

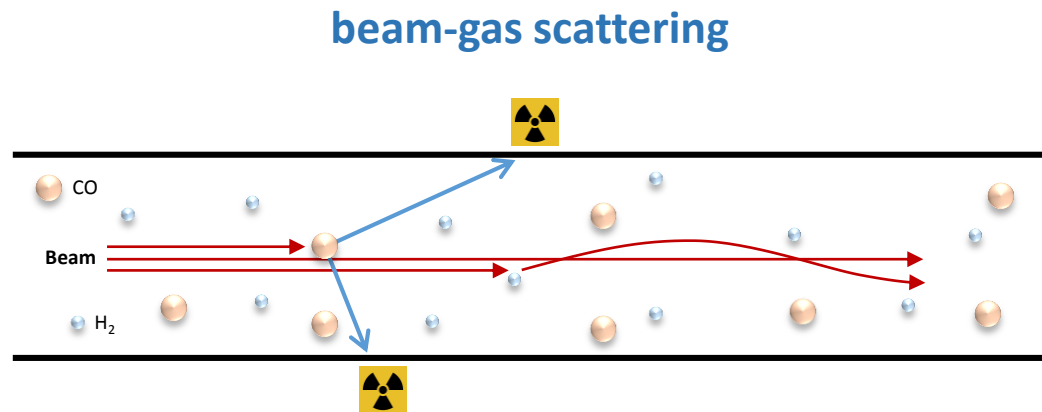


Accelerator Vacuum

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Why vacuum in accelerators ?

- maximize beam lifetime
- minimize emittance growth (hadrons)
- minimize component activation
- minimize impact on detectors, electronic components



Vacuum - Outline

1. Vacuum Basics

pressure, density, gas equation, pumping speed, flow regimes, conductance, pressure profile calculation

2. Accelerator Vacuum

requirements: bremsstrahlung, elastic scattering, emittance growth
beam induced desorption: SR, ions
examples of vacuum chambers

3. Components for Vacuum Systems

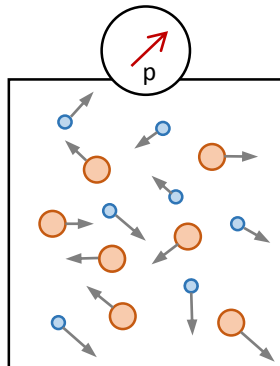
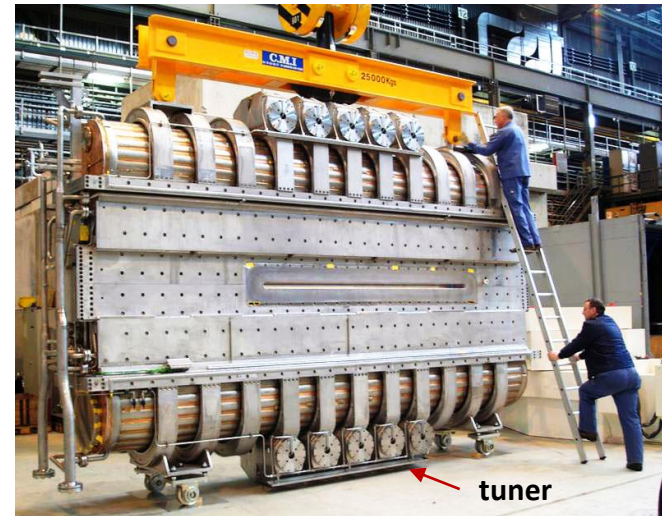
pumps: turbo, ion sputter, NEG, cryo-pump
flange systems



Pressure

cyclotron resonator:
continuous tuning required
due to air pressure variation

pressure = force / area
 $1 \text{ Pa} = 1 \text{ N/m}^2 = 0.01 \text{ mbar}$
 $1 \text{ atm} = 10^5 \text{ Pa}$
 \rightarrow weight of 1 kg/cm^2

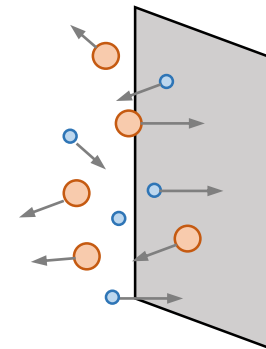


average velocity

$$\bar{v} = \sqrt{\frac{8k_b}{\pi m_0} T}$$

number of molecules
impinging per time
and area

$$\frac{dN}{dA dt} = \frac{1}{4} n \bar{v}$$

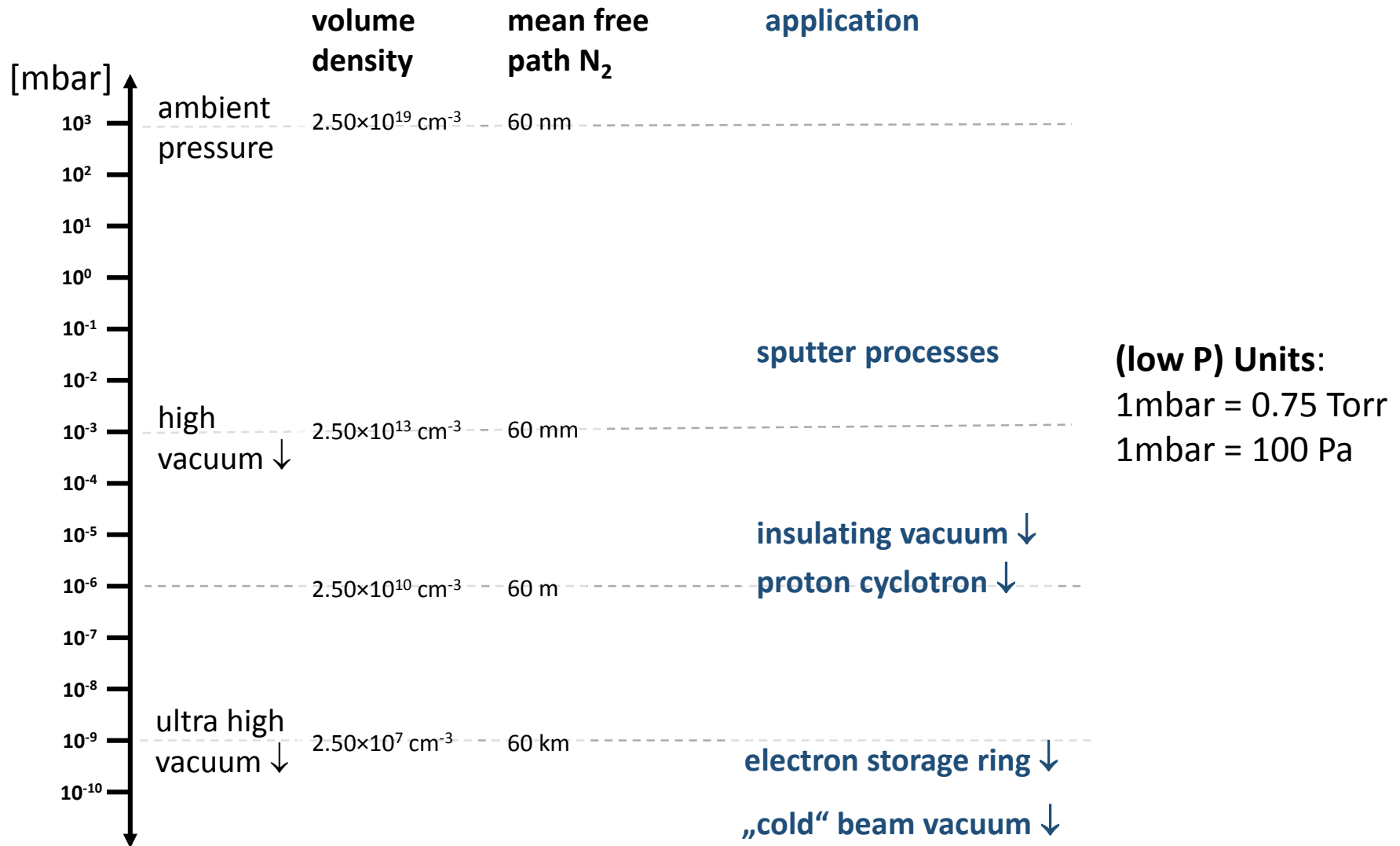


n volume density of molecules

k_b Boltzmann constant, $1.38 \times 10^{-23} \text{ J/K}$



Vacuum Pressure – Orders of Magnitude



Gas Equation and „amount of gas“

$$PV = Nk_bT = nRT$$

$R = 8.314 \text{ Nm / mole K}$

$k_b = 1.38 \times 10^{-23} \text{ J/K}$

N = number of molecules

n = number of moles

thus **PV [mbar l]** is a measure of the amount of gas (for a given temperature)

also: molar volume = 22.4 l / mol

(1atm = 101325 Pa, 273K)

to specify a leak rate:

x [mbar l / s]

example bicycle tire:

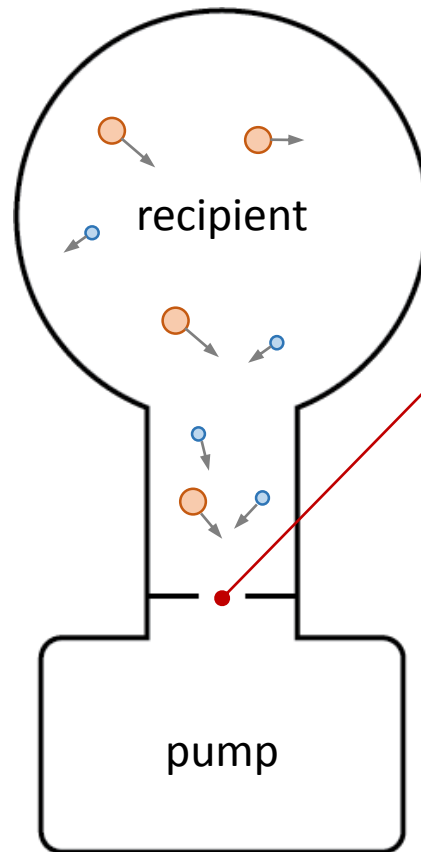
$P = 2.5 \text{ bar}$, $V = 1 \text{ l}$, leak $Q = 2 \times 10^{-4} \text{ mbar l / s}$
after 1 Month (2.5 million sec): $p = 2.0 \text{ bar}$

accelerator section, no pumping, no outgassing:

$P = 10^{-10} \text{ mbar}$, $V = 1000 \text{ l}$, leak $Q = 10^{-9} \text{ mbar l / s}$
after 1 Month (2.5 million sec): $p = 2.5 \cdot 10^{-6} \text{ mbar}$



Pumping



pump = device that
absorbs gas molecules

pumping speed
 $S [l/s] = Q/P$ at pump interface
 S varies for gas species

for example:

typ. ion getter pump:	60 l/s
turbo pump:	100 l/s
cryo pump:	500 l/s

gas load $Q = 10^{-9} \text{ mbar l / s}$

$S = 100 \text{ l/s} \rightarrow P \approx 10^{-11} \text{ mbar}$



Flow Regimes

mean free path of
gas molecules:

$$\lambda = \frac{k_b T}{\sqrt{2} \sigma P}$$

see also Knudsen
Number:

$$Kn = \frac{\lambda}{d}$$

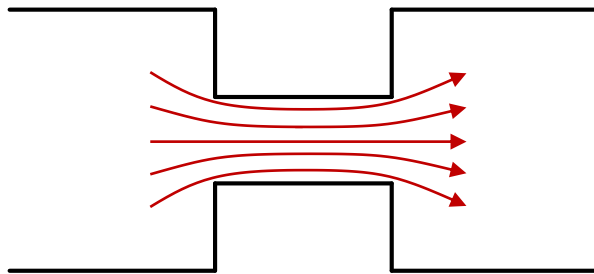
for example:

N_2 , $P = 10^{-6}$ mbar, $\lambda \approx 60$ m
→ molecular flow

viscous flow

$$\lambda \ll d$$

$$Kn \ll 1$$



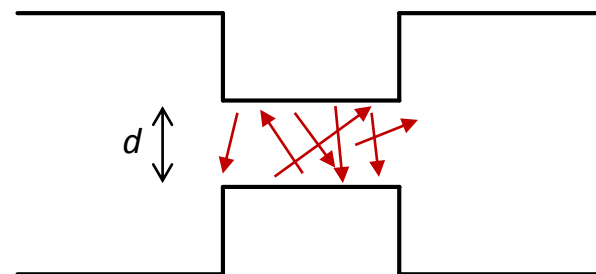
$$Q_{\text{visc}} \propto d^4 \bar{P} \Delta P$$

heart attack!

molecular flow

$$\lambda \gtrsim d$$

$$Kn \gtrsim 1$$



$$Q_{\text{molec}} \propto d^3 \Delta P$$

$d \neq 2 \rightarrow C \neq 8!$

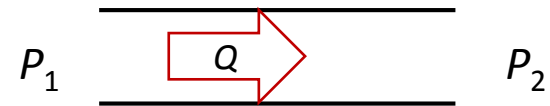


Conductance

conductance is defined as the ratio of the molecular flux Q to the pressure drop ΔP along a vacuum vessel

- function of the shape (eg. diam.) of the vessel
- the type of the gas
- it's temperature

$$C = \frac{Q}{\Delta P}$$



orifice: $C = \sqrt{\frac{k_b T}{2\pi M}} A, \quad C_{\text{air}} = 11.6 [\text{l/s}] A [\text{cm}^2]$

tube: $C = \sqrt{\frac{2\pi k_b T}{M}} \frac{d^3}{l}, \quad C_{\text{air}} = 12.1 [\text{l/s}] \frac{d^3 [\text{cm}]}{l [\text{cm}]}$

M = molecular mass
A = area
d = diameter
l = length

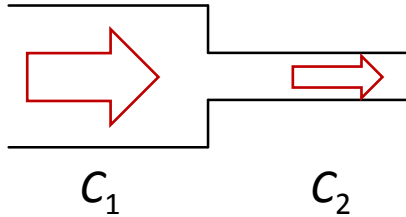
example:

tube $d=8\text{cm}$, $l=30\text{cm}$: 200l/s

tube $d=1\text{cm}$, $l=30\text{cm}$: 0,4l/s



Conductance - Combining Vessels

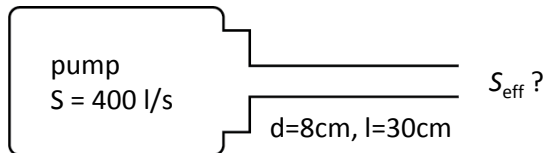


$$C_{\text{total}} = \left(\frac{1}{C_1} + \frac{1}{C_2} \right)^{-1}$$

$$C_{\text{total}} \approx C_2 \quad \text{for } C_2 \ll C_1$$



$$C_{\text{total}} = C_1 + C_2$$



example:
ion getter pump 400l/s connected by
 $d=8\text{cm}$, $l=30\text{cm}$ tube: $S_{\text{eff}} = 136 \text{ l/s}$



Sources of gas

main sources of gas in accelerator vacuum:

- thermal desorption
- beam induced desorption (synchrotron radiation, beam impact, electron cloud ...) → dynamic pressure, discussed later
- diffusion out of bulk materials
- permeation through materials
- virtual and real leaks

in practice, outgassing of water:
 $q(t) \approx 3 \times 10^{-9} \text{ mbar l / s cm}^2 / t [\text{h}]$
baking! exponential dependence on T

thermal desorption

chem./phys. binding

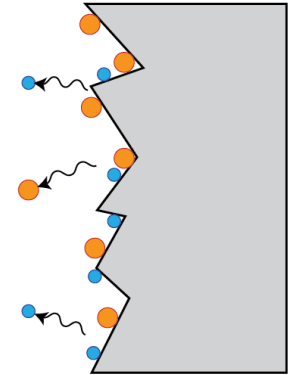
char. time = sojourn time

e.g. $E_d = 1 \text{ eV}$, $T = 293 \text{ K}$

$\tau = 5 \text{ h}$

$$q(t) \propto \frac{1}{t}$$

$$\tau \propto \exp\left(\frac{E_d}{k_b T}\right)$$



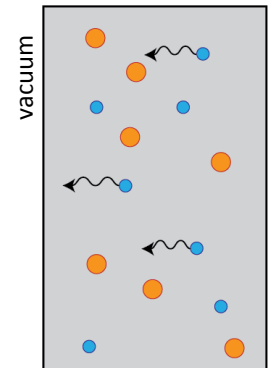
bulk diffusion

diffusion coefficient D

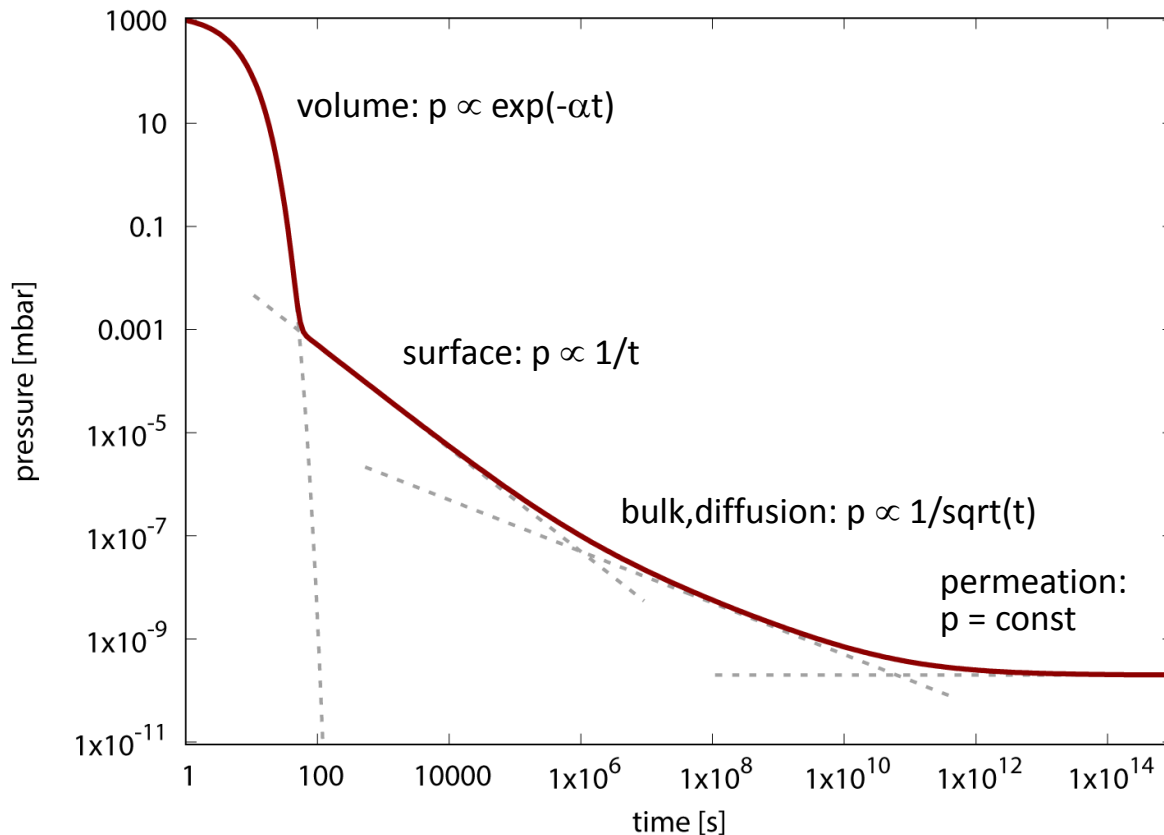
mainly H_2 relevant

$$q(t) \propto \sqrt{D(T)/t}$$

$$D(T) \propto \exp\left(-\frac{E_{\text{diff}}}{k_b T}\right)$$



Pump Down Processes



log. scale:
different effects dominate
after varying times



Pressure Computation for 1-dimensional Systems

starting from definition of conductance $C = Q / \Delta P$
introduce correct sign and specific conductance:

$$Q = - \underbrace{C \Delta s}_{\text{specific conductance}} \frac{\Delta P}{\Delta s}$$

$$Q(s) = -\mathcal{C} \cdot \partial P(s) / \partial s$$

compare conductance of circular tube:

$$C = \underbrace{\sqrt{\frac{2\pi k_b T}{M}} d^3}_{\mathcal{C}} \frac{1}{l}$$

gas&tube specific length

continuity equation, change of flow by pumping and outgassing:

$$\partial Q(s) / \partial s = q - \mathcal{S} P(s)$$

1-dim diffusion equation:

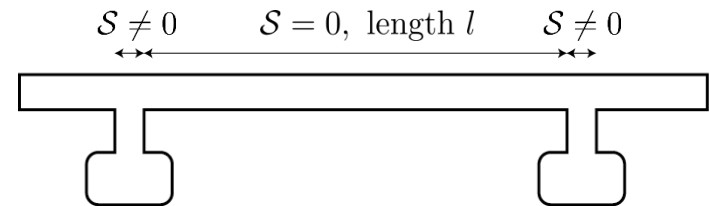
$$\frac{\partial}{\partial s} \mathcal{C} \frac{\partial}{\partial s} P(s) - \mathcal{S} P(s) + q = 0$$

\mathcal{C}	$\left[\frac{\text{l m}}{\text{s}} \right]$	specific conductance
\mathcal{S}	$\left[\frac{1}{\text{s m}} \right]$	specific pumping speed
q	$\left[\frac{\text{mbar l}}{\text{s m}} \right]$	specific outgassing rate



Quadratic Solution for lumped Pumps

$$P(s) = \frac{ql}{S} + \frac{q}{8C} (l^2 - 4s^2)$$



the parabolic profile results in following average and maximum pressure:

$$P_{\text{avg}} = ql \left(\frac{1}{S} + \frac{l}{12C} \right), \quad P_{\text{max}} = ql \left(\frac{1}{S} + \frac{l}{8C} \right)$$



pumping speed



conductance limited

choose distance and pumping speed to achieve desired pressure and to reasonably balance both terms

example:

7cm tube, $q_0 = 5 \times 10^{-12}$ mbar l / s cm², $S = 100$ l/s

→ $l = 5$ m, $P_{\text{avg}} = 1 \times 10^{-9}$ mbar

→ $l = 3$ m, $P_{\text{avg}} = 5 \times 10^{-10}$ mbar



General Solution by Matrix Transport of Q, P

$$\begin{pmatrix} P(s) \\ Q(s) \end{pmatrix} = \begin{pmatrix} \cosh(\alpha s) & -\frac{1}{\alpha c} \sinh(\alpha s) \\ -\alpha c \sinh(\alpha s) & \cosh(\alpha s) \end{pmatrix} \begin{pmatrix} P(0) \\ Q(0) \end{pmatrix} + \frac{q}{\alpha} \begin{pmatrix} \frac{1}{\alpha c} (1 - \cosh(\alpha s)) \\ \sinh(\alpha s) \end{pmatrix} \quad \alpha = \sqrt{\frac{S}{c}}$$

$$\lim_{\alpha \rightarrow 0} : \begin{pmatrix} P(s) \\ Q(s) \end{pmatrix} = \begin{pmatrix} 1 & -s/c \\ 0 & 1 \end{pmatrix} \begin{pmatrix} P(0) \\ Q(0) \end{pmatrix} + qs \begin{pmatrix} -\frac{s}{2c} \\ 1 \end{pmatrix}$$

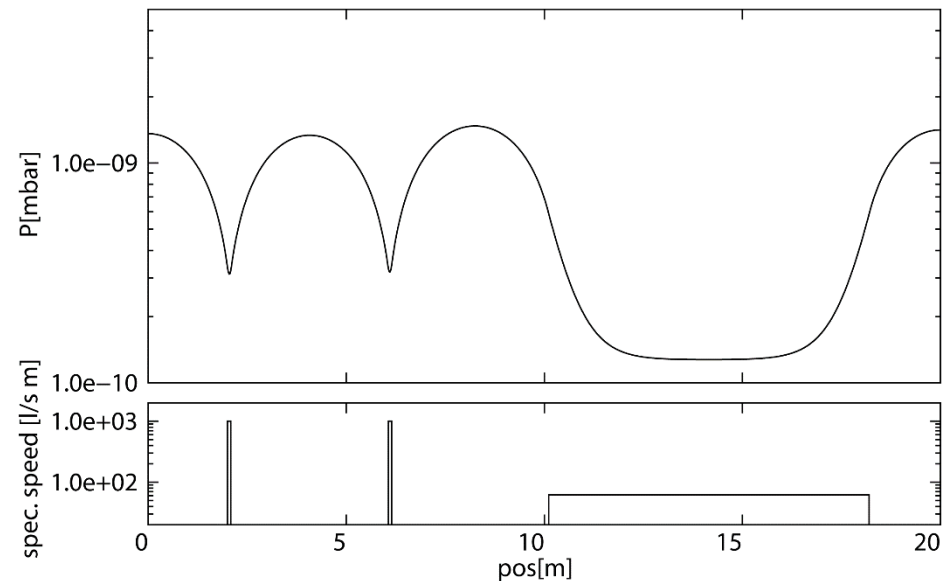
[V. Ziemann, SLAC/Pub/5962]

example calculation:

lumped pumps: $S=100$ l/s

distrib. pumps: $S = 60$ l/s m

outgassing: $q_0=5 \times 10^{-12}$ mbar l / s cm²



Time Dependent Diffusion Equation

$$\nu \frac{\partial}{\partial t} P(s, t) = \frac{\partial}{\partial s} C \frac{\partial}{\partial s} P(s, t) - \mathcal{S} P(s, t) + q$$

↑
specific volume [l/m]

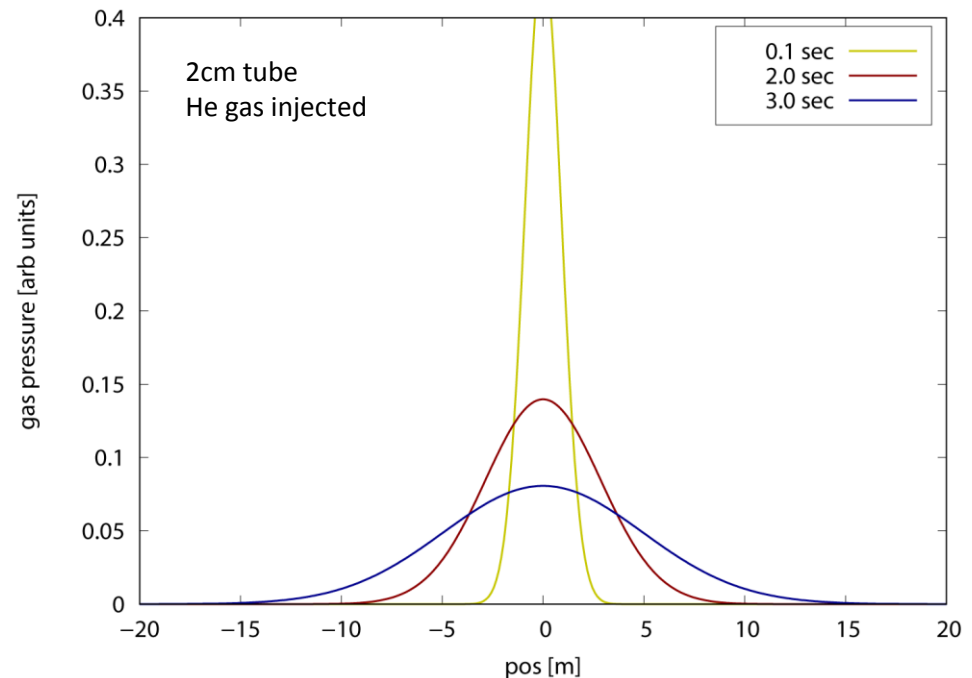
compare
classical
diffusion eq.: $\frac{\partial}{\partial t} f(x, t) = \frac{\partial}{\partial x} \mathcal{D} \frac{\partial}{\partial x} f(x, t)$

$$\rightarrow \mathcal{D} = \frac{\langle \Delta x^2 \rangle}{\langle \Delta t \rangle} = \frac{c}{\nu}$$

example:

tube 7cm, diffusion time over 5m:
N₂: 2.3 s; He: 0.9 s

tube 2cm, diffusion time over 5m:
N₂: 8 s; He: 3 s

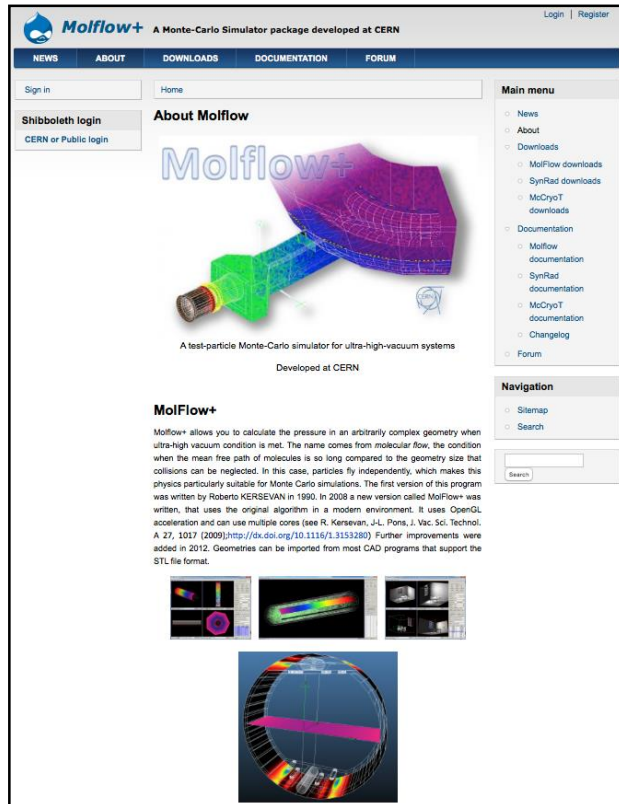


Monte Carlo Code Molflow+ (2008)

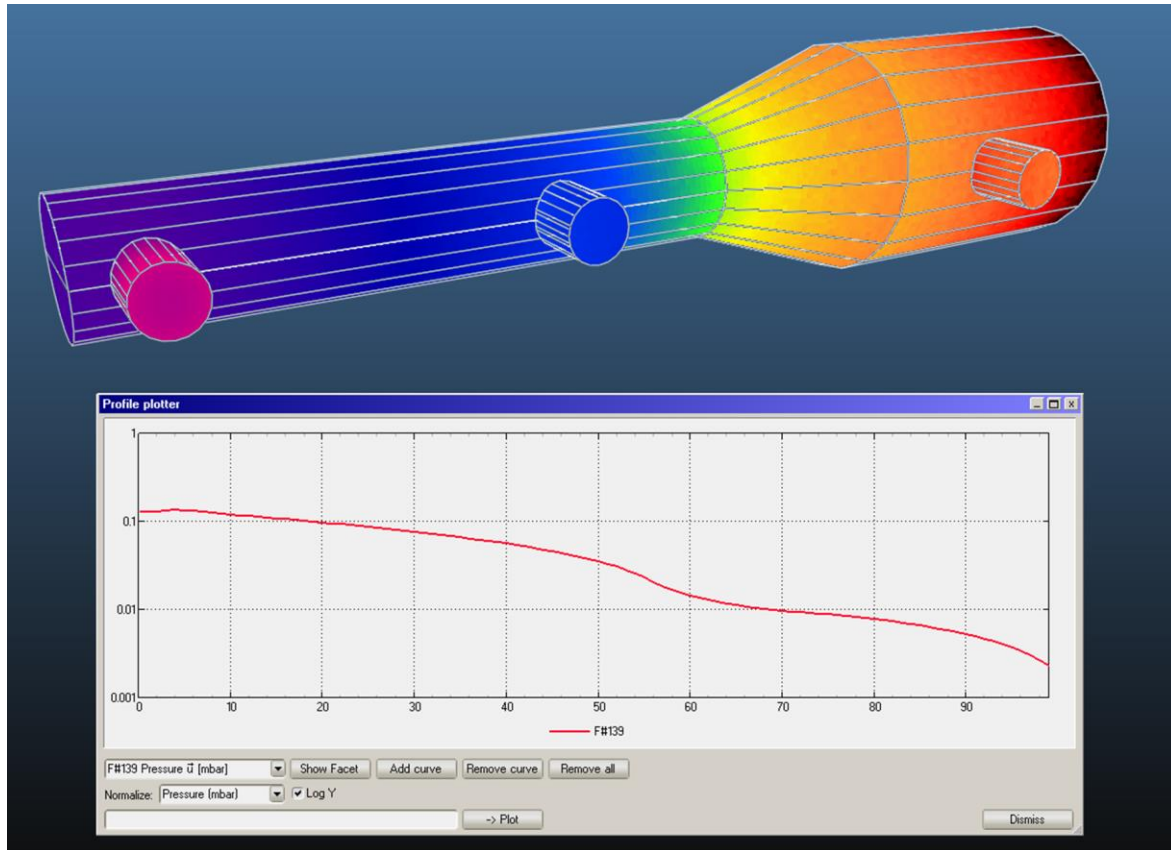
C++ code, OpenSource since 2018

J-L. Pons (ESRF), M. Ady,
R.Kersevan (CERN)

Web site for info and downloads:



The screenshot shows the Molflow+ website interface. At the top, it says "Molflow+ A Monte-Carlo Simulator package developed at CERN". Below this are navigation tabs: NEWS, ABOUT, DOWNLOADS, DOCUMENTATION, and FORUM. There are links for "Sign in", "Home", "Shibboleth login", and "CERN or Public login". The "Main menu" on the right lists: News, About, Downloads (Molflow downloads, SynRad downloads, McCryoT downloads), Documentation (Molflow documentation, SynRad documentation, McCryoT documentation), Changelog, and Forum. The "Navigation" section includes "Sitemap" and "Search". The main content area features the "About Molflow" section with a large image of a 3D model of a particle accelerator component and the text: "A test-particle Monte-Carlo simulator for ultra-high-vacuum systems Developed at CERN". Below this is the "MolFlow+" section, which describes the software's capabilities and history, mentioning its development by Roberto KERSEVAN in 1990 and its use of OpenGL acceleration. At the bottom, there are several small thumbnail images showing different 3D models and simulation results.

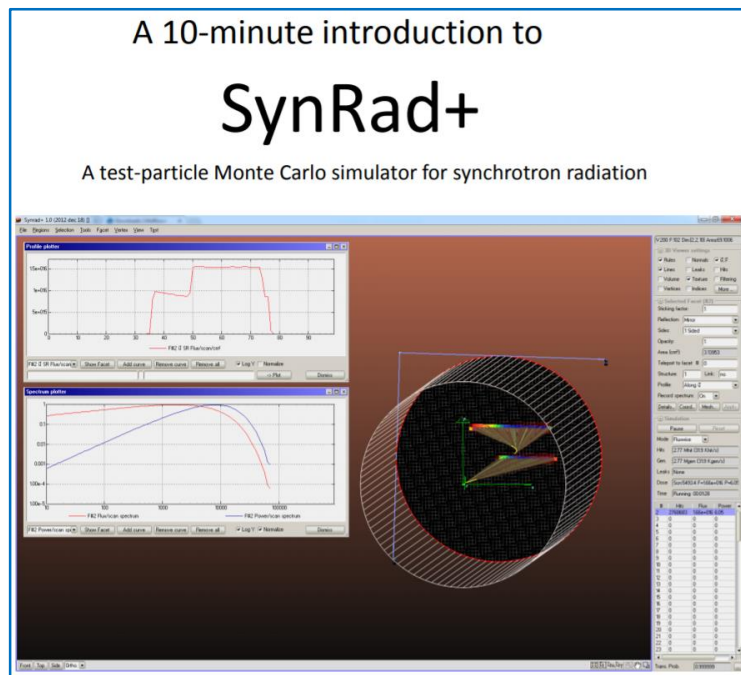


example calculation:
100k molecules tracked, computation
time: few seconds, pressure profile



Synrad+ for calculation of synchrotron radiation

- Monte Carlo code computes photons generated by the beam and projects them onto the vacuum chamber surface
- in a second step the molecular outgassing is computed
- the result serves as input for Molflow+ to compute the pressure distribution



- SR spectrum + flux
- calculates beam orbit from lattice file (MAD-X)
- dipole approximation only, no undulator interference effects

<https://molflow.web.cern.ch/content/synrad-documentation>

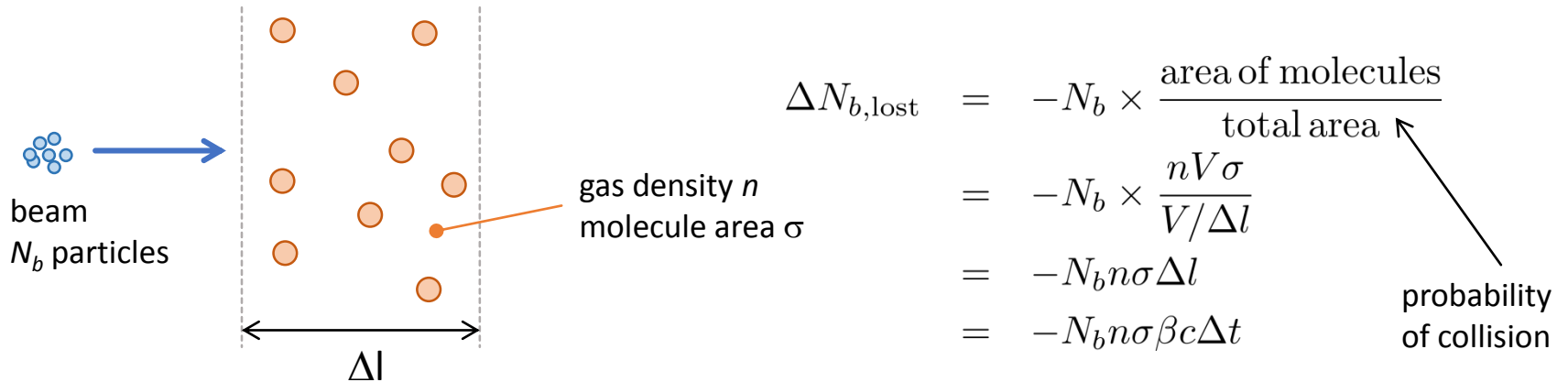


Next:

Accelerator Vacuum

requirements: bremsstrahlung, elastic scattering, emittance growth
beam induced desorption: SR, ions

Generic Beam Lifetime due to Beam-Gas Interaction



results in differential equation:

$$\frac{dN_b}{dt} = -N_b \sigma \beta c n$$

σ = cross section for generic „loss process“

solution:

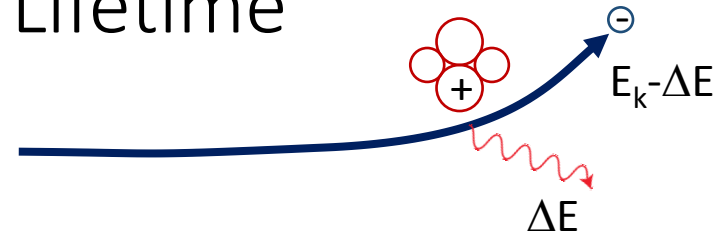
$$N_b(t) = N_0 \exp(-\sigma \beta c n t), \quad \tau \approx \frac{1}{\sigma c n}$$

specific loss processes by gas scattering

- bremsstrahlung (electrons)
- elastic scattering (Coulomb, nuclear)
- inelastic scattering (nuclear)
- multiple Coulomb: p-emittance growth



Electrons: Bremsstrahlung Lifetime



Bremsstrahlung

particle loses energy
in Coulomb field of
gas molecule;
is lost if leaving
energy acceptance

$$\sigma_{\text{inel}} \approx -\frac{4}{3} \frac{V_n}{N_A} \frac{1}{X_0} \ln \delta_E$$

V_n = 22.4l, molar Volume
 N_A Avogadro Number
 δ_E = $\Delta E/E$, energy acceptance
 X_0 gas specific radiation length

resulting lifetime:

$$\tau_{\text{brems}} [\text{h}] = \frac{-0.695}{\ln(\delta_E)} \left(\sum_i \frac{P_i [\text{pbar}]}{X_{0,i} [\text{m}]} \right)^{-1}$$

radiation length:
(normal condition)

	H ₂	He	CH ₄	H ₂ O	CO	Ar	Air
X_0 [m]	7530	5670	696	477	321	117	304

example HERA-e:

$\delta_E = 8 \times 10^{-3}$; $P_{\text{tot}} = 10^{-8}$ mbar
 composition: 75% H₂, 25% CO
 $\tau_{\text{brems}} = 16 \text{ h}$

[e.g. particle data booklet]



Electrons: Elastic Coulomb Scattering

Rutherford Scatting

diff. cross section for occurrence of scattering angle θ :

$$\frac{d\sigma_i}{d\Omega} = \frac{Z_i^2 r_e^2}{4\gamma^2} \frac{1}{\sin^4(\theta/2)}$$

consider total cross-section for loss of electron, i.e. scattering beyond aperture A_y :

$$\sigma_{i,\text{el}} \approx \frac{2\pi Z_i^2 r_e^2}{\gamma^2} \frac{1}{\theta_0^2}, \quad \theta_0 = A_y / \beta_y$$

resulting lifetime: $\tau_{\text{el}} [\text{h}] = 2839 \frac{E^2 [\text{GeV}^2] A_y^2 [\text{mm}^2]}{\beta_y^2 [\text{m}^2]} \left(\sum_i P_i [\text{pbar}] \sum_j k_{ij} Z_j^2 \right)^{-1}$

example HERA-e:

pressure: $P_{\text{tot}} = 10^{-8}$ mbar

composition: 75% H_2 , 25% CO

$Z_{\text{eff}} = \text{rms}(Z_i) = 3.6$

$A_y = 20$ mm, $\beta_{y,\text{avg}} = 25$ m

$\tau_{\text{elastic}} = 5.200$ h \rightarrow insignificant

sum over gas types and atoms per molecule



Hadron Beam Emittance Growth

multiple elastic scattering in the absence of radiation damping leads to diffusive emittance growth:

definition of emittance growth time:

$$\tau_{\varepsilon} = \left(\frac{1}{\varepsilon_x} \frac{d\varepsilon_x}{dt} \right)^{-1}$$

growth rate:

$$\frac{d\varepsilon}{dt} = \overline{\beta_y} \frac{d(\theta_0^2)}{dt} = \overline{\beta_y} \frac{(13.6)^2}{(cp)^2 [\text{MeV}^2]} \frac{c}{P_0} \sum_i \frac{P_i}{X_{0,i}}$$

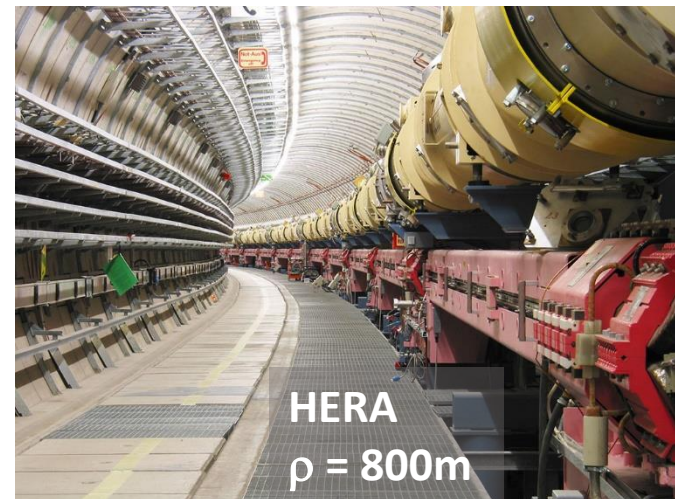
example HERA-p ε growth rate:

$E_k = 920 \text{ GeV}$, $\beta_{y,avg} = 50 \text{ m}$

$P_{\text{tot}} = 5 \times 10^{-11} \text{ mbar @ } 4.2 \text{ Kelvin, H}_2$

emittance: $\varepsilon_x = 5 \times 10^{-9} \text{ m} \cdot \text{rad}$

$\tau_{\varepsilon} = 2.000 \text{ h}$



p

e



Synchrotron Radiation induced Desorption

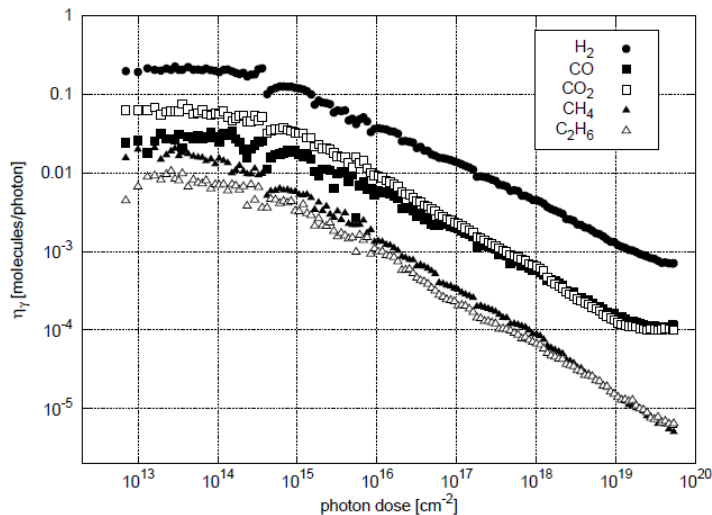
dynamic vacuum

- SR photons generate photoelectrons, these desorb gas molecules from the surface
- desorption yield η per photon is reduced with integrated dose (conditioning)

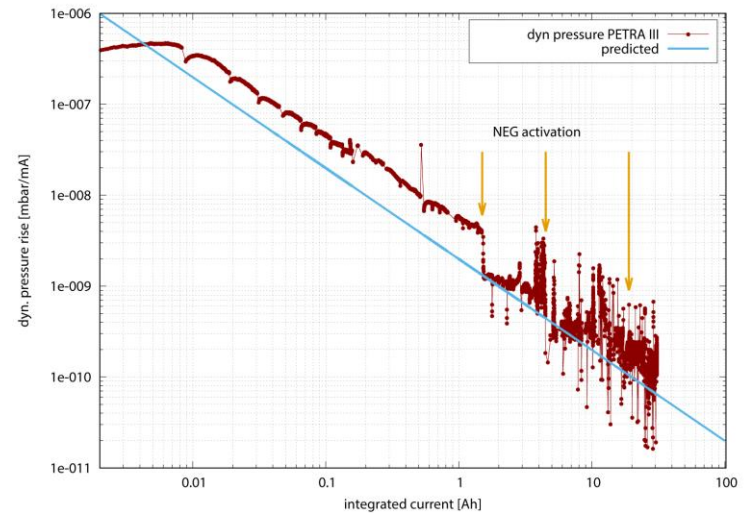
SR photons per length and time: $\frac{dN_\gamma}{dt ds} = 1.28 \cdot 10^{17} \frac{I [\text{mA}] E [\text{GeV}]}{\rho [\text{m}]}$

resulting specific outgassing: $q = \eta_\gamma k_b T \frac{dN_\gamma}{dt ds}$

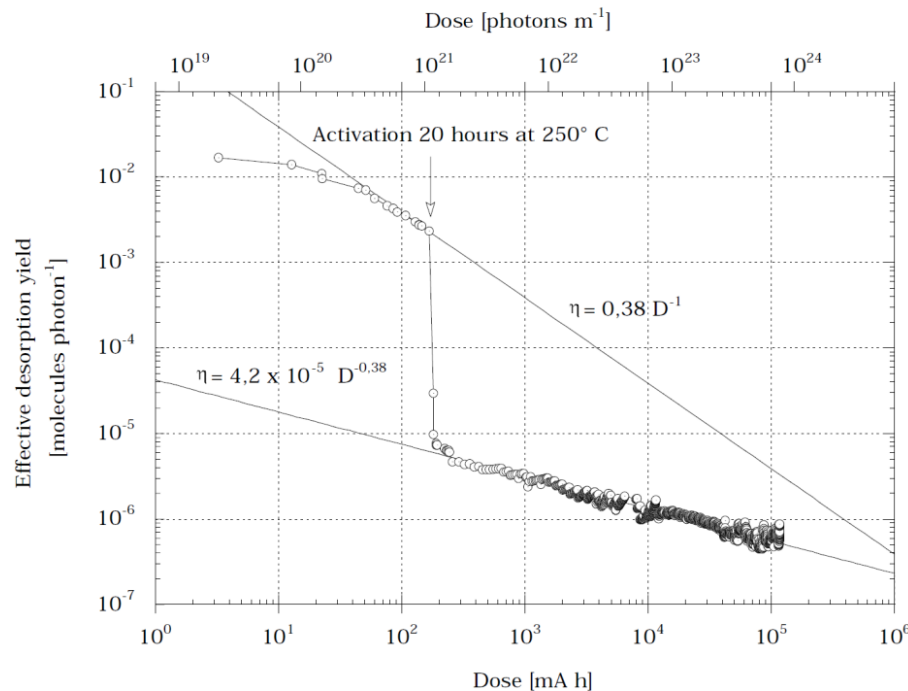
measured desorption yield for different gases
[G.Vorlaufer]



measured dynamic pressure rise as a function of integrated current [PETRA-III, DESY]



Reduced desorption by NEG Coating



- NEG coating reduces SR desorption immediately
- conditioning is slower afterwards
- however, NEG coated chambers lead to good conditions in practice

Synchrotron Radiation-Induced Desorption from a NEG-Coated Vacuum Chamber, P. Chiggiato, R. Kersevan (1999)



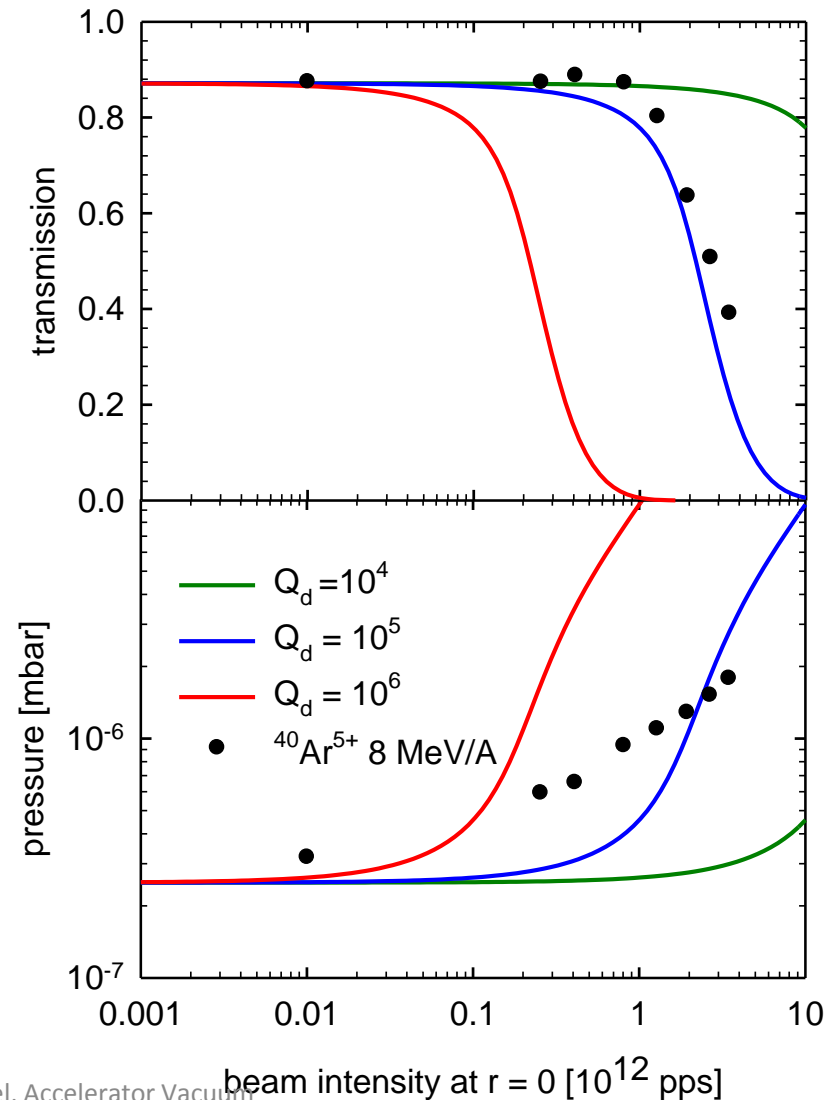
Heavy Ion induced Gas Desorption

demonstration of transmission breakdown by gas desorption

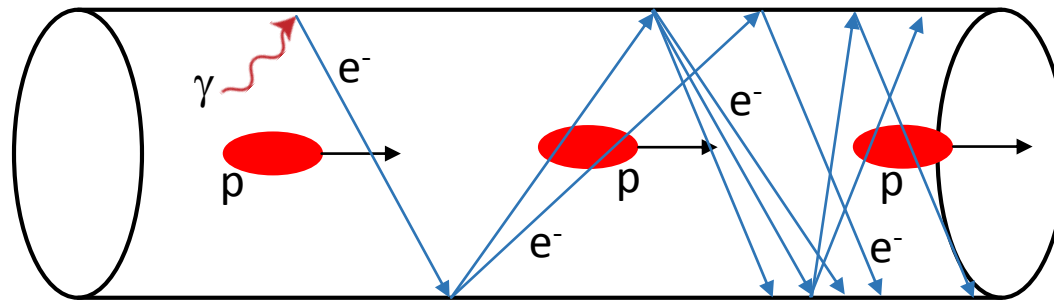
[measurements & simulations
in AGOR cyclotron, KVI-Groningen,
S.Brandenburg et al]

- transmission of $^{40}\text{Ar}^{5+}$ 8 MeV per nucleon
- base vacuum 3×10^{-7} mbar
- injected intensity up to 6×10^{12} pps
- beampower: ≤ 320 W

→ release of 10^5 (!) gas molecules
per lost ion is compatible with data



Dynamic effect in LHC: Electron Cloud Effect



$$E(e^-) \approx 1..100\text{eV}$$

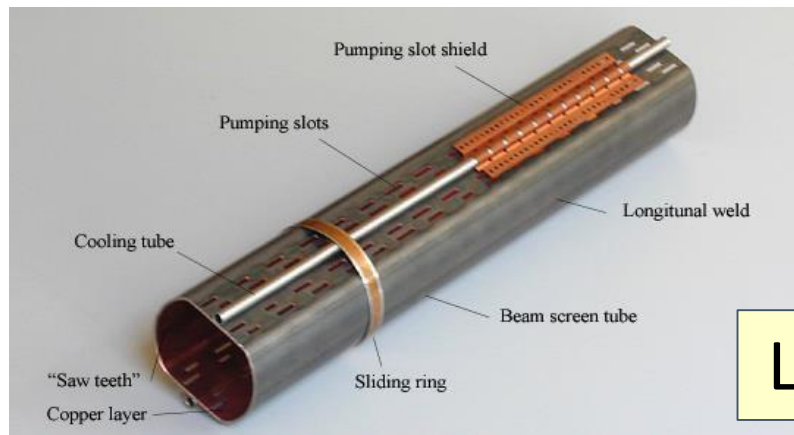
- photoelectrons can start avalanche effect resulting in intense electron clouds
- crucial: secondary electron yield (SEY), i.e. how many e^- released per incoming e^-
- results in pressure bump, heat load in cold systems (problem at LHC)
- may affect beam stability
- depends on bunch spacing and beam intensity

mitigations:

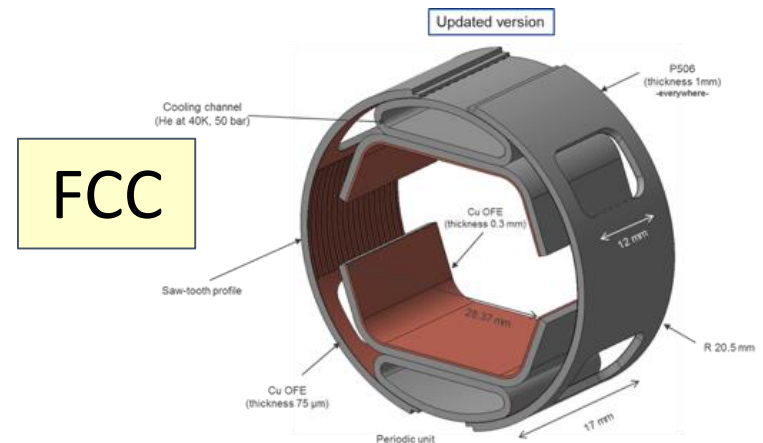
- wall coating, e.g. graphite, TiN (low SEY)
- weak magnetic solenoid field



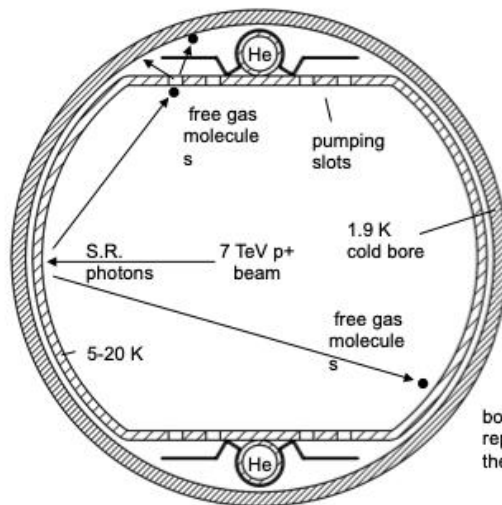
Specialized Chambers: LHC & FCC with Beam Screens



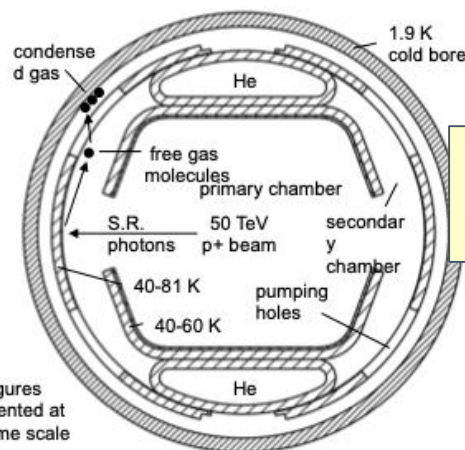
LHC



FCC



LHC - 173 l/(s·m) for H_2 at 5 K
0.22 W/m emitted SR



FCC-hh - 898 l/(s·m) for H_2 at 40 K
35.4 W/m emitted SR

LHC(left), FCC
comparison

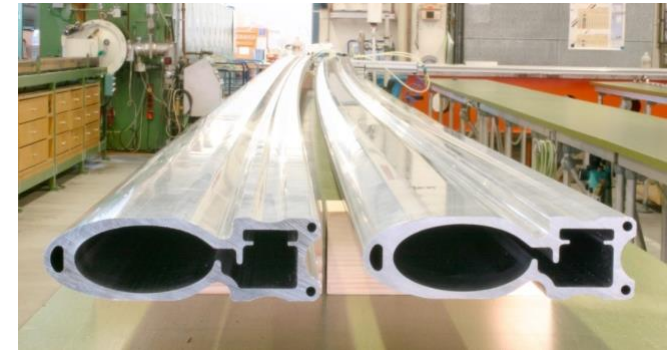
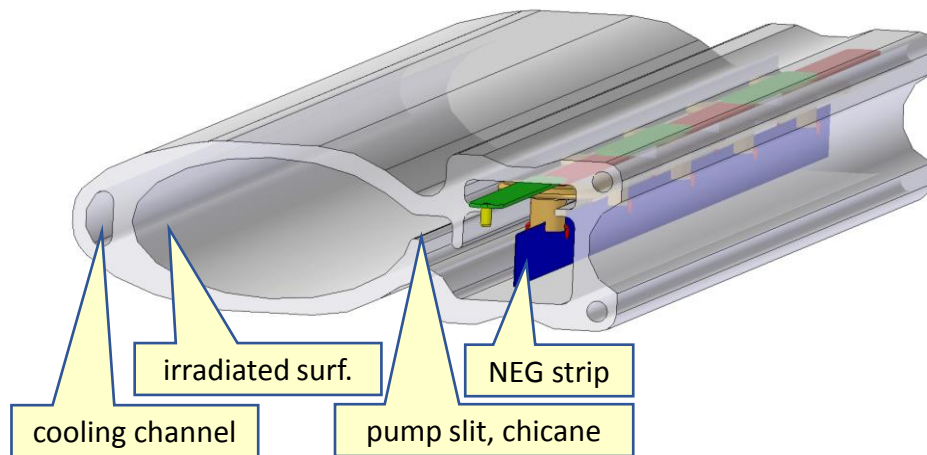
courtesy images:
M.Jimenez et al
F.Perez, M.Morrone, I.Bellafont et al

- At the expense of a **higher complexity** (translated into a higher, but still affordable, cost) the beam induced vacuum effects are mitigated and the **pumping speed** and cooling capacity have been **considerably increased**



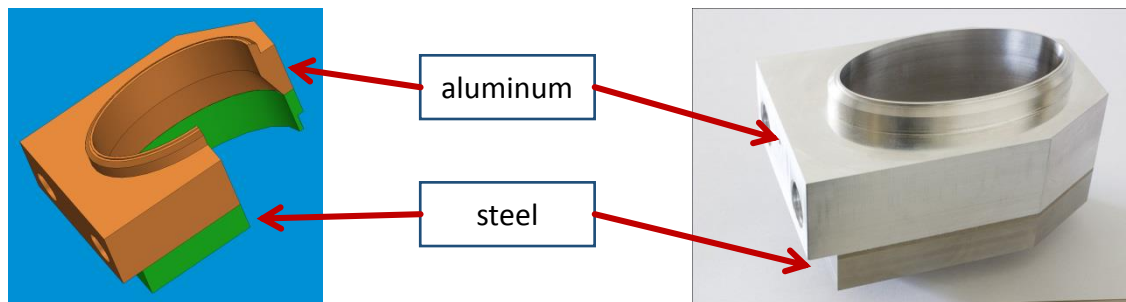
Vacuum Chambers for Electron Synchrotron

profile extruded aluminum, milled and bent
($\rho=196\text{m}$); NEG strip (St707) for pumping



low cost per meter,
however: difficult interface to
stainless steel flanges

solution:
explosion bondings SS/Al with
4cm Al thickness

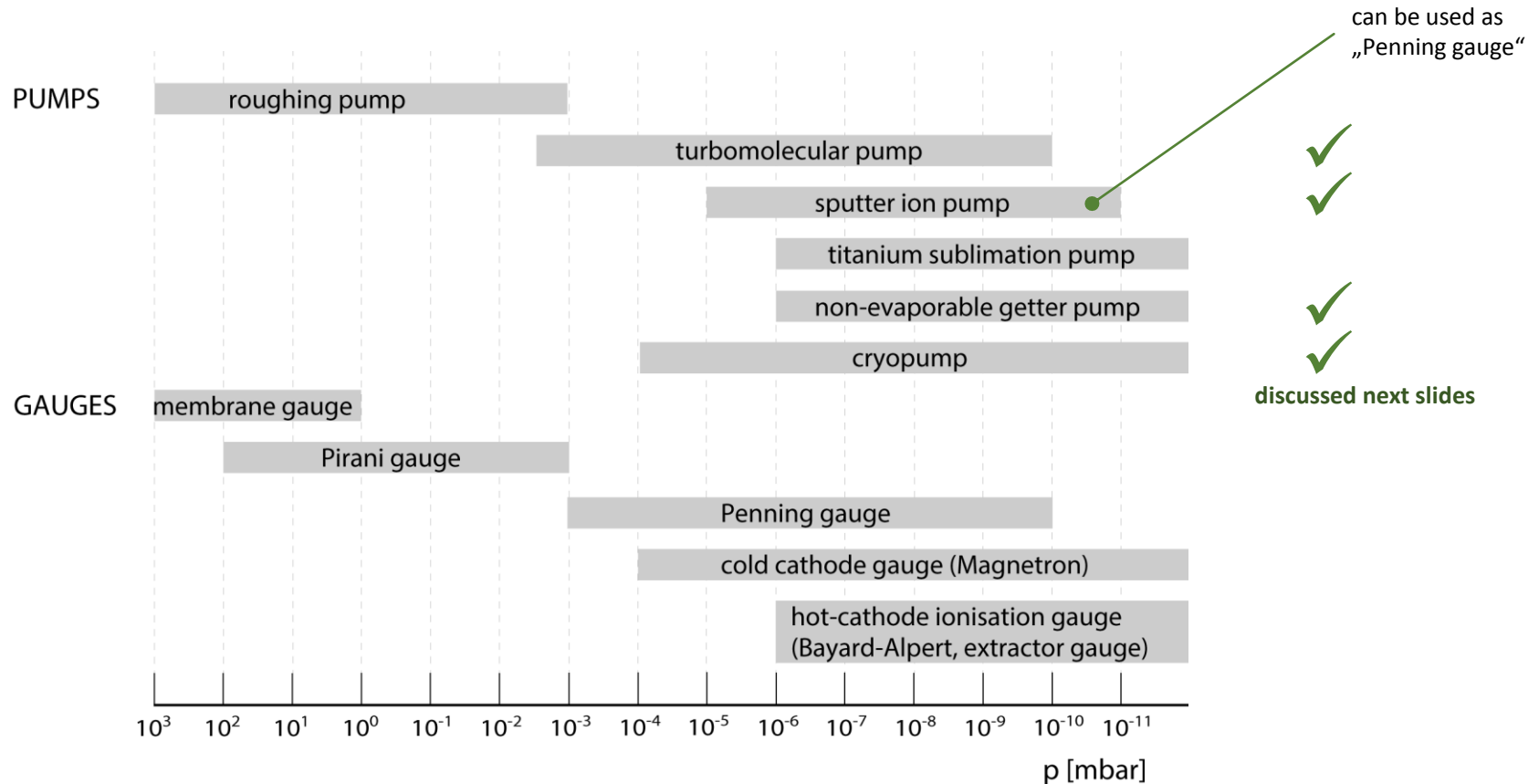


Next:

Components for Vacuum Systems

pumps: overview, turbo, ion sputter, NEG, cryo-pump
flange systems, collimators, residual gas analysis (RGA)

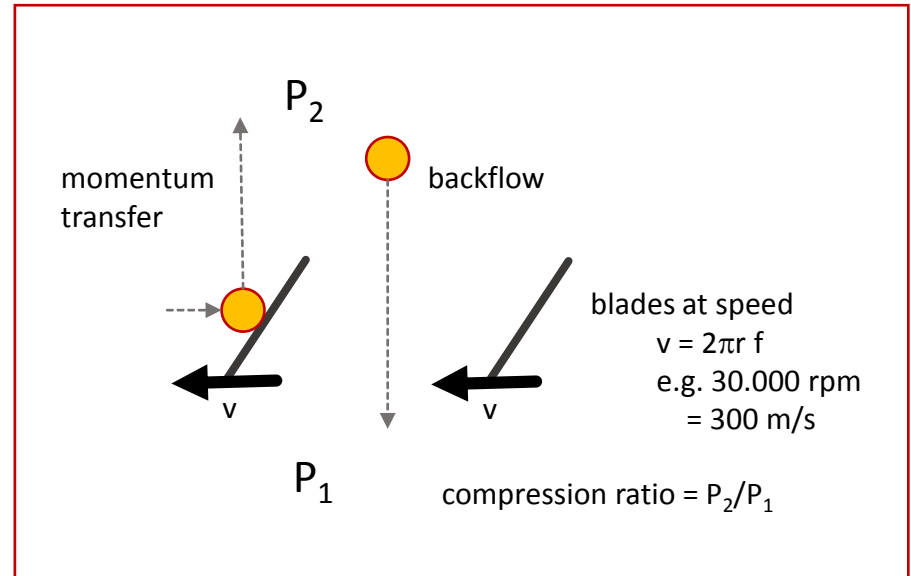
Overview Pumps and Gauges



Turbo Molecular Pump



Wikipedia



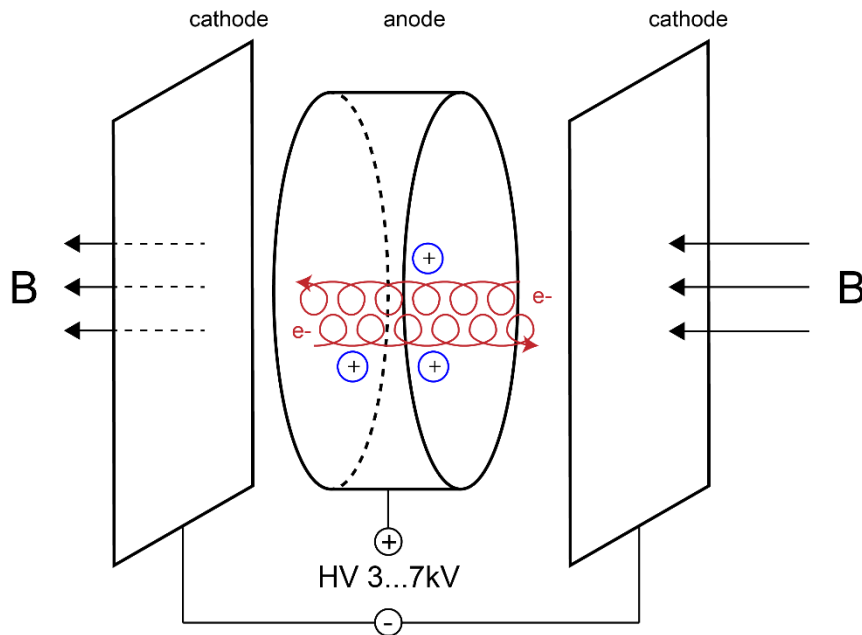
- pumps all gases
- blade speed similar molecule speed(!)
- 30.000 ... 60.000 RPM
- works down to 10^{-10} mbar

molecule	avg speed @ 293K [m/s]	compression ratio
H ₂	1800	10^3
He	1250	10^4
CO	470	10^9



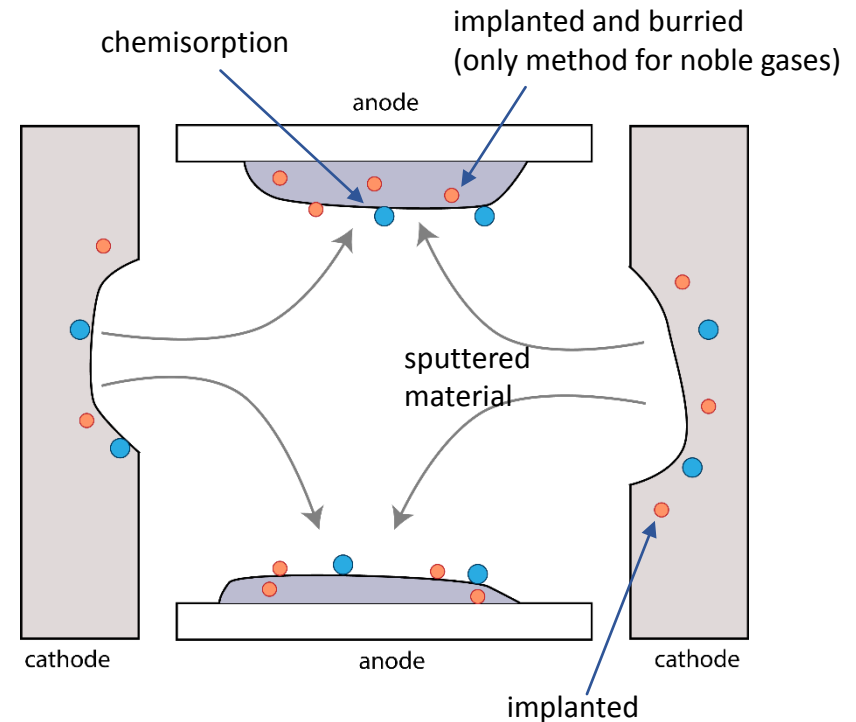
Sputter Ion Pump

single penning cell
electric and magnetic field
gas ionization, acceleration



current is proportional to P
→ can be used as pressure gauge

pumping mechanism
implantation, chemisorption and
burying of gas molecules



Ion Sputter Pumps



courtesy Agilent catalog

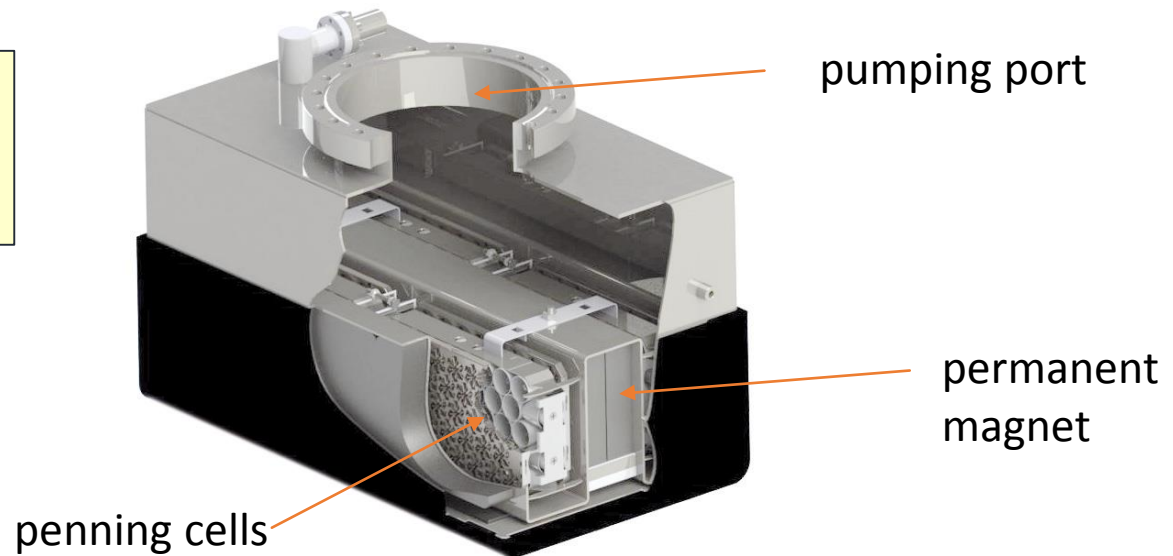
pumping speed:

2 l/s ... 500l/s

weight:

0.3kg ... 120kg

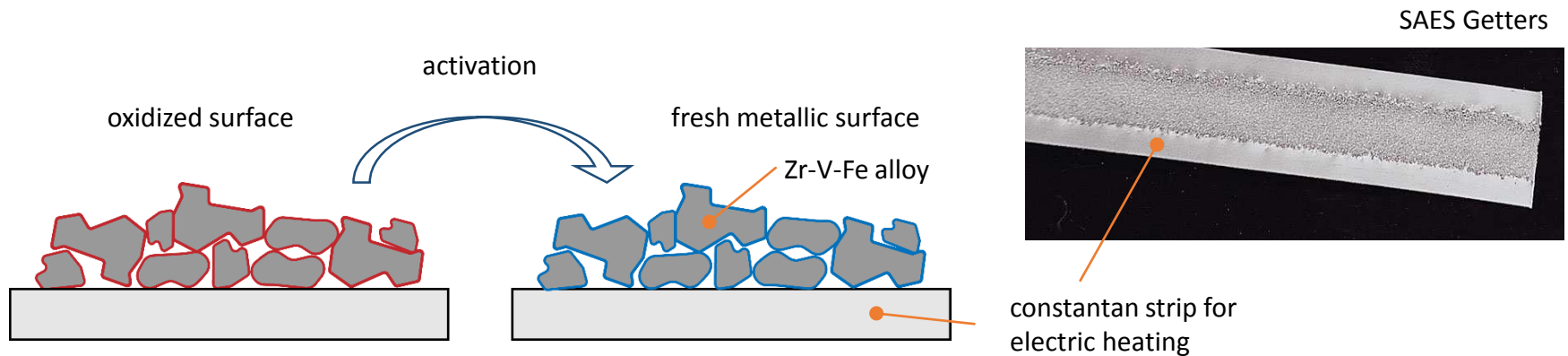
example:
modern Agilent 200
pump



NEG – Non Evaporable Getter Pumps

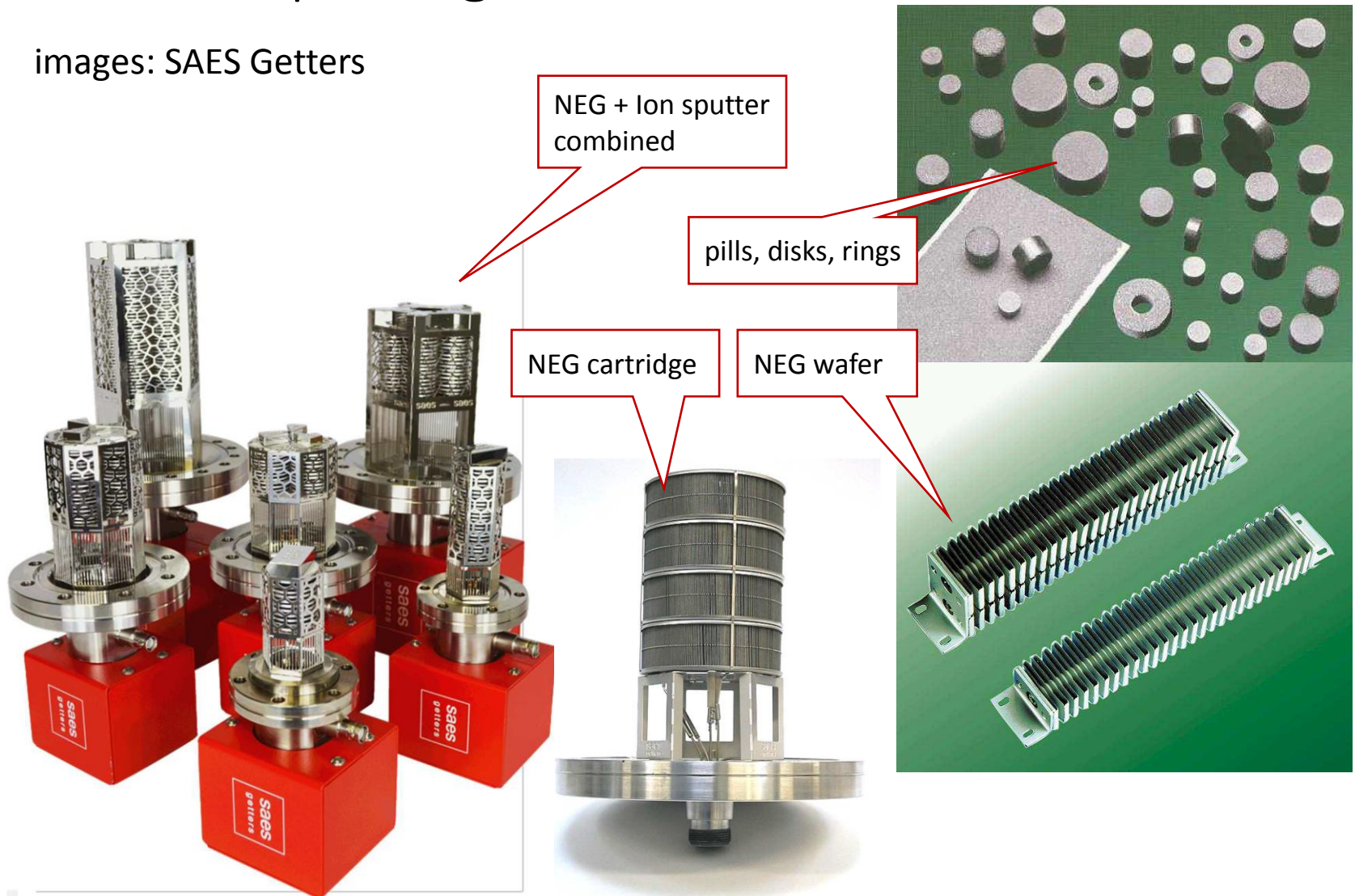
- NEG captures gases by chemical reaction, e.g. H_2O , CO , N_2 permanently, H_2 is dissolved in bulk material
- no pumping of noble gases – combination with sputter ion pumps required
- NEG must be activated by heating

e.g. St707™ @180°C..350°C

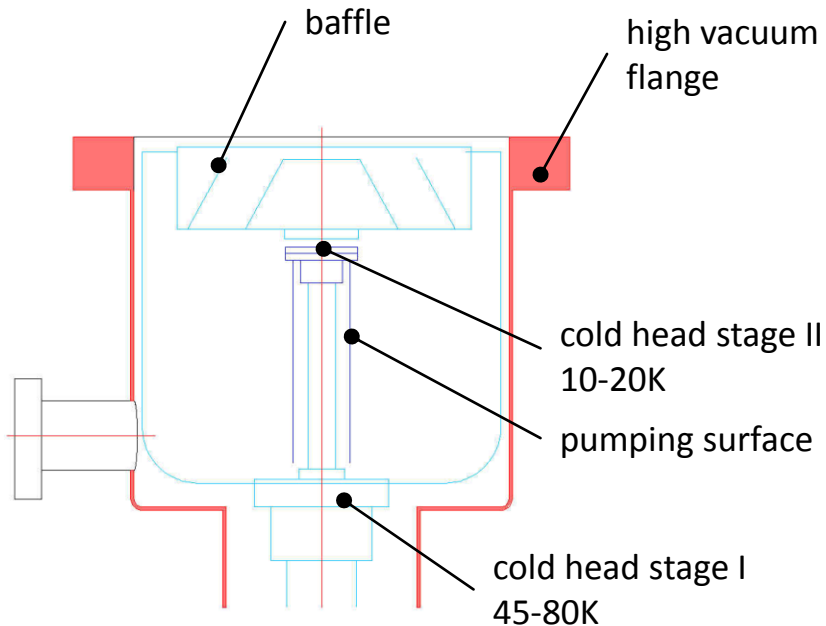


NEG Pump Designs

images: SAES Getters



Cryo Pump



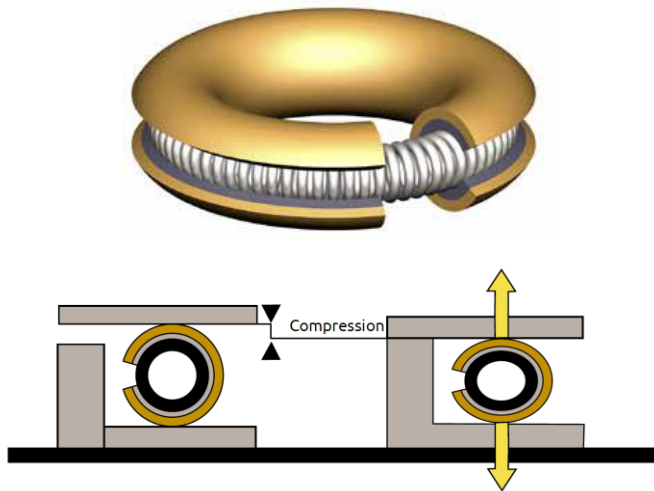
[Lothar Schulz]

- high pumping speed for all gases
- cryo-condensation of N_2 , O_2 and Ar on cold surface
- cold surface partly covered with charcoal: cryosorption for H_2 , He, Ne
- periodic regeneration by warmup

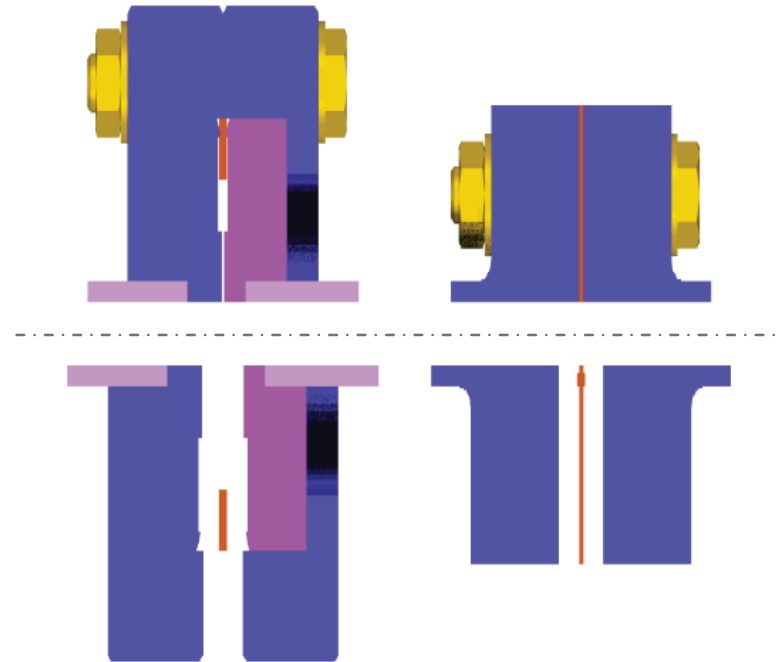


Metal sealed Flange Systems

- low leak rate, UHV compatible
- radiation proof
- safe mounting
- easy leak search



Helicoflex: Technetics Group



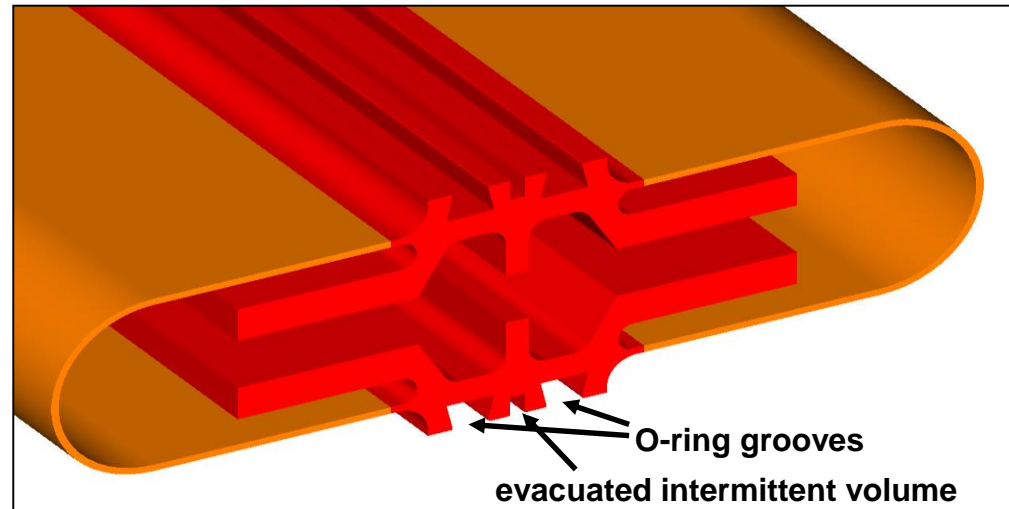
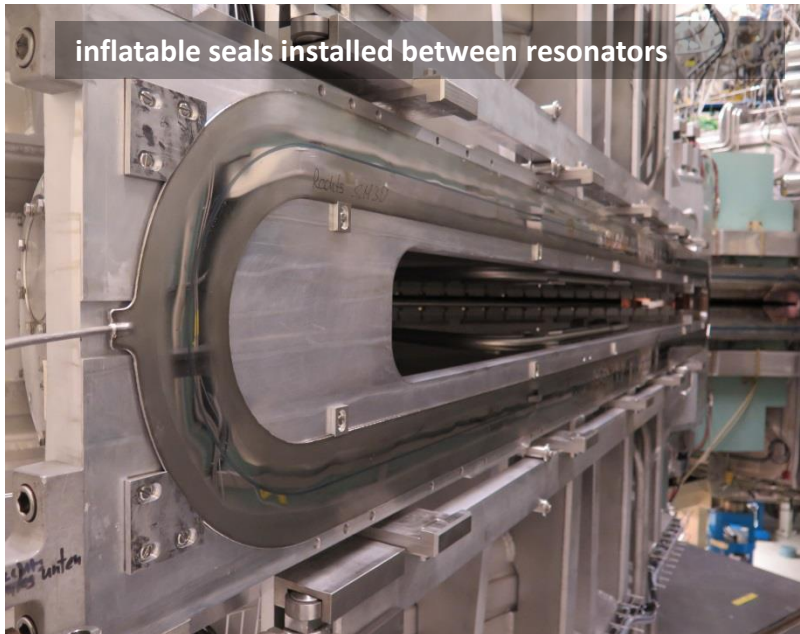
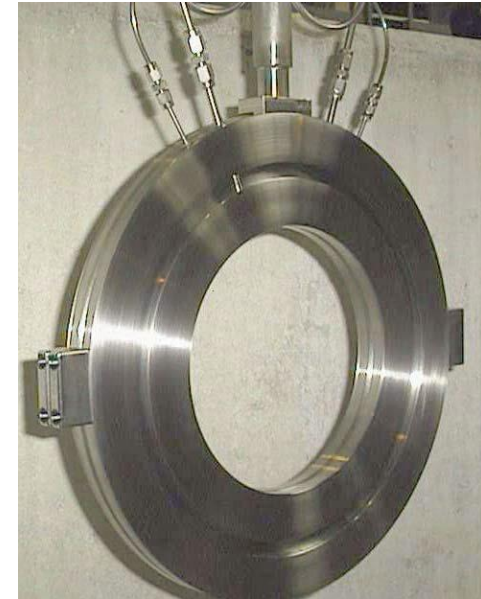
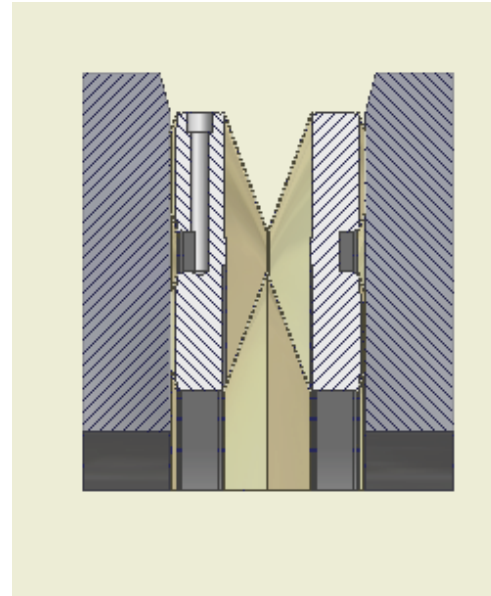
Conflat Flange (CF)

VAT Flange, flat seal



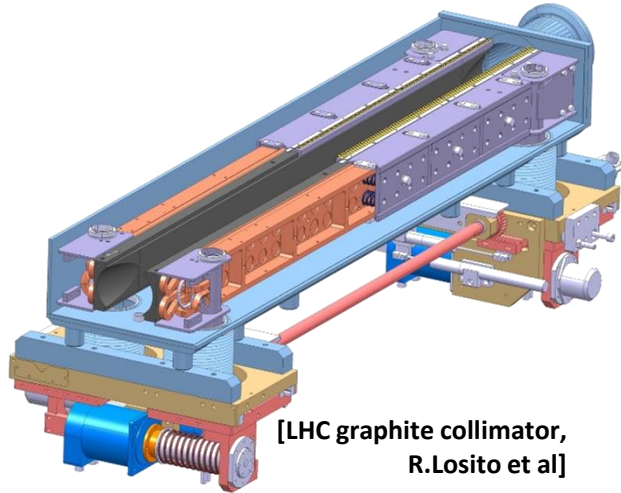
Inflatable Seals

- leak rate $\sim 10^{-6}$ mbar l / s
- quick and simple mounting
- at positions with limited access or high activation

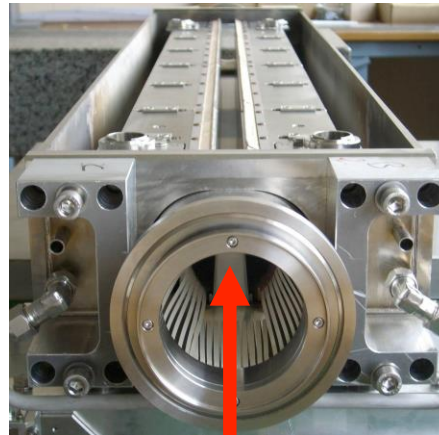


Collimators

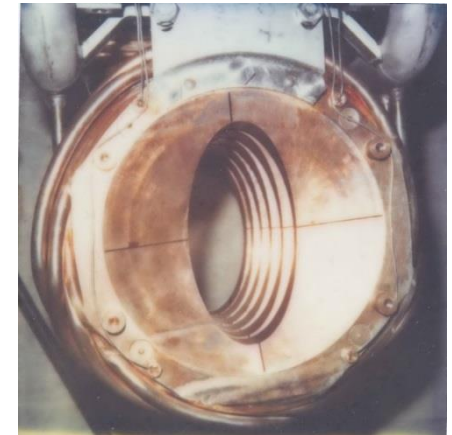
- collimators are parts of the vacuum system with multi-physics aspects
- some materials are not optimal for vacuum, e.g. graphite or graphite with MoGr coating (porosity, outgassing, dust)
- straightness, thermal shock resistance, heat load and heat conductivity, efficient cooling, thermal outgassing, electrical conductivity, mechanical precision and reproducibility, radio-activation and handling



[LHC collimator,
S.Radaelli et al]

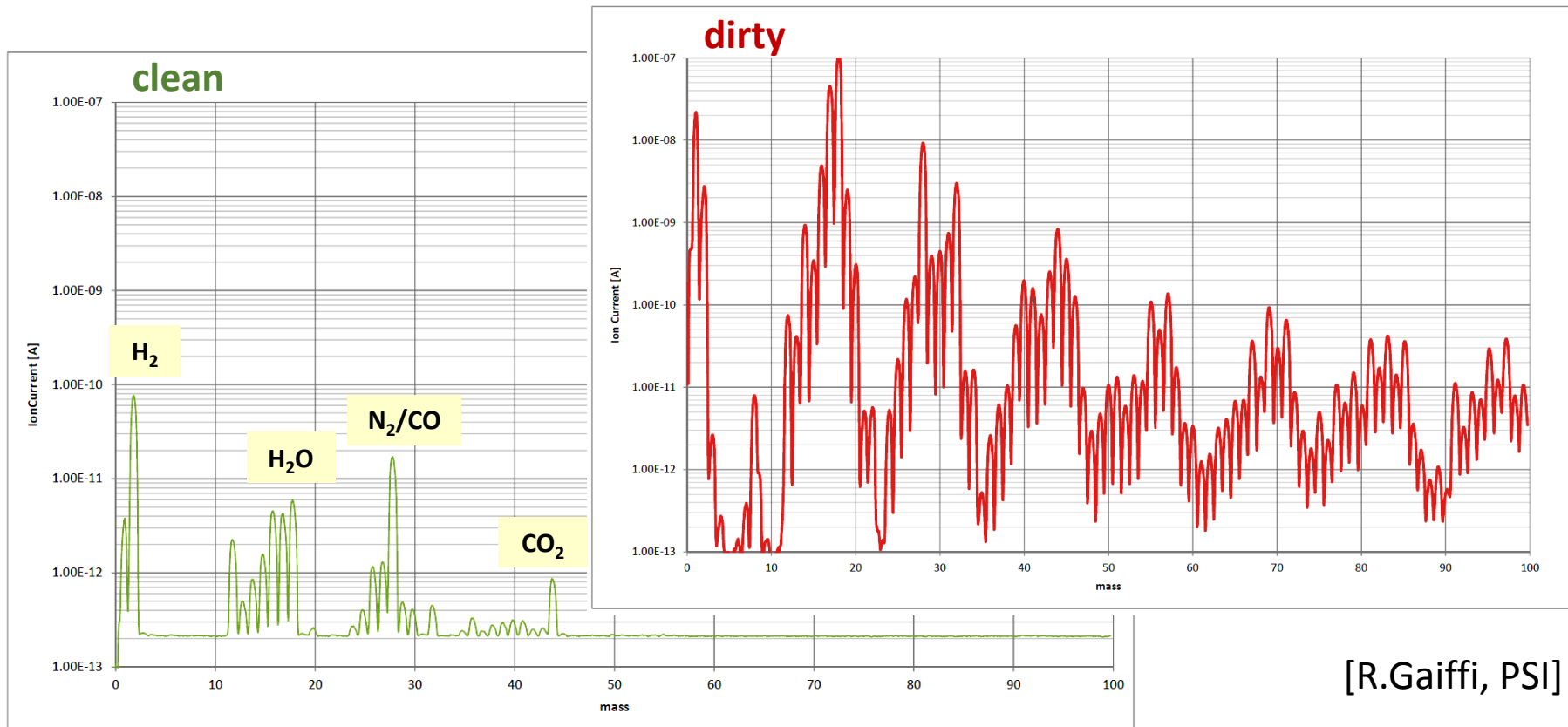


[PSI-HIPA >100kW avg
power, D.Kiselev et al]



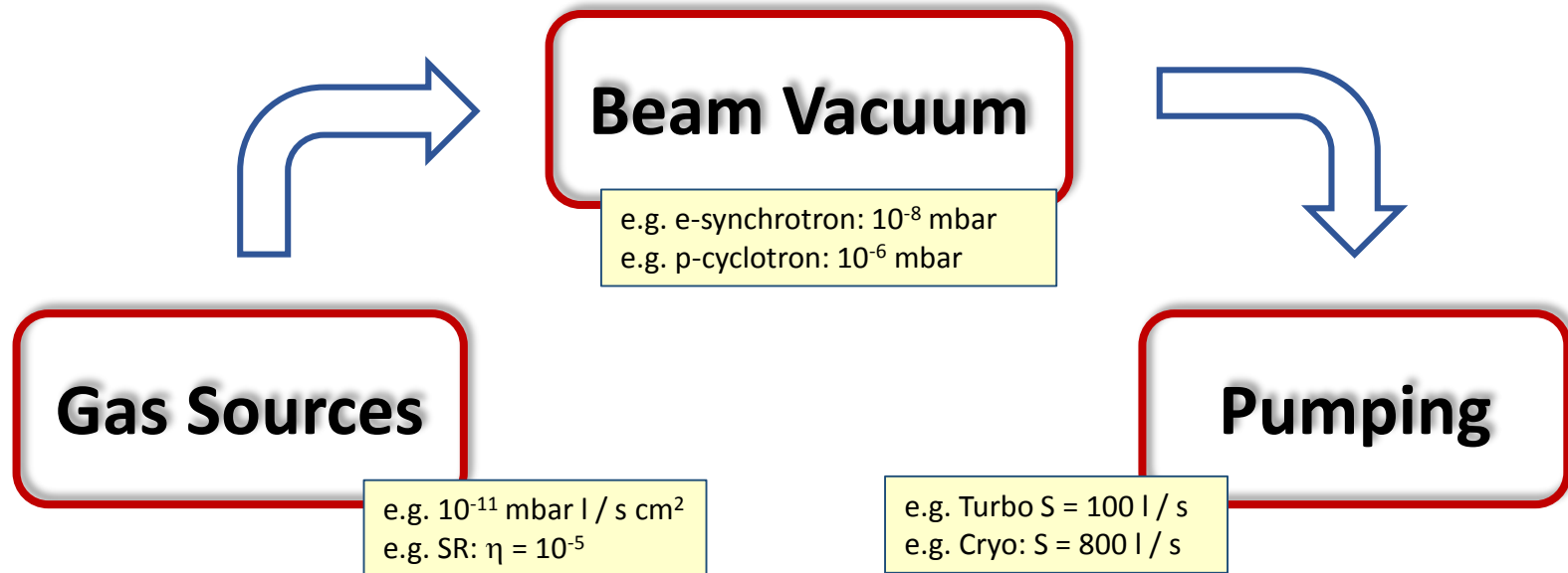
Residual Gas Analysis (RGA)

- quadrupole mass spectrometers to analyze the composition of residual gases
- allows to assess the cleanliness of components and to diagnose problems



Accelerator Vacuum - Summary

- e: bremsstrahlung
- p: emittance growth



- outgassing, permeation/leaks
- beam induced: SR, ions, electron cloud

- lumped: turbo, ion sputter, cryo
- NEG strips, NEG coating

vacuum engineering:

materials & materials preparation, mechanical stability, thermomechanical problems
Pumps, Gauges, Flange Systems, Valves



References

- dedicated CERN accelerator school on vacuum:
<https://cas.web.cern.ch/schools/glumslov-2017>
- The physical basis of ultra-high vacuum, P.A. Redhead, J.P. Hobson, E.V. Kornelsen. AVS.
- Particle Data Group: [Atomic and Nuclear Properties of Materials](#) (radiation length X_0 , interaction length etc)

