

# RF Systems II

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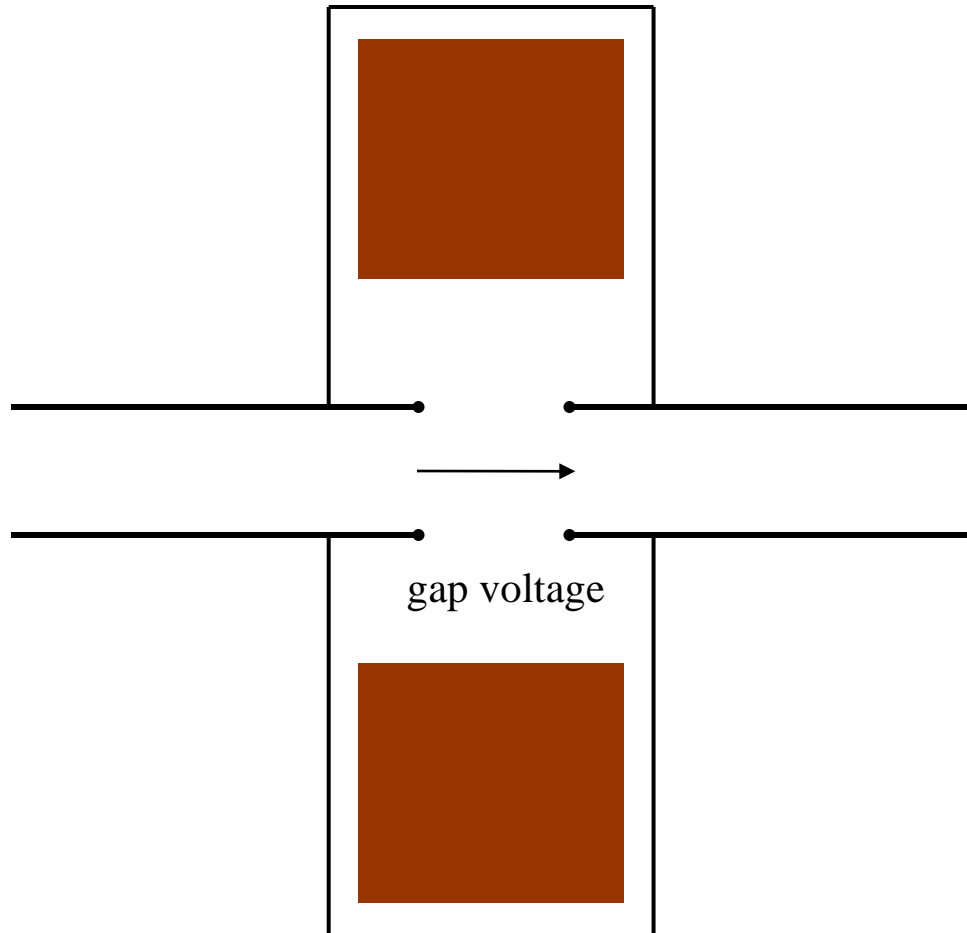


The CERN Accelerator School

**Introduction to Accelerator Physics, Prague, Czech Republic, 31 Aug – 12 Sept 2014**

# Accelerating gap

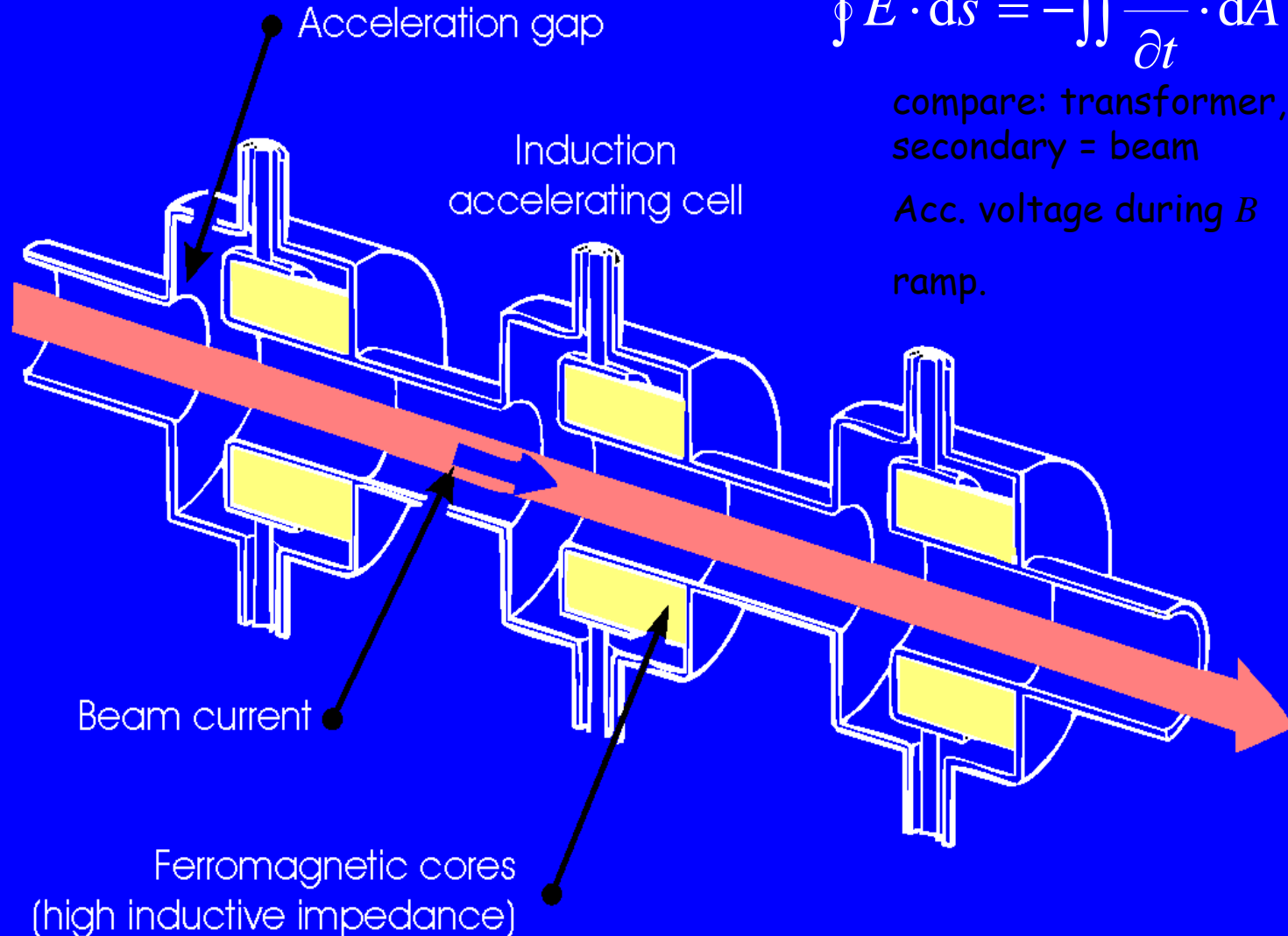
# Accelerating Gap



- We want a voltage across the gap!
- It cannot be DC, since we want the beam tube on ground potential.
- Use  $\oint \vec{E} \cdot d\vec{s} = - \iint \frac{d\vec{B}}{dt} \cdot d\vec{A}$
- The “shield” imposes a
  - upper limit of the voltage pulse duration or – equivalently –
  - a lower limit to the usable frequency.
- The limit can be extended with a material which acts as “open circuit”!
- Materials typically used:
  - ferrites (depending on  $f$ -range)
  - magnetic alloys (MA) like Metglas®, Finemet®, Vitrovac®...
- resonantly driven with RF (ferrite loaded cavities) – or with pulses (induction cell).

# Linear induction accelerator

Linear induction accelerator

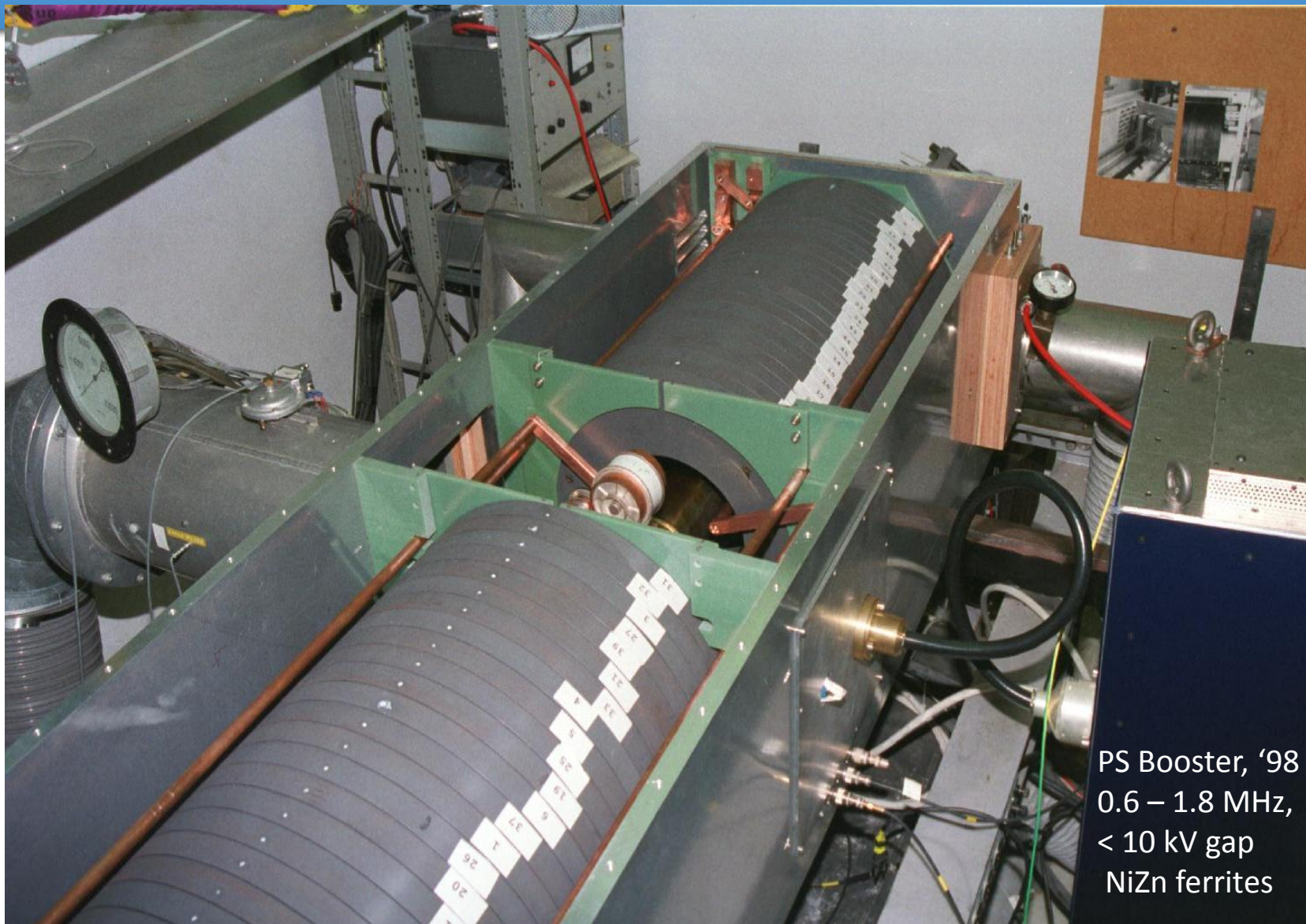


$$\oint \vec{E} \cdot d\vec{s} = -\iint \frac{\partial \vec{B}}{\partial t} \cdot d\vec{A}$$

compare: transformer,  
secondary = beam

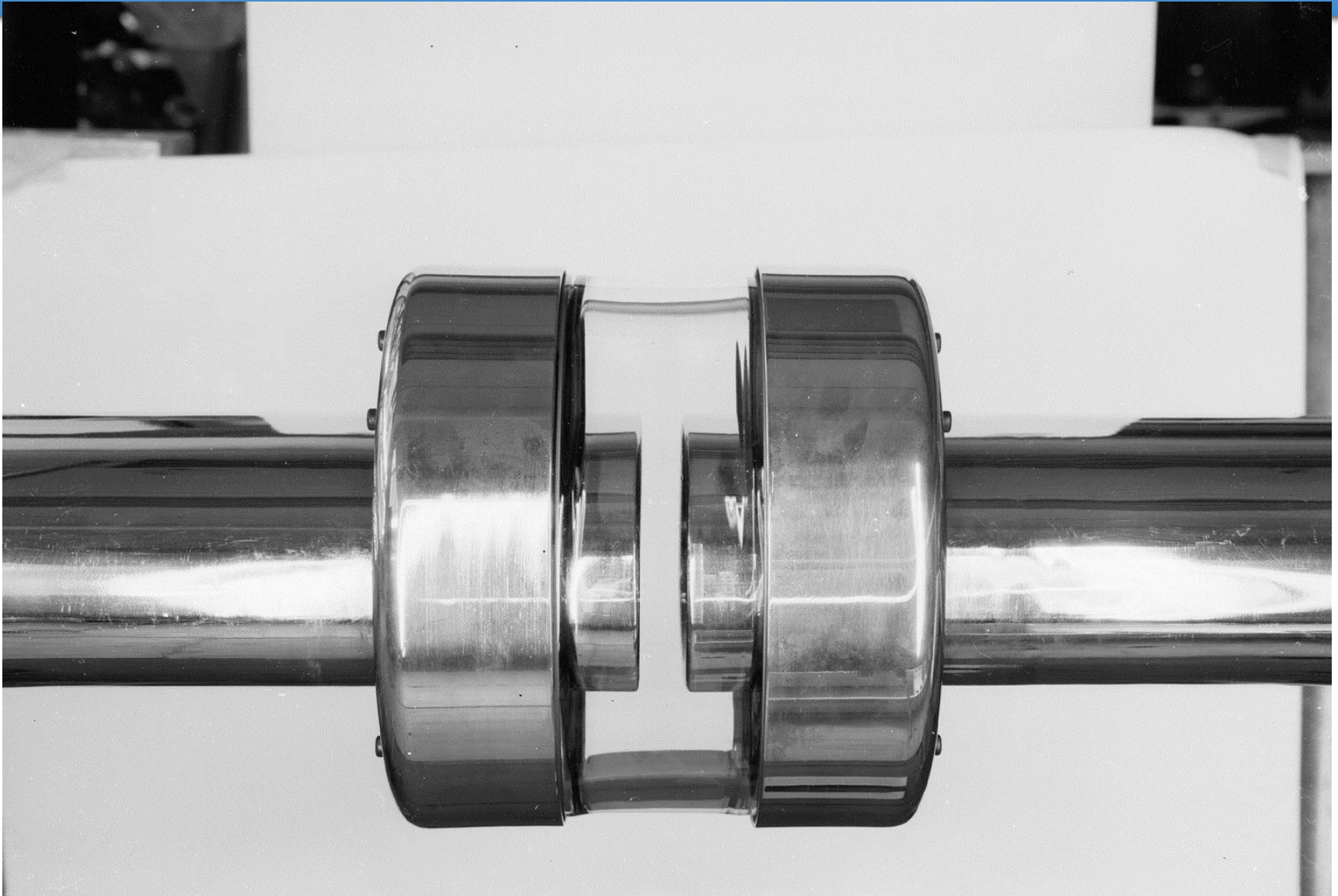
Acc. voltage during  $B$   
ramp.

# Ferrite cavity



PS Booster, '98  
0.6 – 1.8 MHz,  
< 10 kV gap  
NiZn ferrites

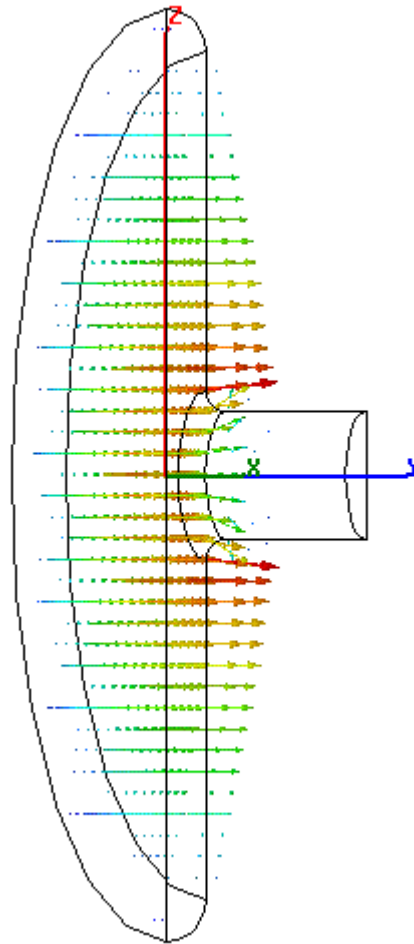
# Gap of PS cavity (prototype)



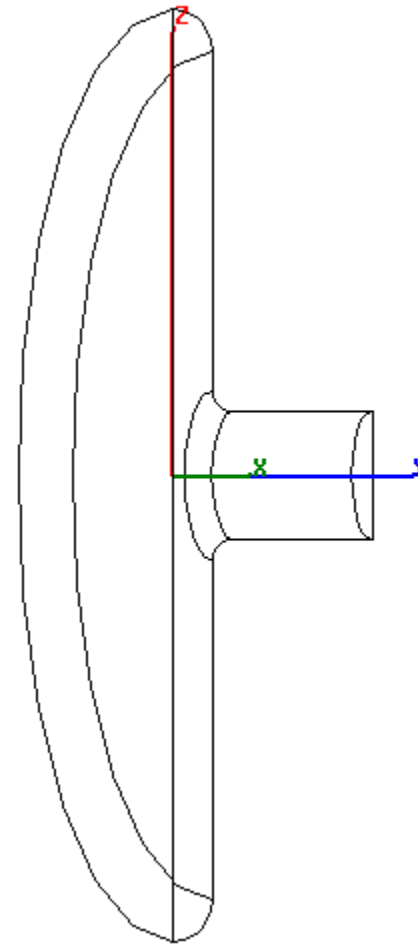
# Characterizing a cavity

# Reminder: The pillbox cavity

TM<sub>010</sub>-mode (only 1/4 shown)



electric field



magnetic field



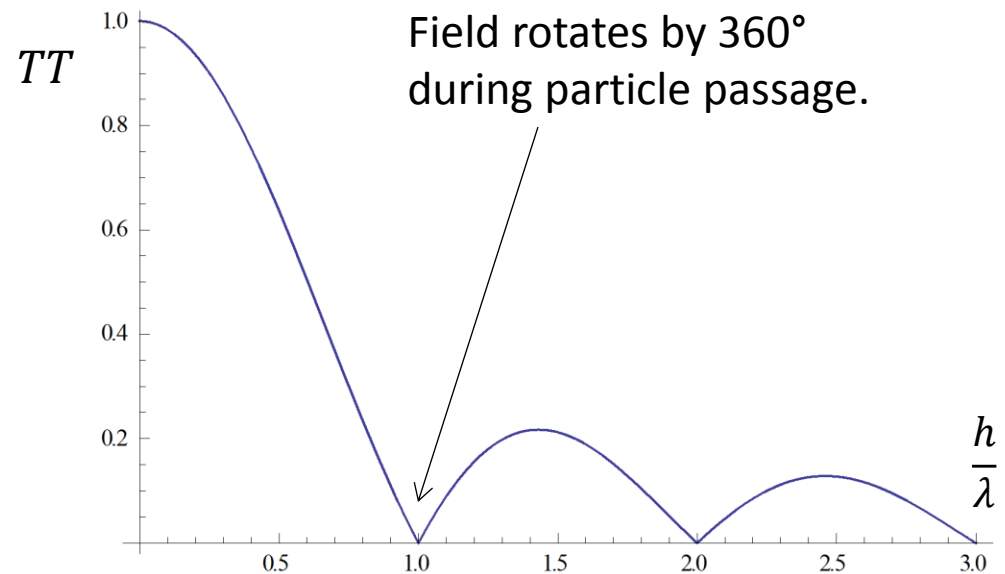
# Transit time factor

The transit time factor is the ratio of the acceleration voltage to the (non-physical) voltage a particle with infinite velocity would see.

$$TT = \frac{|V_{acc}|}{|\int E_z dz|} = \frac{|\int E_z e^{j\frac{\omega}{\beta c}z} dz|}{|\int E_z dz|}$$

The transit time factor of an ideal pillbox cavity (no axial field dependence) of height (gap length)  $h$  is:

$$TT = \sin\left(\frac{\chi_{01}h}{2a}\right) / \left(\frac{\chi_{01}h}{2a}\right)$$



# Stored energy

- The energy stored in the electric field is

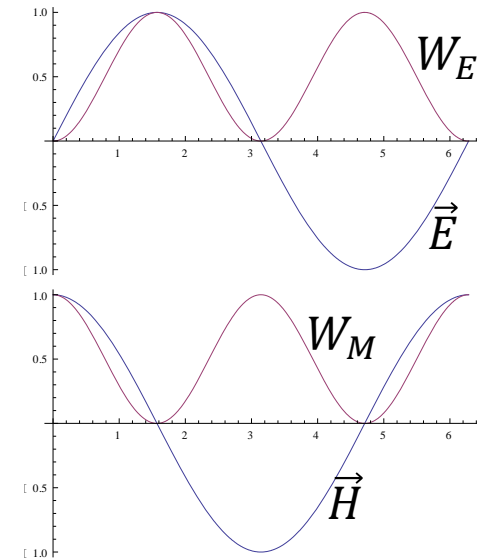
$$W_E = \iiint_{cavity} \frac{\epsilon}{2} |\vec{E}|^2 dV.$$

- The energy stored in the magnetic field is

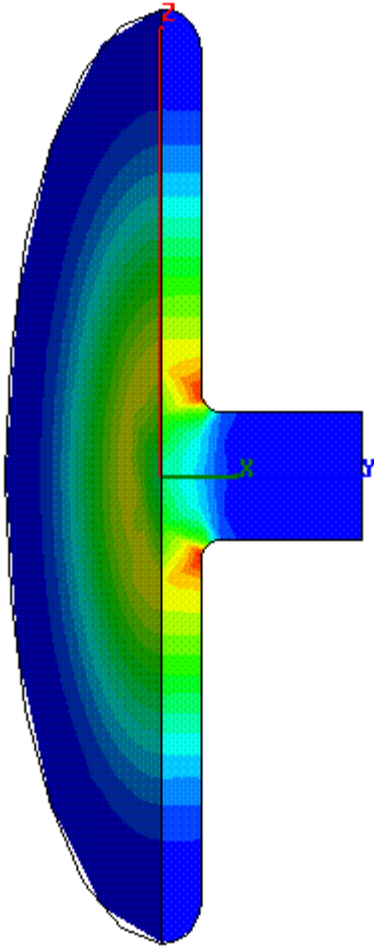
$$W_M = \iiint_{cavity} \frac{\mu}{2} |\vec{H}|^2 dV.$$

- Since  $\vec{E}$  and  $\vec{H}$  are  $90^\circ$  out of phase, the stored energy continuously swaps from electric energy to magnetic energy. On average, electric and magnetic energy must be equal.
- In steady state, the Poynting vector describes this energy flux.
- In steady state, the total energy stored (constant) is

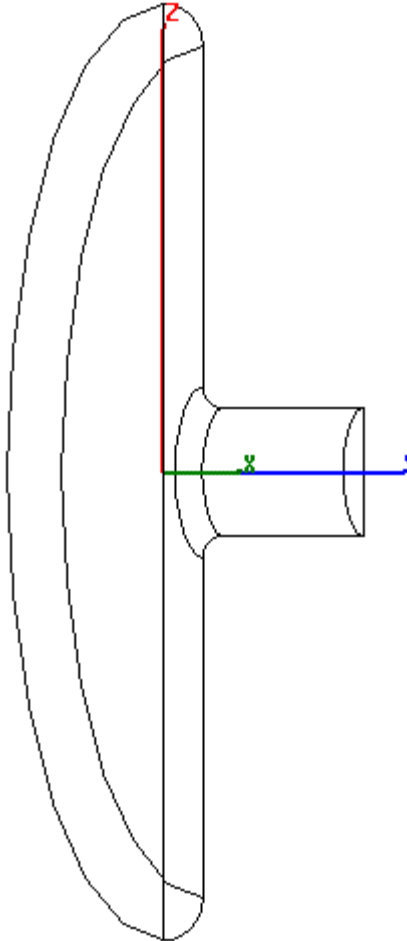
$$W = \iiint_{cavity} \left( \frac{\epsilon}{2} |\vec{E}|^2 + \frac{\mu}{2} |\vec{H}|^2 \right) dV.$$



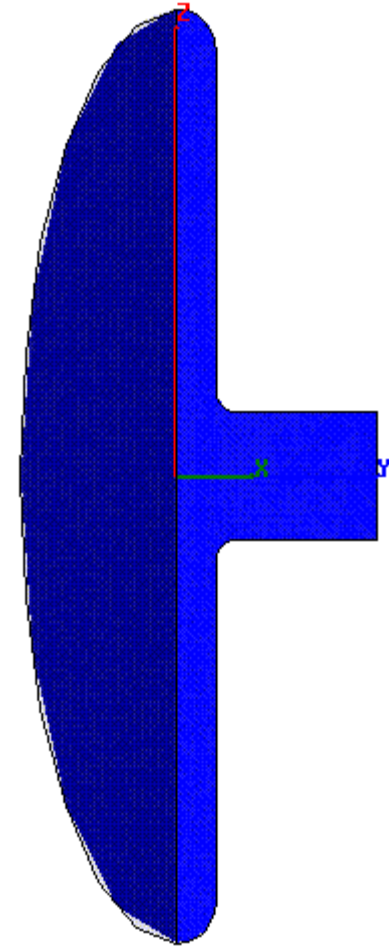
# Stored energy and Poynting vector



electric field energy



Poynting vector



magnetic field energy

# Wall losses (valid for good conductor)

- The losses  $P_{loss}$  are proportional to the stored energy  $W$ .
- The tangential magnetic field on the metallic surface is linked to a surface current  $\vec{J}_A = \vec{n} \times \vec{H}$  (flowing in the skin depth).
- This surface current  $\vec{J}_A$  sees a surface resistance  $R_A = \sqrt{\frac{\omega\mu}{2\sigma}}$ , resulting in a local power density flowing into the wall of  $R_A |H_t|^2$ .
- $R_A$  is related to skin depth  $\delta$  as  $\delta\sigma R_A = 1$ .
- The total wall losses result from

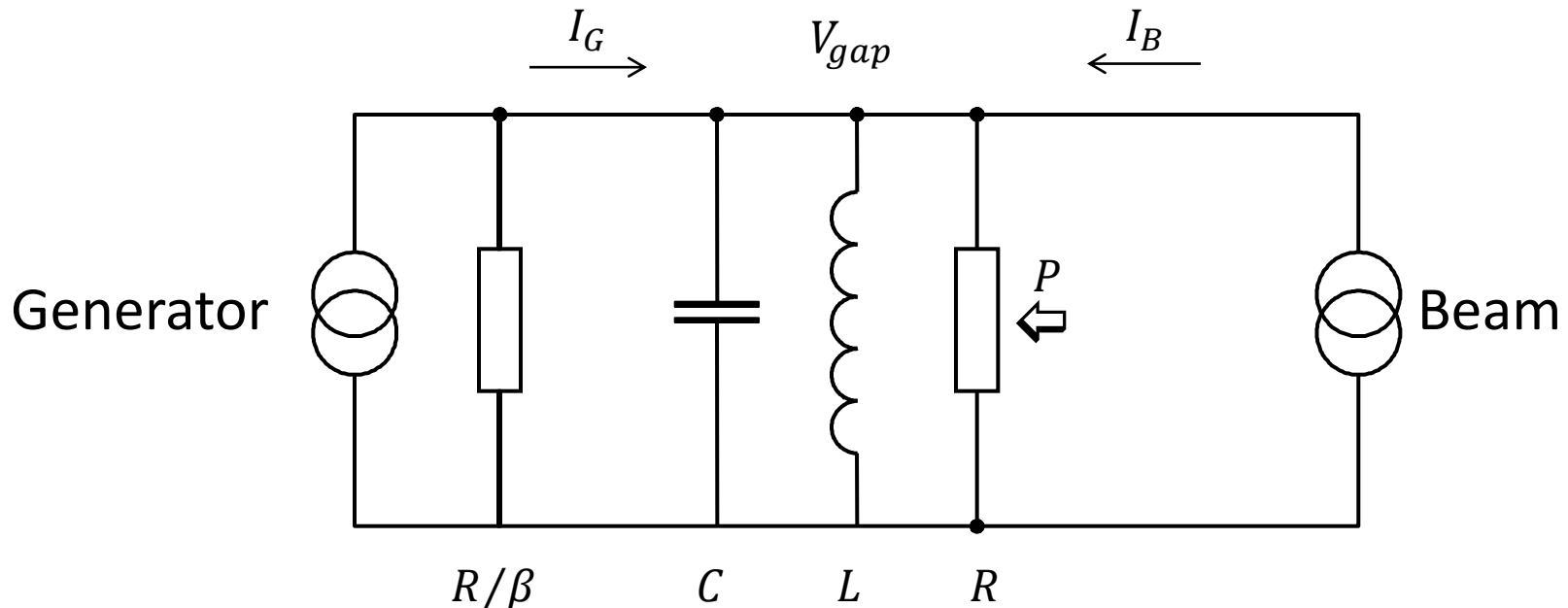
$$P_{loss} = \iint_{wall} R_A |H_t|^2 dA$$

- The cavity  $Q$  (caused by wall losses) is defined as

$$Q = \frac{\omega_0 W}{P_{loss}}$$

# Cavity resonator – equivalent circuit

Simplification: single mode



$\beta$ : coupling factor

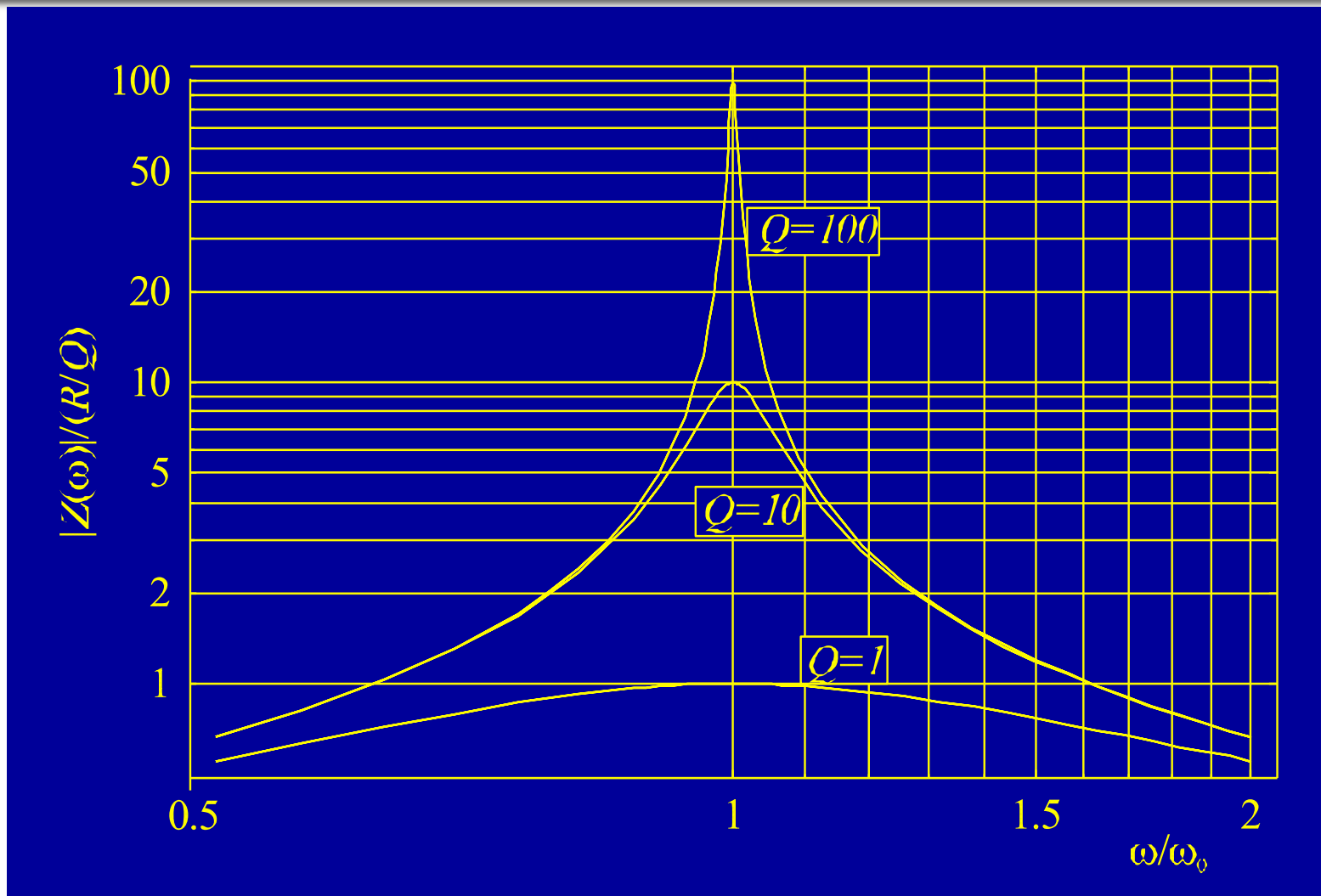
$R$ : shunt impedance

$$\sqrt{L/C} = \frac{R}{Q}: \text{R-upon-Q}$$

Cavity

We have used this before  
when explaining the “fast  
feedback”

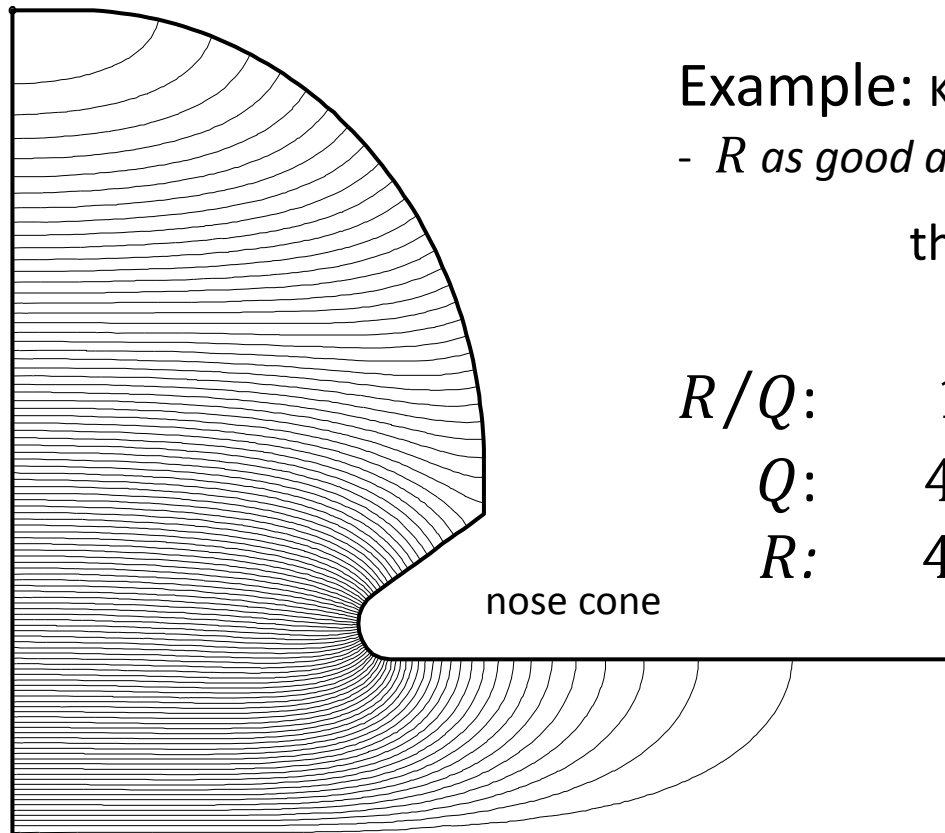
# Resonance



# Reentrant cavity

Nose cones increase the transit time factor, round outer shape minimizes losses.

Nose cone example Freq = 500.003

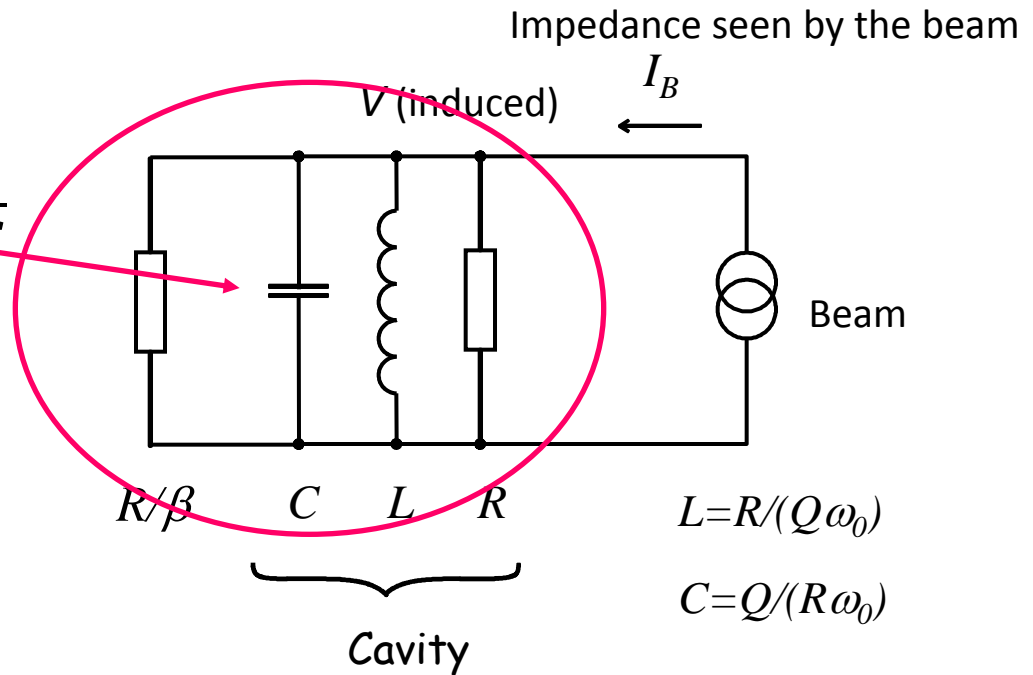


**Example:** KEK photon factory 500 MHz  
- *R as good as it gets* -

	this cavity	optimized pillbox
$R/Q$ :	111 $\Omega$	107.5 $\Omega$
$Q$ :	44,270	41,630
$R$ :	4.9 M $\Omega$	4.47 M $\Omega$

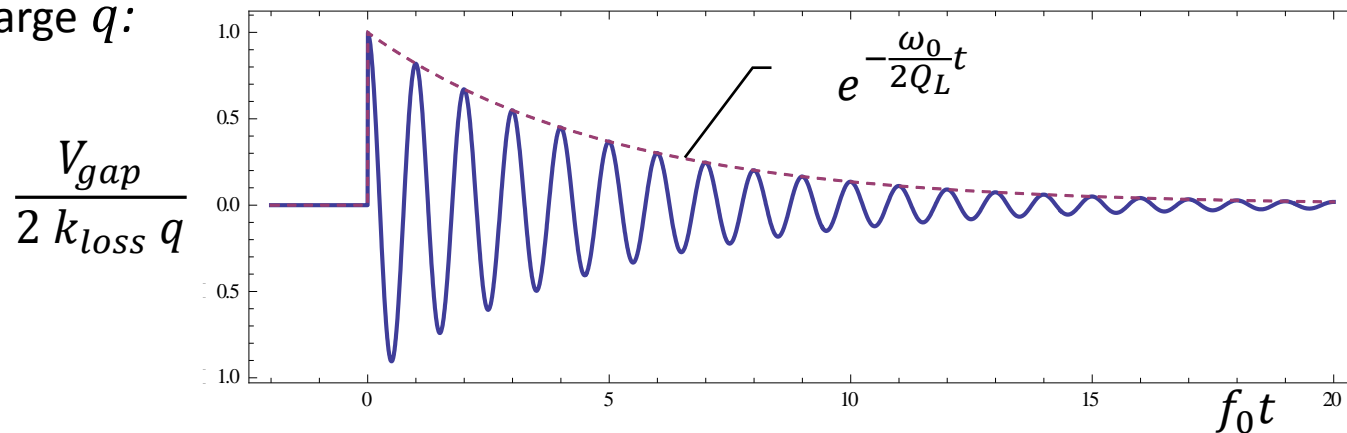
# Loss factor

$$k_{loss} = \frac{\omega_0}{2} \left( \frac{R}{Q} \right) = \frac{|V_{gap}|^2}{4W} = \frac{1}{2C}$$



Energy deposited by a single charge  $q$ :  $k_{loss}q^2$

Voltage induced by a single charge  $q$ :





# Summary: relations $V_{gap}$ , $W$ , $P_{loss}$

$V_{gap}$   
gap voltage

$$\frac{R}{Q} = \frac{|V_{gap}|^2}{2\omega_0 W}$$

$$k_{loss} = \frac{\omega_0 R}{2} \frac{R}{Q} = \frac{|V_{gap}|^2}{4W}$$

$$R = \frac{|V_{gap}|^2}{2P_{loss}}$$

$W$   
Energy stored

$P_{loss}$   
wall losses

$$Q = \frac{\omega_0 W}{P_{loss}}$$

# Let's talk about RF → beam efficiency!

- With zero beam current, RF power fed into the cavity excites a gap voltage, but it will be entirely lost in the cavity walls; this is characterized by the shunt impedance  $R$ :

$$|V_{acc}| = \frac{1}{2} \left( \sqrt{(4P)R} \right)$$

- A non-zero beam current induces a voltage reducing the gap voltage\*); this is known as **beam loading** and normally considered a disadvantage.

$$|V_{acc}| = \frac{1}{2} \left( \sqrt{(4P + I_{beam}^2 R)R} - I_{beam} R \right)$$

- But: if we define the RF to beam efficiency as “increase of beam power” divided by “RF input power”, we find that large efficiency can be obtained only with large beam loading (at the expense of reduced accelerating voltage).
- Example: CLIC drive beam accelerated with 98% RF to beam efficiency.

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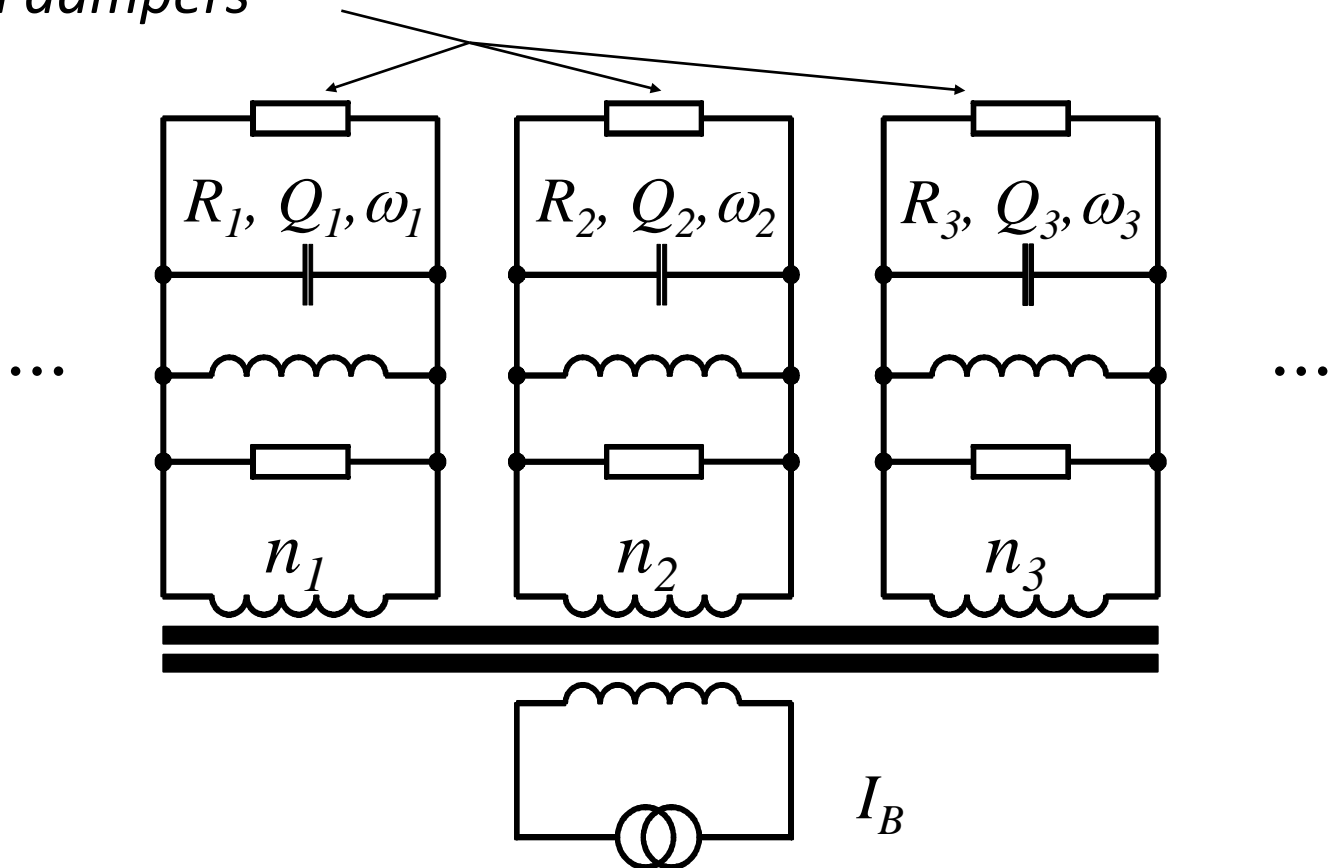
\*) for an accelerated beam! For a decelerated beam the voltage is increased

# Cavity parameters

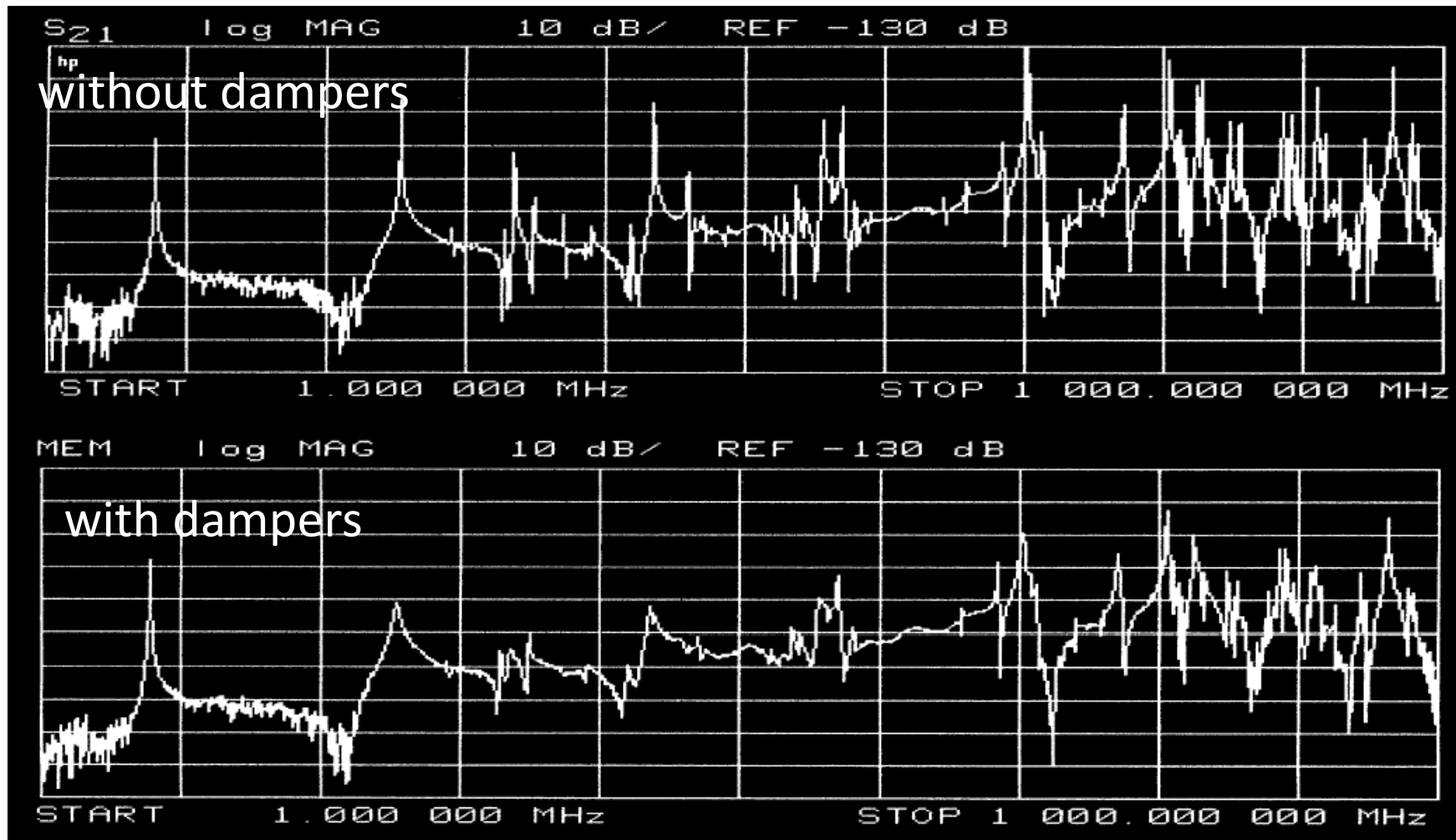
Resonance frequency	$\omega_0 = \frac{1}{\sqrt{L \cdot C}}$	
Transit time factor	$TT = \frac{\left  \int E_z e^{j \frac{\omega}{\beta c} z} dz \right }{\left  \int E_z dz \right }$	
Q factor	$\omega_0 W = Q P_{loss}$	
	<b>Circuit definition</b>	<b>Linac definition</b>
Shunt impedance	$ V_{gap} ^2 = 2 R P_{loss}$	$ V_{gap} ^2 = R P_{loss}$
R/Q (R-upon-Q)	$\frac{R}{Q} = \frac{ V_{gap} ^2}{2 \omega_0 W} = \sqrt{L/C}$	$\frac{R}{Q} = \frac{ V_{gap} ^2}{\omega_0 W}$
Loss factor	$k_{loss} = \frac{\omega_0 R}{2 Q} = \frac{ V_{gap} ^2}{4W} = \frac{1}{2C}$	$k_{loss} = \frac{\omega_0 R}{4 Q} = \frac{ V_{gap} ^2}{4W}$

# Higher order modes (HOM's)

*external dampers*

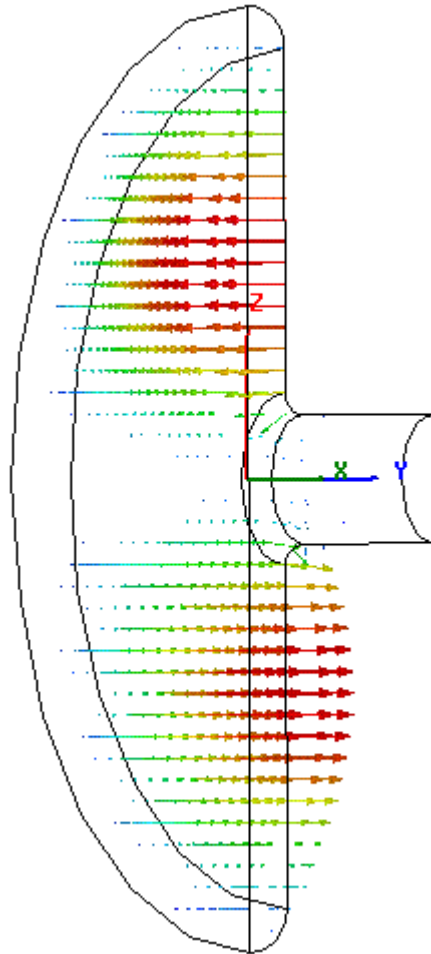


# HOM (measured spectrum)

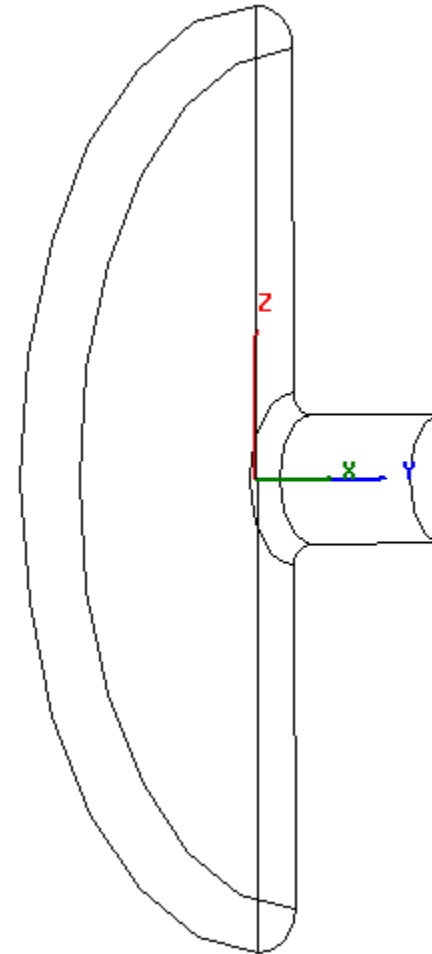


# Dipole mode in a pillbox

TM<sub>110</sub>-mode (only 1/4 shown)

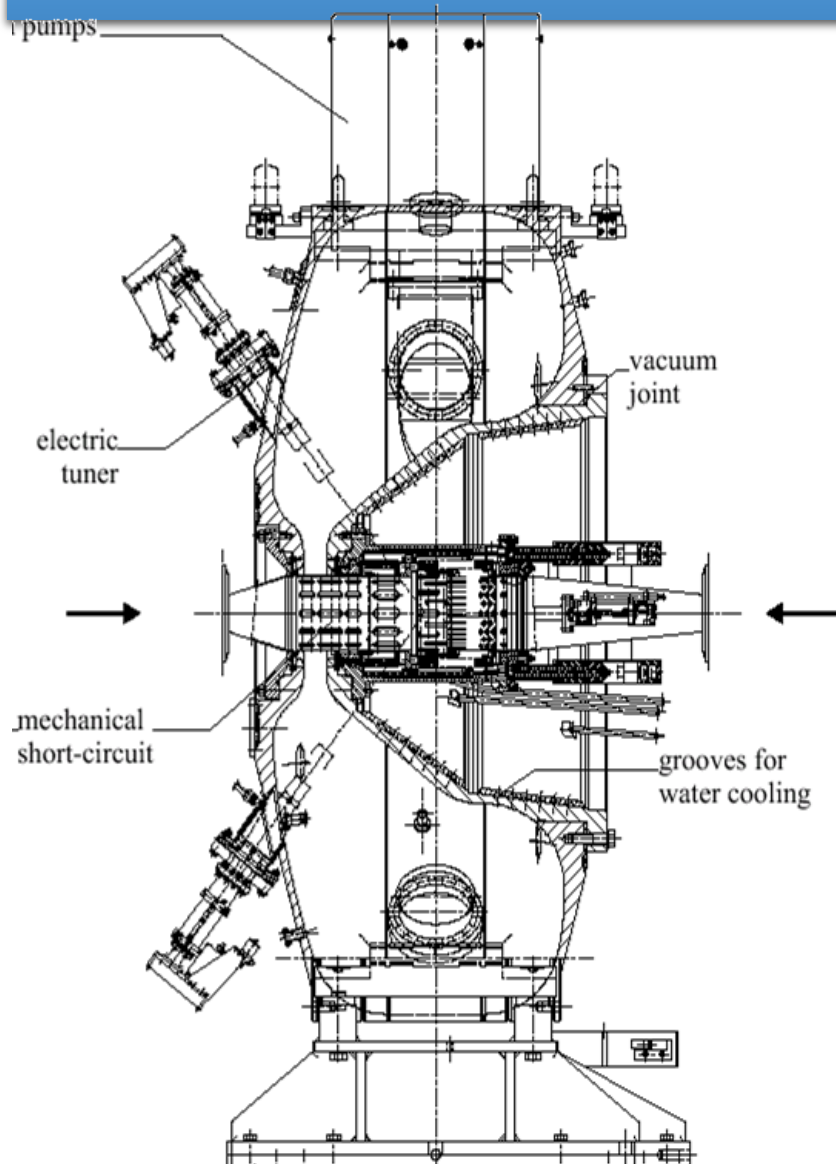


electric field



magnetic field

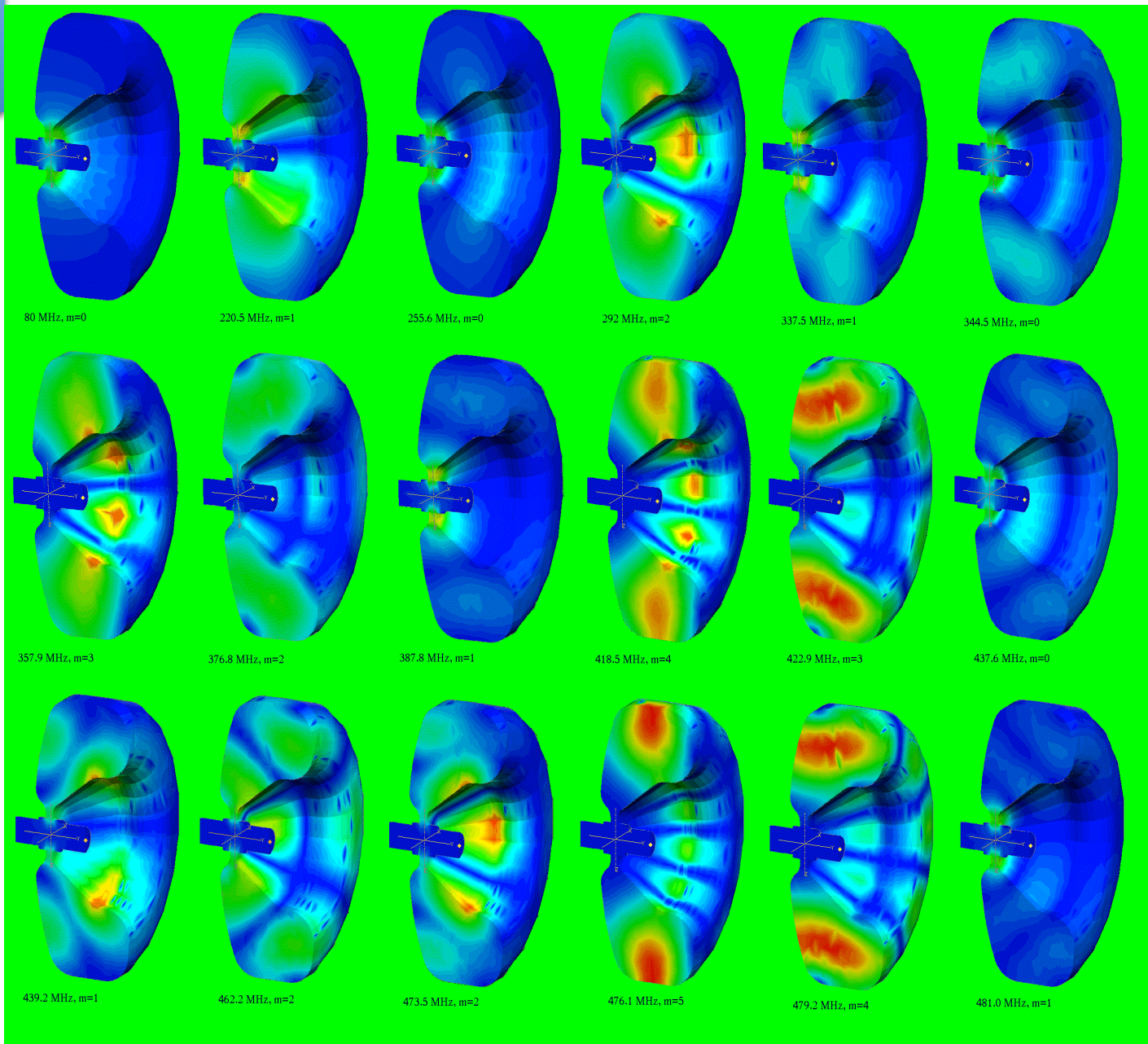
# CERN/PS 80 MHz cavity (for LHC)



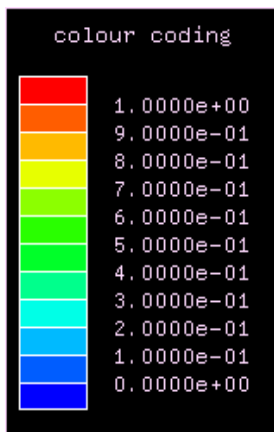
# HOM's

Example shown:

CERN/PS 80 MHz cavity



Colour coding:  $|\vec{E}|$



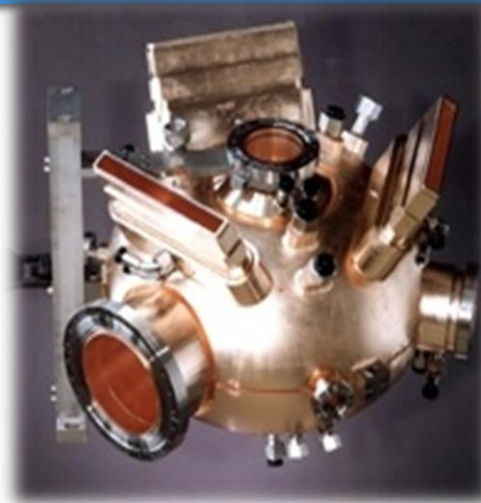


# More examples of cavities

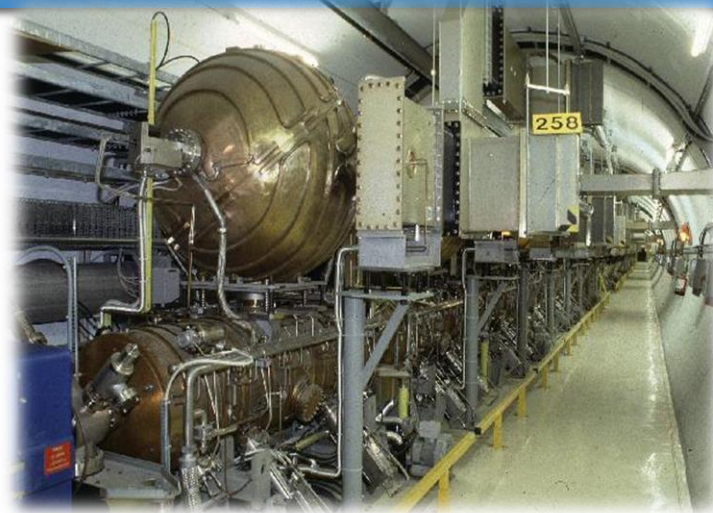
# PS 19 MHz cavity (prototype, photo: 1966)



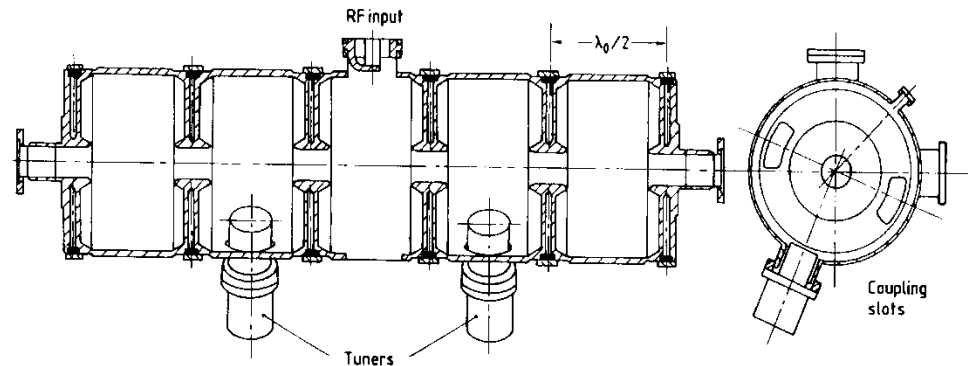
# Examples of cavities



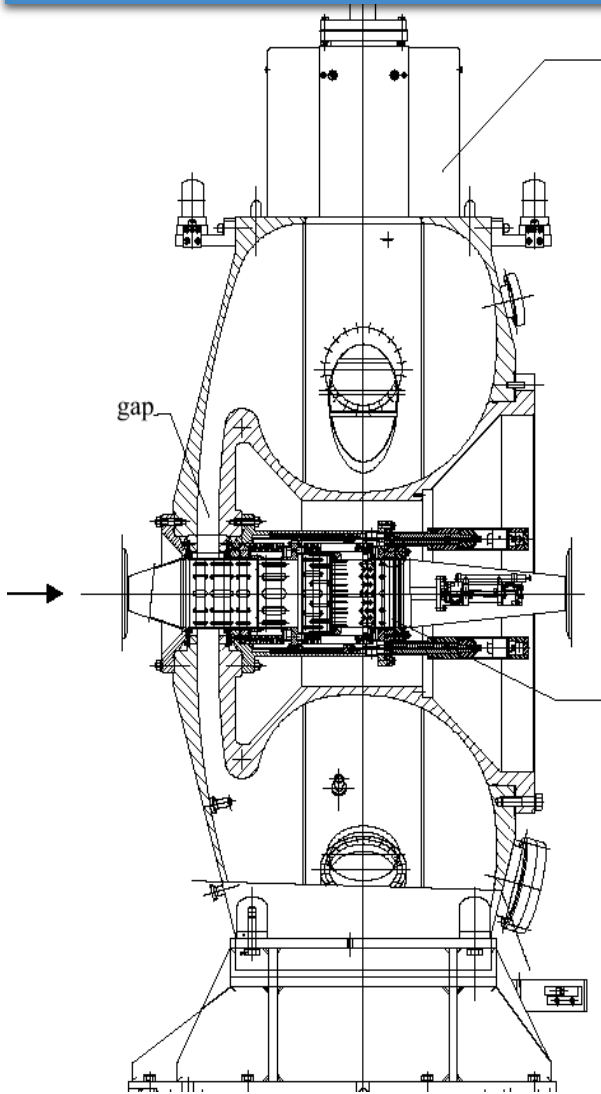
PEP II cavity  
476 MHz, single cell,  
1 MV gap with 150 kW,  
strong HOM damping,



LEP normal-conducting Cu RF cavities,  
352 MHz. 5 cell standing wave +  
spherical cavity for energy storage, 3 MV

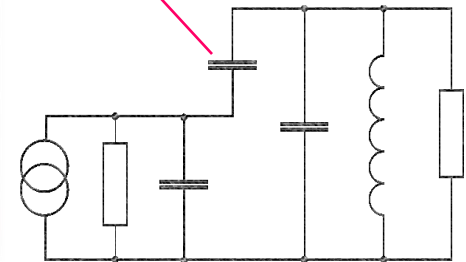


# CERN/PS 40 MHz cavity (for LHC)

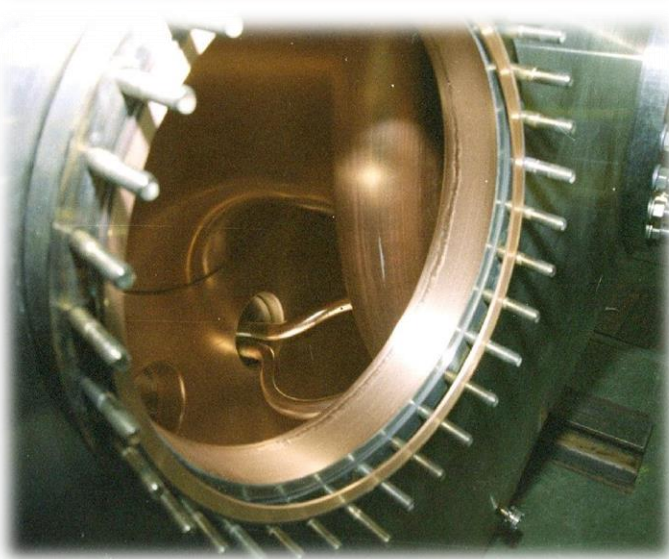


Example for capacitive coupling

Coupling  $C$



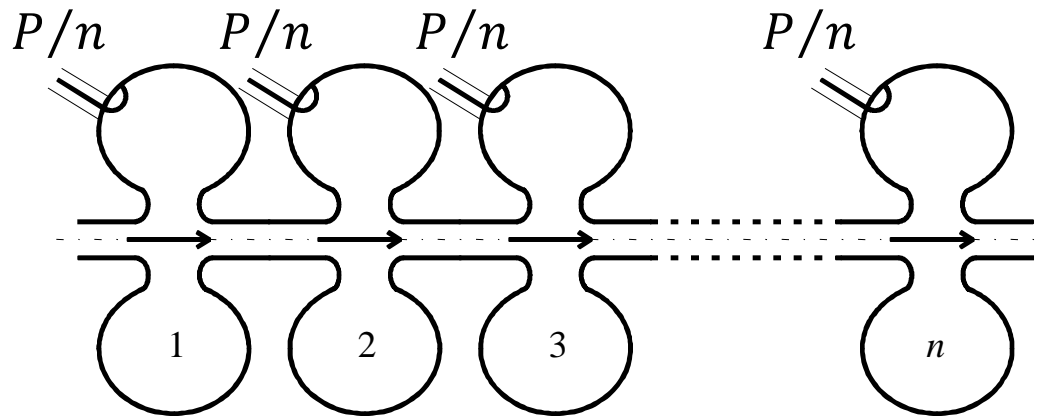
cavity



Many gaps

# What do you gain with many gaps?

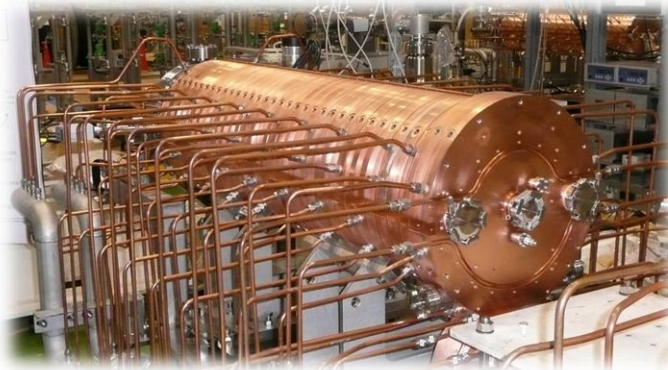
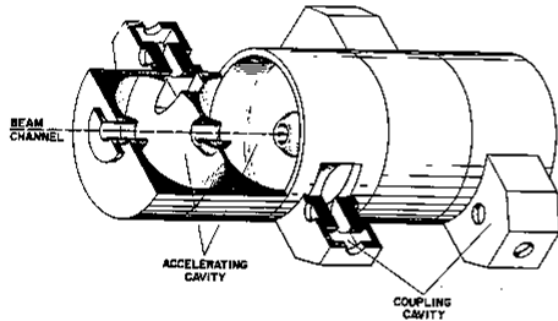
- The  $R/Q$  of a single gap cavity is limited to some  $100 \Omega$ .  
Now consider to distribute the available power to  $n$  identical cavities:  
each will receive  $P/n$ , thus produce an accelerating voltage of  $\sqrt{2RP/n}$ .
- The total accelerating voltage thus increased, equivalent to a total equivalent shunt impedance of  $nR$ .



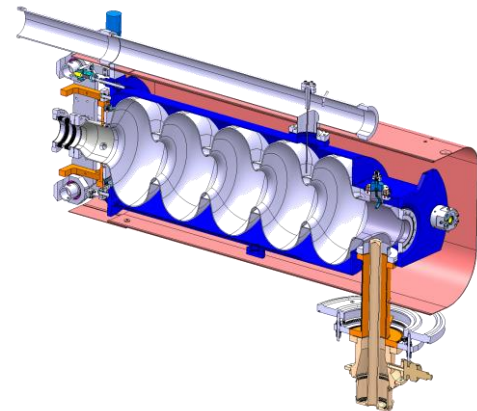
$$|V_{acc}| = n \sqrt{2R \frac{P}{n}} = \sqrt{2(nR)P}$$

# Standing wave multi-cell cavity

- Instead of distributing the power from the amplifier, one might as well couple the cavities, such that the power automatically distributes, or have a cavity with many gaps (e.g. drift tube linac).
- Coupled cavity accelerating structure (example: side coupled)



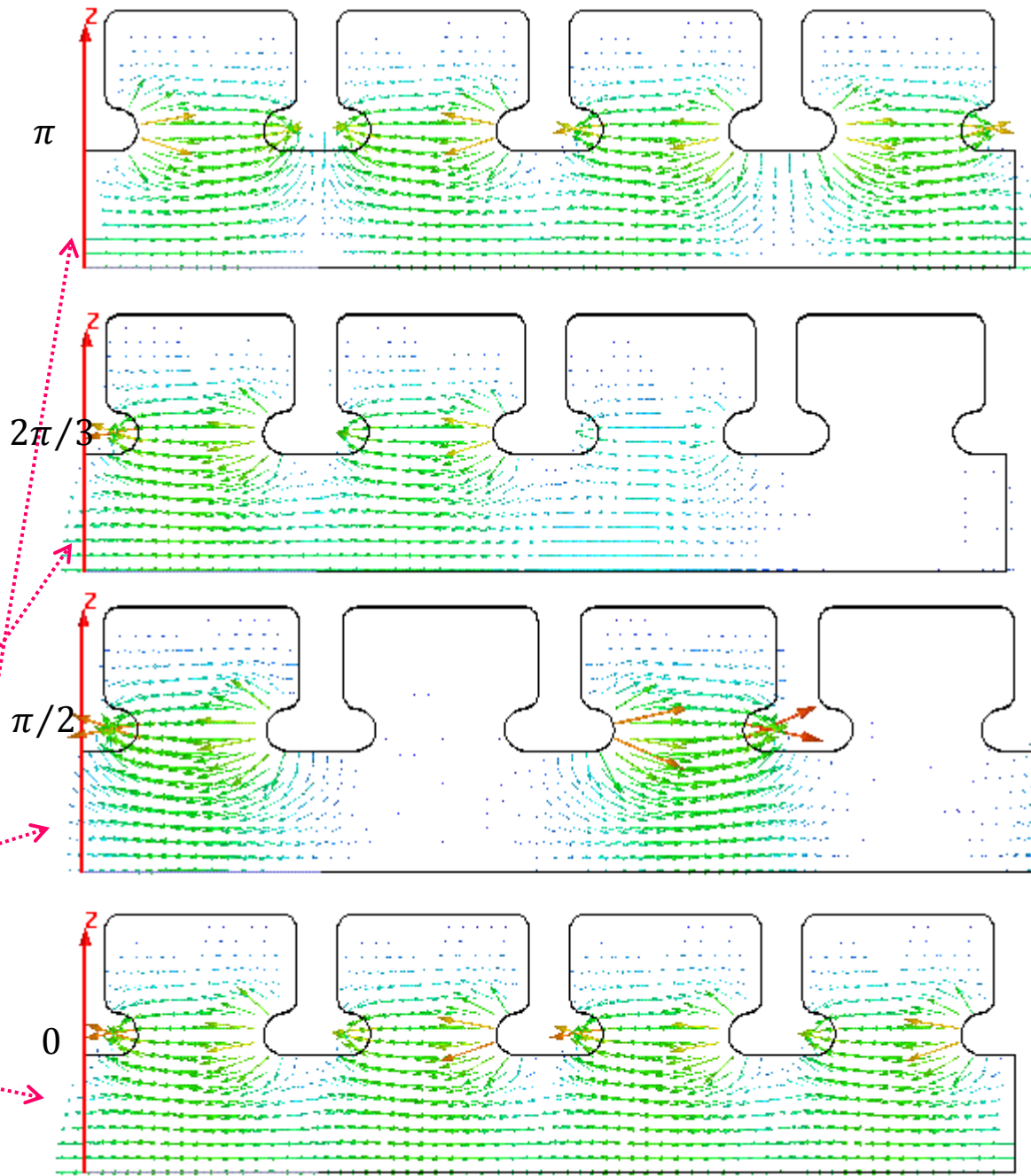
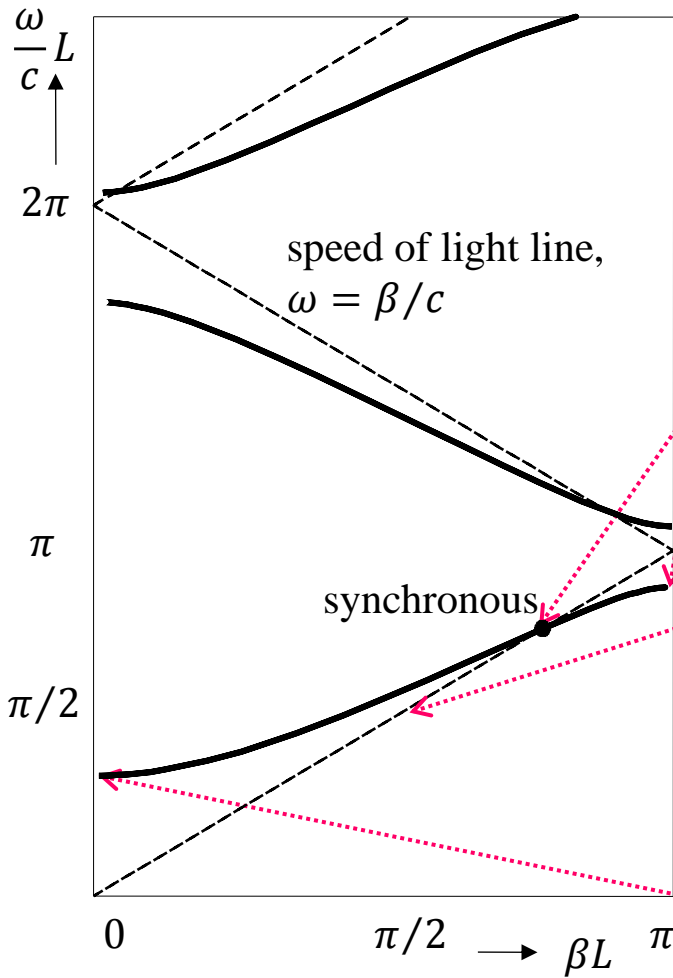
- “Standard” superconducting cavities are standing-wave, multi-cell cavities with a phase shift of  $\pi$  between cells (cell length  $\lambda/2$ )



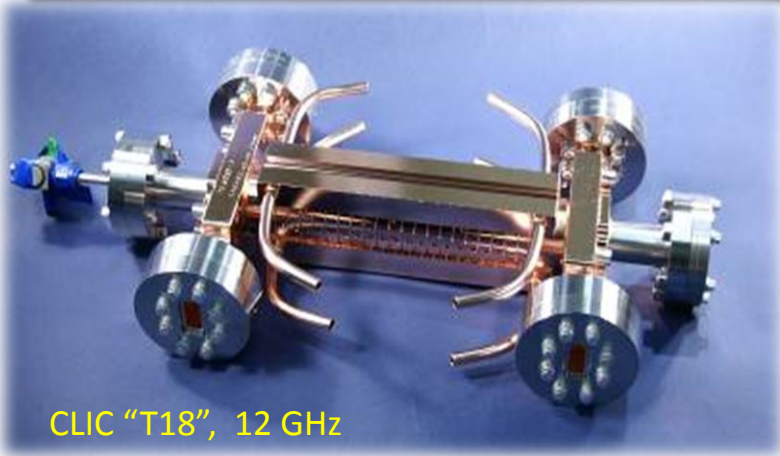
# Travelling wave structures



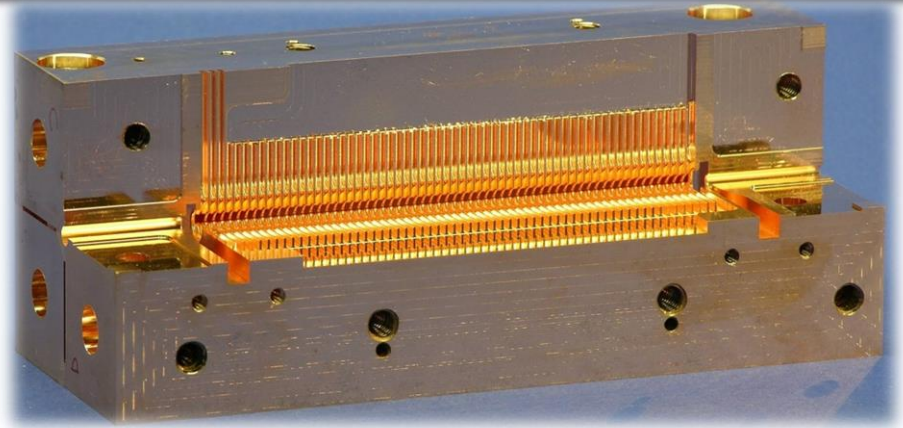
# Brillouin diagram Travelling wave structure



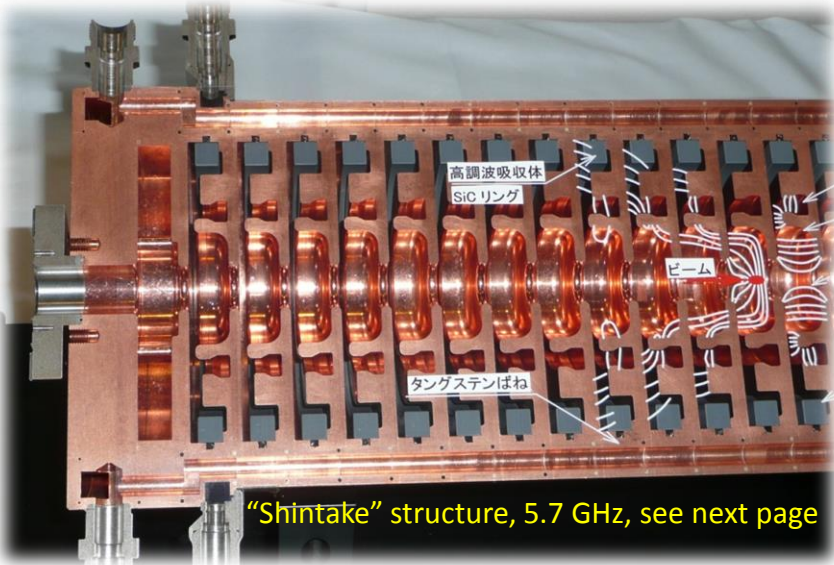
# Travelling wave cavities



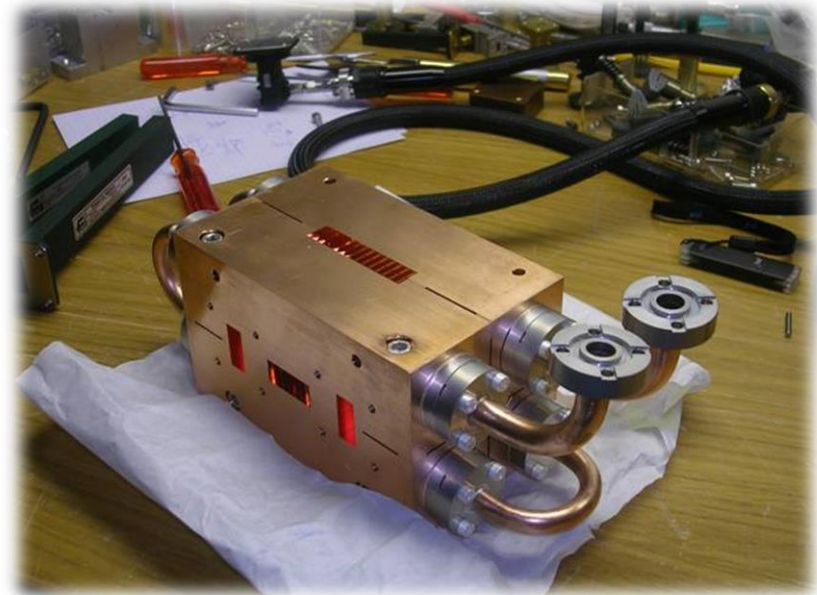
CLIC "T18", 12 GHz



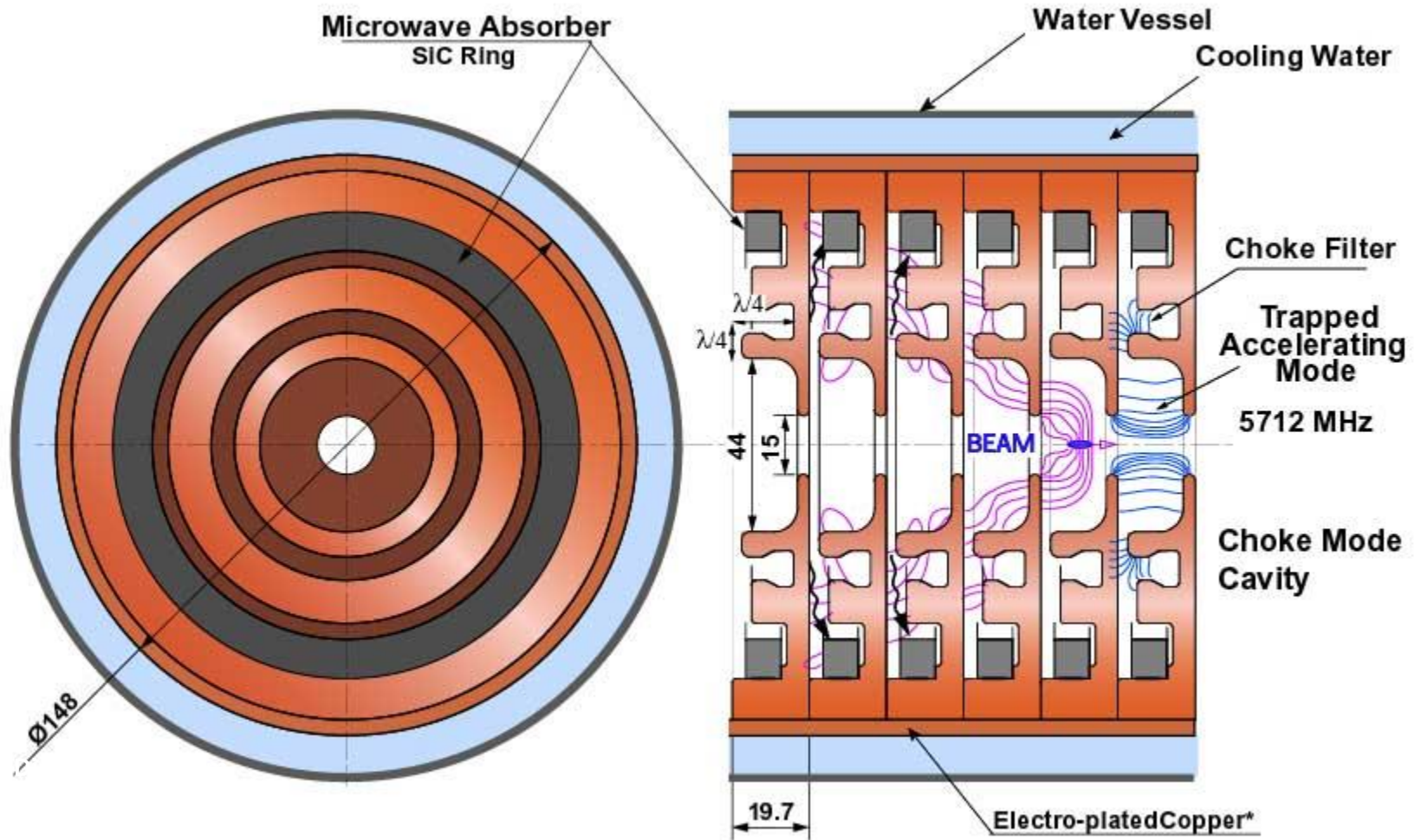
CLIC "HDS", 12 GHz



"Shintake" structure, 5.7 GHz, see next page



# Disc loaded structure with strong HOM damping “choke mode cavity” (“Shintake” structure)



# CERN SPS 200 MHz TW cavity



# Superconducting RF

# RF Superconductivity

- Different from DC, at RF the resistance  $R$  is not exactly zero, but just very small – the resulting  $Q_0$  thus is not infinite, but very large.

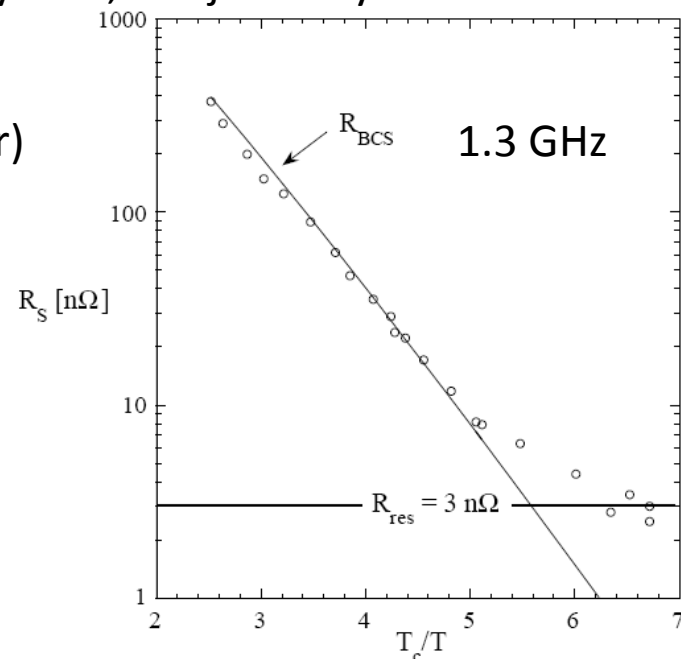
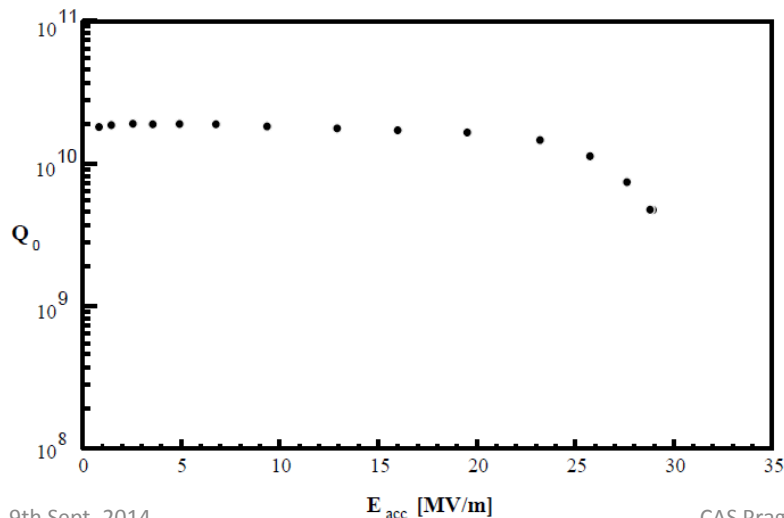
- It is well described by BCS (Bardeen-Cooper-Schrieffer)

$$\text{Theory: } R_{BCS} \propto \frac{\omega^2}{T} \exp\left(-1.76 \frac{T_c}{T}\right)$$

- Surface resistance  $R = R_{BCS} + R_{res}$ .

- Good values for  $Q_0$  are some  $10^{10}$ .

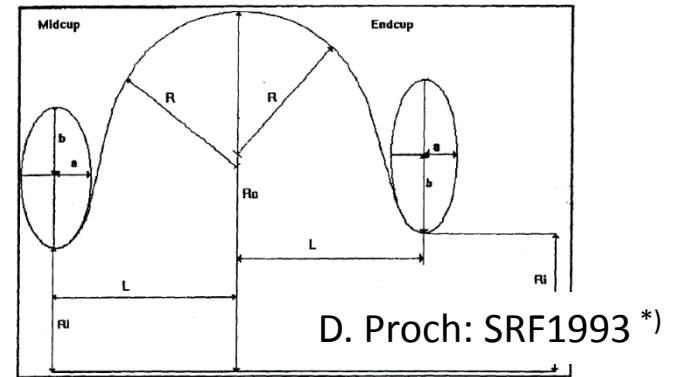
- Typical performance plot of a SC cavity:



- The wall losses are small, but since they occur at low temperature, they are “expensive” to cool! (1000 W/W at 1.8 K!)
- Most used superconductor for RF applications is Nb.

# “Elliptical” multi-cell cavities

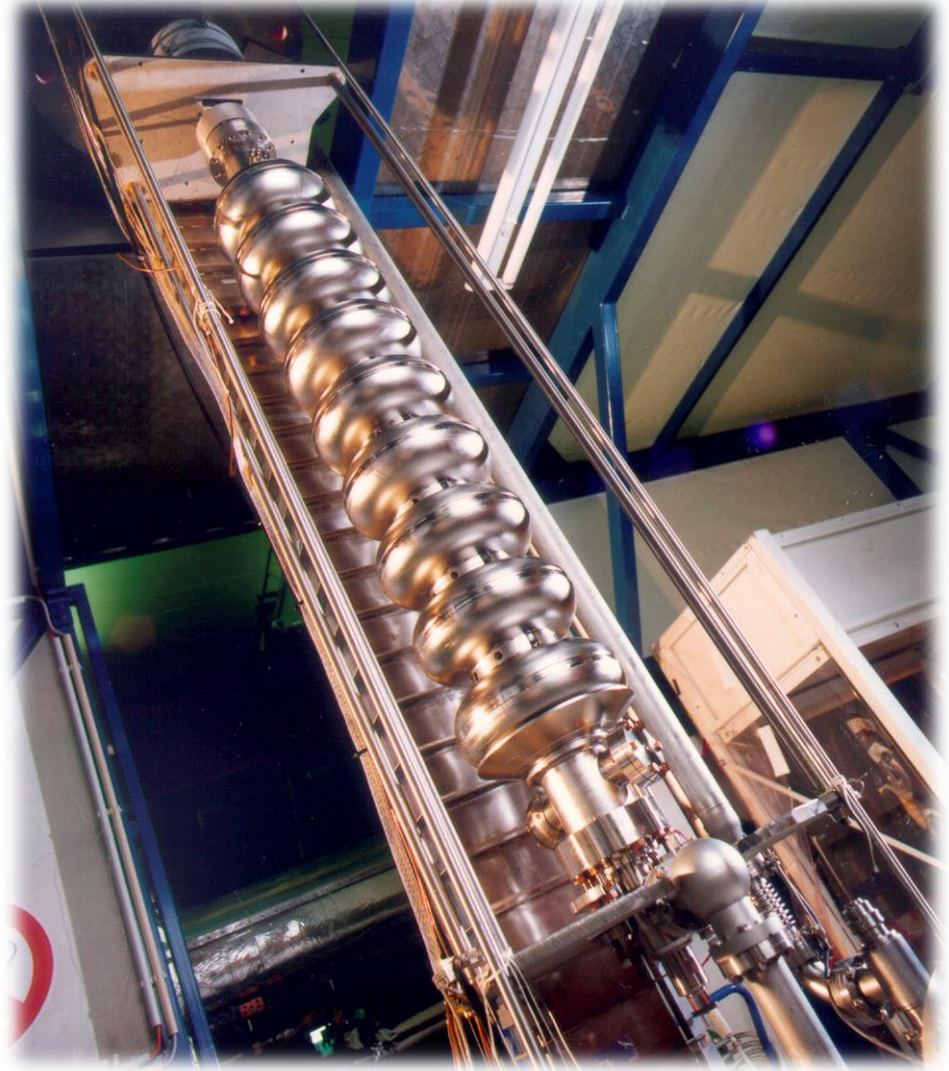
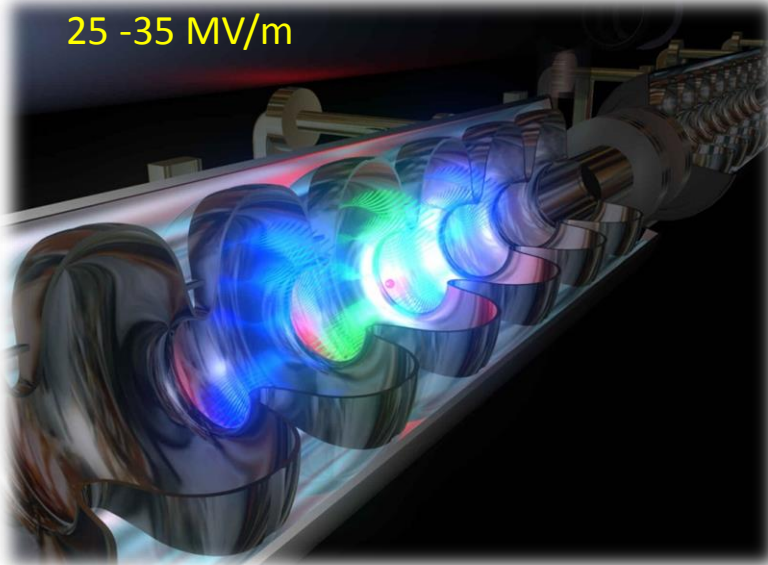
- The elliptical shape was found as optimum compromise between
  - maximum gradient ( $E_{acc}/E_{surf}$ )
  - suppression of multipactor
  - mode purity
  - machinability
- Operated in  $\pi$ -mode, i.e. cell length is exactly  $\beta\lambda/2$ .
- It has become de facto standard, used for ions and leptons! E.g.:
  - ILC/X-FEL: 1.3 GHz, 9-cell cavity
  - SNS (805 MHz)
  - SPL/ESS (704 MHz)
  - LHC (400 MHz, single cell)



\*) : [accelconf.web.cern.ch/accelconf/SRF93/papers/srf93g01.pdf](http://accelconf.web.cern.ch/accelconf/SRF93/papers/srf93g01.pdf)

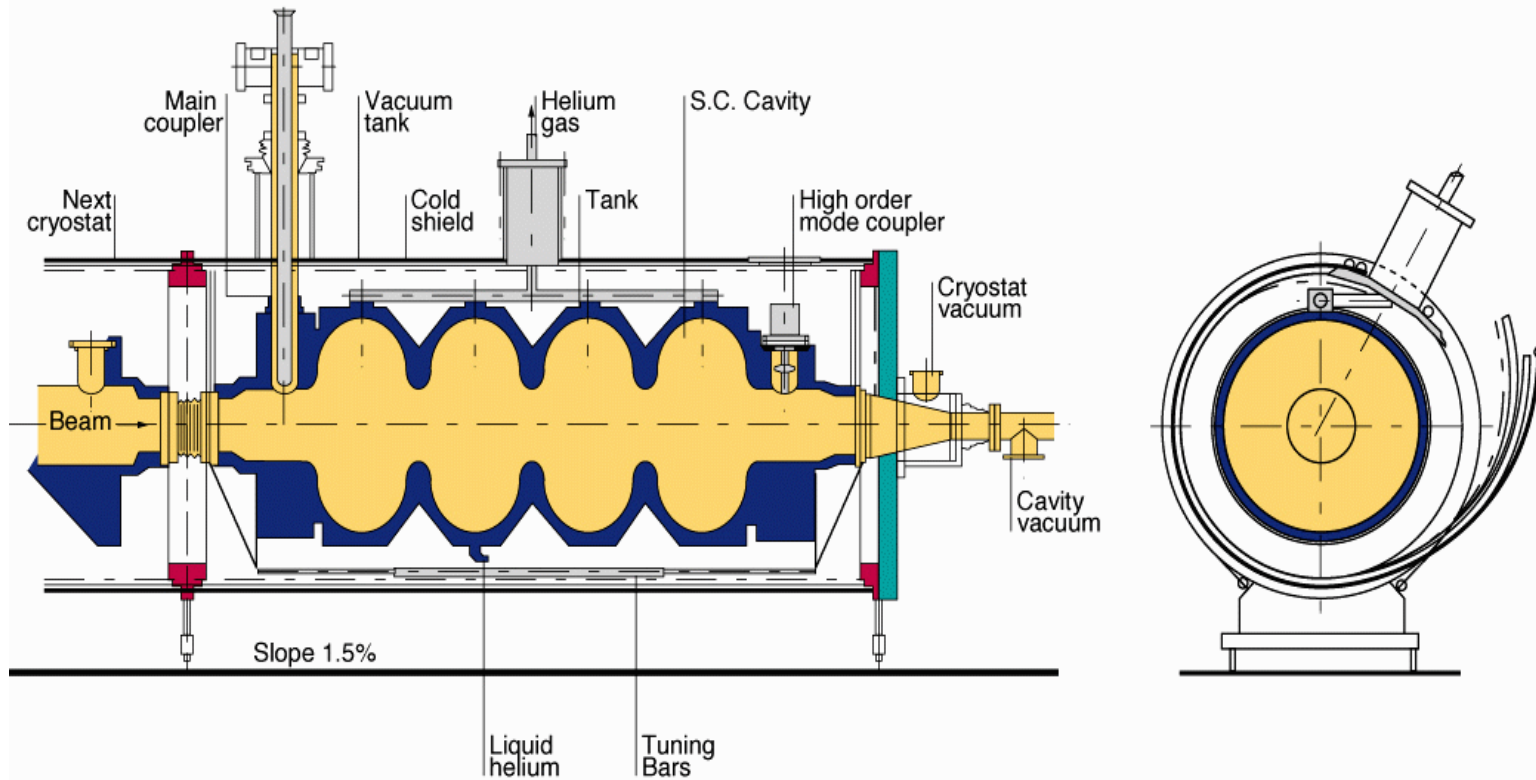
# TESLA/ILC/X-FEL SC cavities, 1.3 GHz

25 -35 MV/m





# LEP Superconducting cavities



10.2 MV/ per cavity

# Nb coating techniques

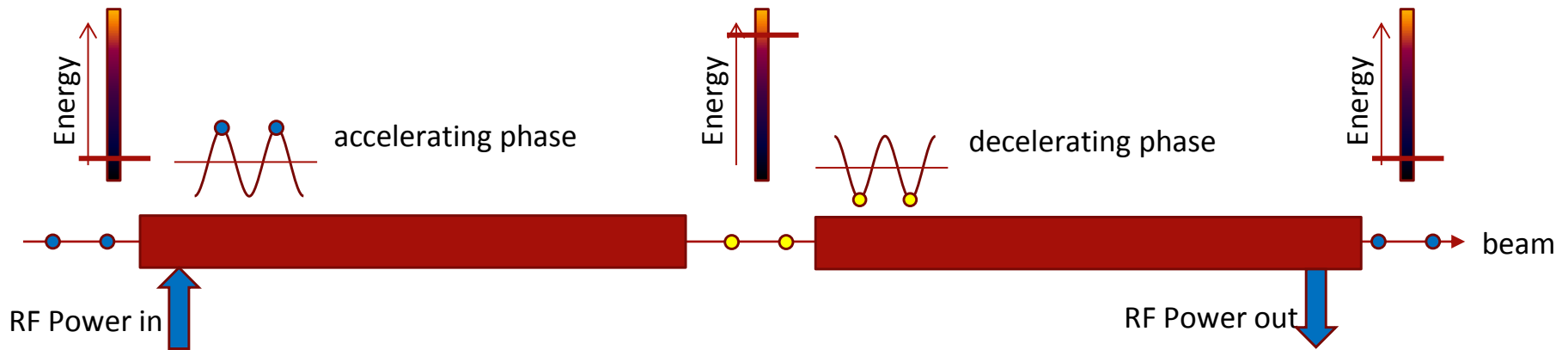
- Sputtering Nb on Cu
  - Advantages:
    - Due to the high cost of Nb, this can reduce cost!
    - The Cu substrate increases the mechanical & thermal stability (quench resistance).
  - Technology initially developed at CERN (Benvenuti, LEP, 1980); experts today at JLAB, Legnaro, Saclay, Sheffield & CERN
  - Technique used today for ALPI (LNL), Soleil, LHC & HIE-Isolde
  - Today, the max. fields are still smaller than for bulk Nb – is this an intrinsic limitation? An interesting field of R&D!
    - Can this technique be extended to new materials? (NbTiN, V<sub>3</sub>Si, Nb<sub>3</sub>Sn, HTS?)
- “Energetic Condensation”- HiPIMS
  - Gas phase deposition of Nb with additional kinetic energy to slow ions.
- Cathodic Arc Deposition
- ...



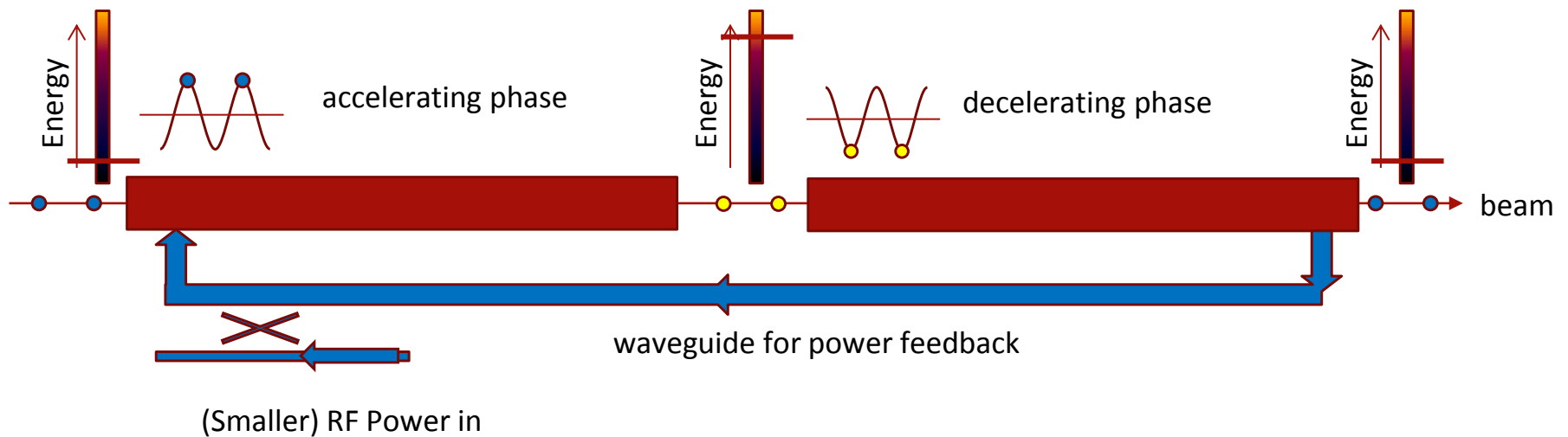
# Energy Recovery Linac

How to reach “power grid → beam” efficiencies above 100%

# Recovering the energy from the beam – the concept



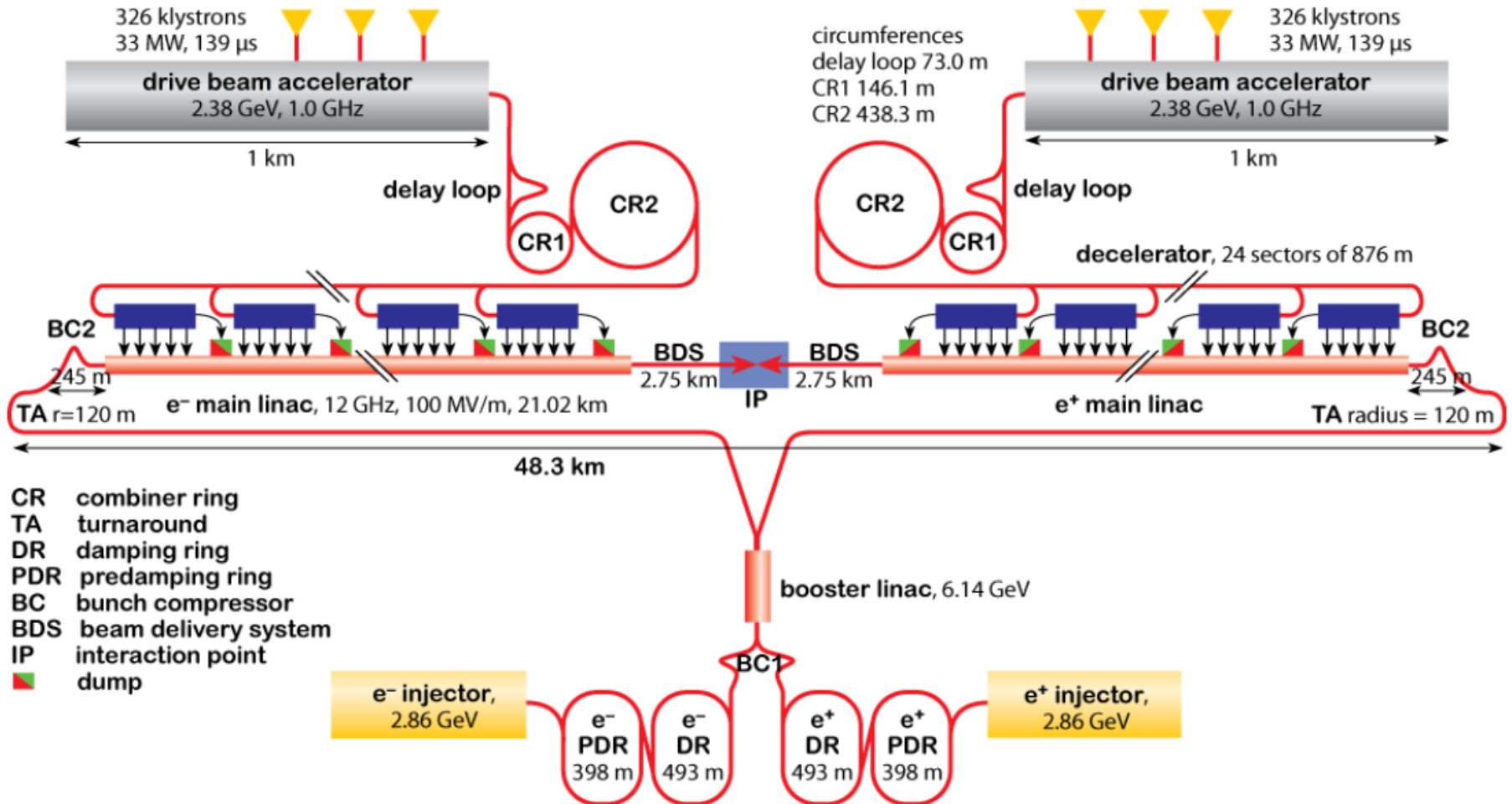
One could use a waveguide and reuse the RF power!



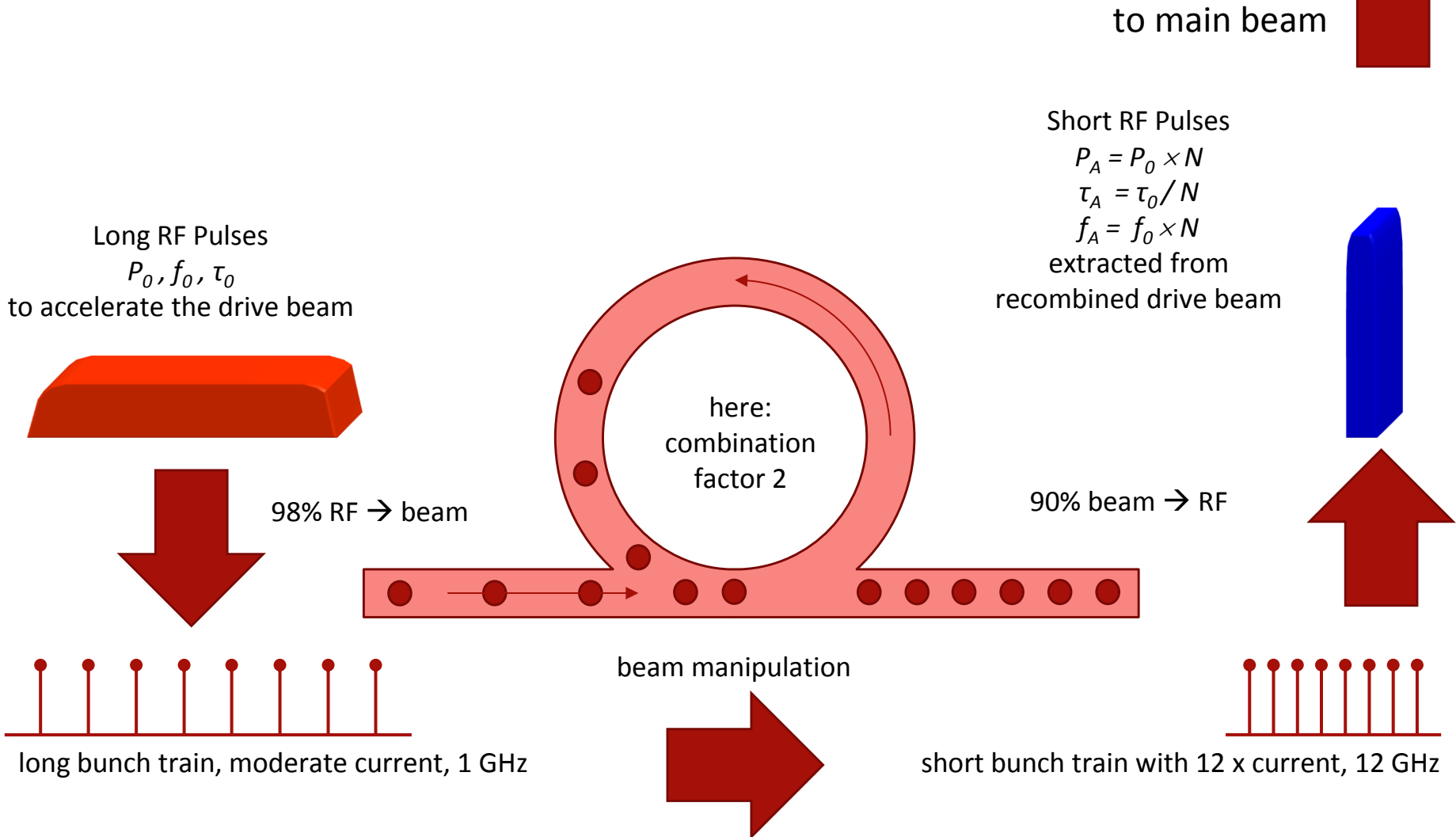
# A word about CLIC

*In the CLIC scheme, 90% of the drive beam power is recovered (to produce the RF power for the main beam)*

## CLIC general layout

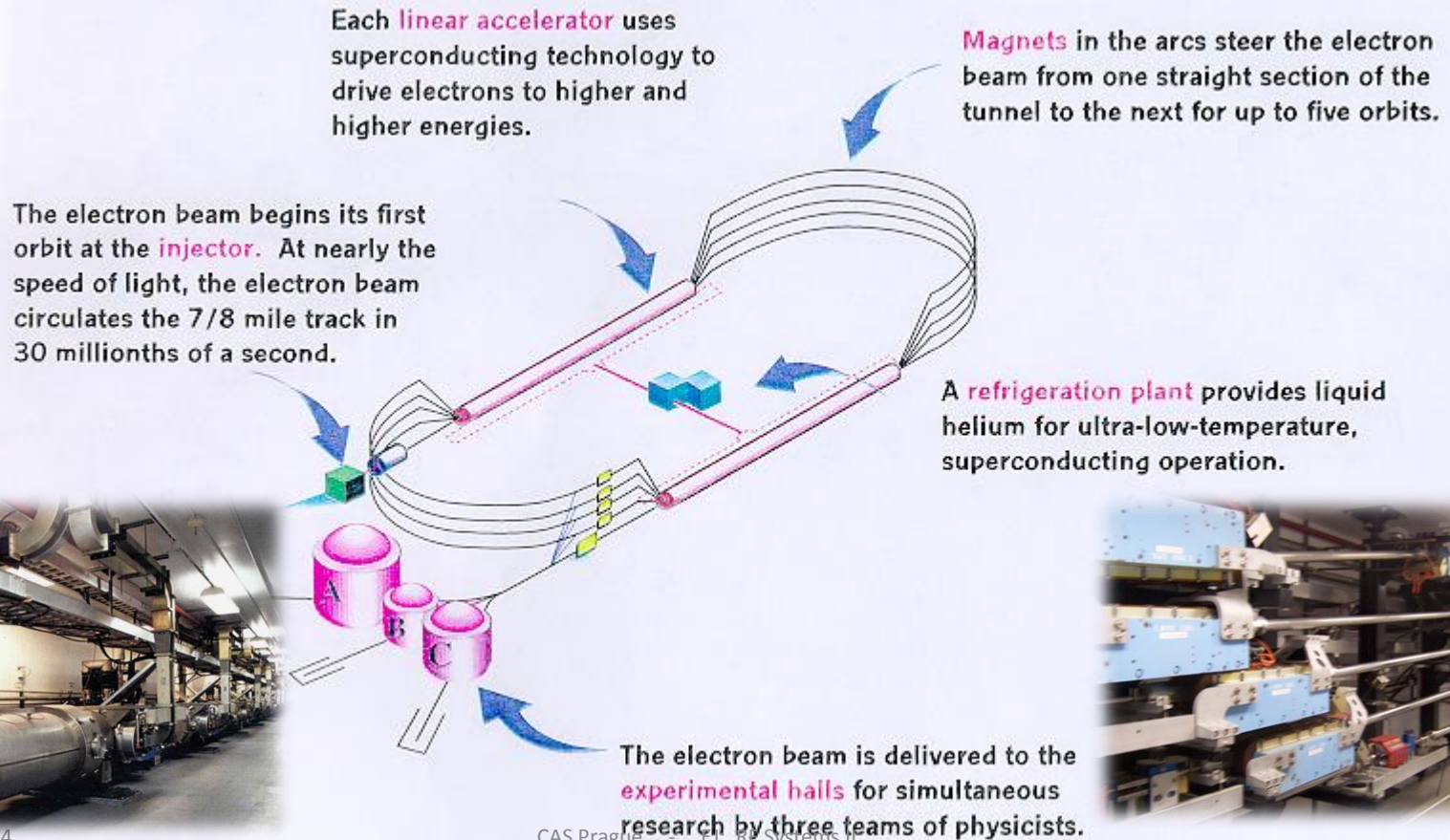


# The CLIC power source idea



# Recirculating Linac

- One could use the same accelerating structure more than once!
- CEBAF (Continuous Electron Beam Accelerator Facility) at JLAB, Newport News, VA, USA has been using this scheme successfully for many years.





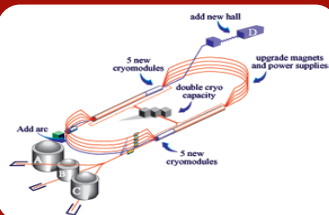
# Recirculating Linac compared to linac and synchrotron

## Linac



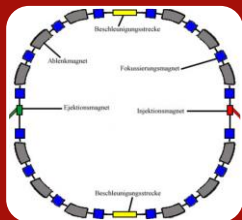
- Accelerating Structure used for 1 passage
- Less efficient
- Only single pass instabilities

## Recirculating Linac



- Accelerating Structure used for some (2-10) passages
- Return arcs different for different energies
- Concerning instabilities, a good compromise

## Synchrotron



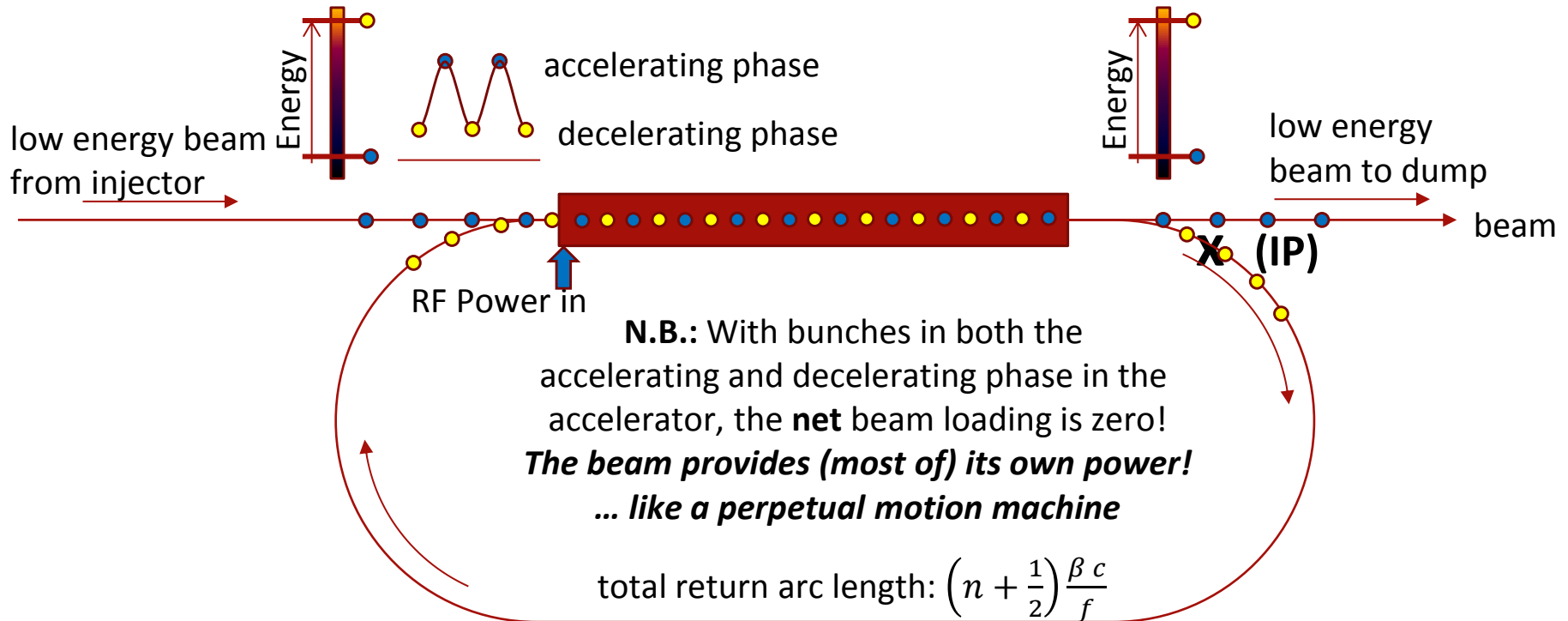
- Accelerator Structure used many times
- Periodic lattice
- Instabilities develop over many turns (coupled bunch, mode coupling)

L. Merminga '07: *In a storage ring, electrons are stored for hours in an equilibrium state, whereas in an ERL it is the energy of the electrons that is stored. The electrons themselves spend little time in the accelerator (from ~1 to 10's of  $\mu$ s) thus never reach equilibrium. As a result, in common with linacs, the 6-dimensional phase space in ERLs is largely determined by the electron source properties by design. On the other hand, in common with storage rings, ERLs have high current carrying capability enabled by the energy recovery process, thus promising high efficiencies.*

<http://accelconf.web.cern.ch/AccelConf/p07/PAPERS/MOYKI03.PDF>

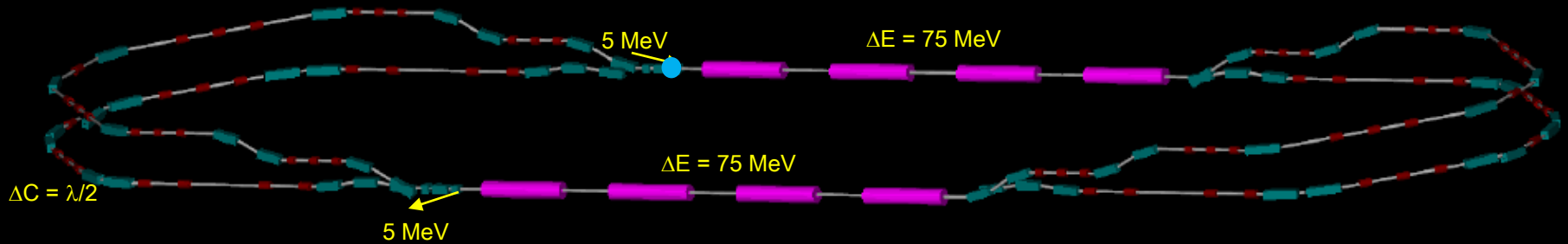
# Energy Recovery Linac:

Combine “Energy recovery” and “recirculating”



# LHeC ERL-TF (300 MeV) – Layout

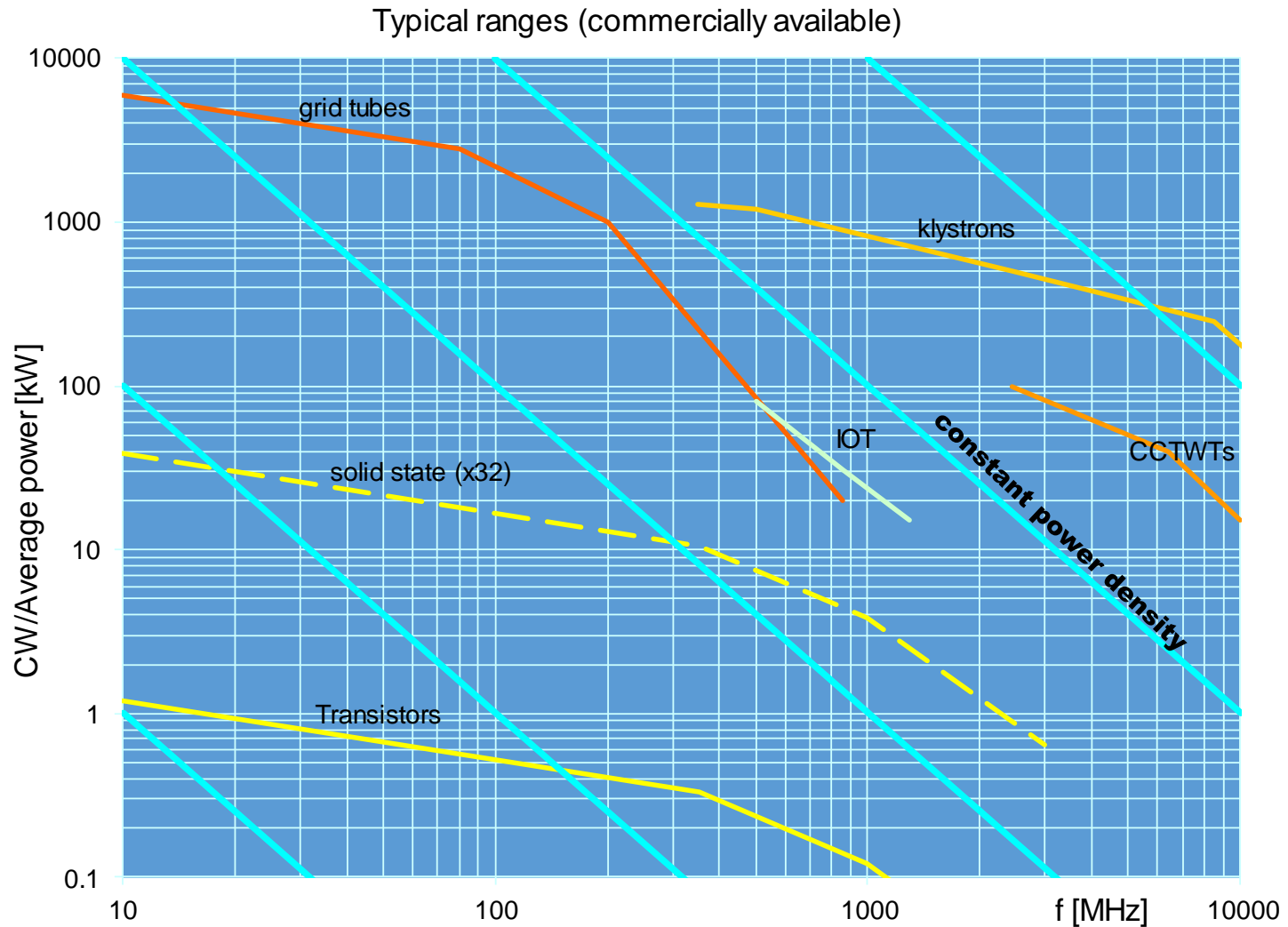
This model and animation by Alex Bogacz, Jefferson Lab



Two passes 'up' + Two passes 'down'

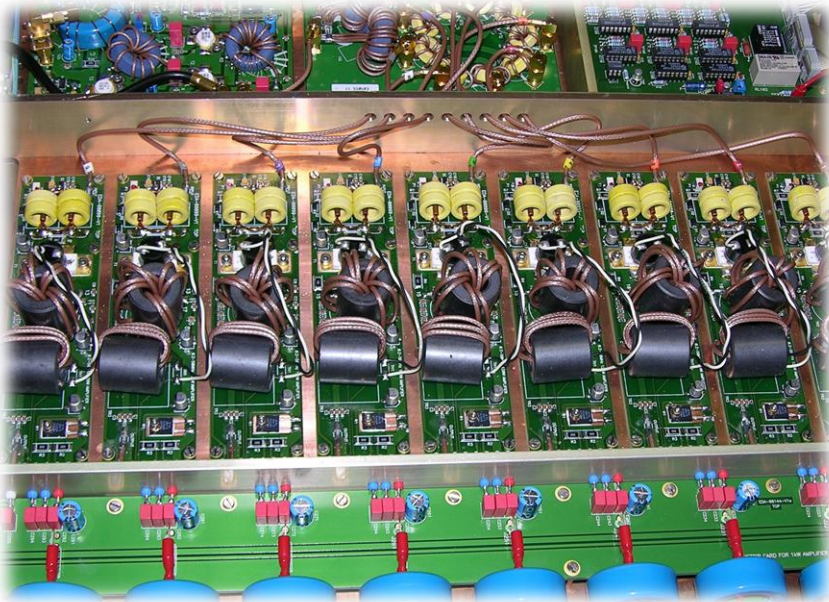
# RF power sources

# RF power sources

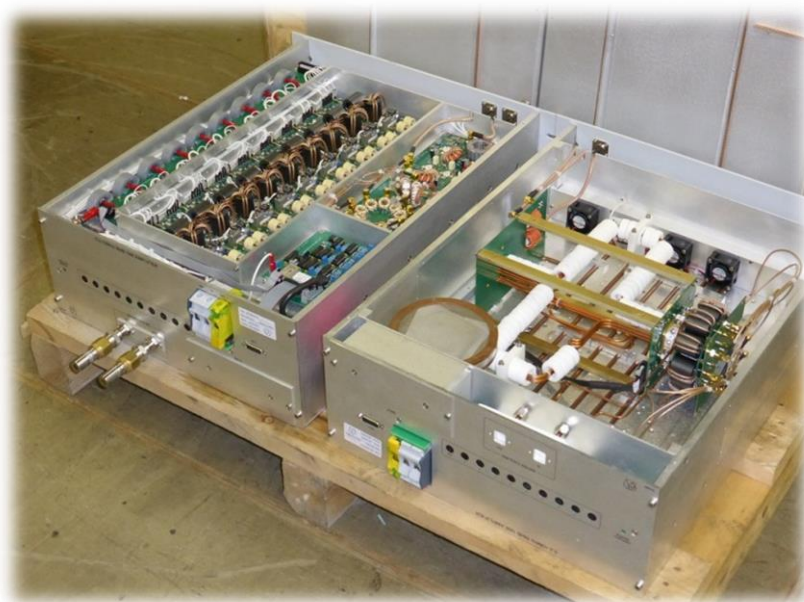


# Example SSPA, 1 kW

(0.2 ÷ 50) MHz, 1 kW solid state amplifier for LEIR



M. Paoluzzi

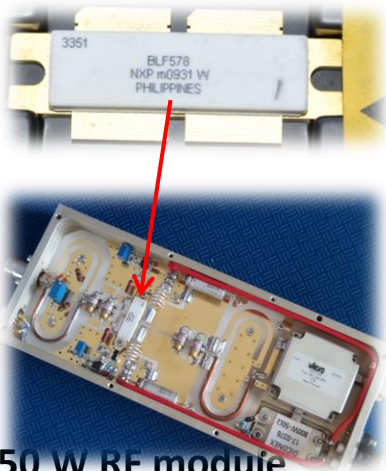


(0.2 ÷ 10) MHz, 1 kW SSPA for MedAustron

# Soleil/ESRF Booster SSPA, 150 kW, 352 MHz

- Initially developed by SOLEIL
- Transfer of technology to ELTA / AREVA

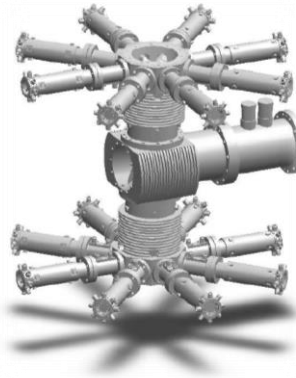
## Pair of push-pull transistors



## 650 W RF module

- 6<sup>th</sup> generation LD MOSFET (BLF 578 / NXP),  $V_{ds} = 50$  V
- Efficiency: 68 to 70 %

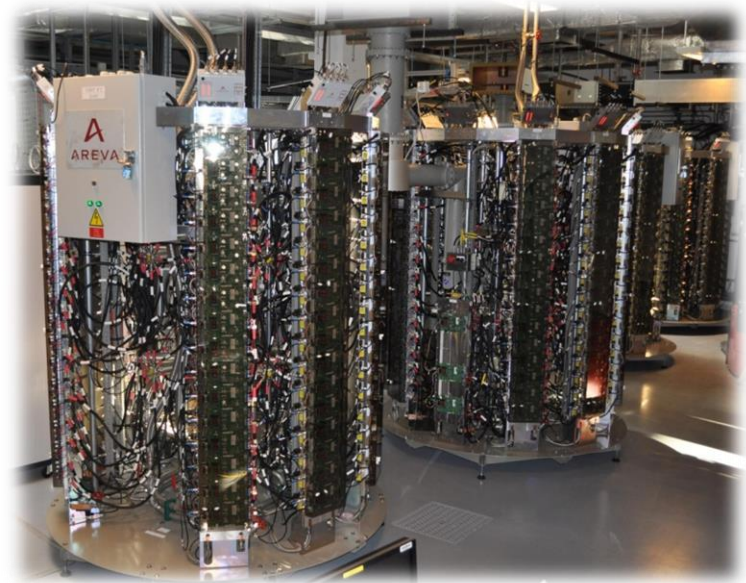
x 128



## 75 kW Coaxial combiner tree

with  $\lambda/4$  transformers

x 2

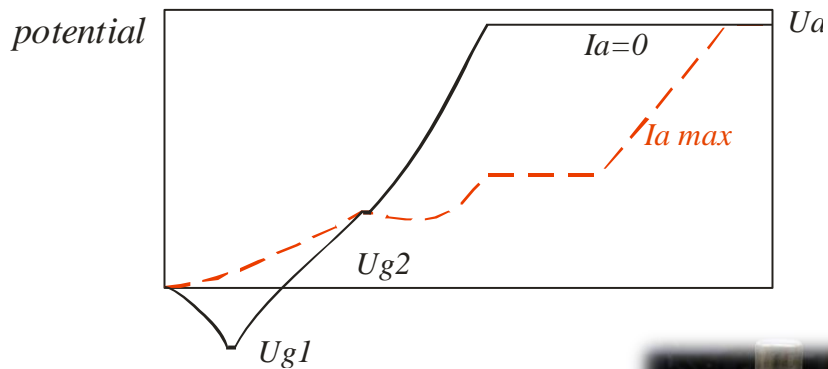
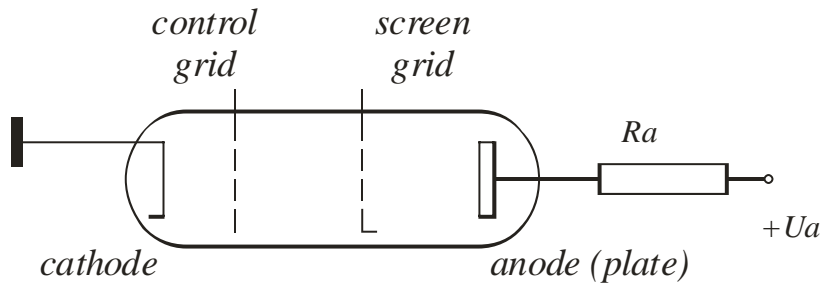


## 150 kW, 352.2 MHz Solid State Amplifiers for the ESRF booster (7 in operation)

Efficiency: > 57 % at nominal power

Taken from J. Jacob, CWRF 2014

# Tetrodes



**4CX250B**  
(Eimac/CPI),  
< 500 MHz, 600 W  
(Anode removed)



**RS 1084 CJ** (ex Siemens, now Thales),  
< 30 MHz, 75 kW

**YL1520** (ex Philips, now Richardson),  
< 260 MHz, 25 kW



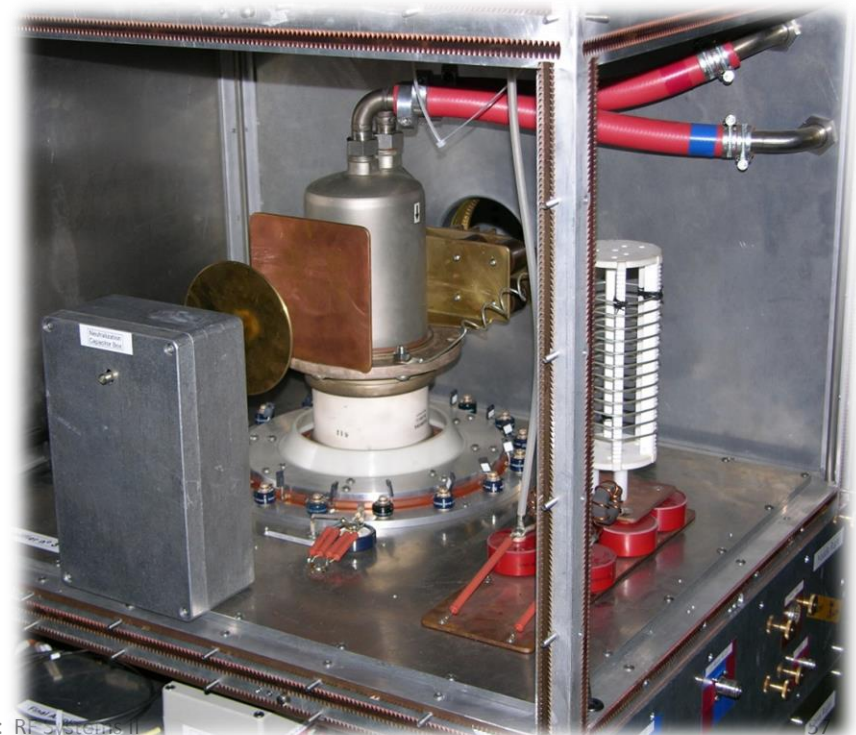
# High power tetrode amplifier

**CERN Linac3: 100 MHz, 350 kW**

50 kW Driver: TH345, Final: RS 2054 SK

**CERN PS: 13-20 MHz, 30 kW**

Driver: solid state 400 W, Final: RS 1084 CJSC

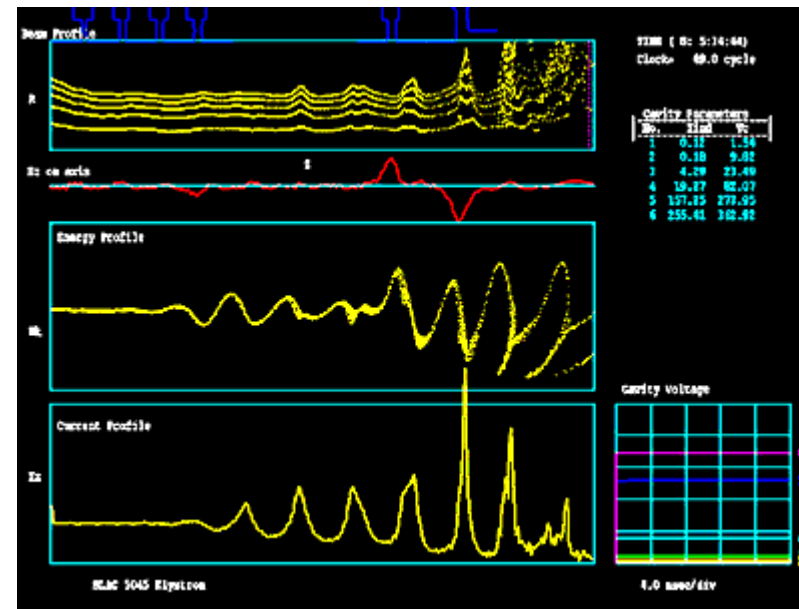
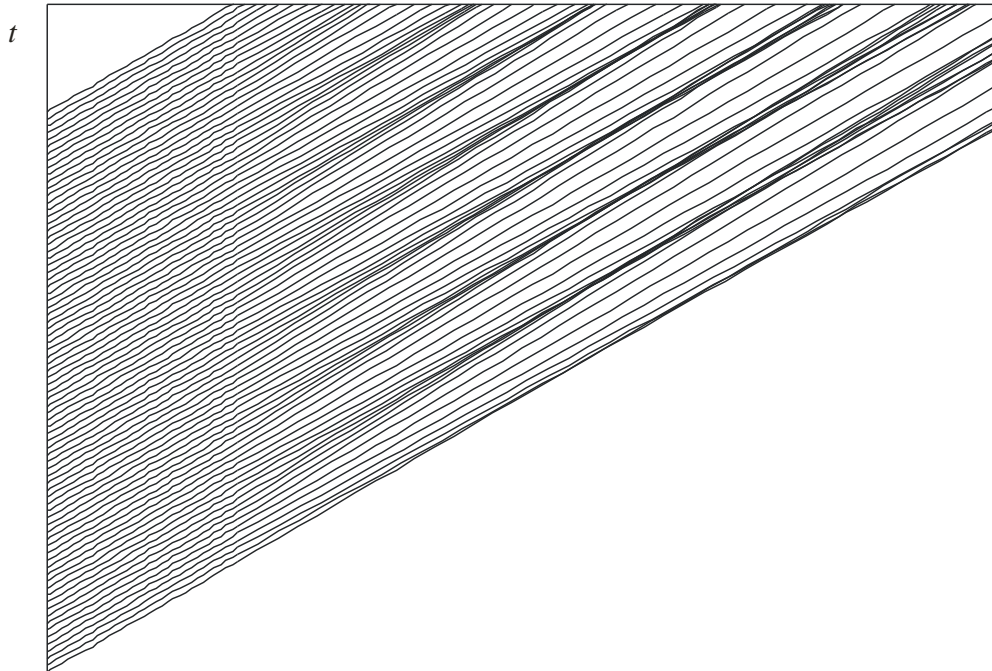


# Klystron principle

velocity  
modulation

drift

density  
modulation



RF in

RF out

z

$-V_0$

Cathode

Collector

# Klystrons



**CERN CTF3 (LIL):**  
3 GHz, 45 MW,  
4.5  $\mu$ s, 50 Hz,  $\eta$  45 %



**CERN LHC:**  
400 MHz, 300 kW,  
CW,  $\eta$  62 %

# Some examples

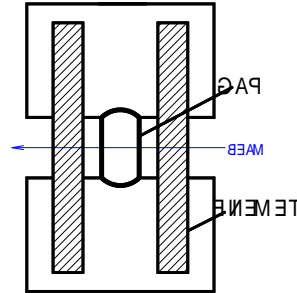
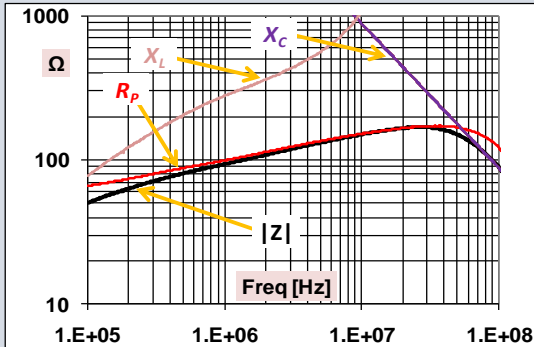
Some Power RF systems at CERN

# Finemet<sup>®</sup> based wide-band cavity

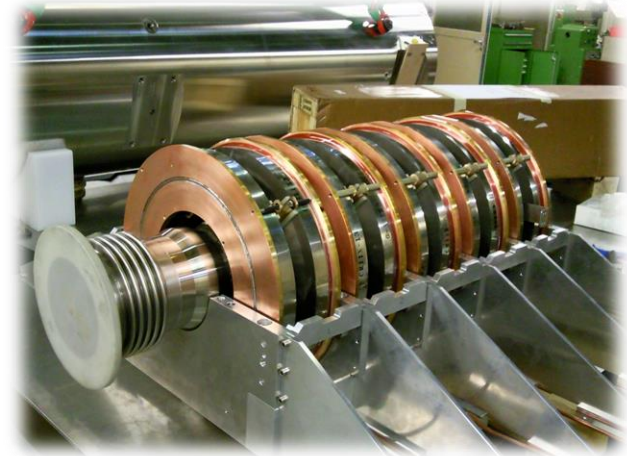
## Finemet exhibits wideband response

$C_p$  mostly depends on geometry and drives the high frequency response. The capacitive effect is enhanced by the final stage output capacitance.

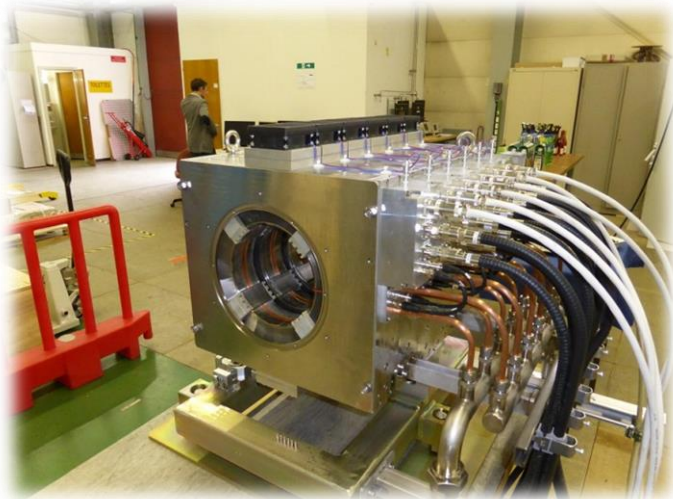
$R_p$  and  $L_p$  drive the low frequency response. They are mostly dependent on Finemet<sup>®</sup> Characteristics.



5-gap finemet cavity



6-gap finemet cavity for MedAustron



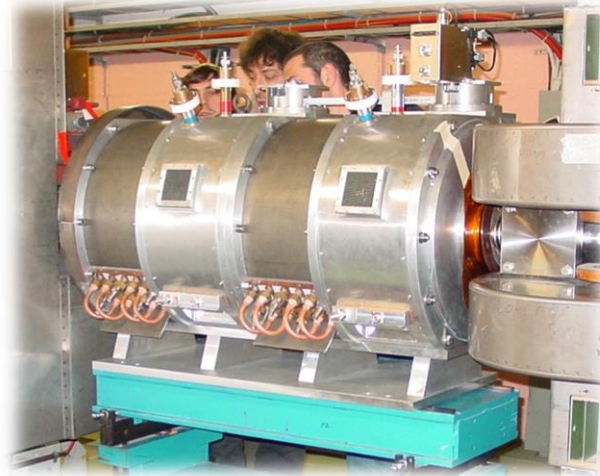
Prototype system installed in ring 4 of CERN PSB



# CERN PS RF Systems



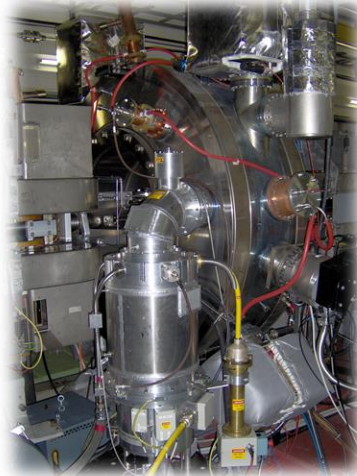
10 MHz system,  $h=7\dots 21$



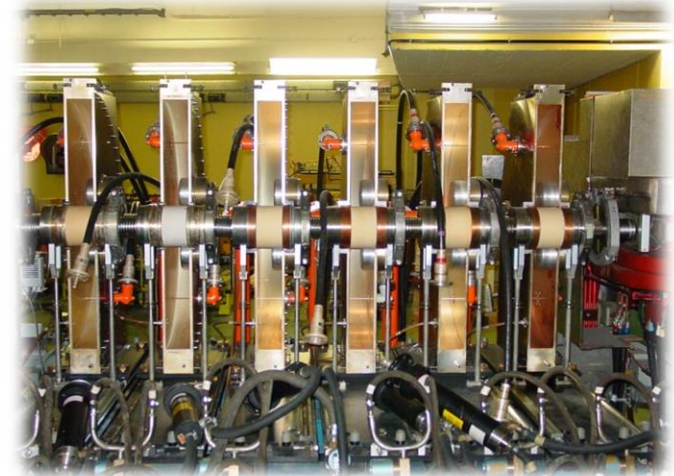
13/20 MHz system,  $h=28/42$



40 MHz system,  $h=84$



80 MHz system,  $h=168$



200 MHz system

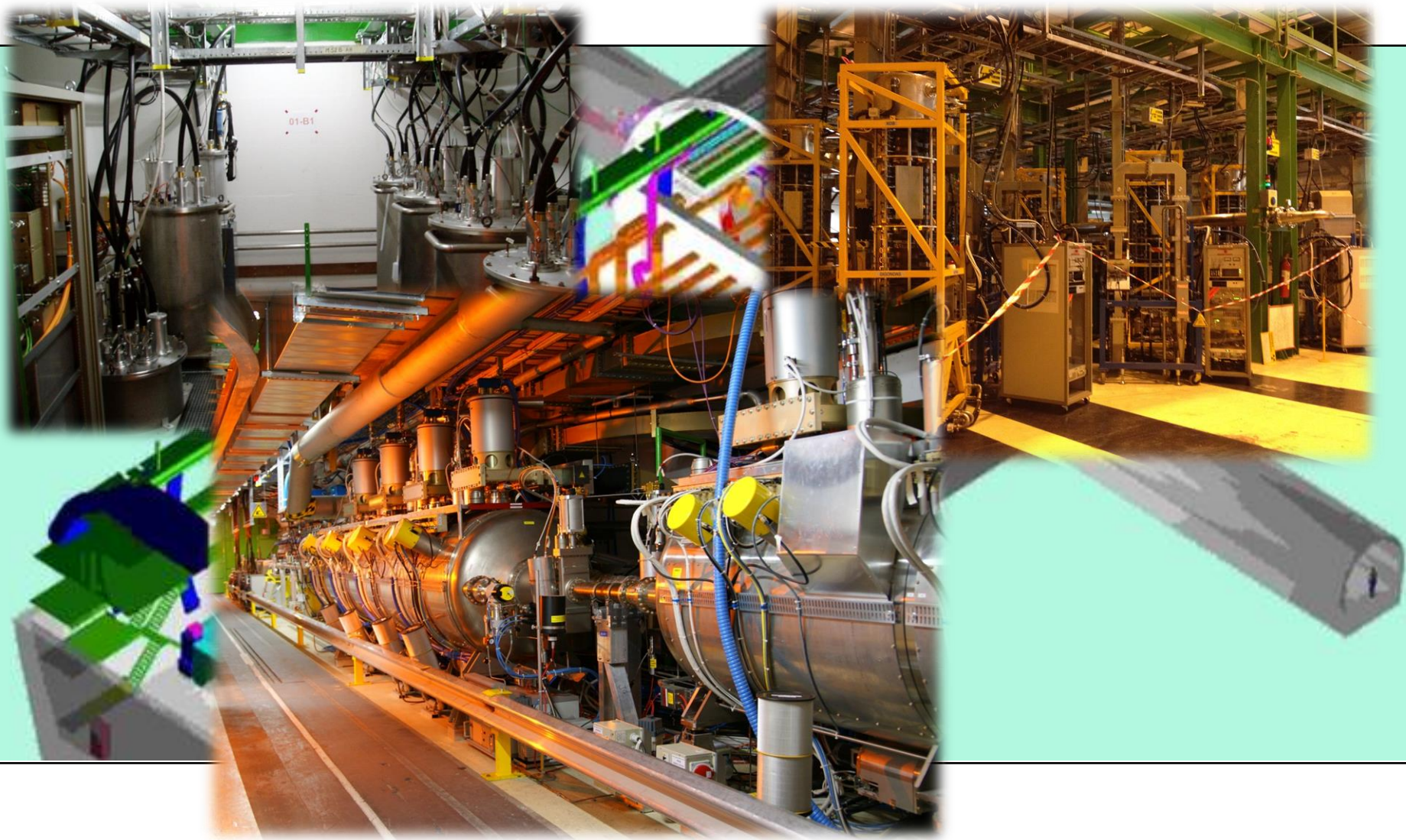
# SPS 200 MHz RF system



“Siemens”:  
4 x 550 kW (28 tetrode amplifiers)

← “Philips”:  
4 x 550 kW (72 tetrode amplifiers)

# LHC 400 MHz High-Power RF System





# End of RF Systems II

Thank you for your attention!