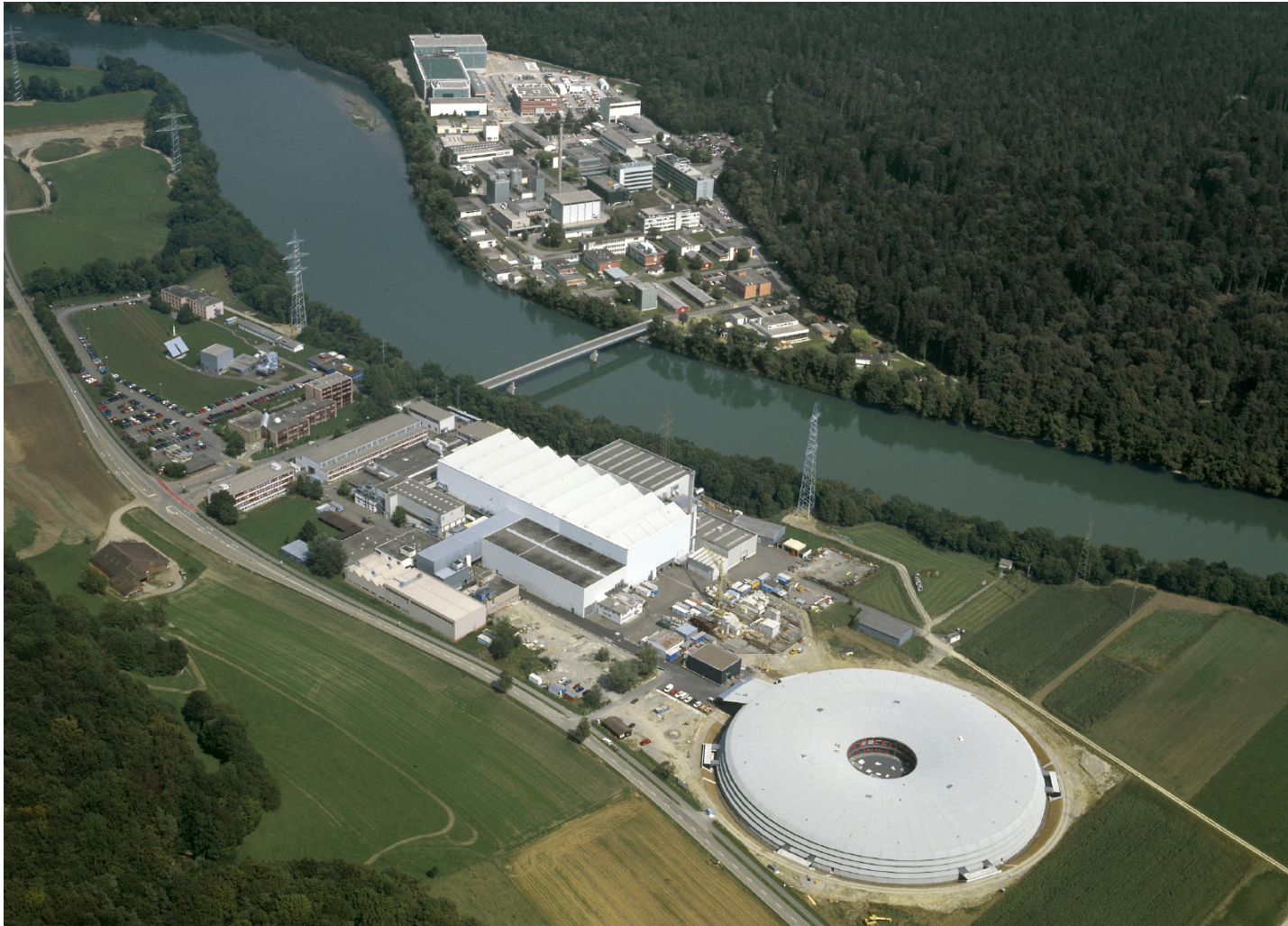
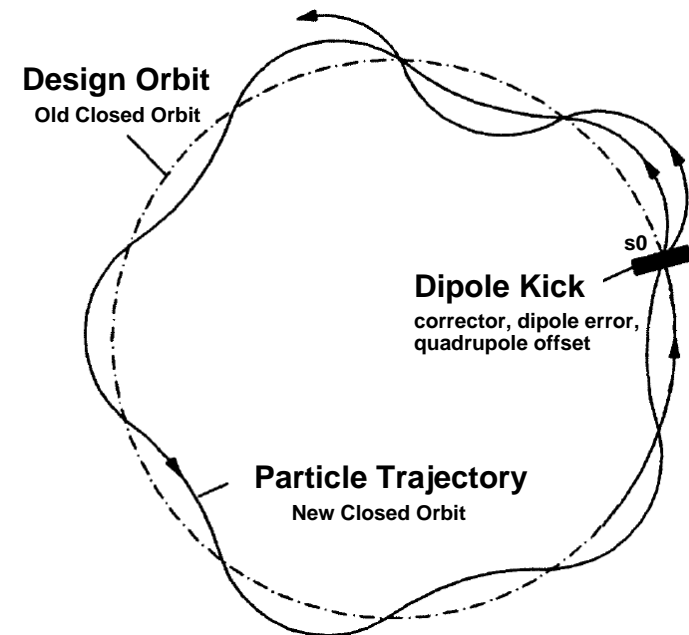


# SLS at the Paul Scherrer Institute (PSI), Villigen, **Switzerland**

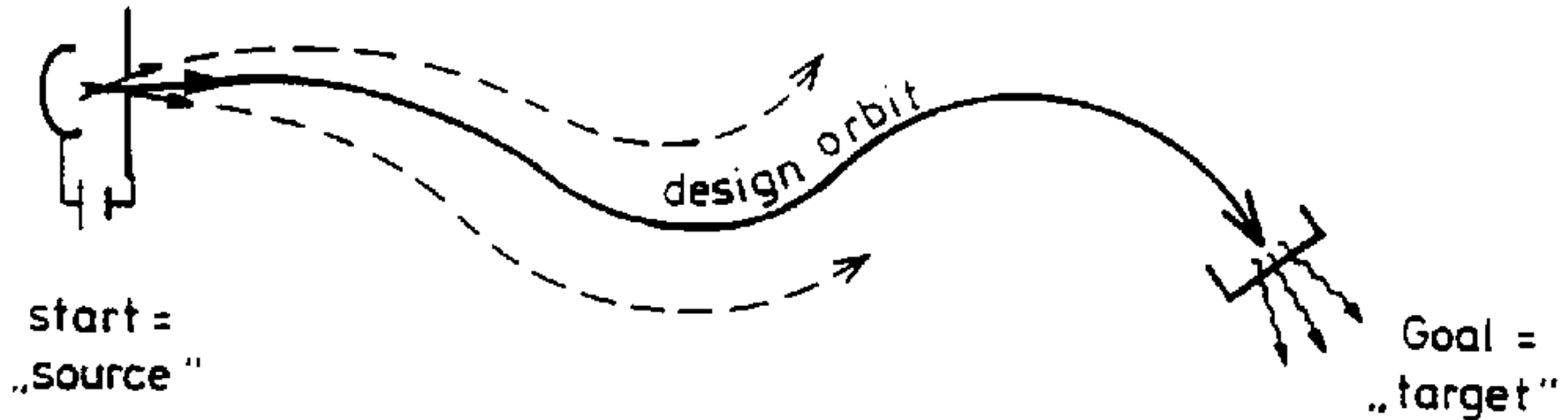


## Overview

- What is an Orbit ?
- How is it measured ?
- What is a Closed Orbit ?
- How does the Closed Orbit change with Energy ?
- Motion around the Closed Orbit
- How does the Closed Orbit change with Errors ?
- BPM and Corrector Layout
- Corrector / BPM Response Matrices
- What is a Bare Orbit ?
- Local Orbit Manipulations
- How is a Closed Orbit corrected ?
- What is SVD doing ?
- Inverse Response Matrices, SVD Eigenvalues
- How to correct Off-Energy Orbits ?
- How is the position of the BPMs measured ?

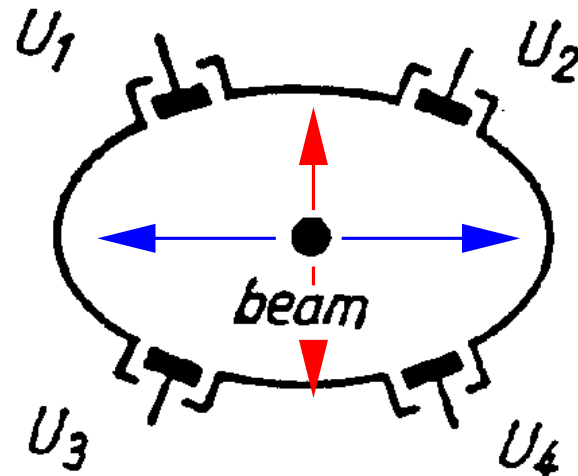


## What is an Orbit ?



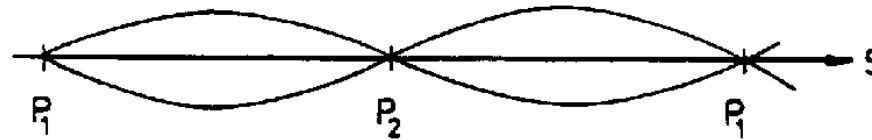
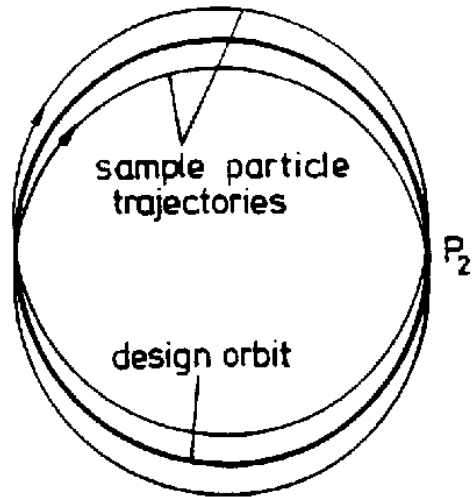
- A certain arrangement of magnets (“Optics”) defines a trajectory (“Orbit”), on which charged particles move from “Start” to “Goal”.
- For the initial design condition and without magnet errors the particles move along the so-called “Design Orbit”.
- Variation of the initial conditions, alignment and magnet errors lead to a deviation from the “Design Orbit”.

## How is it measured ?



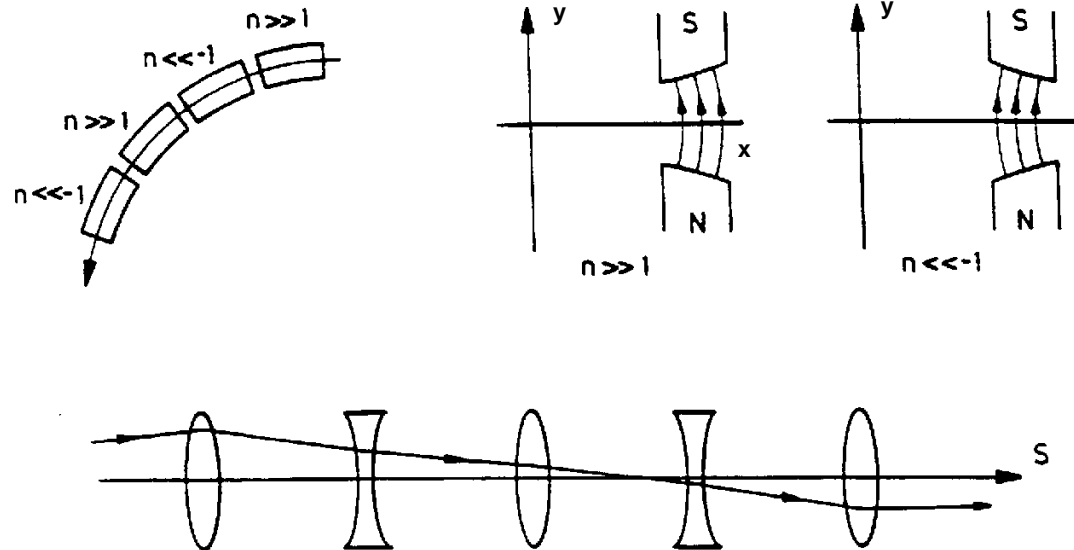
- As an example a “Button” Beam Position Monitor (BPM) is shown.
- The particle beam “Beam” in the middle of the vacuum chamber couples to buttons of the monitor and generates signals  $\Sigma U_i$ , which allow to determine it’s position
- **Horizontal Beam Position** =  $c_M ((U2 + U4) - (U1 + U3)) / \Sigma U_i$
- **Vertical Beam Position** =  $c_M ((U1 + U2) - (U3 + U4)) / \Sigma U_i$ ,  $c_M$  = monitor constant.
- At the SLS 73 “button” BPMs are part of a digital BPM System. Orbit deviations are measured to better than  $1 \mu\text{m}$  @ 4 kHz sampling rate.

## What is a Closed Orbit and what is “weak” focussing ?



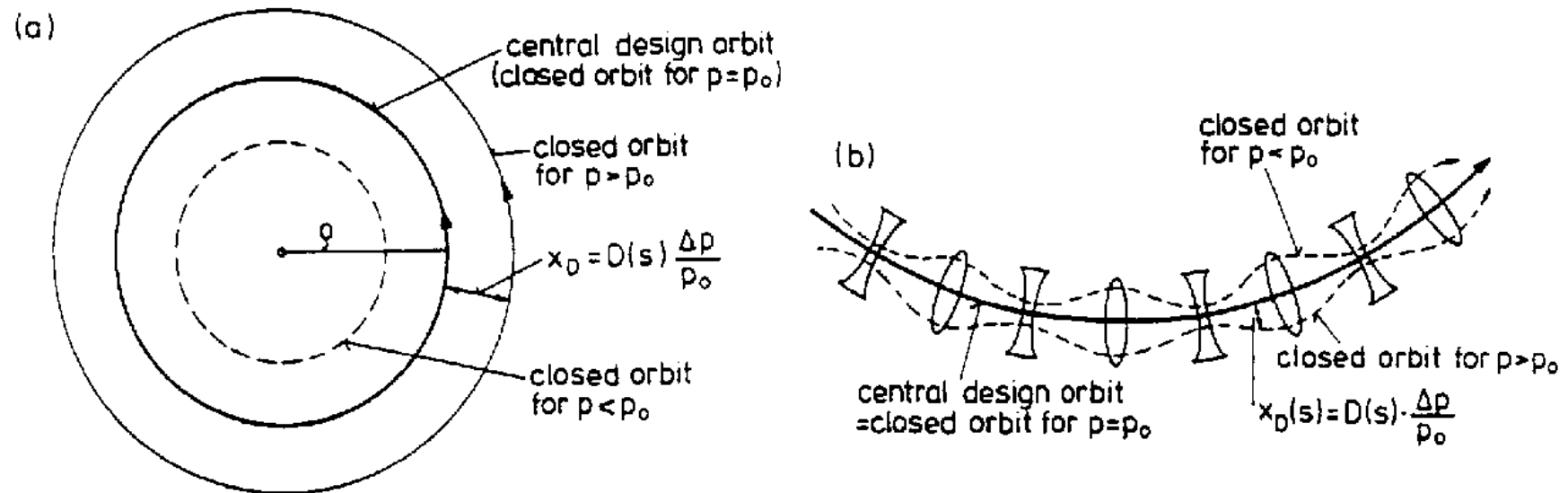
- A periodic closed particle trajectory is called “Closed Orbit”.
- The “Design Closed Orbit” is the closed orbit, which is established at design energie  $p_0$ , if the Optics has no errors. Generally this orbit is centered in the magnets and BPMs.
- Particles with different initial conditions than the closed orbit particle oscillate around the “Closed Orbit”.
- In the case of a homogenous magnetic field there is just “weak” fokussing: particles move on different circles depending on the initial angles at  $P_1$  and  $P_2$  (left). Along the “Design Orbit” these trajectories look like oscillations around this orbit (right).

## What is “strong” focussing ?



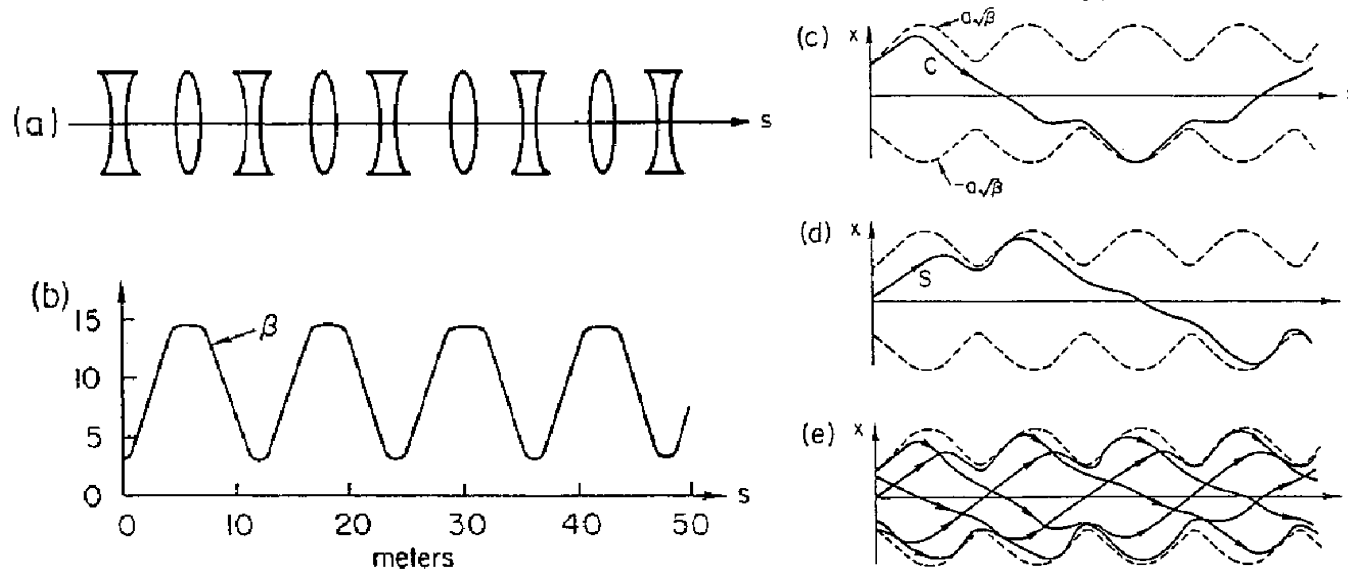
- In the case of “strong” (de)focussing quadrupoles are alternately (de)focussing the particles.
- This allows to have smaller magnet apertures, since the particles with varying initial conditions are kept closer to the “Closed Orbit”.
- In the SLS a total number of 177 quadrupoles is installed.
- The “strong” focussing increases the number of oscillations per turn (“Tune”). In the SLS this leads to  $\approx 20$  horizontal and  $\approx 8$  vertical full oscillations per turn.

## How does the Closed Orbit change with Energy ?



- In a homogenous magnetic field the radius of the “Closed Orbit” is proportional to the energy  $p$  (shown are the cases  $p < p_0$ ,  $p = p_0$  and  $p > p_0$ ). Thereby the “Closed Orbit” is getting shorter and longer which is also called “Path Length Change” (a).
- The right cartoon (b) visualizes the more complex situation in case of “strong” focussing.
- In general the so-called “Dispersion Function”  $D(s)$  describes the change of the particle position  $x_D$  at a given longitudinal position  $s$ :  $x_D = D(s)(p - p_0)/p_0$ .

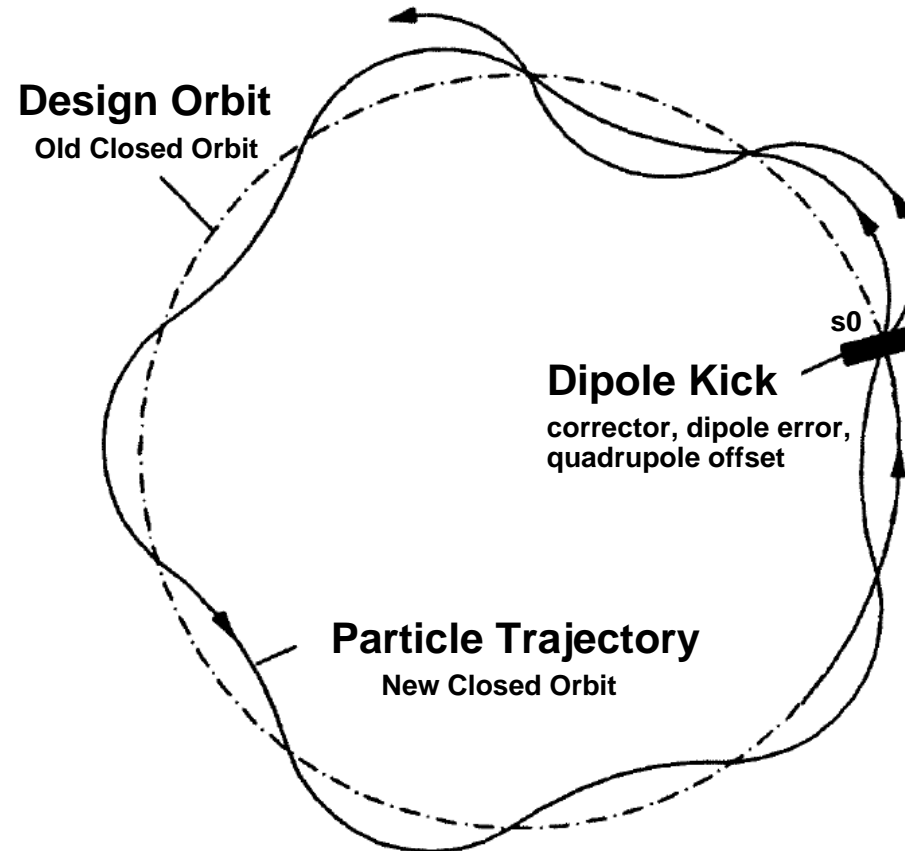
## Motion around the Closed Orbit



- Particles are performing “Betatron Oscillations” around the “Closed Orbit” (c-e).
- These oscillations are not closed, because otherwise the motion would be resonant !
- The “optics” in cartoon (a) is characterized by an amplitude function “Beta Function”  $\beta(s)$  which defines the envelope  $a\sqrt{\beta(s)}$  for these oscillations in cartoons (c-e).
- The “Beam Size” at a longitudinal position  $s$  is proportional to  $\sqrt{\beta}$  and to the constant  $a = \sqrt{\epsilon}$  where  $\epsilon$  is the so-called emittance which appears to be an invariant of motion.

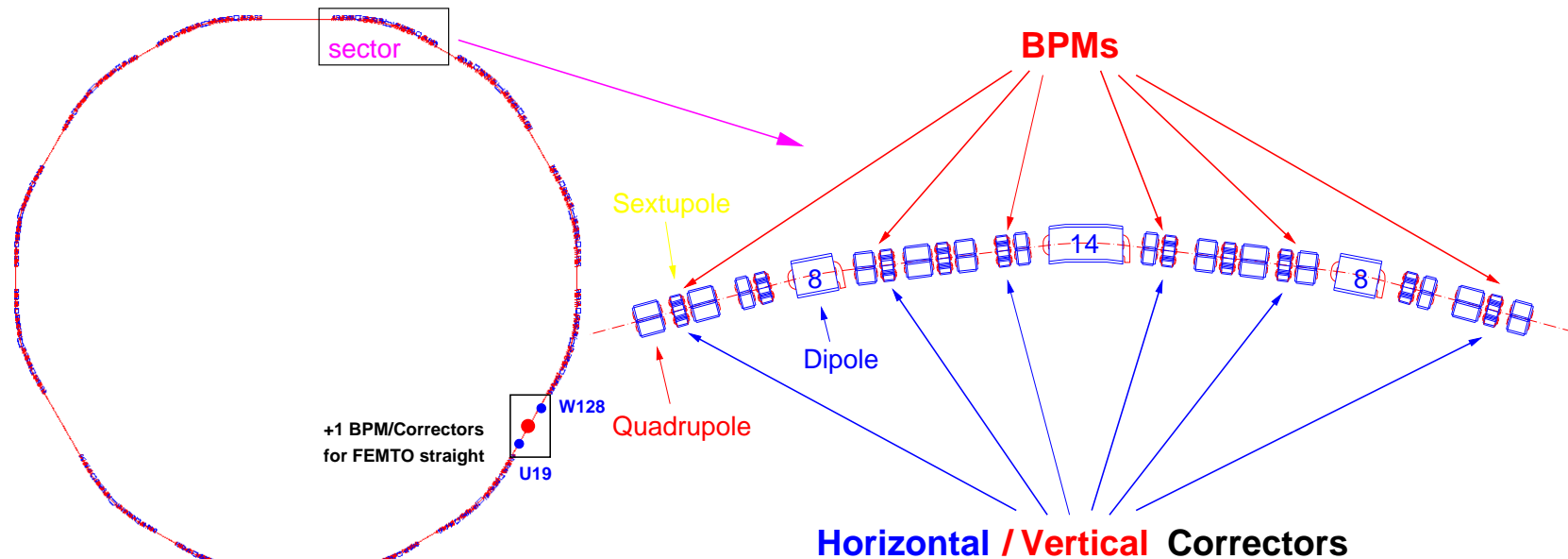


## How does the Closed Orbit change with Errors ?



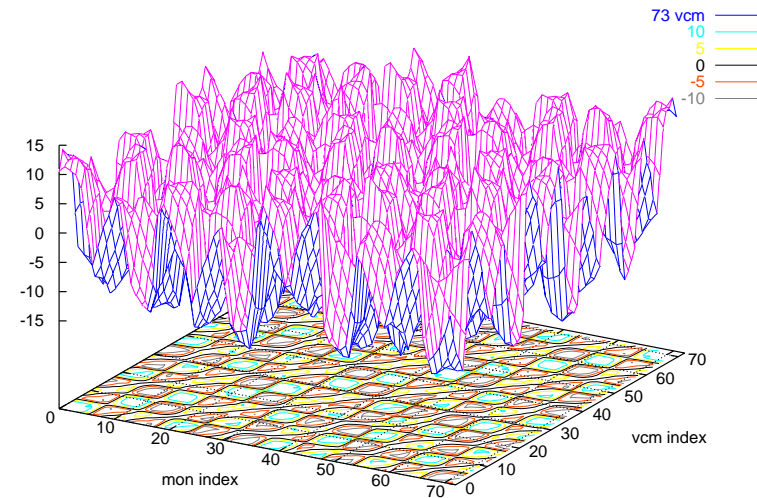
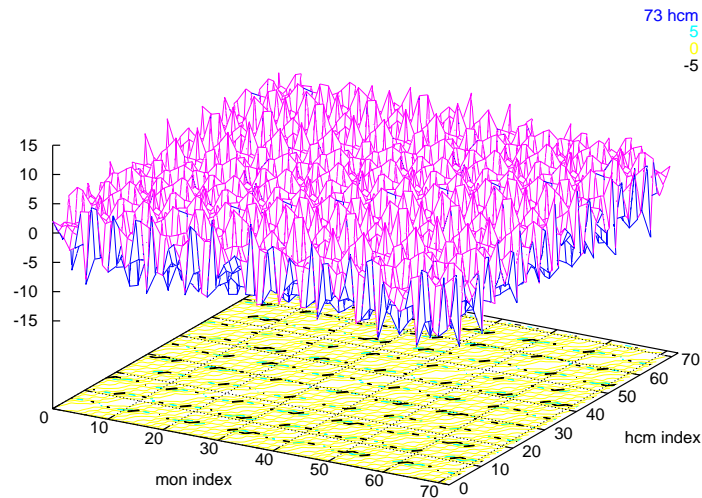
- The “Closed Orbit” is distorted under the influence of a magnet alignment/strength error or the deliberate change of a corrector. The RMS deviation from the “Old Closed Orbit” is proportional to  $\sqrt{\beta(s)}$  at the location  $s_0$ .

## BPM and Corrector Layout (SLS)



- The SLS Storage Ring is divided into 12 **sectors**.
- Pairs of 6 **BPMs** and 6 **horizontal/vertical** Dipole Corrector Magnets are distributed over one **Sector** (+1 **BPM/Correctors** set for FEMTO straight).
- The Corrector Magnets are implemented as extra windings on the **Sextupoles**, the **BPMs** are adjacent to the **Quadrupoles** (nonzero orbit in a quadrupole field leads to a dipole kick).

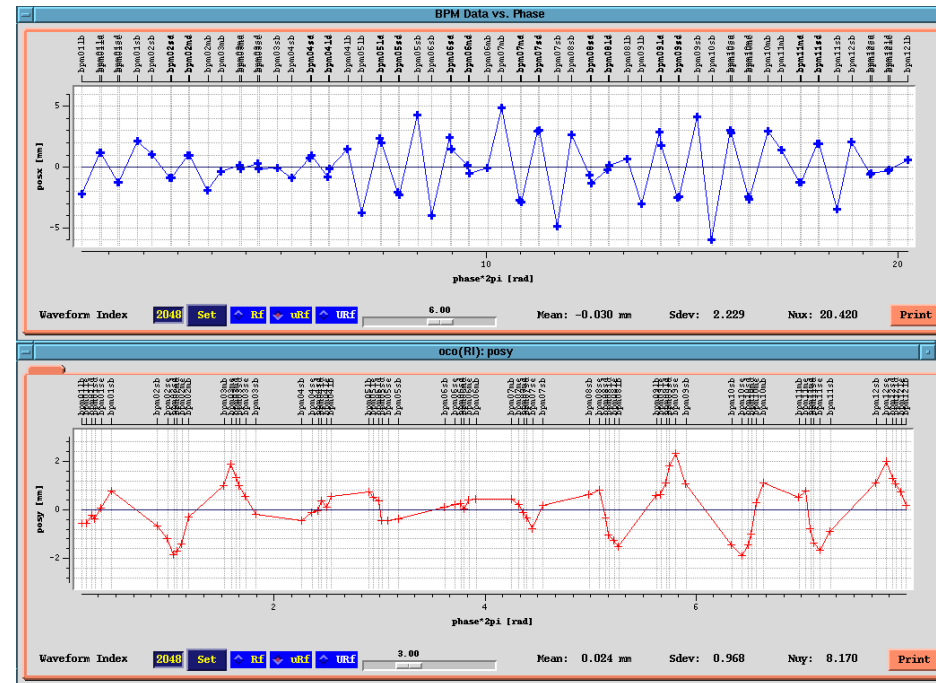
## Corrector / BPM Response Matrices (SLS)



$$A_{ij} = \frac{\sqrt{\beta_i \beta_j}}{2 \sin \pi \nu} \cos [\pi \nu - |\phi_i - \phi_j|]$$

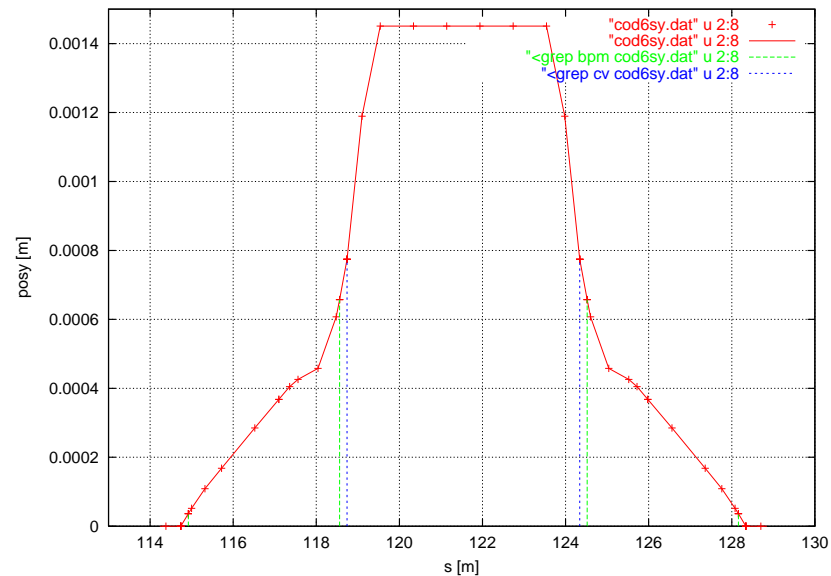
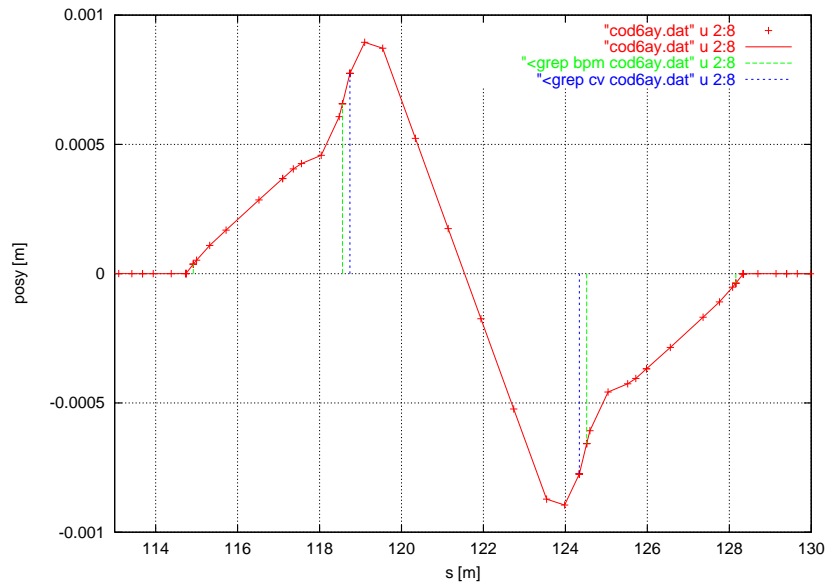
- “Response Matrix”: Differences from the “Closed Orbit” (“Difference Orbit”) due to a kick of corrector  $i$  are recorded at **BPM** positions  $j = 1..73$ .
- $\nu_x = 20.44$  ( $\approx 3$  BPMs/Correctors per unit phase,  $\phi = \int_0^s 1/\beta(s) ds$ )
- $\nu_y = 8.74$  ( $\approx 9$  BPMs/correctors per unit phase)

## What is a “Bare Orbit” ? (SLS)



- A “Bare Orbit” is a “Closed Orbit” without any corrections applied ( $\nu_x=20.42$ ,  $\nu_y=8.17$ ).
- The “Bare Orbit” is determined by the superposition of all magnet errors.
- $x_{rms} = 2.3$  mm,  $y_{rms} = 1$  mm gives upper limit for alignment errors of Quadrupoles/Sextupoles  $< 30$   $\mu$ m.
- The ratio of the RMS of the resulting “Closed Orbit” excitation and the originating RMS magnet distortions is called “Amplification Factor” ( $A_x=12$ ,  $A_y=8$ ).

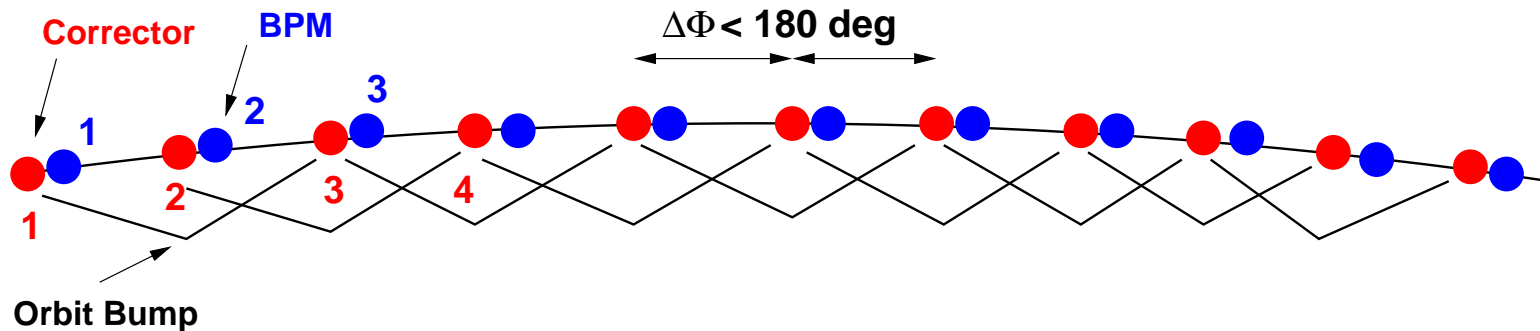
## Local Orbit Manipulations (SLS)



- The example depicts so-called **vertical** asymmetrical (left) and symmetrical (right) “4-Bumps” for an undulator beamline at SLS (well defined corrections involving 4 corrector magnets in order to independently vary position and angle at the location of the insertion device (ID) (angle and position steering by  $\approx -400 \mu\text{rad}$  and  $\approx 1.4 \text{ mm}$  is shown).
- “3-Bumps” consist of 3 magnets and are used to change position or angle at a given location.
- The corrector magnets in a bump have fixed phase- and beta function dependent kick ratios, in order to close the bump (no residual oscillation outside of the bump).

## How is a Closed Orbit corrected ?

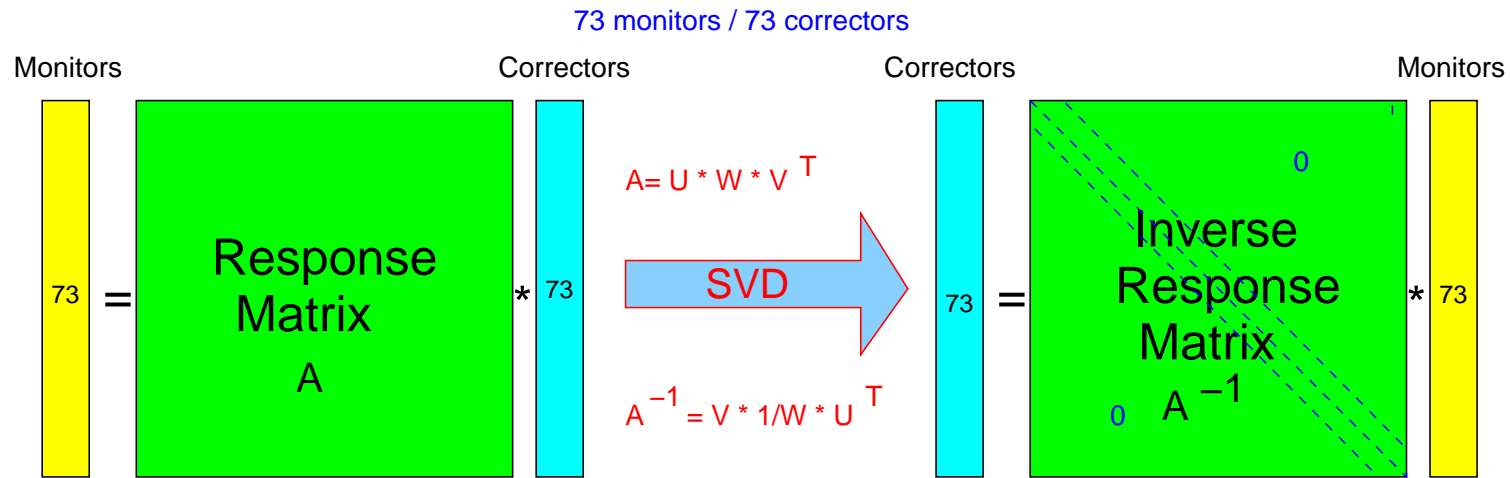
- **Sliding Bump** - Phase advances between **Correctors**  $0^\circ < \Delta\phi < 180^\circ$ , **Correctors 1,2,3** allow to zero the orbit in **BPM 2** near **Corrector 2**. **1** opens “Orbit Bump”, **2** provides kick for **3** to close it again. Continue (“Slide”) with **2,3,4** to zero orbit in **BPM 3** ... iterate until orbit is minimized in all **BPMs** !



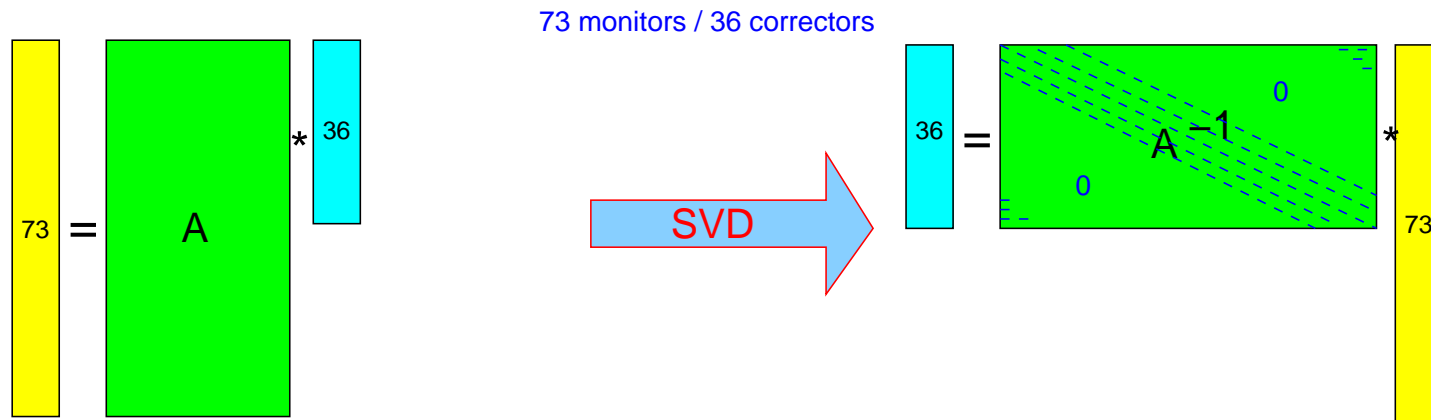
- **MICADO** - Finds a set of “Most Effective Correctors”, which minimize the RMS orbit in all **BPMs** at a minimum (“most effective”) RMS **Corrector** kick by means of the SIMPLEX algorithm. The number of **Correctors** (= iterations) is selectable.
- **Singular Value Decomposition (SVD)** - Decomposes the “Response Matrix”

$$A_{ij} = \frac{\sqrt{\beta_i \beta_j}}{2 \sin \pi \nu} \cos [\pi \nu - |\phi_i - \phi_j|]$$
 containing the orbit “response” in **BPM i** to a change of **Corrector j** into matrices  $U, W, V$  with  $A = U * W * V^T$ .  $W$  is a diagonal matrix containing the sorted Eigenvalues of  $A$ . The “inverse” correction matrix is given by  $A^{-1} = V * 1/W * U^T$ . SVD makes the other presented schemes obsolete !-

# What is SVD doing ?

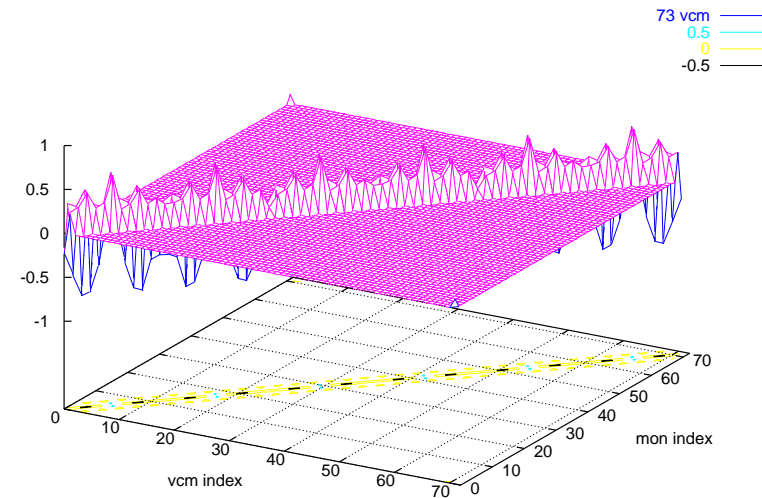
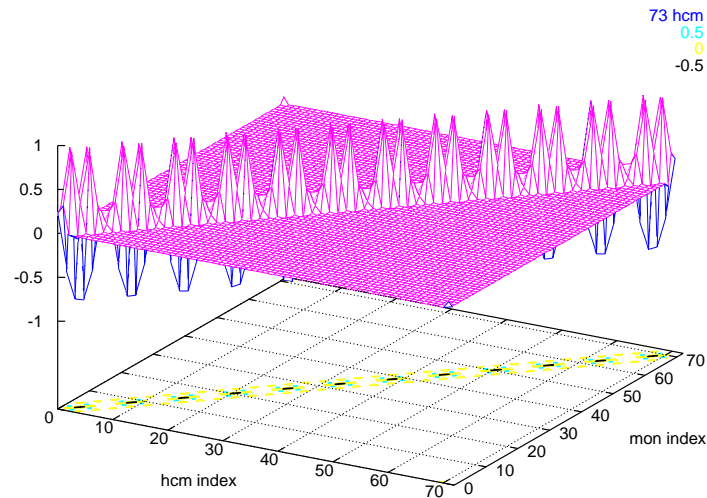


=> Minimization of the RMS orbit (=0 in case of "Matrix Inversion" using all Eigenvalues)



=> Minimization of the RMS orbit (monitor averaging)

## Inverse Corrector / BPM Response Matrices (SLS)

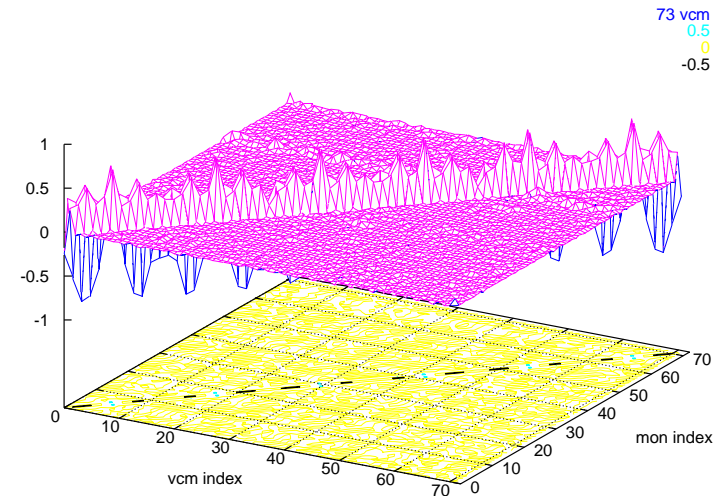
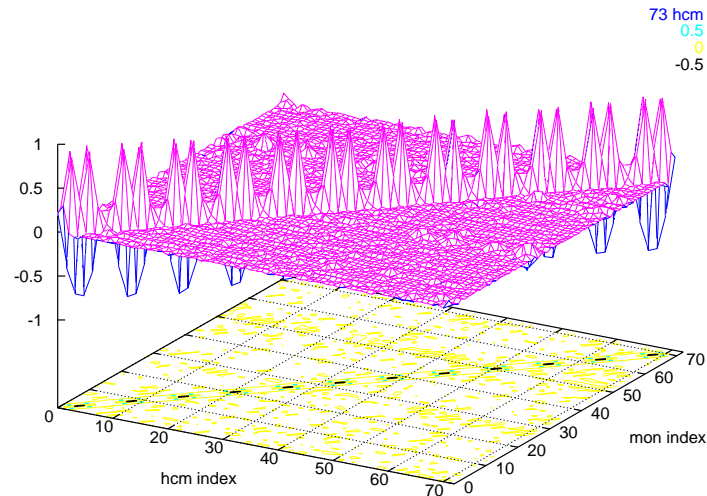


$$A_{ij}^{-1} = (V * 1/W * U^T)_{ij}$$

- $A_{ij}^{-1}$  is a sparse “*tridiagonal*” matrix (3 large (+1 small) adjacent coefficients are nonzero since BPM and Corrector positions are slightly different)  
→ “Sliding Bump Scheme” iteratively inverts  $A$
- $A_{ij}^{-1}$  contains *global* information although it is a “*tridiagonal*” matrix !  
→ Implementation of a Fast Orbit Feedback (FOFB)



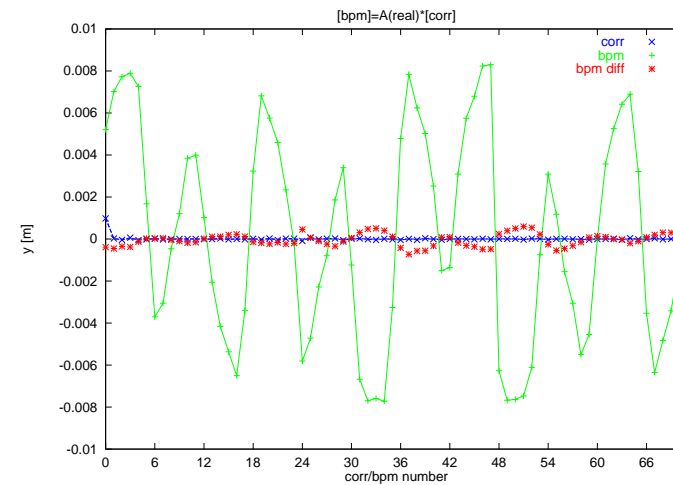
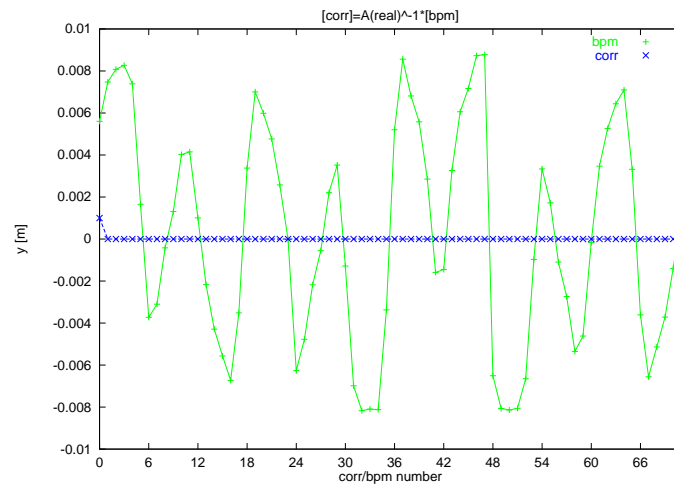
# Inverse Measured Corrector / BPM Response Matrices (SLS)



- Horizontal  $\beta$  Beat:  $\approx 4\%$  (RMS  $\Delta(\beta - \beta_0)/\beta_0$ )
- Vertical  $\beta$  Beat:  $\approx 3\%$

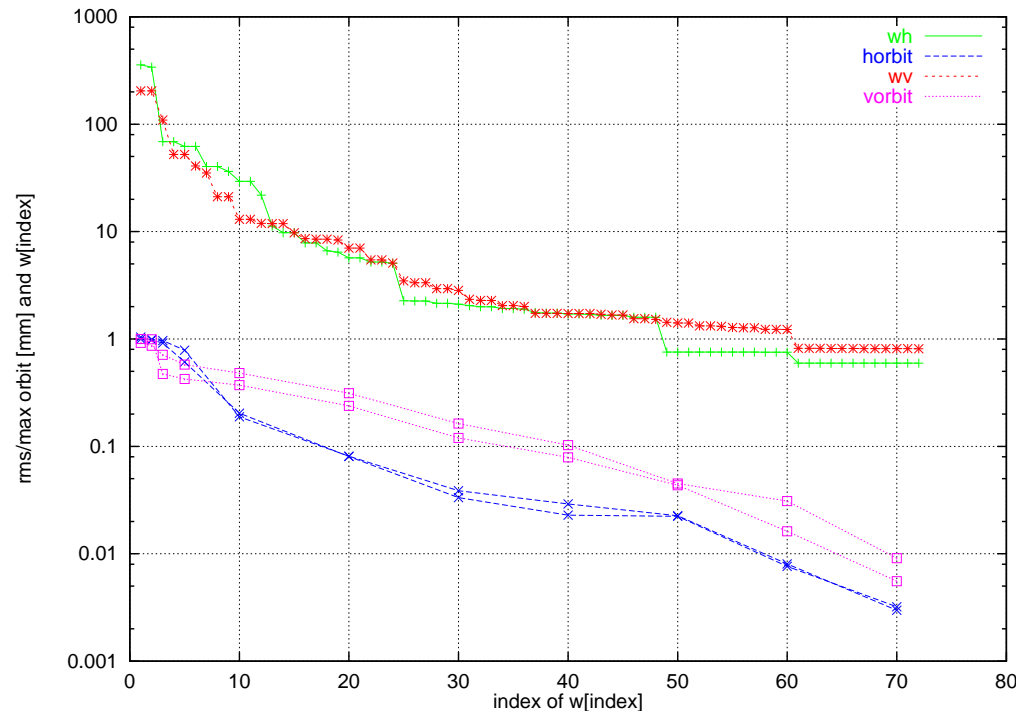
$\rightarrow A(\text{real})_{ij}^{-1}$  is still a sparse “tridiagonal” matrix plus some noise

## Single Corrector Example



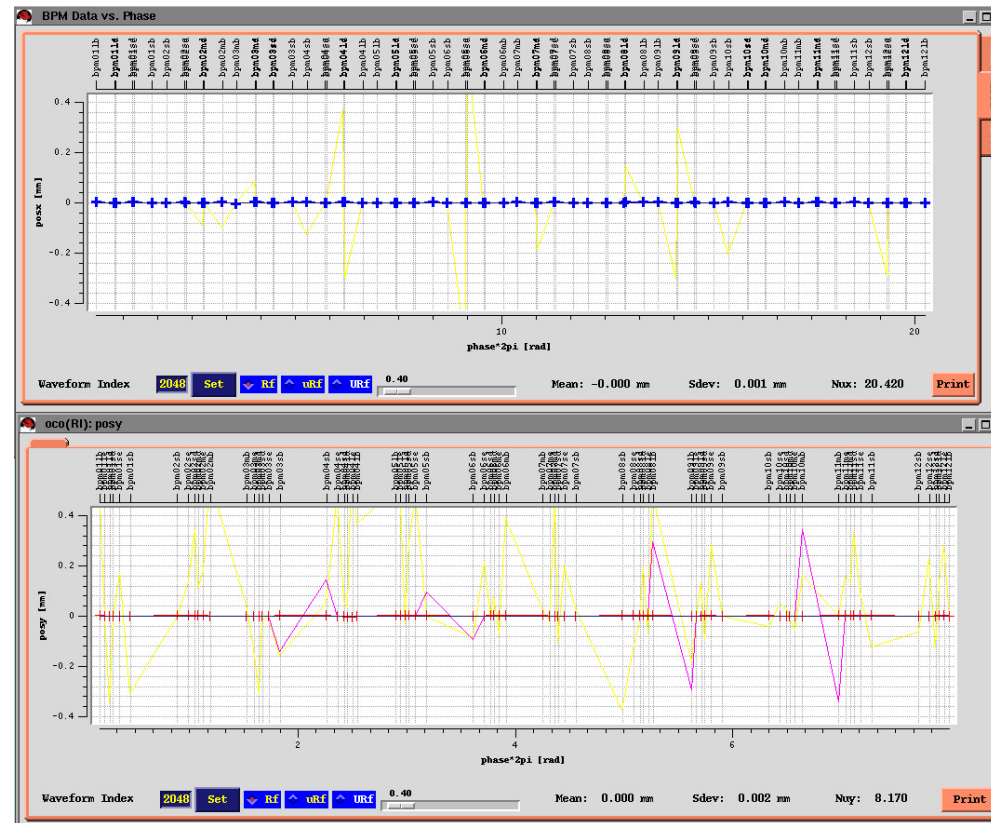
- Vertical  $\beta$ tron oscillation in a machine with distortions
- The measured  $A(\text{real})_{ij}^{-1}$  would predict *one* corrector
- $A(\text{ideal})_{ij}^{-1}$  for the ideal machine predicts *one* corrector plus some noise on the other correctors
- Residual  $\beta$ tron oscillation after the correction (removed by iteration)

## SVD Eigenvalues



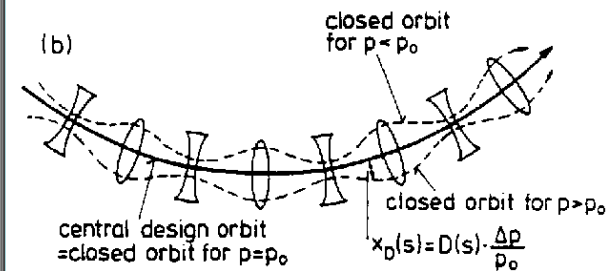
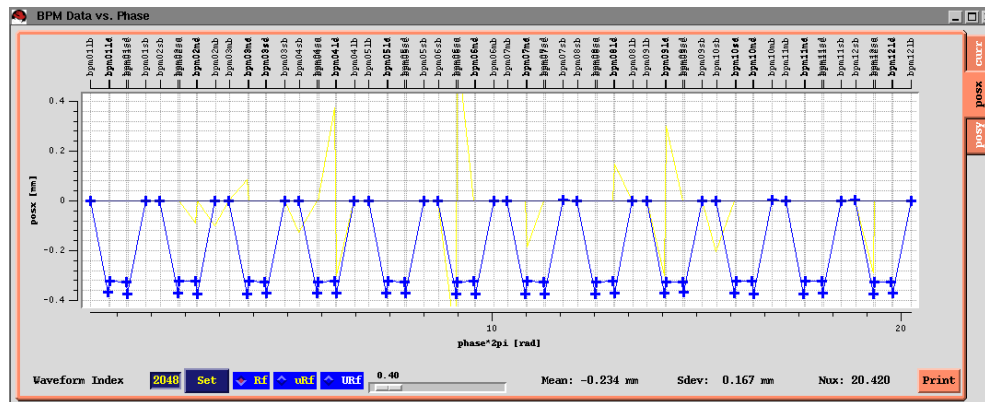
- Range of Eigenvalues  $0.5 < W < 500$
- Eigenvalue Cutoff @  $i_0$  ( $W_i = 0$  for  $i > i_0$ ) determines the minimum achievable RMS Orbit and Corrector Strength after Correction → “MICADO” like: the largest Eigenvalues correspond to the “Most Effective Corrector” patterns
- No Cutoff corresponds to “Matrix Inversion”. The RMS Orbit after Correction is Zero !

## Closed Orbit after Correction - Golden Orbit



- Closed Orbit after correction deviates by  $x_{rms} \approx y_{rms} \approx 1 \mu\text{m}$  from the so-called “Golden Orbit”, which contains some extra steering for the IDs ( $\rightarrow$ No Cutoff).
- At SLS corrector values are at RMS values of  $\approx 140 \mu\text{rad}$  (1.3 A) and  $\approx 130 \mu\text{rad}$  (1.2 A).

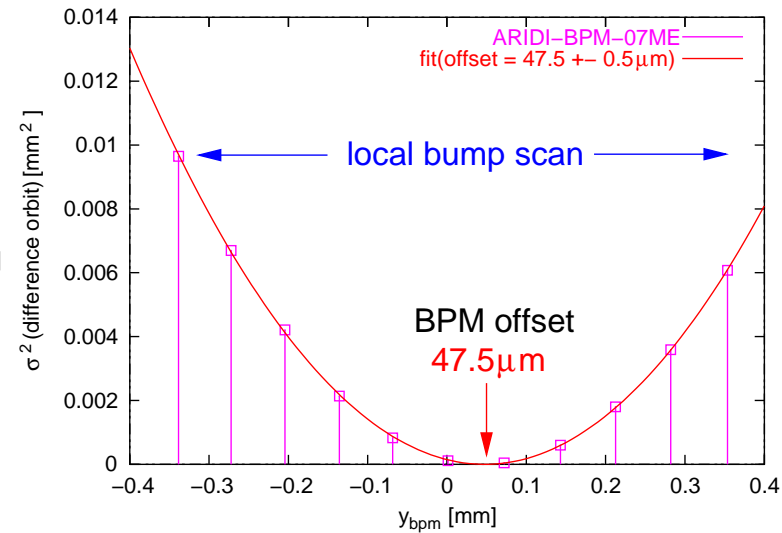
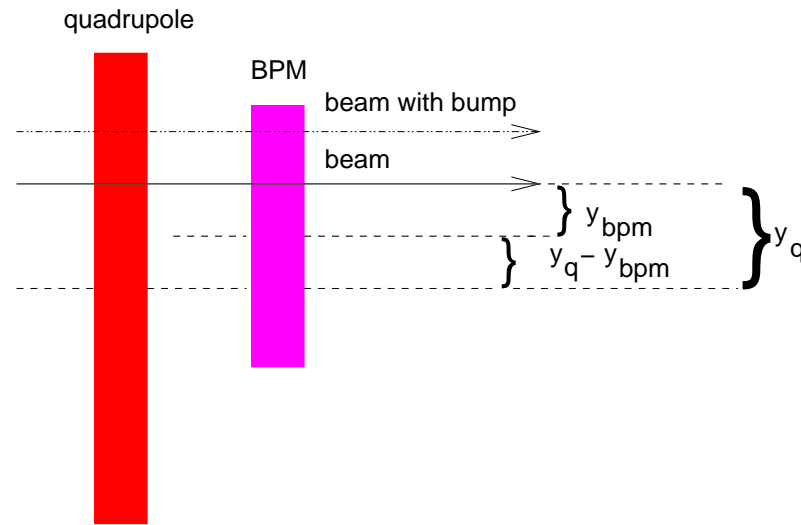
## How to correct Off-Energy Orbits ?



- In the case of “strong focussing” (b) the Orbit Deviation @ a location  $s$  is given by  $x_0(s) = D(s)\Delta p/p_0$  with  $\Delta p = p - p_0$ ,  $D(s)$  denotes the Dispersion.  
 $\Delta L/L_0 = \alpha_c \Delta p/p_0$  with the so-called “Momentum Compaction Factor”  
 $\alpha_c = 1/L_0 \int_0^{L_0} D(s)/\rho(s) ds (\approx 6 \cdot 10^{-4} \text{ at the SLS})$
- $p$  variations due to “Path Length”  $\Delta L/L_0$  (thermal or modelling effects) changes have to be corrected by means of the RF Frequency  $f$  with  $\Delta f/f = -\alpha_c \Delta p/p_0$  and NOT by the Orbit Correctors !

→ Fit  $\Delta p/p_0$  part of the Orbit using SVD on a 1 column response matrix containing dispersion values  $D_{i0}$  @ the BPMs and change the RF frequency by  $-\Delta f$  to correct for  $\Delta p/p_0$  !

## How is the position of BPMs measured ?



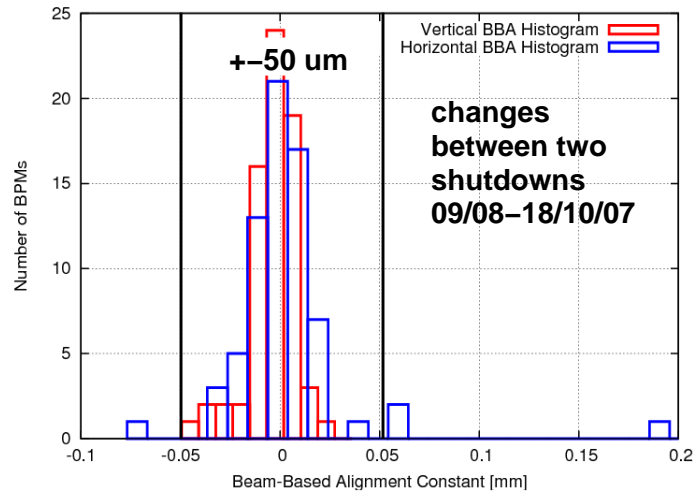
The so-called “Beam-Based Alignment” (BBA) (with respect to quadrupoles) technique is based on the fact that if the strength of a single quadrupole  $q$  in the ring is changed, the resulting difference in the closed orbit  $\Delta y(s)$  is proportional to the original offset  $y_q$  of the beam at  $q$ :

$$\Delta y''(s) - (k(s) + \Delta k(s))\Delta y(s) = \Delta k(s)y_q(s).$$

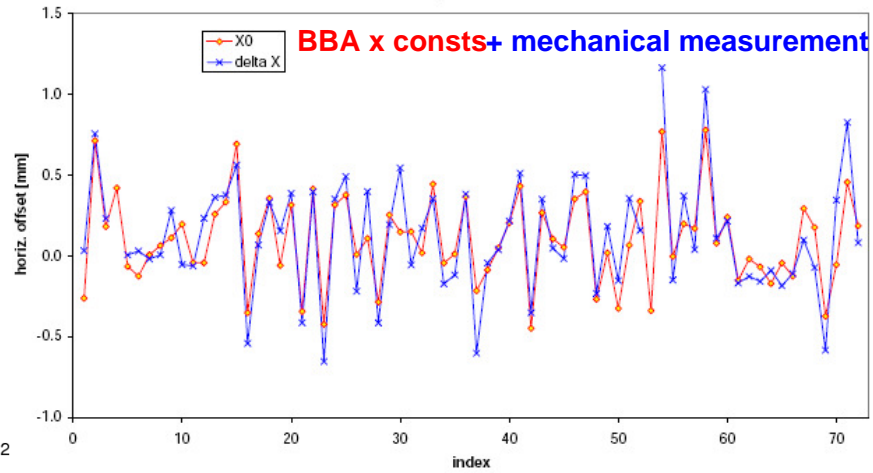
The difference orbit is thus given by the closed orbit formula for a single kick, but calculated with the perturbed optics including  $\Delta k(s)$ . From the measured difference orbit the kick and thus  $y_q$  can be easily determined and compared to the nominal orbit  $y_{bpm}$  in the BPM adjacent to the quadrupole, yielding the offset between BPM and quadrupole axis. The error of the position  $y_{bpm}$  is given by the resolution of the BPM system (Method can also be applied to sextupoles).

# Comparing BBA with Mechanical Measurements

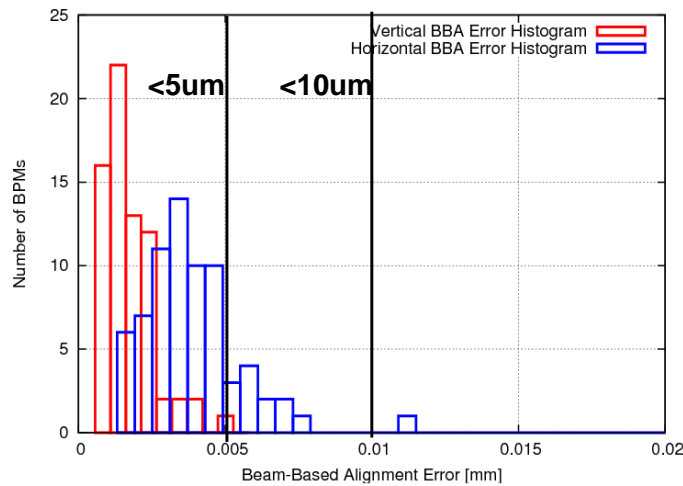
BBA dx/dy histograms for the SLS



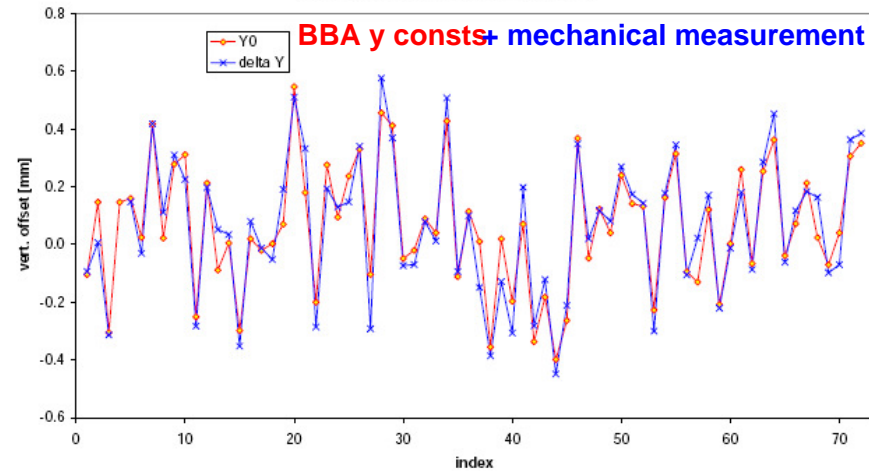
BPM horizontal offsets X0 and measured displacement delta X



BBA dx/dy error histograms for the SLS



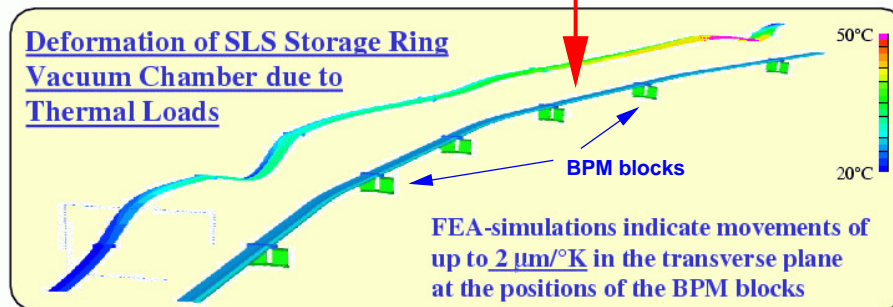
BPM vertical offsets Y0 and measured displacements delta Y



## Measuring BPM Positions with Linear Encoders (SLS)

FEA-simulations indicate:

chamber moves  $\sim 2 \mu\text{m}/\text{K}$  @ BPM blocks

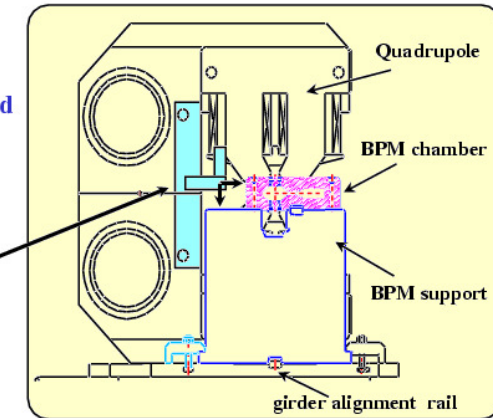
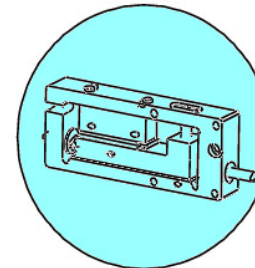


### POMS System

- Dial gauges sense transverse movements of BPM block in reference to adjacent quadrupole magnets.
- Linear encoders of type Renishaw RGH24Z50A00A with  $0.5 \mu\text{m}$  resolution are used as sensing devices.
- Complete integration into EPICS control system through serial SSI-interface and 32 channel VME-SSI card.

Measure BPM/Quadrupole offsets with  $0.5 \mu\text{m}$  resolution in  $x$  and  $y$  !  $\longrightarrow$   
 100 nm @ one undulator beamline

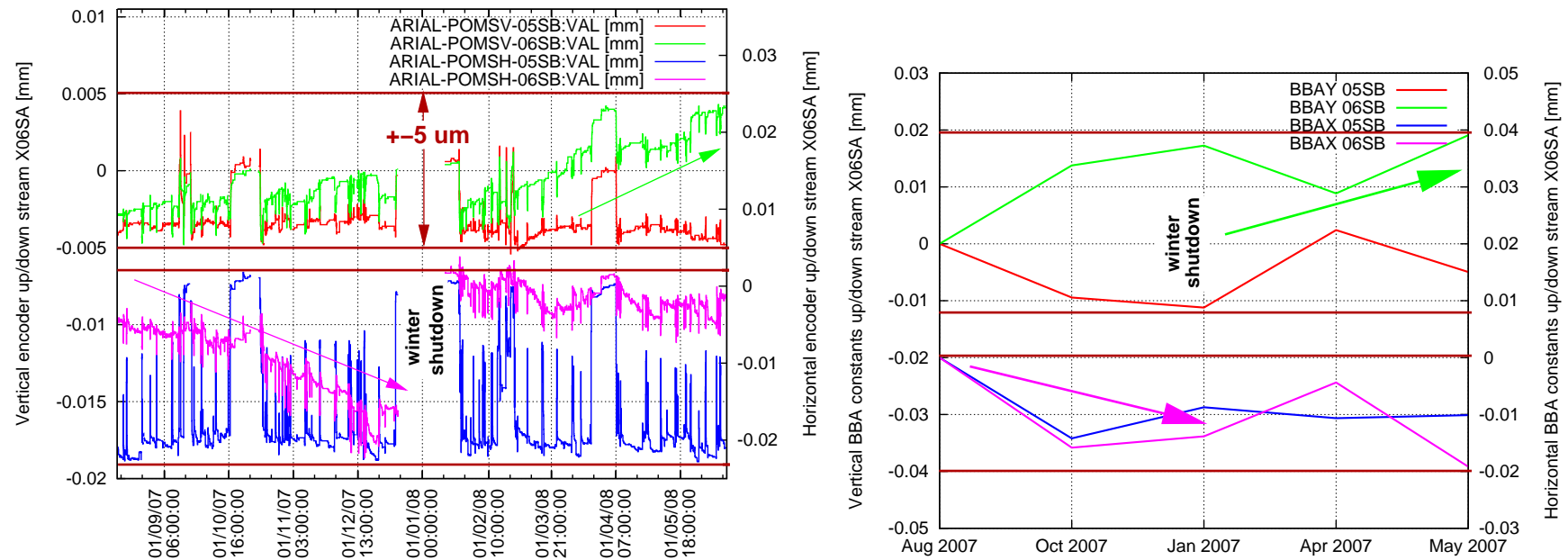
Dial gauges equipped with linear encoders as sensing devices attached to quadrupole magnets



- 6 BPMs per sector (+1 BPM in 5L / FEMTO)
- BPMs rigidly attached to girders (BPM support mounted on girder alignment rail)
- BPM supports serve as supports for the vacuum system ( $\longrightarrow$  BPM chamber)
- Initially planned to be used within the FOFB loop (NOT necessary  $\longrightarrow$  Top-Up)

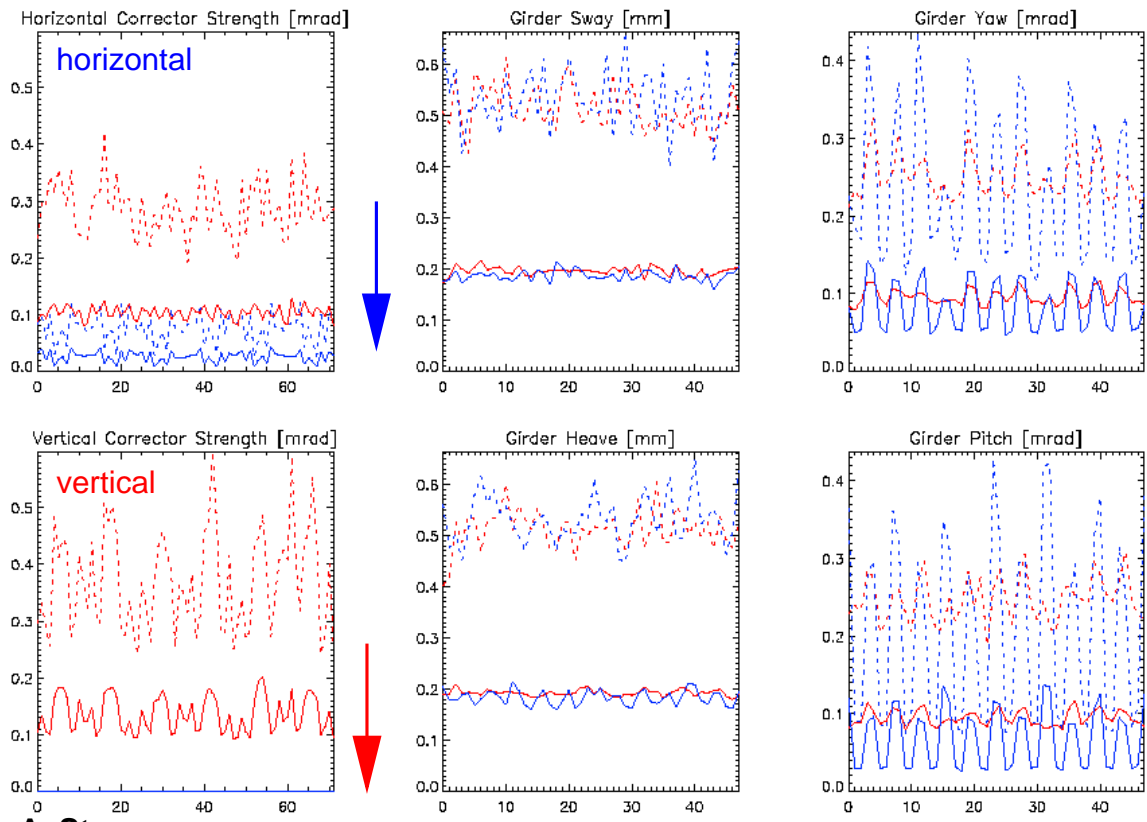


## Comparing BBA with Linear Encoders (SLS)



- Readings of the linear encoders (100 nm resolution) at an undulator beamline readings over  $\approx 10$  months stay within a band of  $\pm 5/10 \mu\text{m}$  in the x/y plane (Please note: SLS linear encoders don't have a calibrated zero position).
- The corresponding BBA constants are only roughly following these changes since they are also accounting for drifts of the electronics.

# What is Beam-Based Girder Alignment ?



rms \_\_\_\_\_  
max - - - - -  
**OCO only**  
**BBGA + OCO**  
SLS/D0 mode

**simulation**

200 seeds  
(12 rejected).  
error settings  
(rms, cut 2s):

- 50 μm magnet + BPM vs. girder,
- 300 μm girder abs.
- 100 μm girder vs. girder

A. Streun

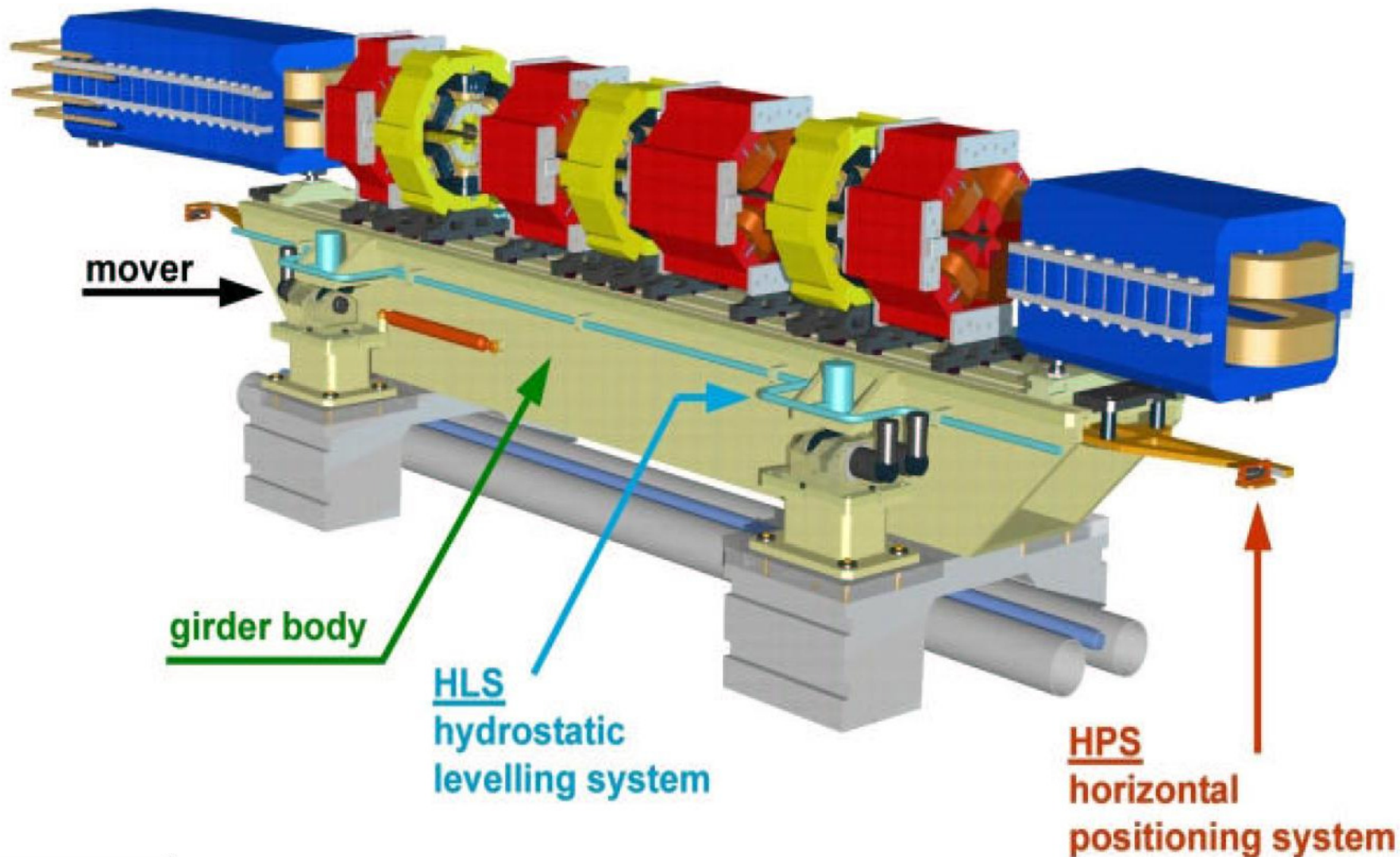
**Reshuffle Machine Errors → Minimize Distortions**

SVD weighting factor filter  $\omega_i/\omega_o >$   
SVD weighting factors used (from 96)

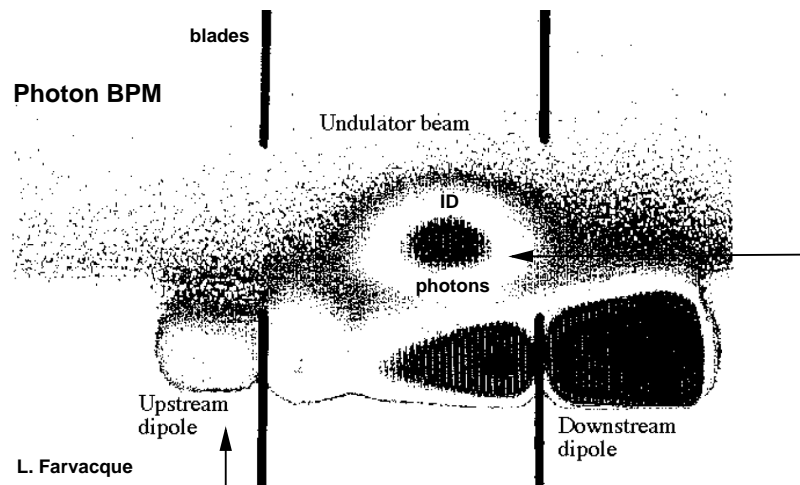
**saved magnetic corrector strength (rms)**      **75 %**      **100 %**

horizontal	vertical	girder remote control
0.001	0	
60	96	

**Girder Design (SLS)**



# BPMs Using the Photon Beam (X-BPMs)



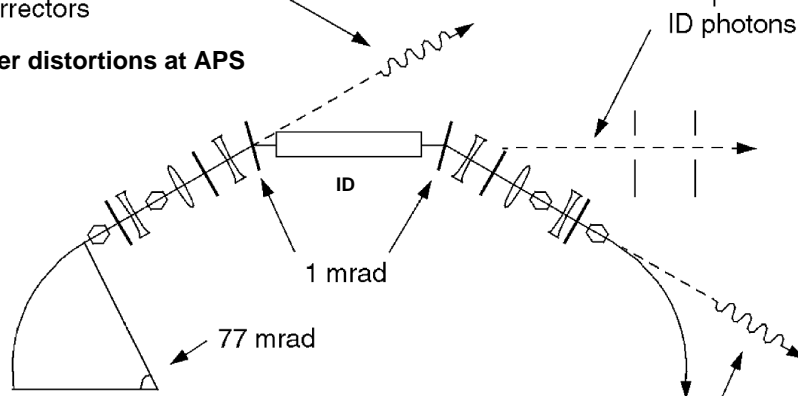
stray radiation from up- and down-stream magnets bias the reading of a Photon BPM

**Solution**

change strength of up- and down-stream dipoles (APS: 78→77 mrad)  
add 2 extra magnets (APS: 1 mrad)  
to account for the difference.

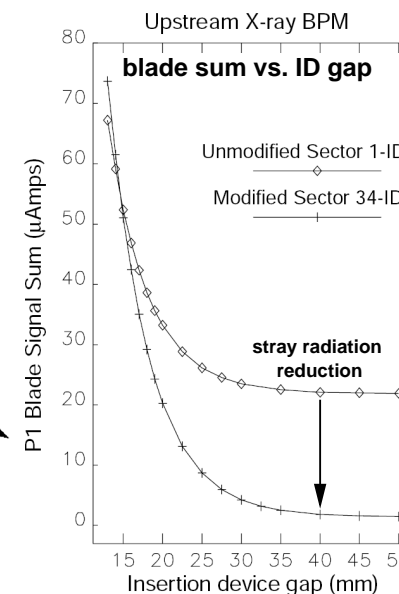
L. Farvacque  
Stray radiation from upstream dipole, quadrupoles, sextupoles and correctors

Decker distortions at APS



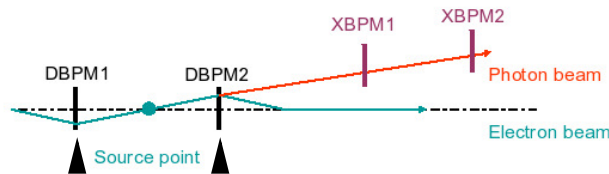
Stray radiation from down-stream dipole, quadrupoles, sextupoles and correctors

G. Decker

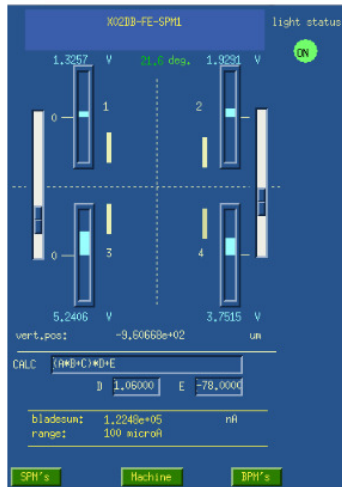


# Calibration of X-BPMs

Calibration using machine bumps [1]:



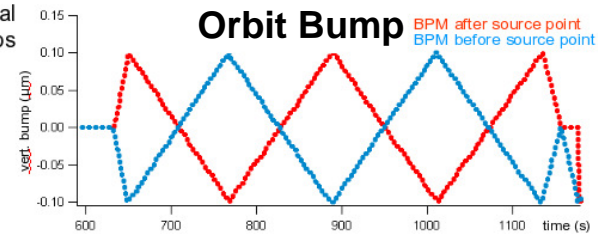
While the FOFB is running the reference positions of DBPM1 and 2 are varied.



Synoptic view of the PBPM in the control system

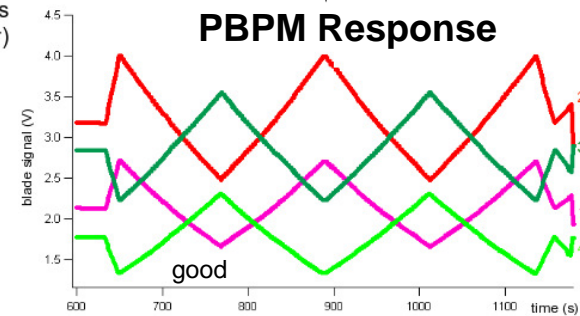
E. van Garderen (please visit her poster :-)

Vertical asymmetrical bumps

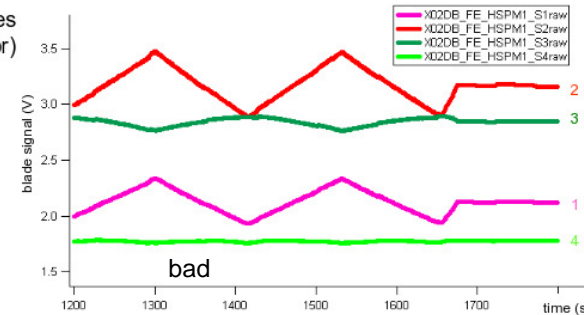


+100 um bump amplitude

Response of the blades (well aligned monitor)



Response of the blades (badly aligned monitor)



Calibration using machine bumps is preferred to calibration using motors as it is a tool to detect alignments.