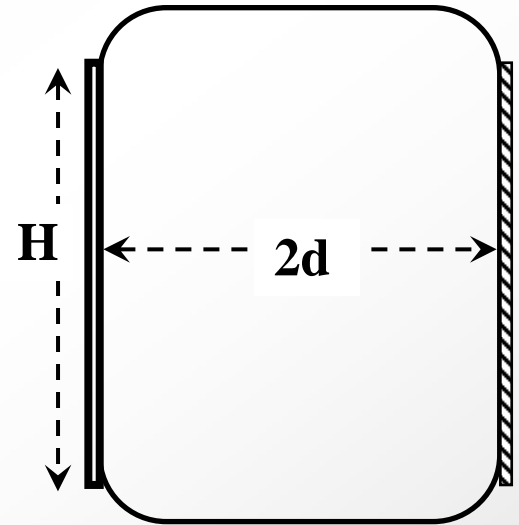
## Square Coil with more turns

One layer coil with width of coil = height of winding

$$2d = H$$

$$B_y(x) = B_1 + B_2 \cdot x + B_3 \cdot x^2 + \dots$$

$$\Psi(x) = B_1 \cdot 2d \cdot N_{turns} + 0 \cdot B_2 + 0 \cdot B_3 + \dots$$



Unsesitive to perturbations from  
both quadrupole and sextupole harmonics  
Still sensitive to the average  $B_1$  on the coil.

# Why not use the Harmonic method ?

- Dipole magnets are bent : how a bent rotating coil ?
- Dipole for small accelerators have wide apertures compared to gap height
- Harmonic method does not measure (easily) pulsed fields (i.e. when  $\Delta B/\Delta t$  cannot be neglected over one coil revolution period)
  - The case for most "accelerator magnets" vs. storage ring magnets

# Static Coils in Pulsed Fields

$$\Psi(t) = B_1(t) \cdot 2d \cdot N_{turns}$$

$B_1(t)$  depends on

➤  $K_{tf} \cdot I(t)$

➤ saturation effect

measured continuously with (recent) integrators

cf. oversampling in P. Arpaia lecture

➤ eddy current effects

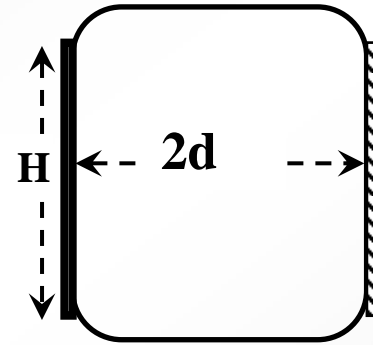
measure at different  $dI/dt$

➤ remanent field (3 ways to compensate)

have bipolar power supply

demagnetise first your magnet

measure at  $I=0$  with Hall plate or flipped coil





# CNAO dipoles : curved and pulsed

Field Rise time  $\approx 2$  s

$\Rightarrow$  no coil movement

Curved 11-coil fluxmeter

& reference coil for cross calibration

$B_{\max} = 1.5$  T

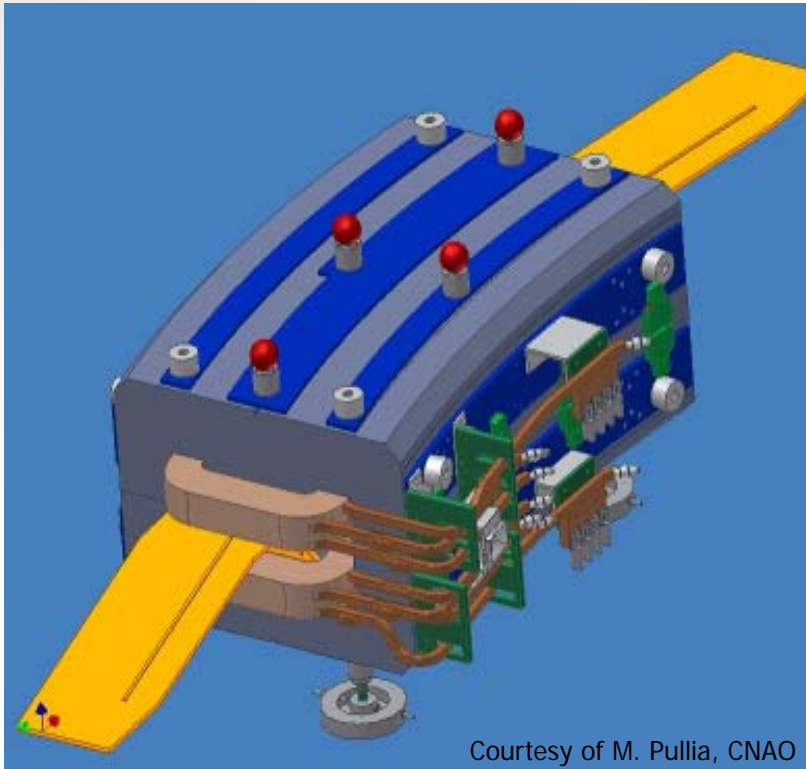
Gap height = 72 mm

Useful aperture  $\approx 130$  mm

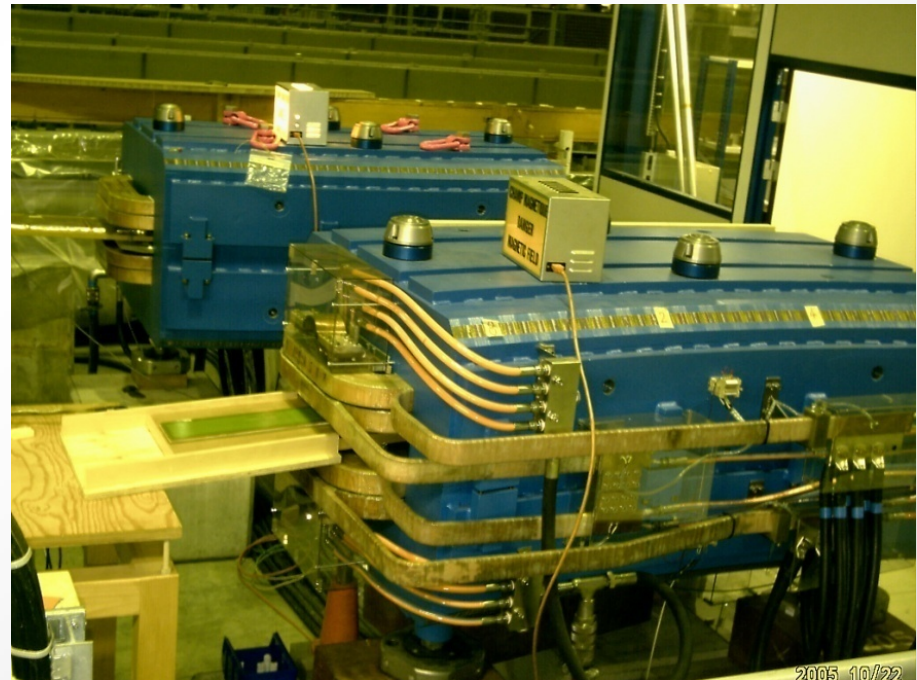
Bending radius = 4.231 m

Bending angle =  $22.5^\circ$

Magnetic length  $\sim 1.67$  m

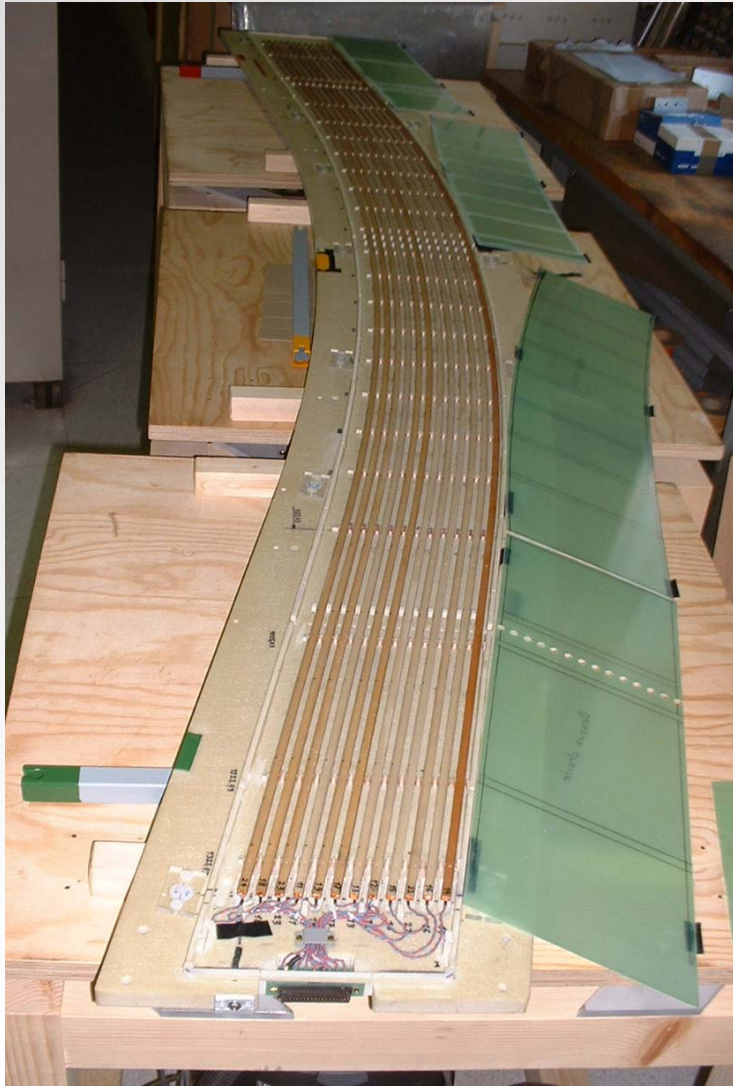


Courtesy of M. Pullia, CNAO



2005 10/22

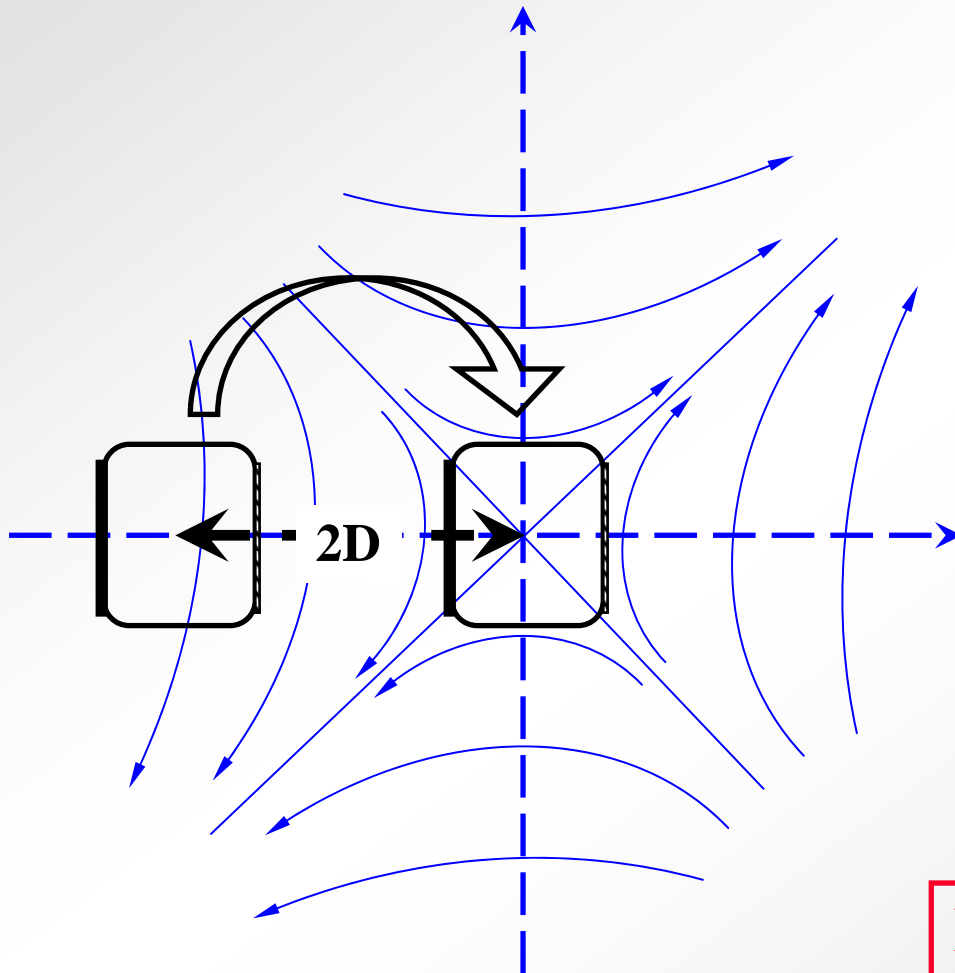
# CNAO : 11 coil Fluxmeter



Reference coil to cross calibrate the 11 measuring coils (@  $10^{-4}$ )

# Measure quadrupole strength & field quality

For combined function magnets



Each coil insensitive to  
local  $B_2$  &  $B_3$

**! but sensitive to  $B_4, B_5, \dots!$**

Coils in opposition  $\Rightarrow$   
insensitive to dipole

Flip by half turn gives

$$B_1(x+D) - B_1(x-D) \approx G(x)$$

Can also be done by  $\frac{1}{4}$  turn

Can be applied with  
pulsed magnets & static coils

**Harmonic coils more accurate**

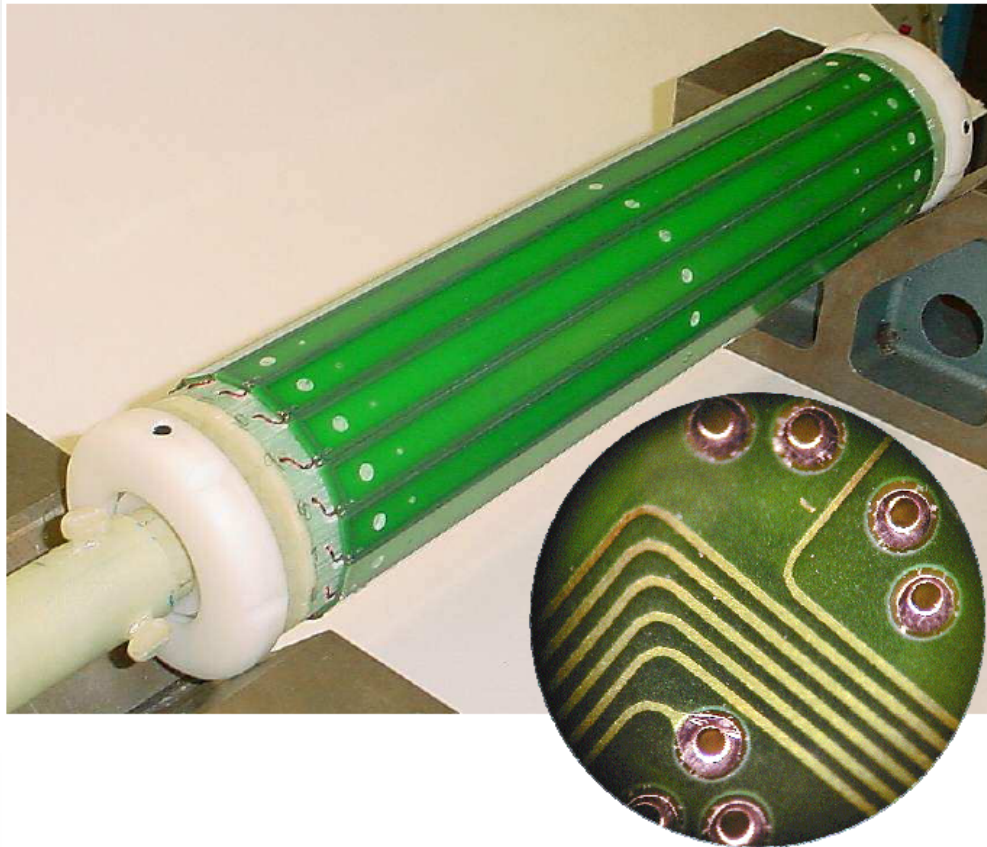
# Dedicated static coils for pulsed magnets

Morgan coils (60's) :

coils on cylinder sensitive to harmonic  $n$

[and  $n \cdot (2m+1)$ ]

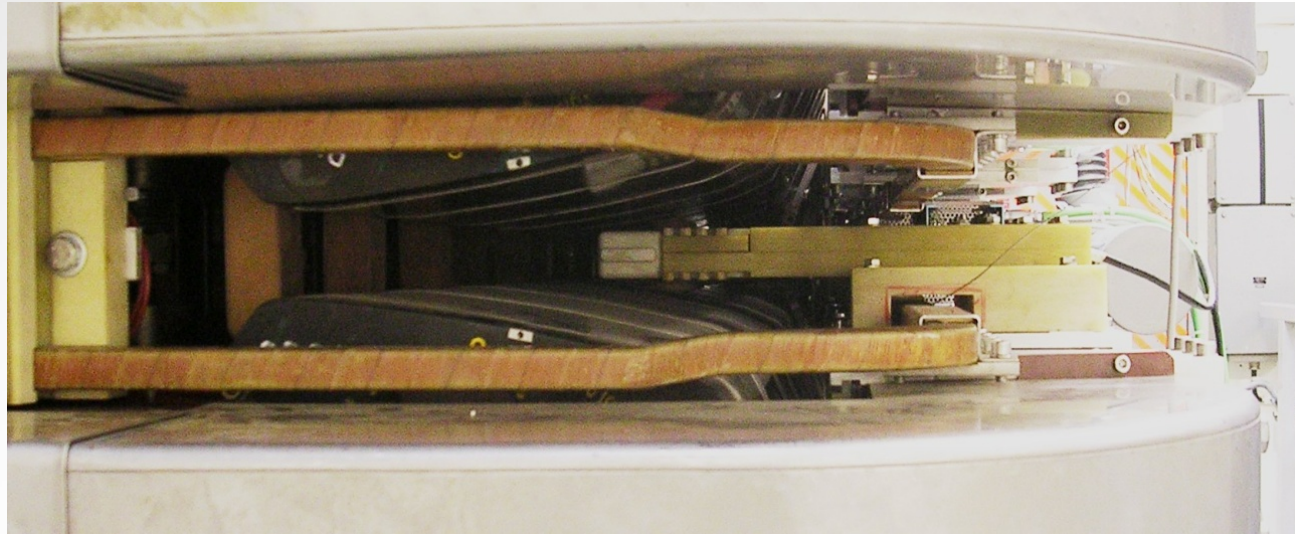
## BNL Harmonic Coil Array



16 Printed Circuit  
coils, 10 layers  
6 turns/layer  
300 mm long  
0.1 mm lines with  
0.1 mm gaps  
Matching coils  
selected from a  
production batch  
Radius =  
35.7 mm (BioMed)  
26.8 mm (GSI)

# BTrain generation in PS reference magnet

PS main magnets  
are  
combined function



Integrator connected to a reference coil sent pulses  
with constant  $\Delta\Psi(t)$  of 0.5 G at closed orbit position

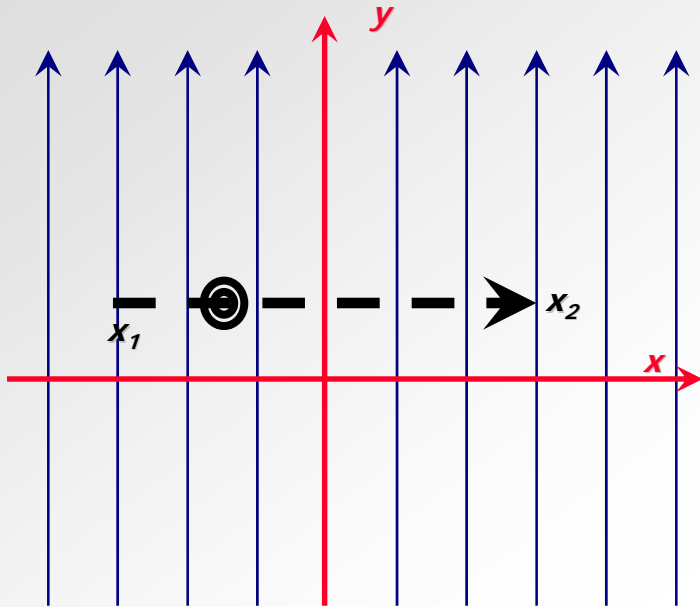
➤ Used only for synchronisation of the field  
⇒ calibrated by the beam

➤ Need a "marker" at  $B_0 = 49$  G (Peaking strip)  
(NMR cannot be used because combined function)

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# Measure Dipole Strength with a Stretched Wire



Dipole :  $B_y = \text{Cst}$  ,  $B_x = 0$

Flux seen by wire going from  $x_1$  to  $x_2$

$$\Psi(x_1, x_2) = \int_{x_1}^{x_2} \int_0^L B_y(x, l) \cdot dx \cdot dl = d \cdot \int B \cdot dl$$

with  $d = x_2 - x_1$

Directly dipole strength  $\int B \cdot dl$

Absolute accuracy given by

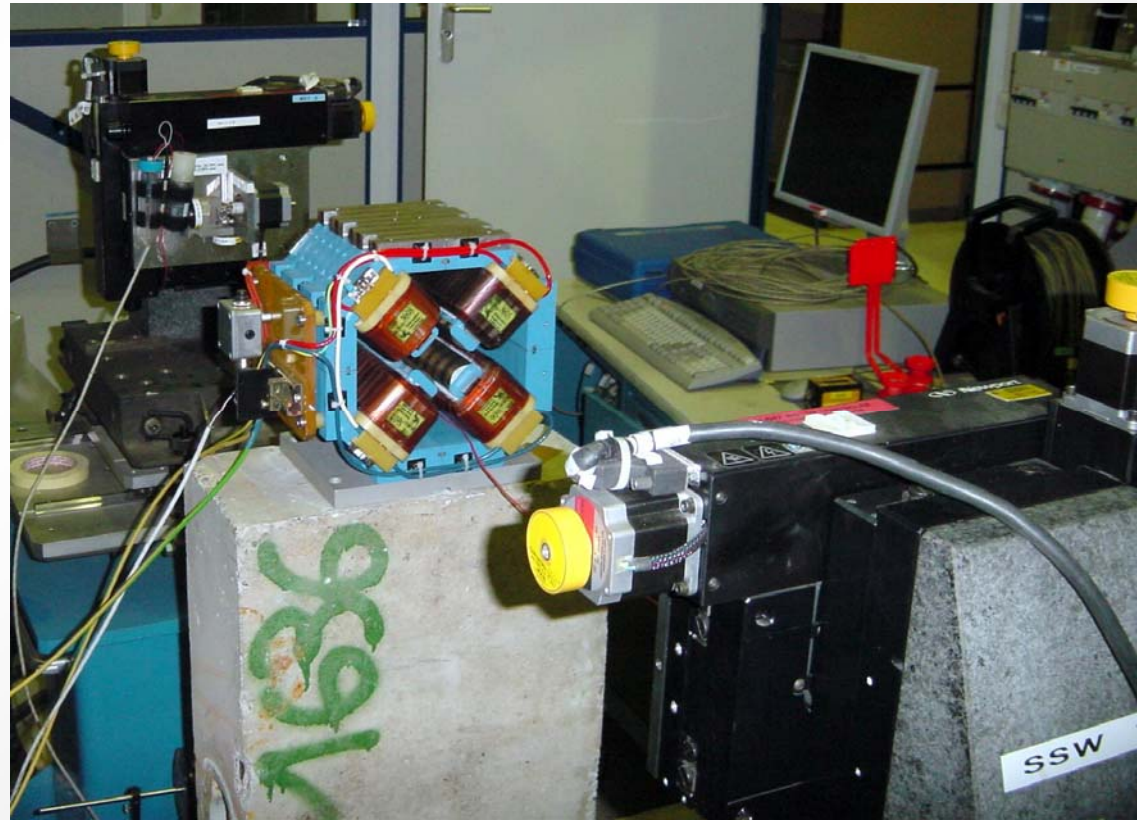
➤ Integrator :  $10^{-4}$  to  $10^{-5}$

➤ Distance :  $1\mu/10\text{mm} = 10^{-4}$

Return wire must not move,  
if possible in field free region

$\chi$ -check with NMR+Hall

@ $5 \cdot 10^{-5}$  , SLAC  $\approx 1978$

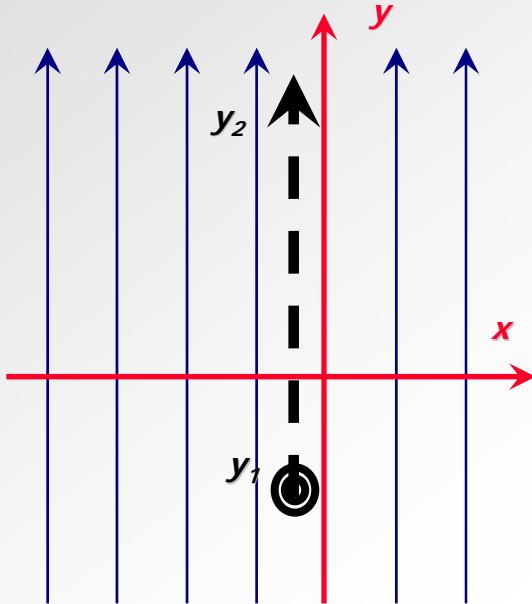


# SSW & Dipole Field Direction

Dipole :  $B_y = Cst$  ,  $B_x = 0$

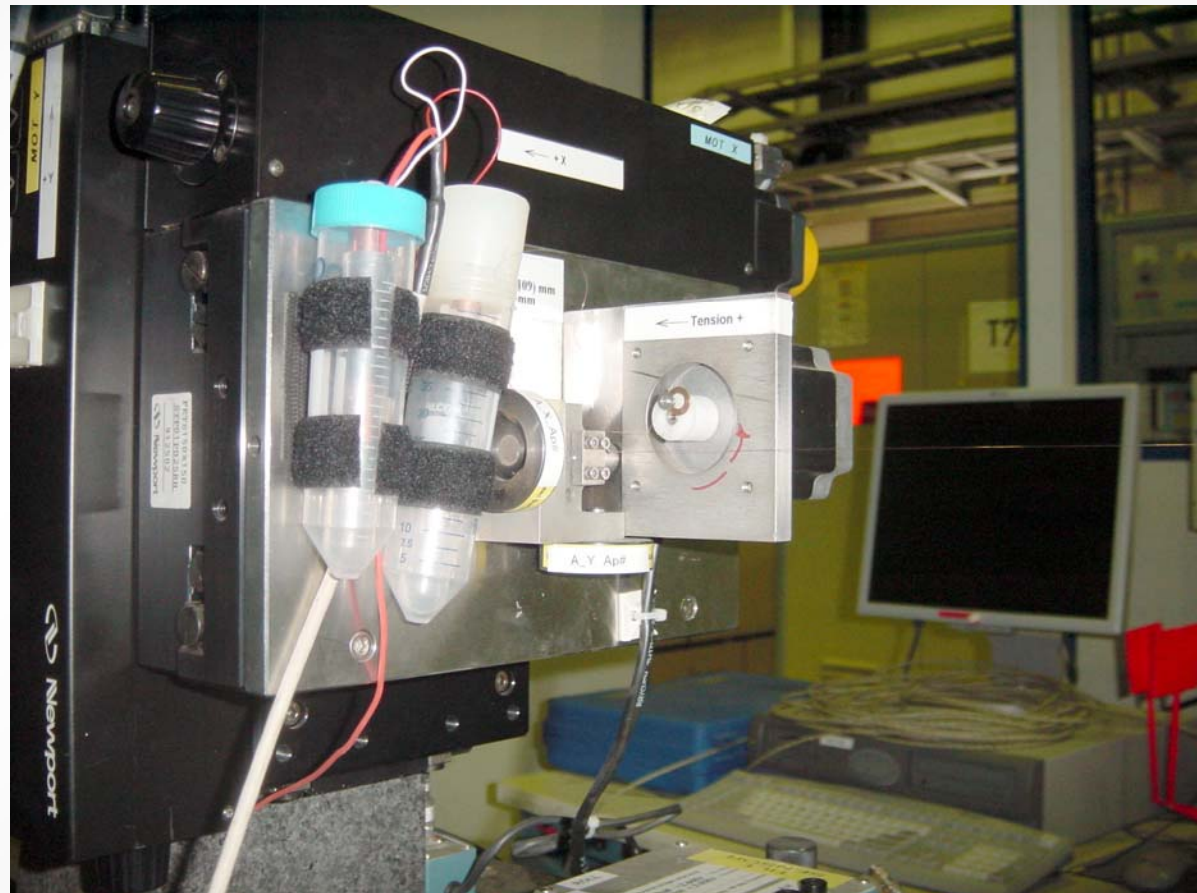
Flux from  $y_1$  to  $y_2 = 0$

if Field (& stages) perfectly vertical



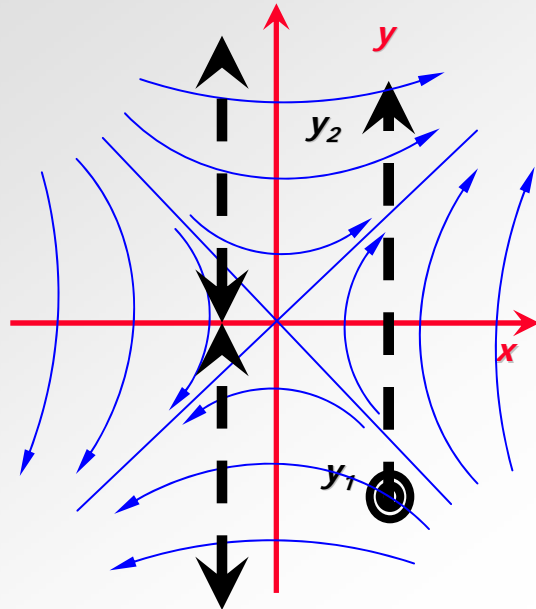
Accuracy  $\approx 0.1$  mrad

System developed by  
FNAL, J. Dimarco





# SSW in Quadrupole



Quadrupole :  $B_y = G \cdot x$  ,  $B_x = G \cdot y$

Flux from  $y_1$  to  $y_2$

$$\Psi(y_1, y_2) = L_{eff} \int_{y_1}^{y_2} G \cdot y \cdot dy = L_{eff} \cdot \frac{G}{2} \cdot (y_2^2 - y_1^2)$$

Wire deflects due to gravity :

Measure at different tensions & extrapolate to  $\infty$  tension

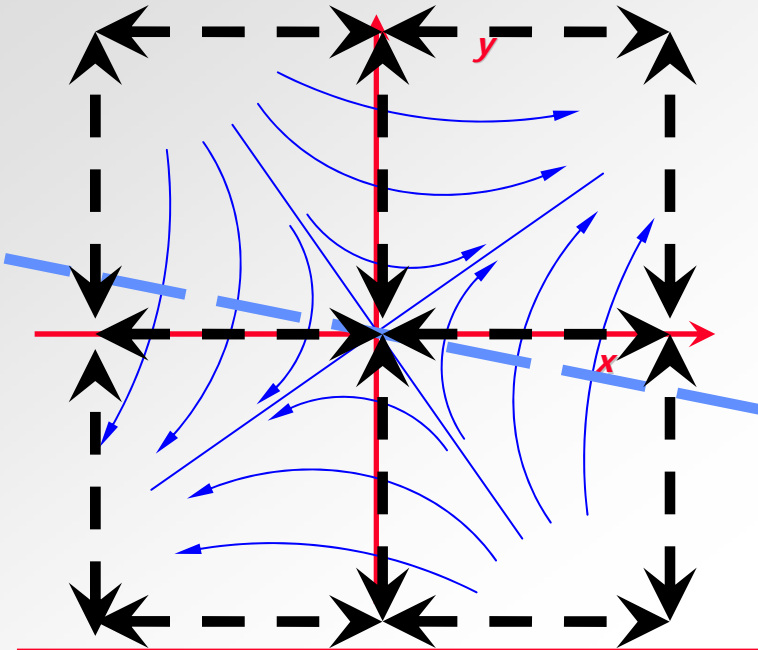
Where is  $y_c=0$  ?

2 intervals meas. , move  $y_c$  until

$$\Psi(y_c, y_c + d) = \Psi(y_c, y_c - d)$$

$$(y_c + d)^2 - y_c^2 = (y_c - d)^2 - y_c^2$$

# SSW in Quadrupole : align 1st your system



Tilt between Quadrupole and SSW

Find  $y_c = 0$  for different  $x$

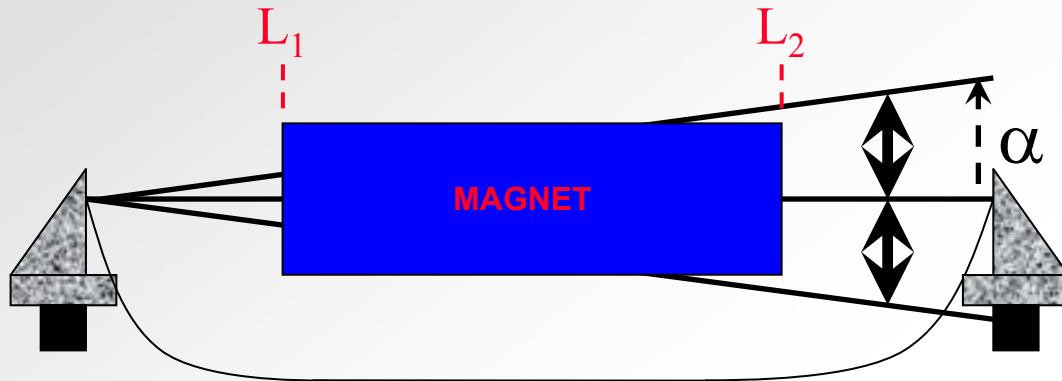
& Center in 2 directions

Iterate :

- Measure 8 (12) intervals
  - Calculate new reference frame of stages
- ! stages  $x$  &  $y$  axis must be parallel !

# Stretched Wire non aligned with Quad Axis

Hyp :  $L_{\text{eff}}$  & Longitudinal position of magnet known



Iterate 2 measurements :

move  $\alpha_c$  until

$$\Psi(\alpha_c, \alpha_c + \alpha) = \Psi(\alpha_c, \alpha_c - \alpha)$$

$$\Psi(\alpha_1, \alpha_2) = \int_{\alpha_1}^{\alpha_2} d\alpha \cdot \int_{L_1}^{L_2} G \cdot x(\alpha, l) \cdot dl$$

$$x = l \cdot \alpha$$

$$\Psi(\alpha_1, \alpha_2) = G \cdot \frac{(\alpha_2^2 - \alpha_1^2)}{2} \cdot \frac{(L_2^2 - L_1^2)}{2}$$

Combine

➤ co-parallel

(cf. previous slide)

➤ counter-parallel

to align axis & wire

Iterate until fully aligned

# Find magnet longitudinal location

If Magnet fully centred, and axis // to wire reference position, then we can measure longitudinal position

$d =$  distance from middle of wire length [i.e.  $L_w/2$ ]

$$\Psi(\alpha_1, \alpha_2) = \int_{\alpha_1}^{\alpha_2} d\alpha \cdot \int_{L_1}^{L_2} G \cdot x(\alpha, l) \cdot dl$$

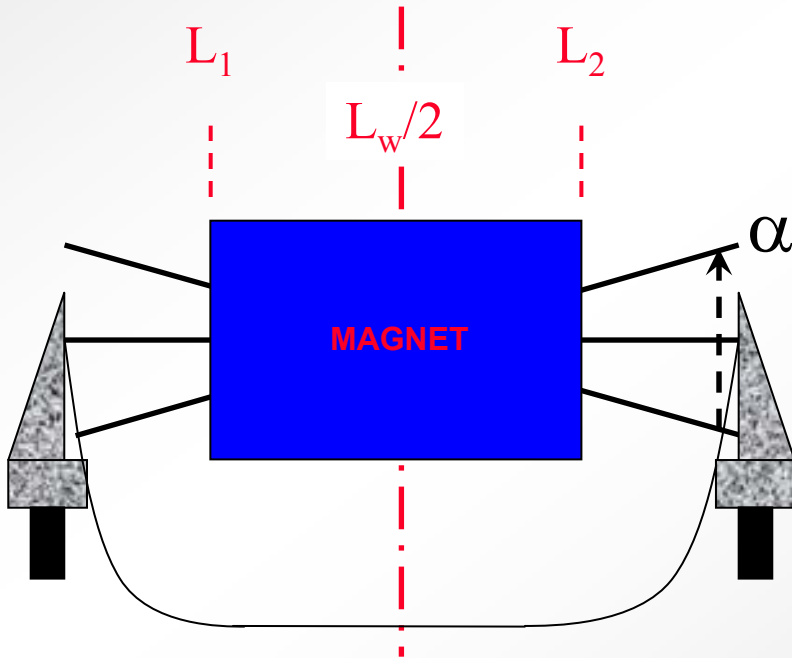
with

$$x = \left( l - \frac{L_w}{2} \right) \cdot \alpha$$

$$L_1 = \frac{L_w}{2} - \frac{L_{eff}}{2} + d$$

$$L_2 = \frac{L_w}{2} + \frac{L_{eff}}{2} + d$$

$$\Psi(\alpha_1, \alpha_2) = G \cdot (\alpha_2^2 - \alpha_1^2) \cdot d \cdot L_w$$



# Accuracy for axis and position finding

TABLE I  
ERRORS IN AXIS DETERMINATION FOR 11 AND 16 m WIRE LENGTHS

	X-axis (m)		Y-axis (m)	
	11m	16m	11m	16m
Magnet End a	-0.000011	0.000100	0.000119	0.000092
Magnet End b	-0.000059	-0.000111	-0.000156	-0.000142
Center	-0.000033	0.000000	-0.000019	-0.000025

## Field Alignment of Quadrupole Magnets for the LHC Interaction Regions

J. DiMarco, H. Glass, M.J. Lamm, P. Schlabach, C. Sylvester, J.C. Tompkins  
Fermilab, Batavia, IL, USA

J. Krzywinski  
Institute of Physics, Polish Academy of Sciences, Warsaw, Poland.

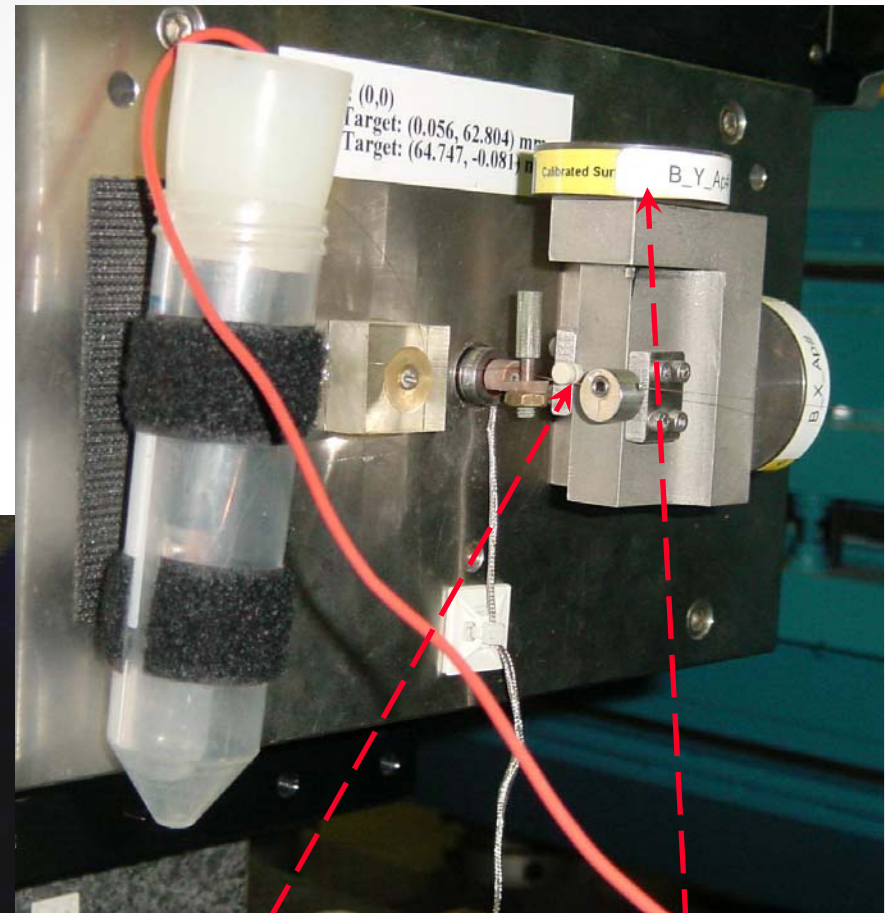
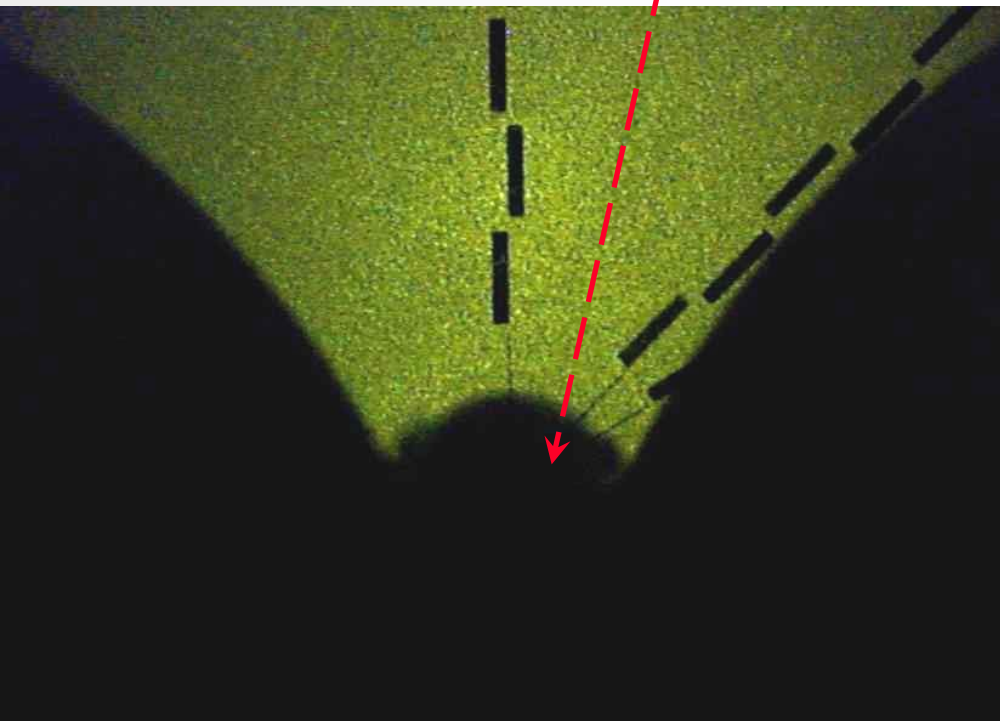
presented at Magnet Technology Conference, Philadelphia, 2007

Longitudinal position within 5 mm

# Wire location for axis search

Contour picture of wire  
0.1 mm squeezed inside  
ceramic balls

Accuracy  $\approx 0.01$  mm



Wire position referred to  
laser tracker fiducial

# Measure the Strength of a quadrupole $\int Gdl$

## ➤ Needed :

Dipole :  $\int Bdl(I)$  or Transfer Function =  $\int Bdl / I$  [T·m/kA]

Quadr :  $\int Gdl(I)$  or Transfer Function =  $\int Gdl / I$  [T/kA]

Requires current stability & accurate current measurement

## ➤ Verify that high order multipoles do not matter.

$$\Psi(x_1, x_2) = \int_{x_1}^{x_2} \int_0^L B_y(x, l) \cdot dx \cdot dl$$

$$B_y(x, l) = B_1 + B_3 \cdot x^3 \text{ in dipole}$$

$$B_y(x, l) = G \cdot x + B_6 \cdot x^5 + (B_4 \cdot x^3) \text{ in quadr.}$$

## ➤ Sag of the wire due to gravity and local field gradient main issue for $\int Gdl$ measurement

# Measure and compensate wire sag

Sagitta due to gravity

Extrapolate to  $\infty$  tension

$$\text{Sag} = \frac{W \cdot g}{8T} L^2$$

$\approx \text{mm}$  for

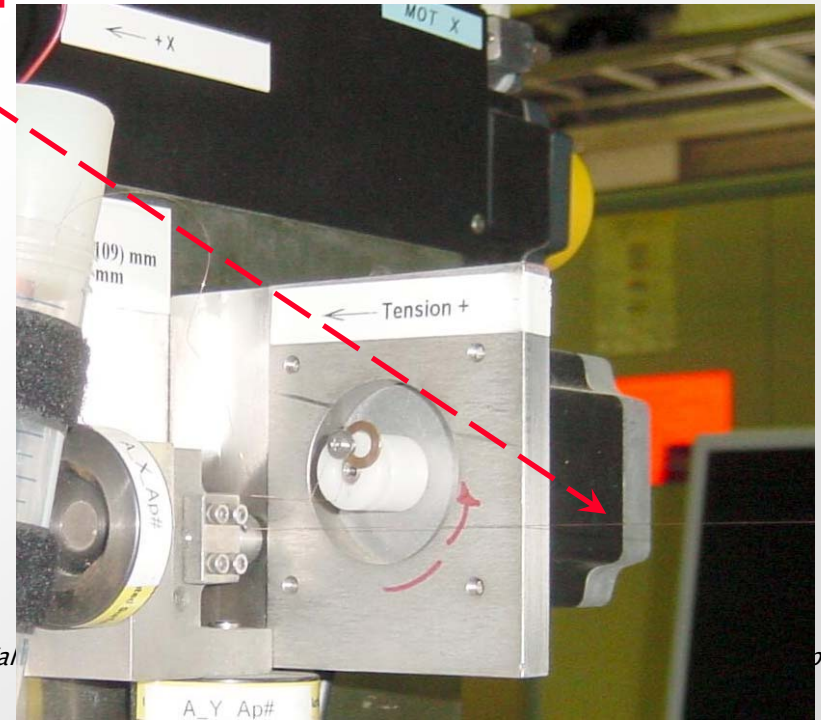
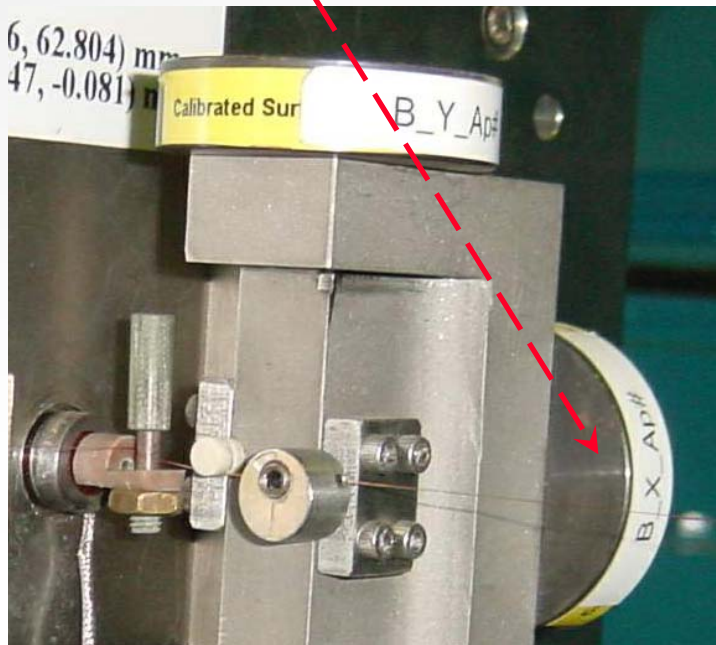
CuBe 0.1 mm wire

T maximum before break

L = 10 m

Tension gauge  
to avoid to  
brake the wire

Actuator to  
change the  
tension





# Extrapolate wire sag to $\infty$ tension

Measure the tension

give kick by moving both stages

measure vibration frequency of wire oscillating in field

$$f = \frac{1}{2l_{wire}} \sqrt{\frac{T}{w}}$$

Observations :

➤ sag depends on tension

and square of gradient

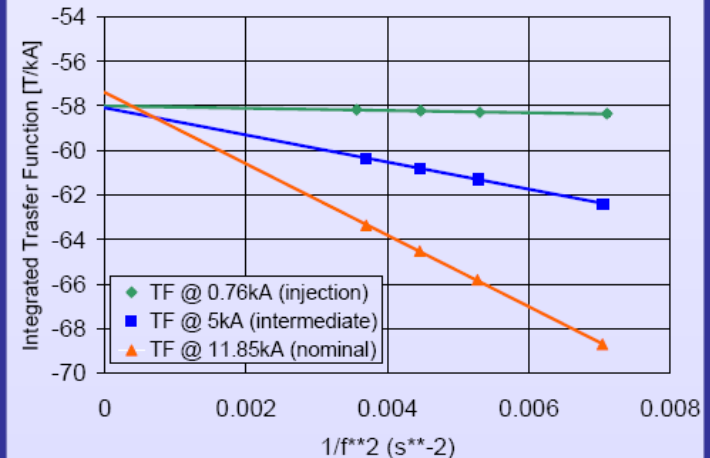
➤ value measured by vertical movement is always higher than by horizontal movement

CuBe is para-magnetic

(no norm for the material you purchase.)

## Magnetic Property of the Wire

Typical dependence of transfer function versus  $1/f^2$



Slope of Gdl for different types of wire:

Wire	0.76kA	5kA	11.85kA	$\chi$
#1	30.4	2000	9480	>0
#2	6.1	500	4977	>0
#3	2.3	50	474	<0
#4	-	-	380	<0

# Measure $\int Gdl$ with Horizontal movement

Magnetic force opens the flux (if CuBe wire is paramagnetic)

With Horizontal displacement

$$F^x_{mag} \propto G^2 \times (x_{step})^2$$

The Gdl obtained from a horizontal movement can be calculated from the linear fit of different wire tensions.

With vertical displacement :

$$F^y_{mag} \propto G^2 \times (y_{step} + Sag)^2$$

so that dependance with T  
no more linear

The Gdl obtained from a vertical movement must be calculated with a parabolic fit of different wire tensions.

could be unstable

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# Vibrating wire to find Quad axis

## ◆ Equation for the string motion driven by AC current:

$$w \frac{\partial^2 x}{\partial t^2} = T \frac{\partial^2 x}{\partial z^2} - \gamma \frac{\partial x}{\partial t} + I(t)B(z) \quad \text{boundary} \quad x(0,t) = x(l,t) = 0$$

$w$  = linear wire density,  $T$  = tension,  $\gamma$  = damping

$I(t) = I_0 \exp(i\omega t)$  [driving AC current],  $B(z)$  = transverse magnetic field

## ◆ Solution - sum of standing waves

$$x(z,t) = \sum_n x_n \sin\left(\frac{\pi n}{l} z\right) \exp(i\omega t); \text{ where } x_n = \text{standing waves amplitudes}$$

$$x_n = \frac{I_0}{w} \frac{1}{\omega^2 - \omega_n^2 - i\gamma\omega} B_n; \quad \omega_n = \frac{\pi n}{l} \sqrt{\frac{T}{w}}$$

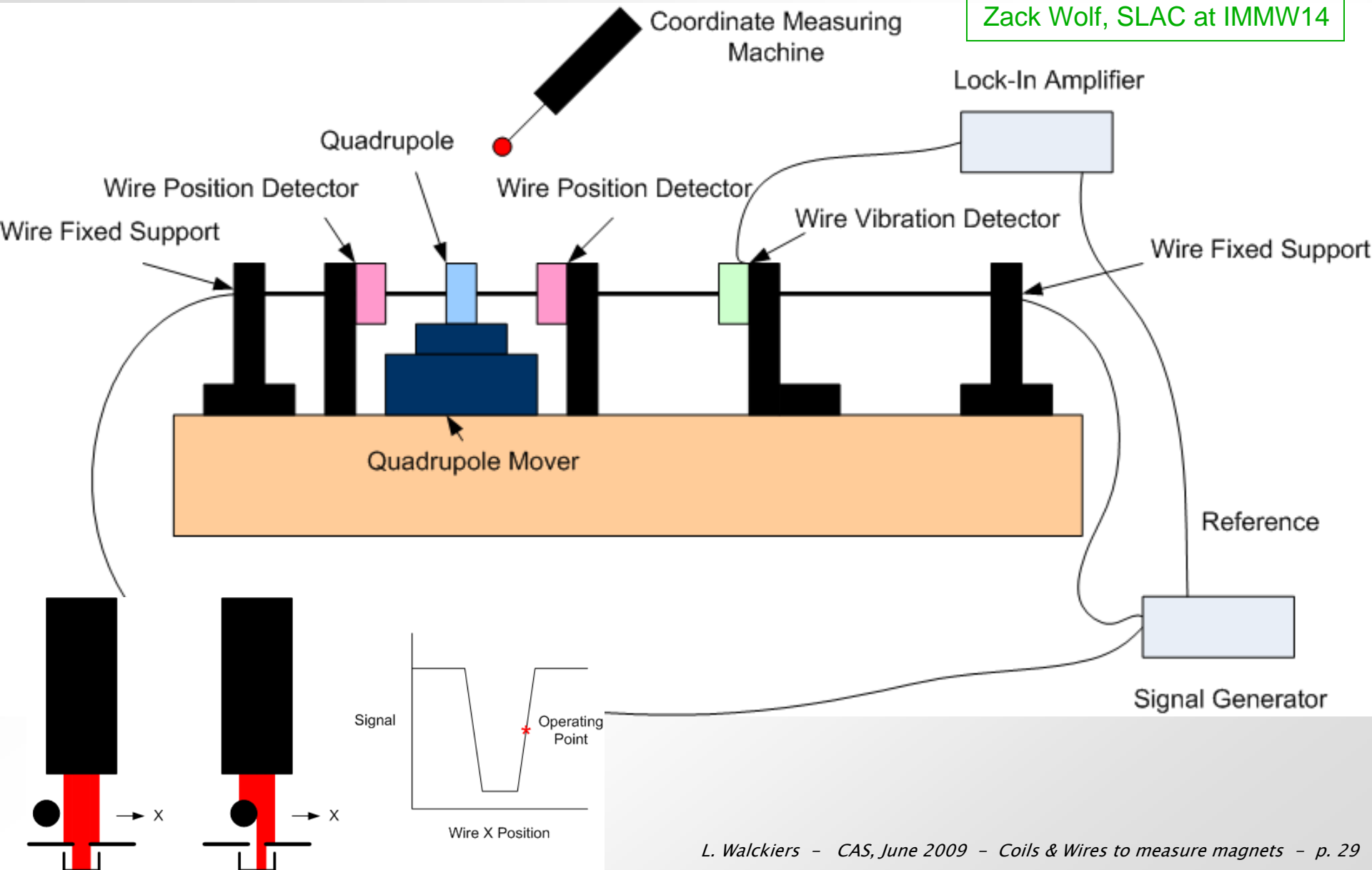
$$B_n \text{ are coefficients of a sinus waves expansion } B(z) = \sum_n B_n \sin\left(\frac{\pi n}{l} z\right)$$

## ◆ Measuring $x_n$ one can find $B_n$ and reconstruct $B(z)$ !!!

A. Temnykh,  
Vibrating wire  
field-measuring  
technique, Nuc.  
Inst., A 399  
(1997) 185-194

# Vibrating wire system overview

Zack Wolf, SLAC at IMMW14



# Measure the wire motion

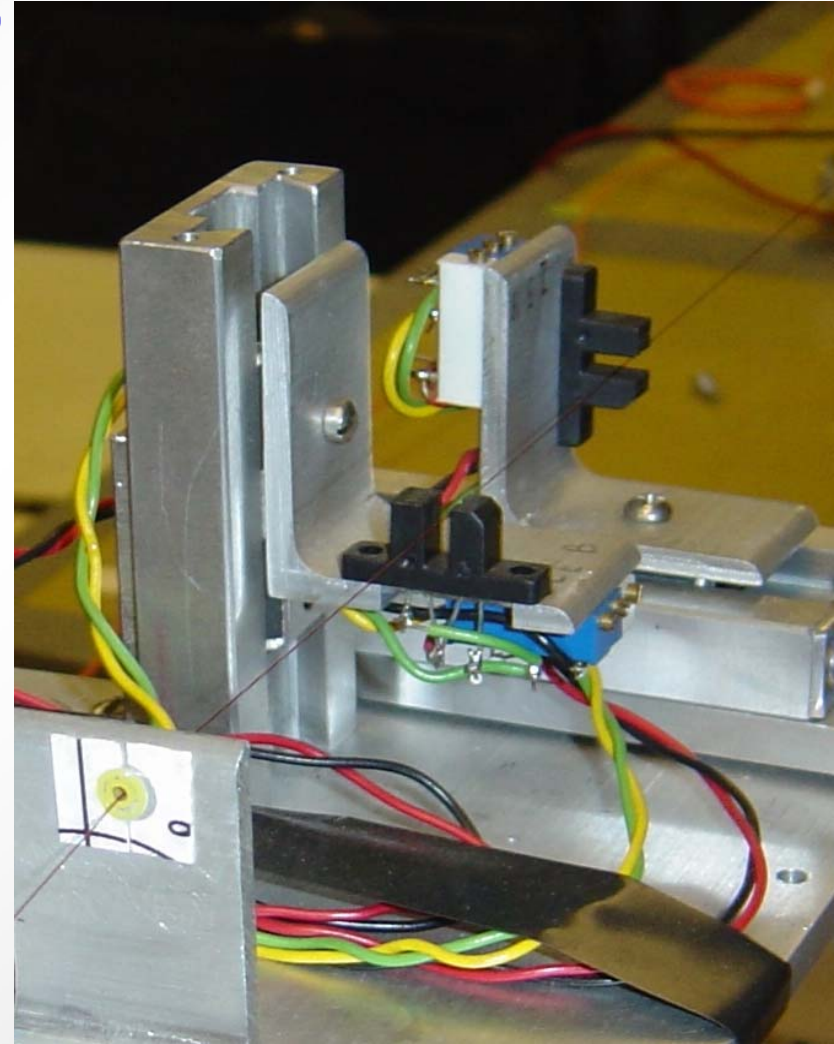
The wire motion in vertical (horizontal) plane is caused by the Lorentz forces between wire current and horizontal (vertical) magnetic field.

⇒ need to measure wire motion in vertical and horizontal planes.

Assembly of optical sensors used shows ~10% coupling between vertical and horizontal wire motion

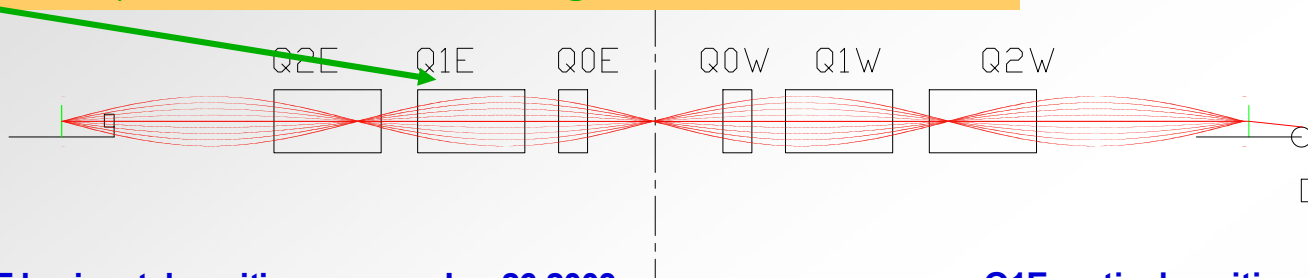
Need ~1% or less.

⇒ Calibration needed

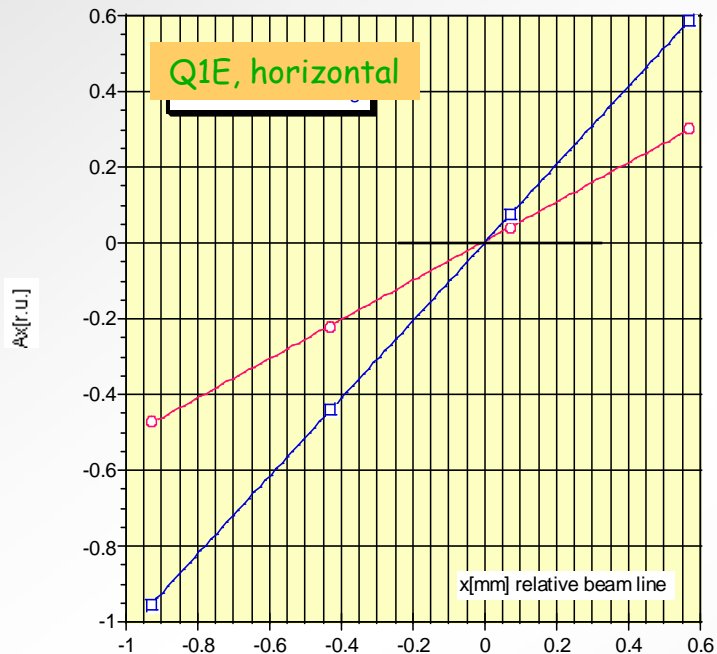


# Super-conducting magnets survey

For Q1E survey the 4<sup>th</sup> order standing wave has been used.

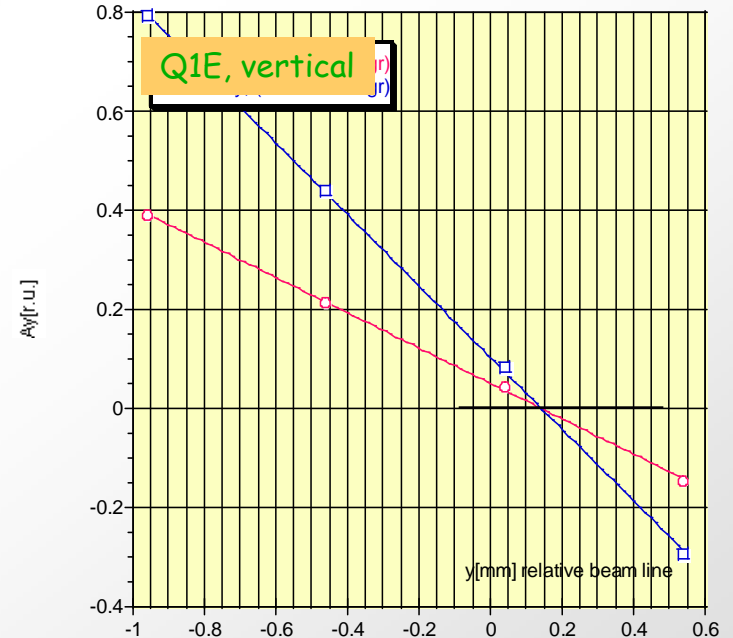


Q1E horizontal position survey, Jun 26 2003



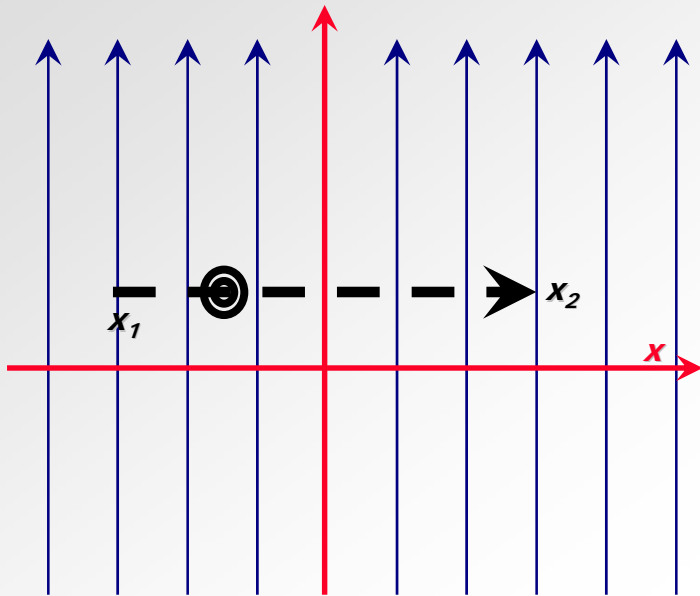
1) I(Q1E) = 231A  
 $x = -0.010 \pm 0.004$ mm  
 2) I(Q1E) = 466A  
 $x = -0.002 \pm 0.001$ mm

Q1E vertical position survey, Jun 26 2003



1) I(Q1E) = 231A  
 $y = 0.142 \pm 0.007$ mm  
 2) I(Q1E) = 466A  
 $y = 0.141 \pm 0.010$ mm

# SSW to measure undulators & wigglers



➤ Verify  $\int B dl = 0$ , i.e. no perturbation for the beam  
SSW in displacement is ideal

➤ Measure amplitude of  $B_y(z)$  by pulsed SSW  
[ESRF, Grenoble]

Coils wound on frames do not have constant width

➤ not to use with wigglers

➤ could also give problems with normal magnets



# Coils & Wires : conclusions

**Simple coil measure  $B_y(x)$  or  $G_y(x)$  with**

- **static field and flip or displaced coils**
- **pulsed field & static coil**

**Single Stretched Wire is the reference for :**

- **Dipole & quadrupole strength**
- **Dipole & Quad. axis & field direction**

**Vibrating SSW : axis search (small aperture)  
magnet strength (limited accuracy)**

**For full 2D measurements : harmonic coils**

$$B_y + i \cdot B_x = \sum C_n \cdot z^{n-1}$$