

# RF, part II

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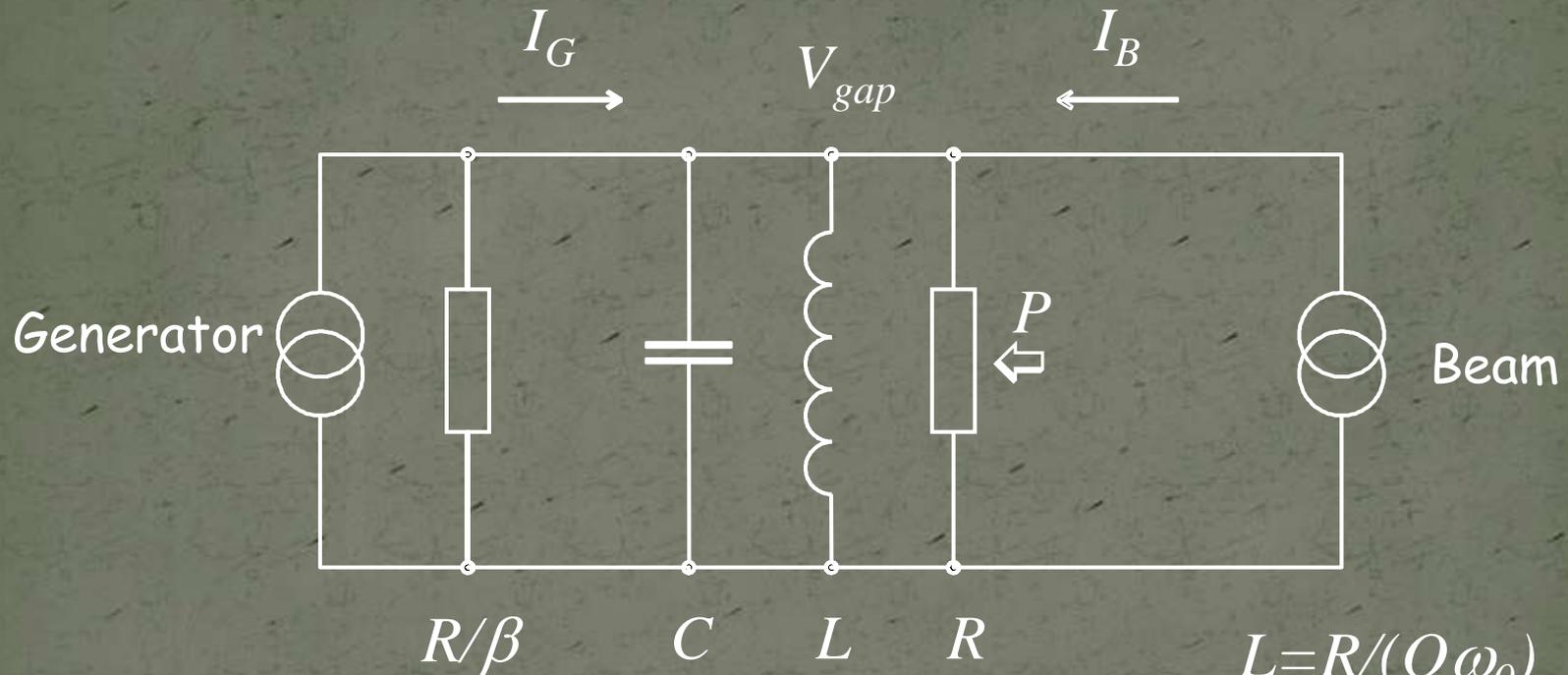
Erk Jensen, CERN BE-RF

# Characterizing a cavity

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# Cavity resonator – equivalent circuit

Simplification: single mode



$\beta$ : coupling factor

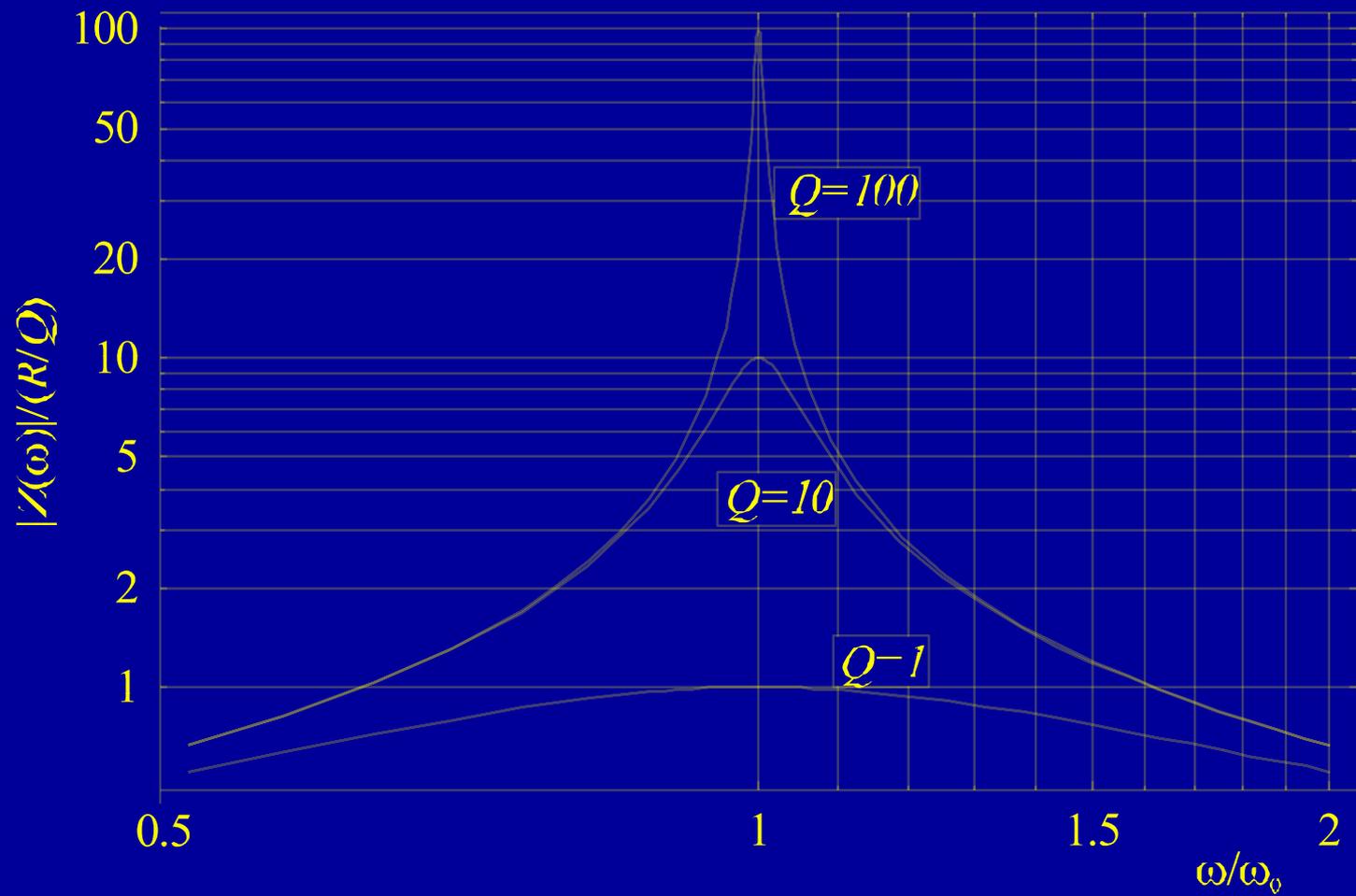
Cavity

$R$ : Shunt impedance

$\sqrt{L/C}$ : R-upon-Q

**We have used this before when explaining the “fast feedback”**

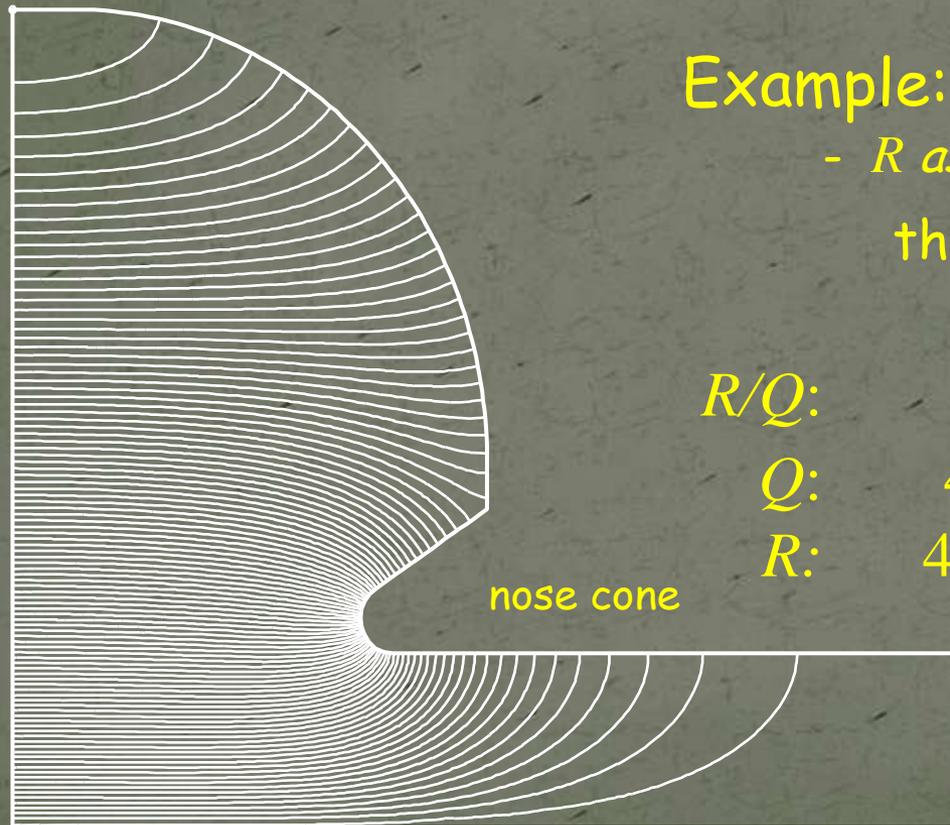
# Resonance



# Reentrant cavity

Nose cones increase transit time factor, round outer shape minimizes losses.

Nose cone example Freq = 500.003



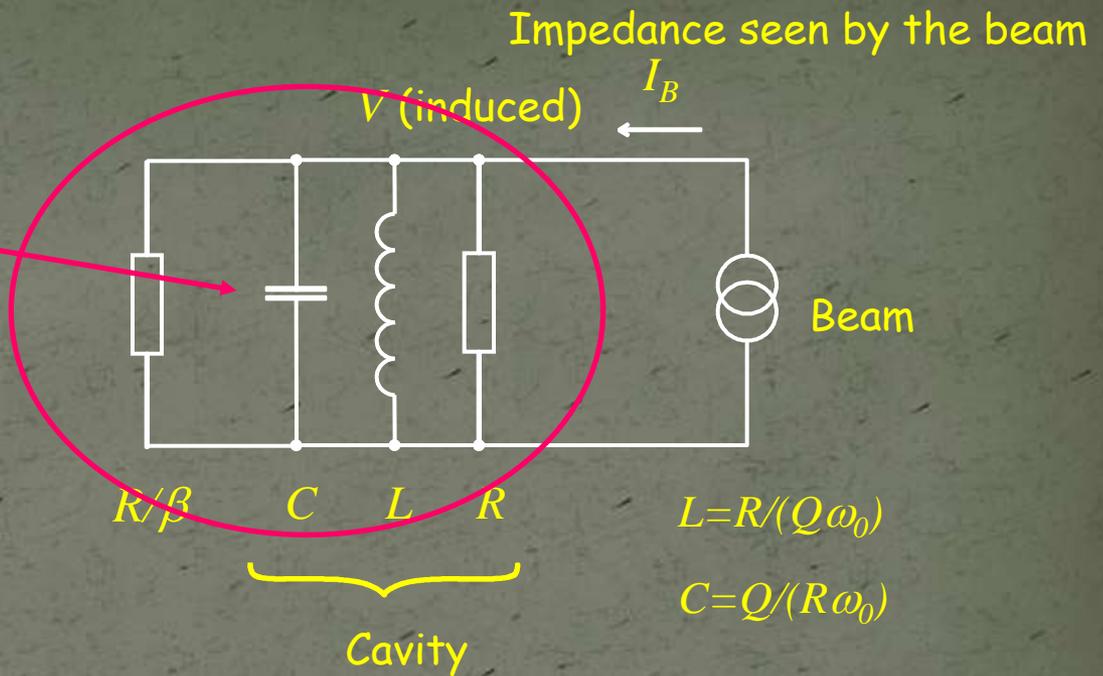
Example: KEK photon factory 500 MHz  
- *R as good as it gets* -

	this cavity	optimized pillbox
$R/Q$ :	111 $\Omega$	107.5 $\Omega$
$Q$ :	44270	41630
$R$ :	4.9 M $\Omega$	4.47 M $\Omega$

nose cone

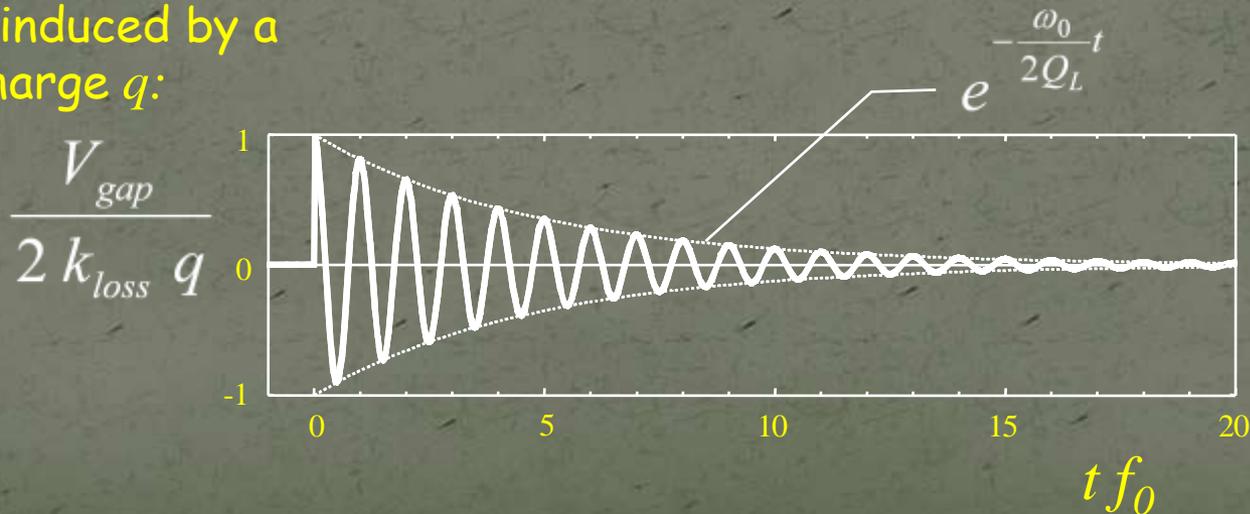
# Loss factor

$$k_{loss} = \frac{\omega_0 R}{2 Q} = \frac{|V_{gap}|^2}{4W} = \frac{1}{2C}$$

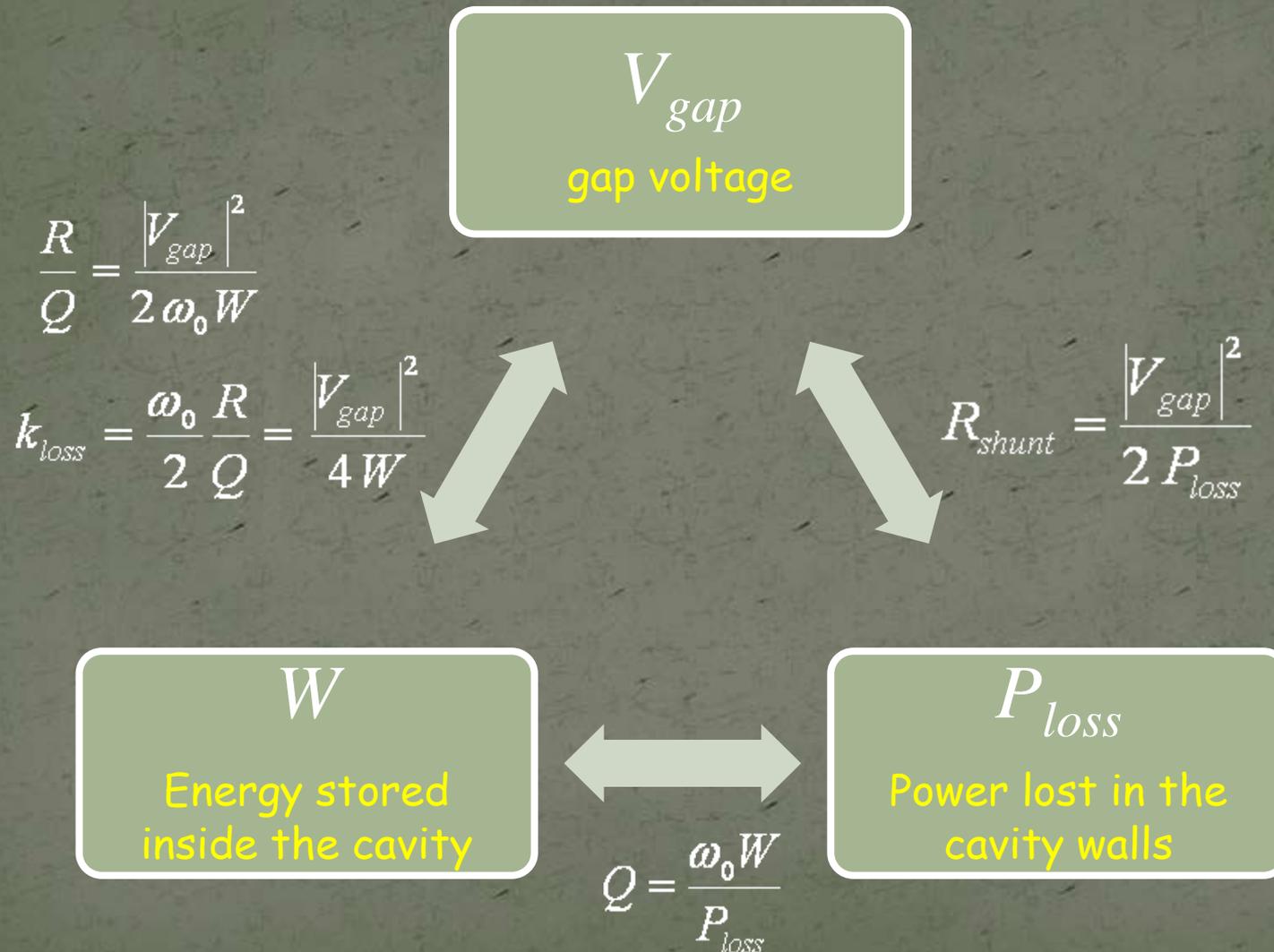


Energy deposited by a single charge  $q$ :  $k_{loss} q^2$

Voltage induced by a single charge  $q$ :



# Summary: relations $V_{gap}$ , $W$ , $P_{loss}$



# Beam loading – RF to beam efficiency

- The beam current “loads” the generator, in the equivalent circuit this appears as a resistance in parallel to the shunt impedance.
- If the generator is matched to the unloaded cavity, beam loading will cause the accelerating voltage to decrease.
- The power absorbed by the beam is  $-\frac{1}{2}\text{Re}\{V_{gap} I_B^*\}$ , the power loss  $P = \frac{|V_{gap}|^2}{2R}$ .
- For high efficiency, beam loading shall be high.
- The RF to beam efficiency is  $\eta = \frac{1}{1 + \frac{V_{gap}}{R|I_B|}} = \frac{|I_B|}{|I_G|}$ .

# Cavity parameters

- Resonance frequency

$$\omega_0 = \frac{1}{\sqrt{L \cdot C}}$$

- Transit time factor

field varies while particle is traversing the gap

$$\frac{\left| \int E_z e^{j \frac{\omega}{c} z} dz \right|}{\left| \int E_z dz \right|}$$

Circuit definition

- Shunt impedance

gap voltage – power relation

$$\left| V_{gap} \right|^2 = 2 R_{shunt} P_{loss}$$

- $Q$  factor

$$\omega_0 W = Q P_{loss}$$

- $R/Q$

independent of losses – only geometry!

$$\frac{R}{Q} = \frac{\left| V_{gap} \right|^2}{2 \omega_0 W} = \sqrt{\frac{L}{C}}$$

- loss factor

$$k_{loss} = \frac{\omega_0 R}{2 Q} = \frac{\left| V_{gap} \right|^2}{4 W}$$

Linac definition

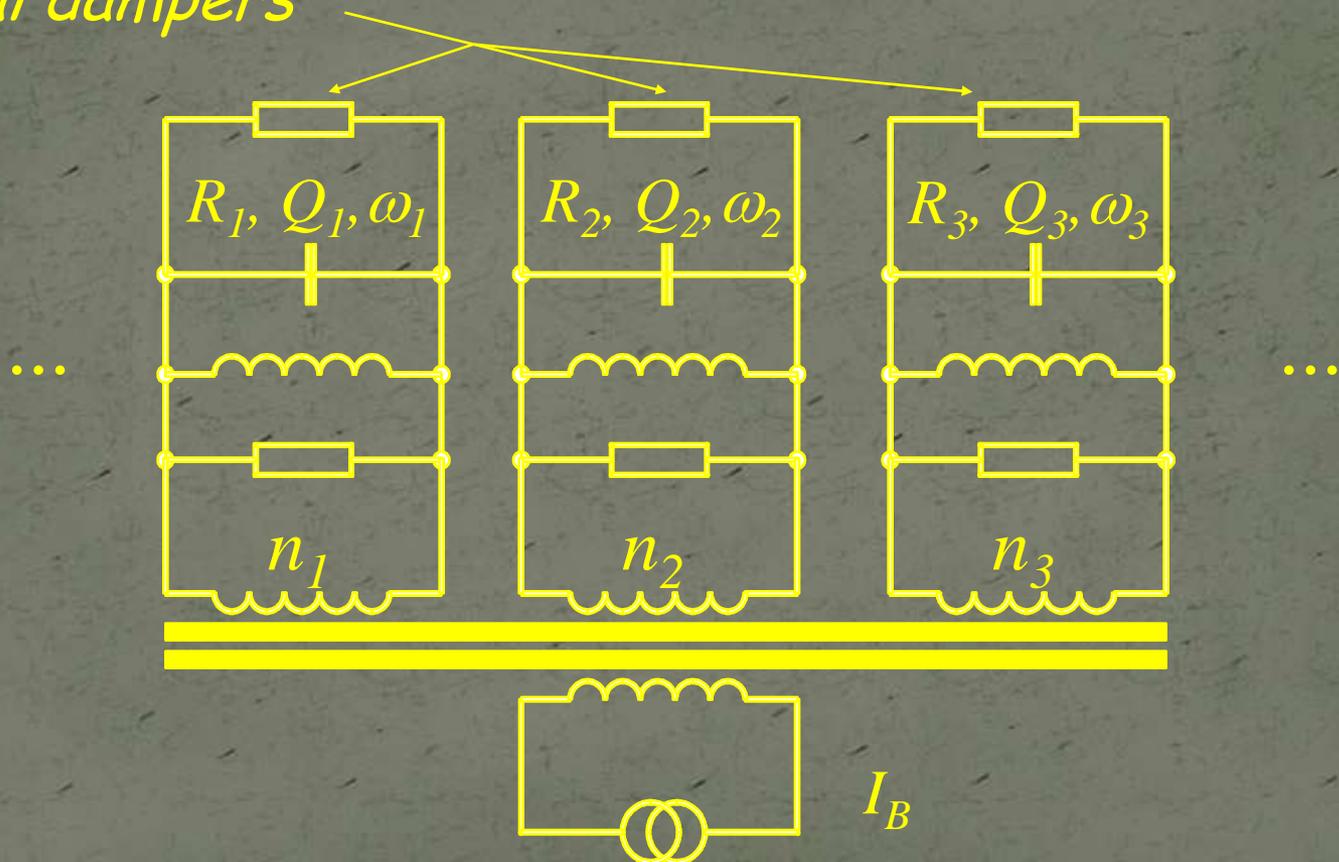
$$\left| V_{gap} \right|^2 = R_{shunt} P_{loss}$$

$$\frac{R}{Q} = \frac{\left| V_{gap} \right|^2}{\omega_0 W}$$

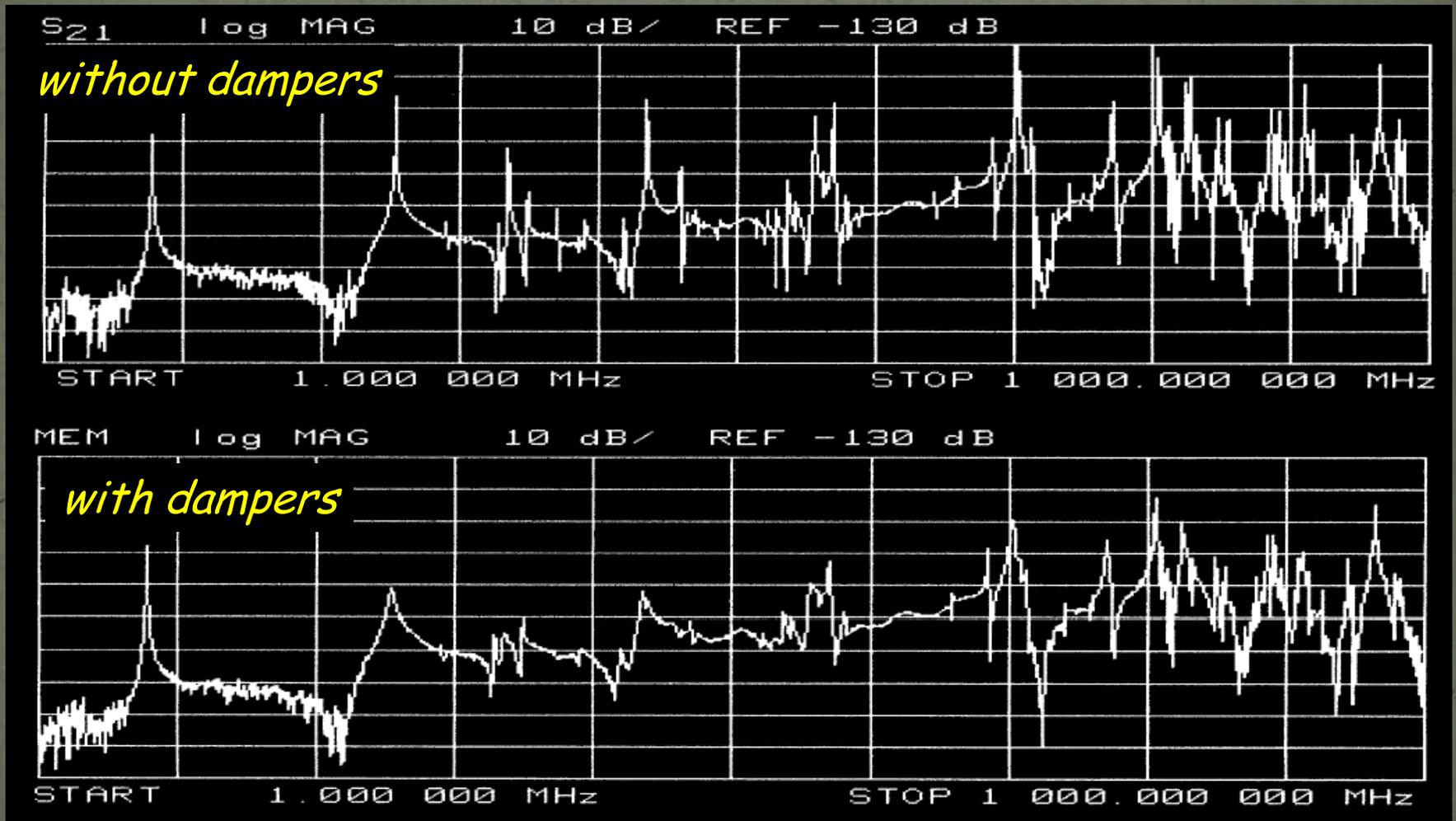
$$k_{loss} = \frac{\omega_0 R}{4 Q} = \frac{\left| V_{gap} \right|^2}{4 W}$$

# Higher order modes (HOM's)

*external dampers*



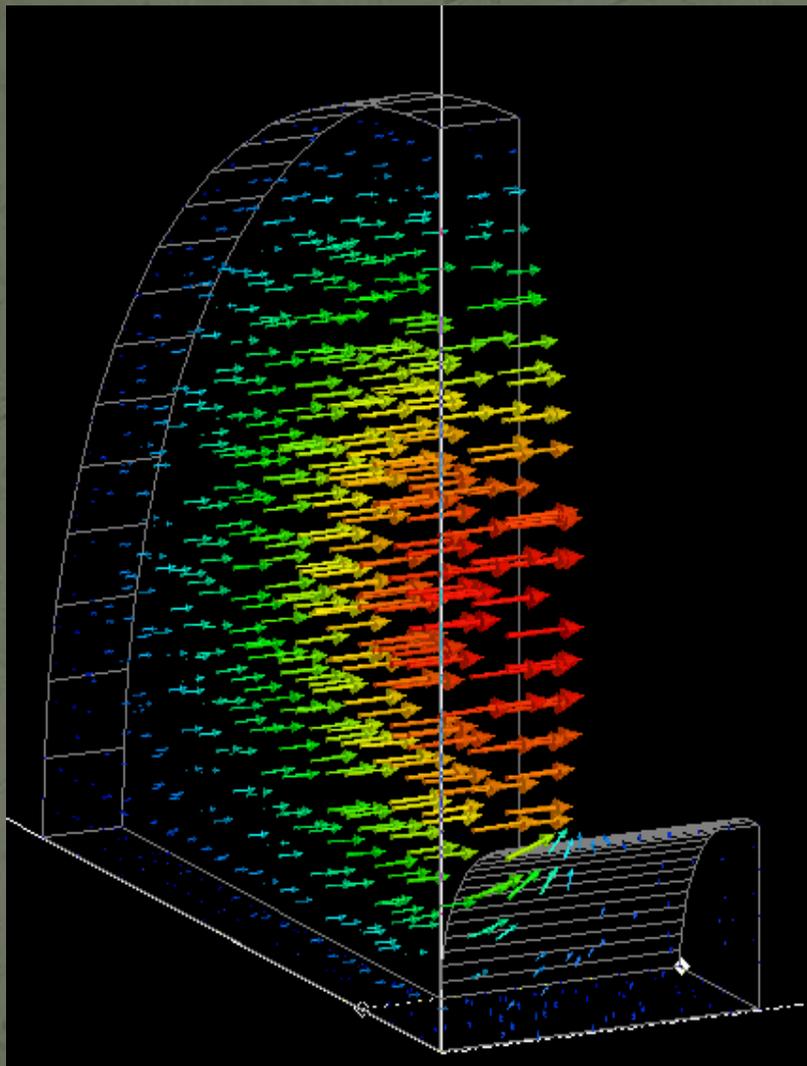
# HOM (measured spectrum)



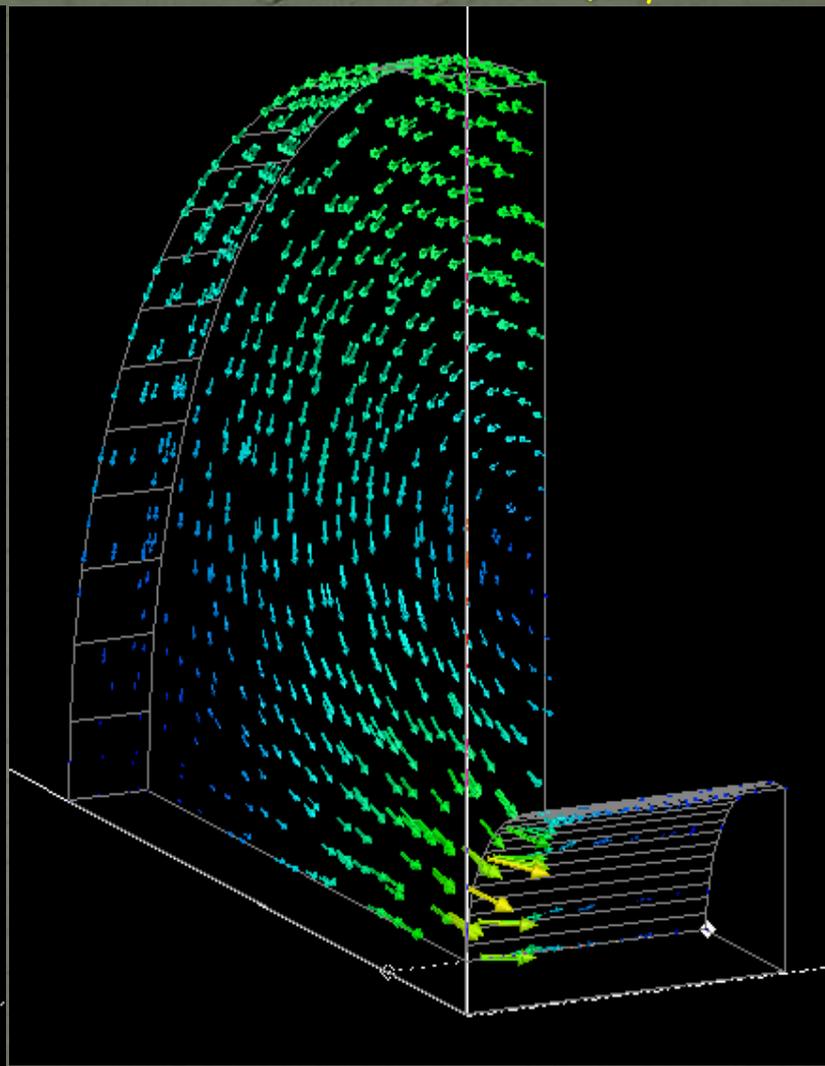
# Pillbox: Dipole mode

$(TM_{110})$

(only 1/8 shown)



electric field (@ 0°)



magnetic field (@ 90°)

# Panofsky-Wenzel theorem

For particles moving virtually at  $v=c$ , the integrated transverse force (kick) can be determined from the transverse variation of the integrated longitudinal force!

$$j \frac{\omega}{c} \vec{F}_{\perp} = \nabla_{\perp} F_{\parallel}$$

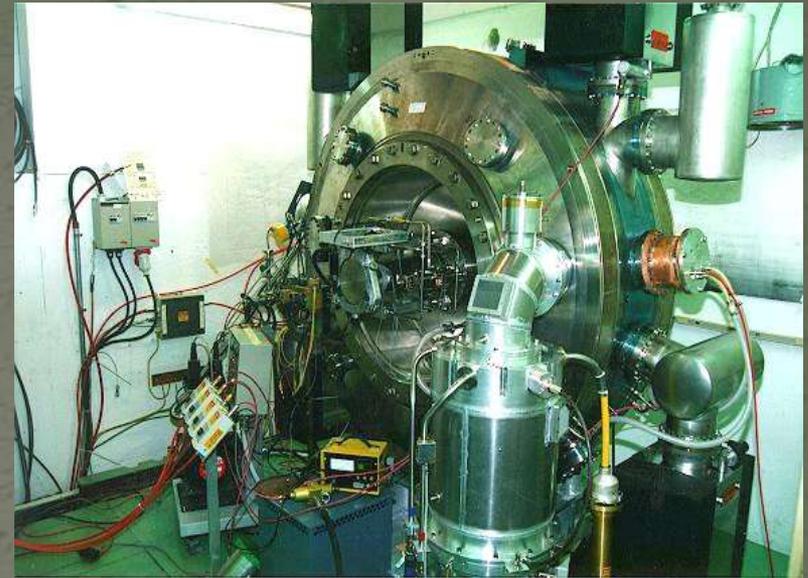
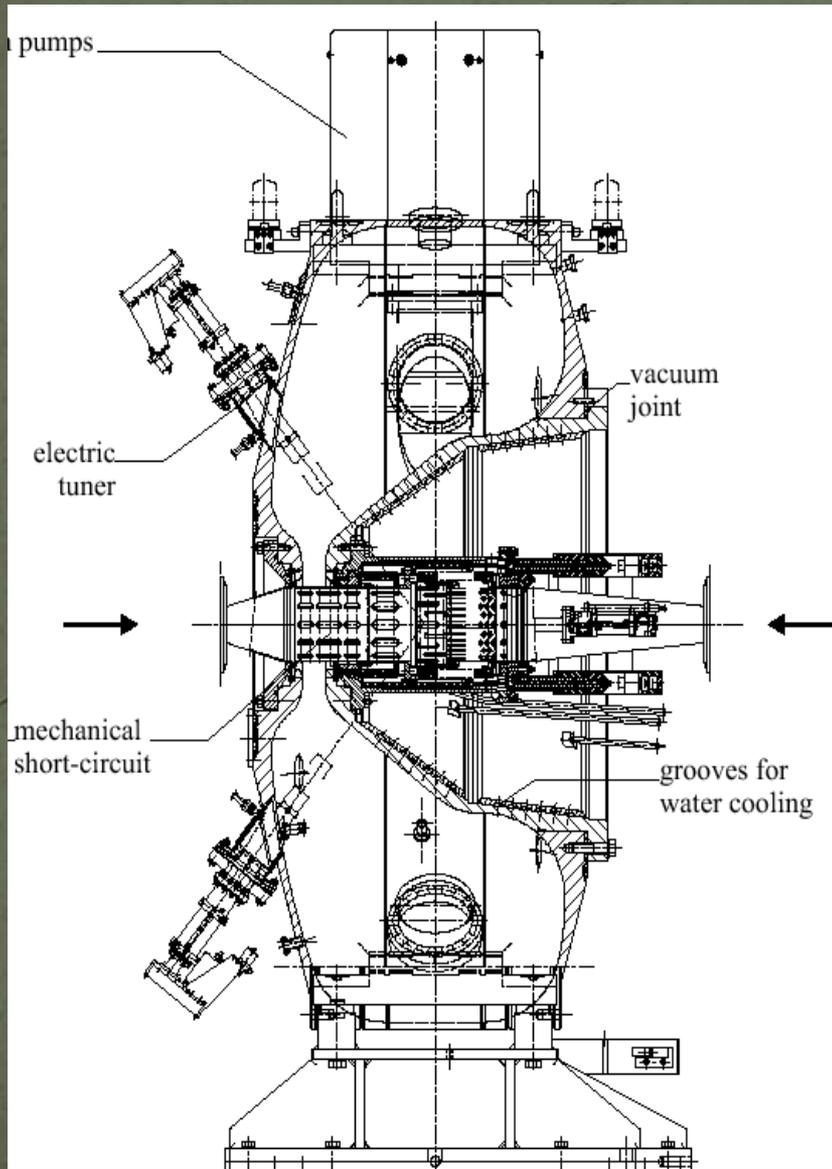
Pure TE modes: No net transverse force !

Transverse modes are characterized by

- the transverse impedance in  $\omega$ -domain
- the transverse loss factor (kick factor) in  $t$ -domain !

W.K.H. Panofsky, W.A. Wenzel: "Some Considerations Concerning the Transverse Deflection of Charged Particles in Radio-Frequency Fields", RSI **27**, 1957]

# CERN/PS 80 MHz cavity (for LHC)



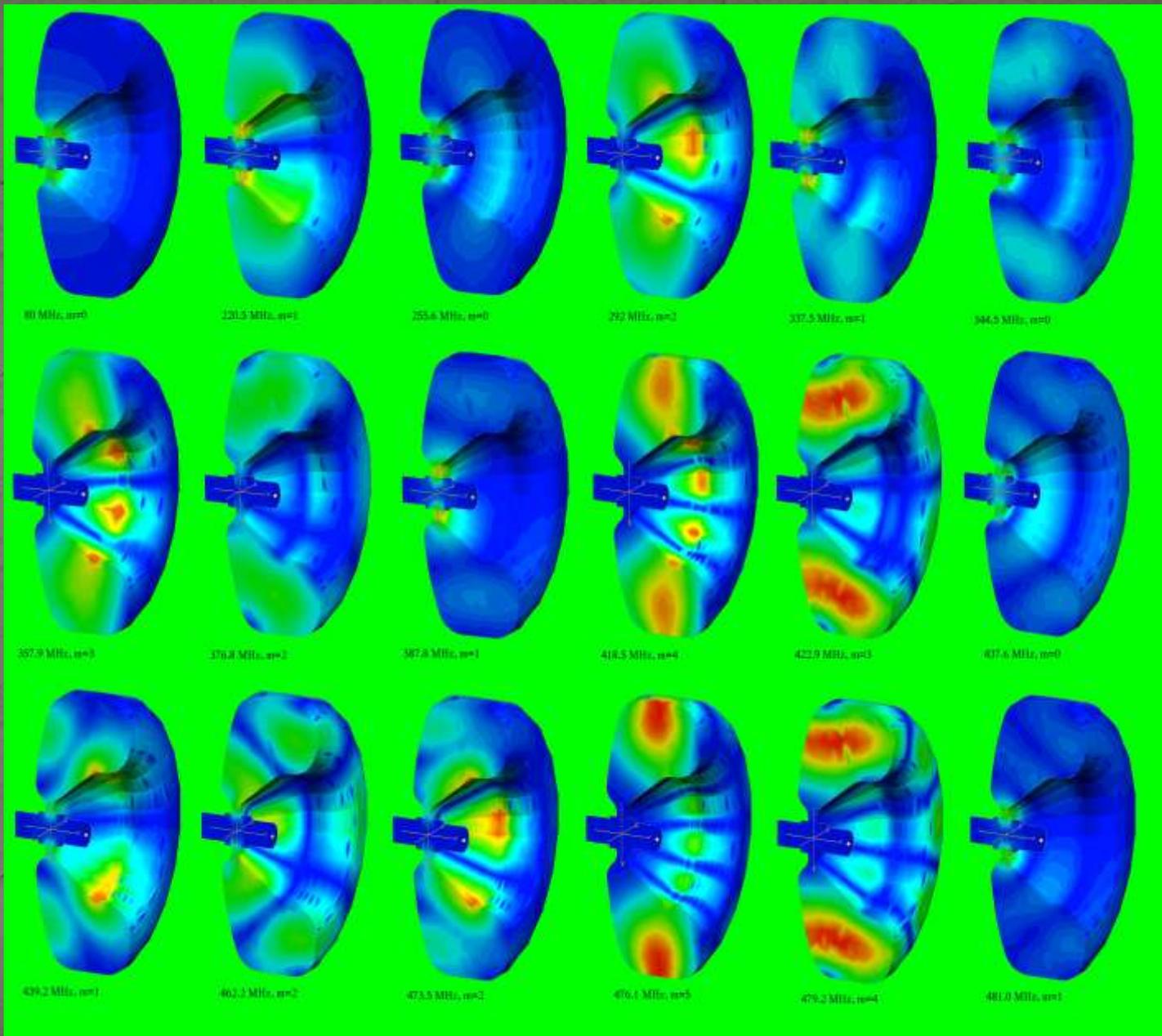
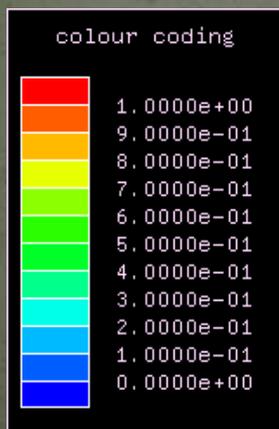
inductive (loop) coupling, low self-inductance

# HOM's

Example shown:  
80 MHz cavity  
PS for LHC.

Color-coded:

$$|\vec{E}|$$



# More examples of cavities

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# PS 19 MHz cavity (prototype, photo: 1966)



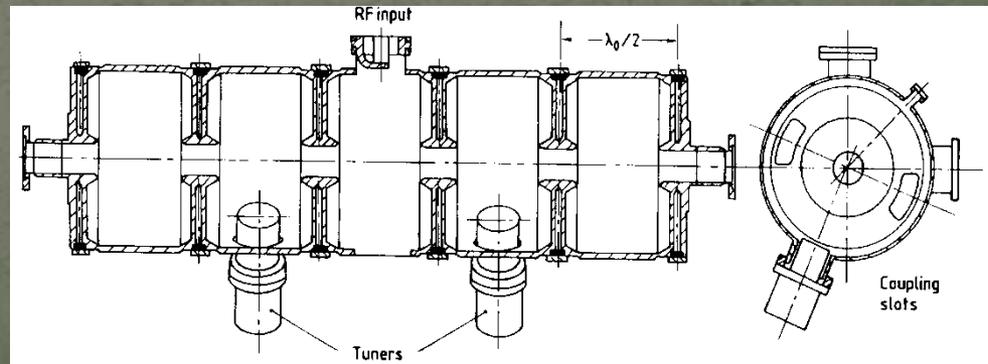
# Examples of cavities



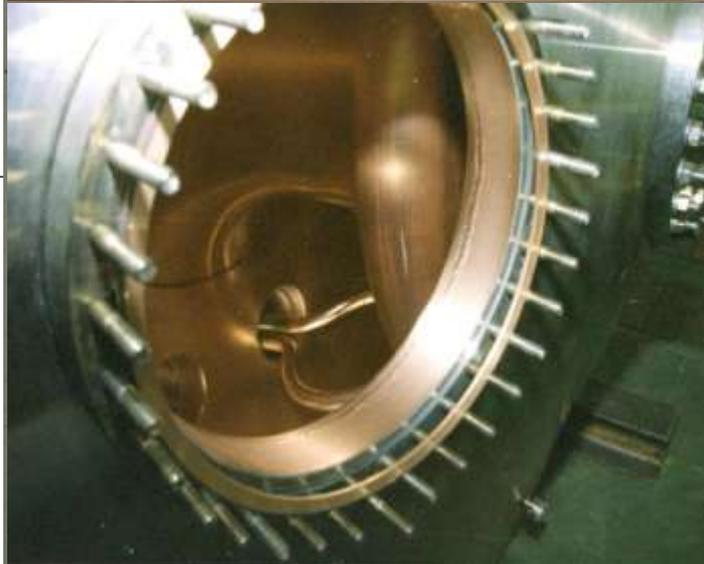
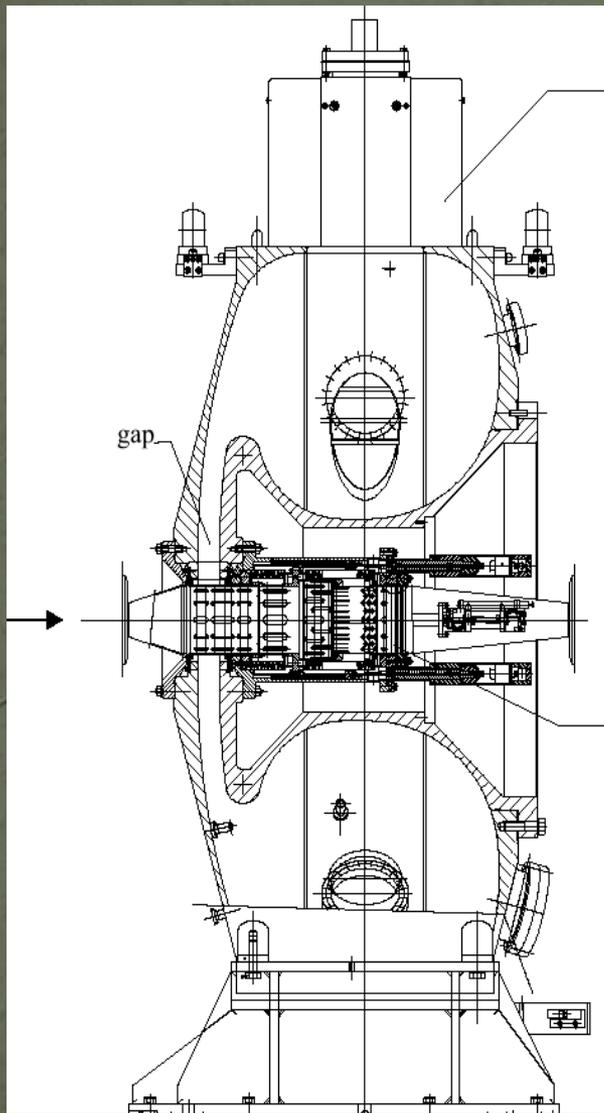
PEP II cavity  
476 MHz, single cell,  
1 MV gap with 150 kW,  
strong HOM damping,



LEP normal-conducting Cu RF cavities,  
350 MHz. 5 cell standing wave + spherical  
cavity for energy storage, 3 MV

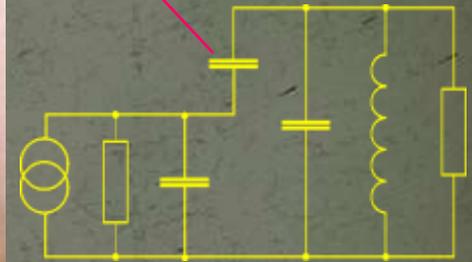


# CERN/PS 40 MHz cavity (for LHC)



example for  
capacitive  
coupling

coupling  $C$



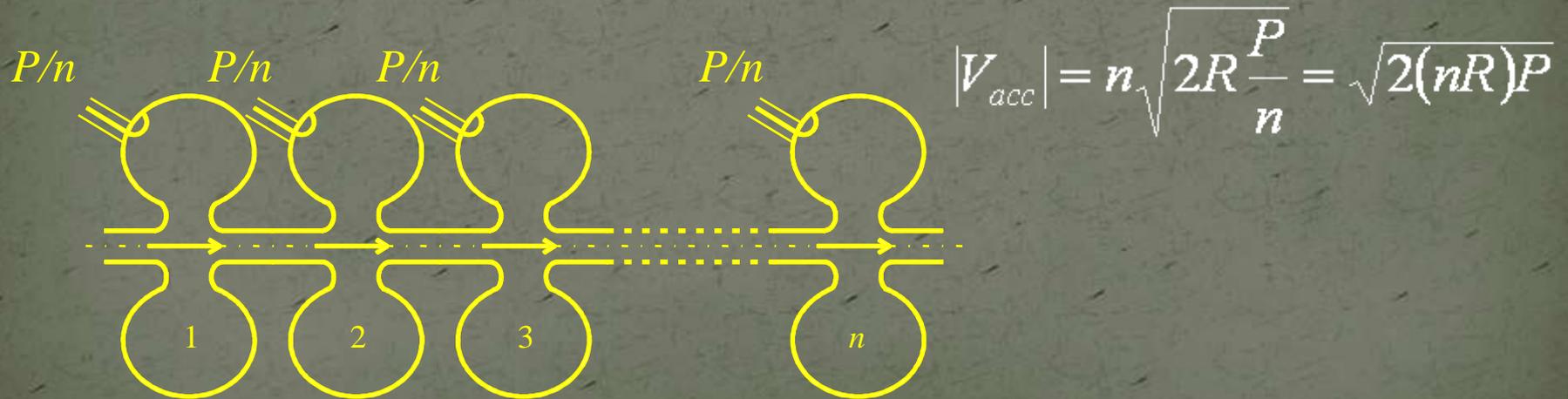
cavity

# Many gaps

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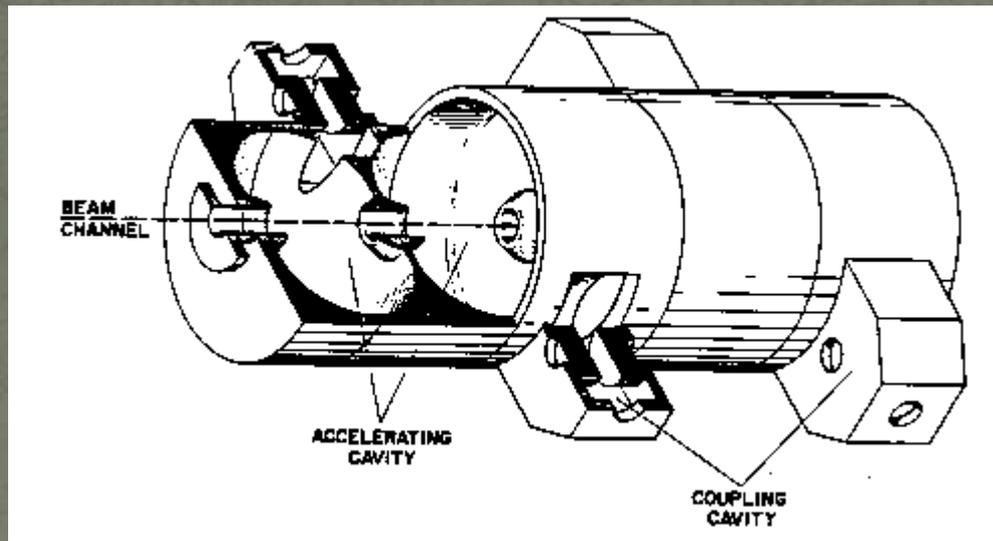
# What do you gain with many gaps?

- The  $R/Q$  of a single gap cavity is limited to some  $100 \Omega$ . Now consider to distribute the available power to  $n$  identical cavities: each will receive  $P/n$ , thus produce an accelerating voltage of  $\sqrt{2RP/n}$ . The total accelerating voltage thus increased, equivalent to a total equivalent shunt impedance of  $nR$ .



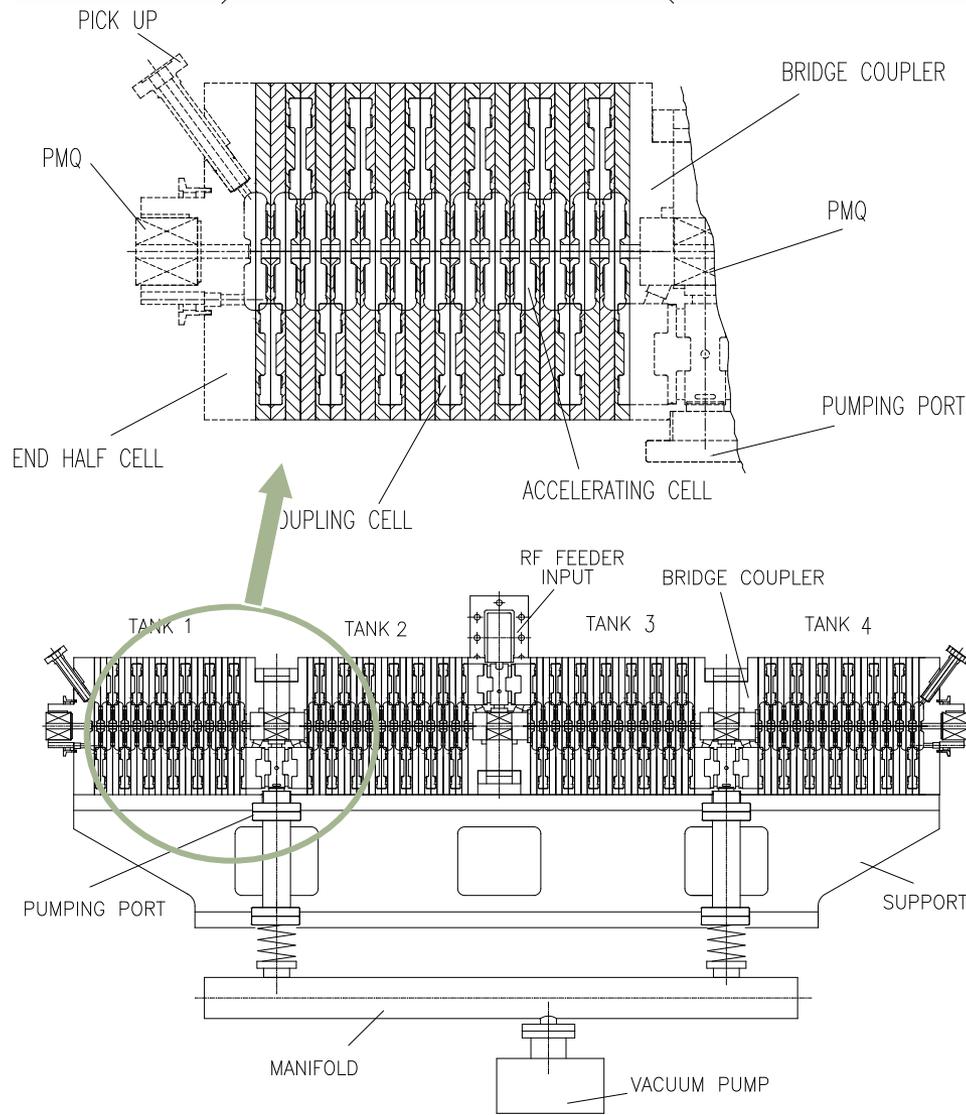
# Standing wave multicell cavity

- Instead of distributing the power from the amplifier, one might as well couple the cavities, such that the power automatically distributes, or have a cavity with many gaps (e.g. drift tube linac).
- Coupled cavity accelerating structure (side coupled)



- The phase relation between gaps is important!

# Side Coupled Structure : example LIBO



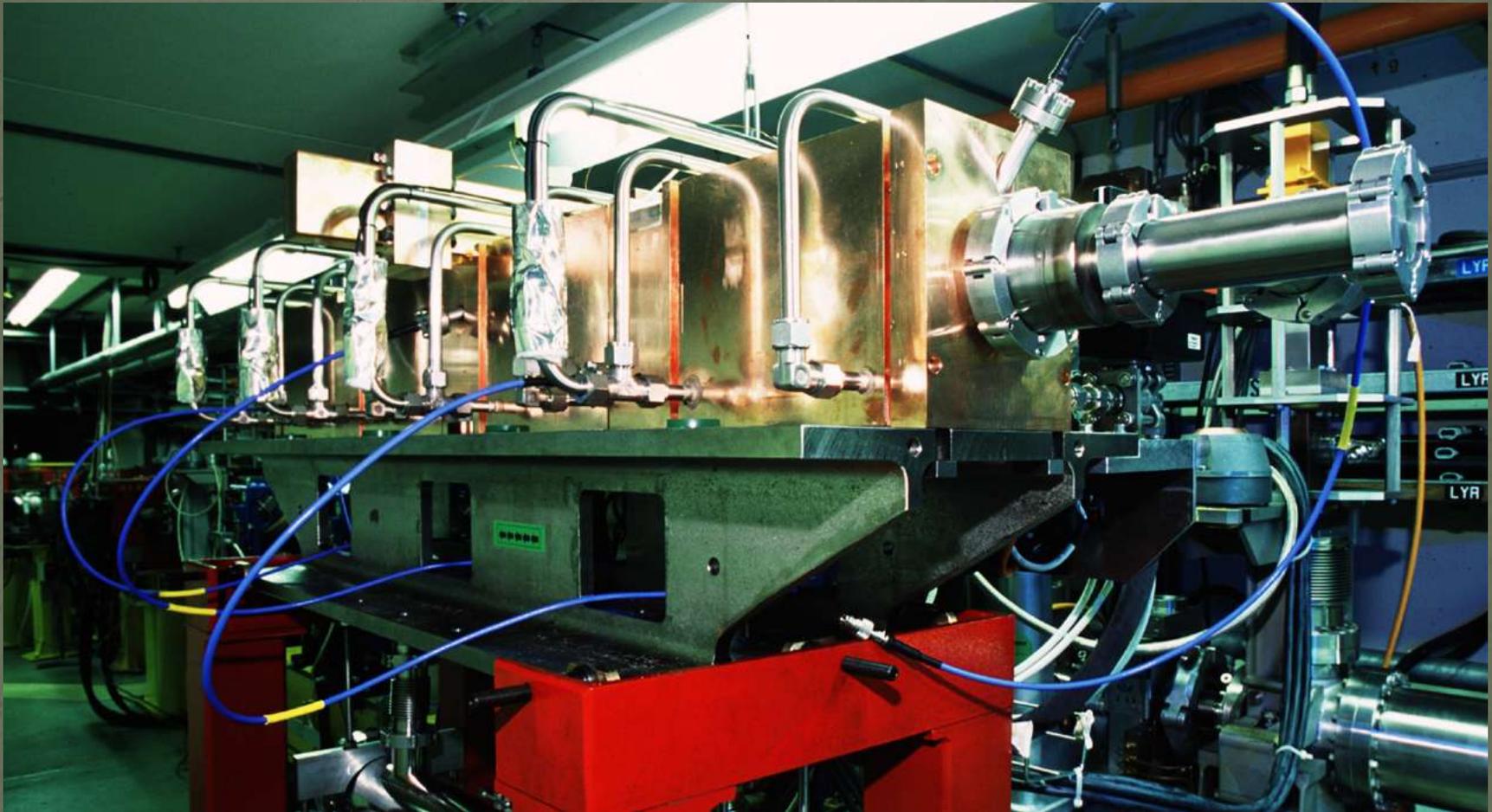
A 3 GHz Side Coupled Structure to accelerate protons out of cyclotrons from 62 MeV to 200 MeV

Medical application: treatment of tumours.

Prototype of Module 1 built at CERN (2000)

Collaboration CERN/INFN/Tera Foundation

# LIBO prototype

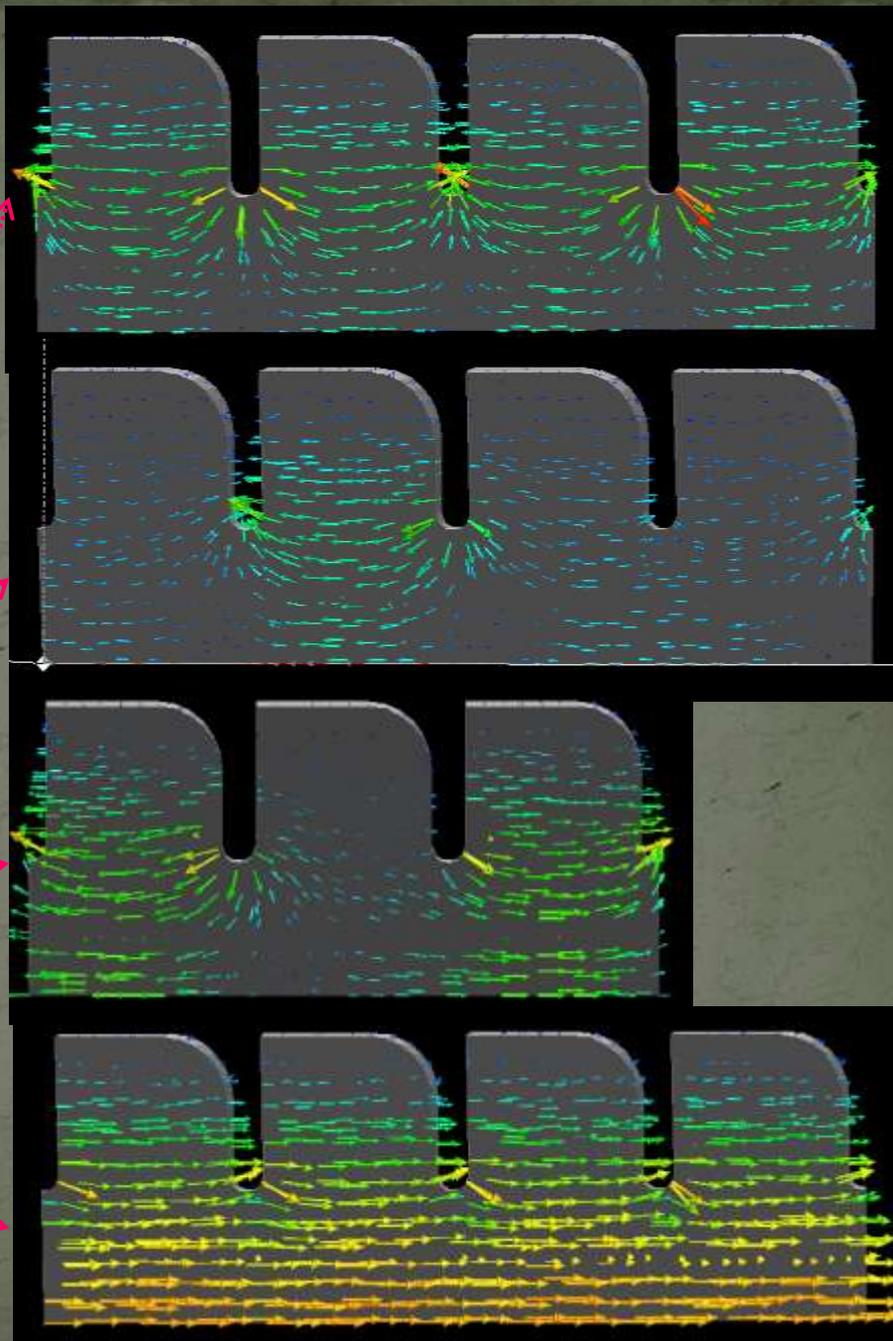
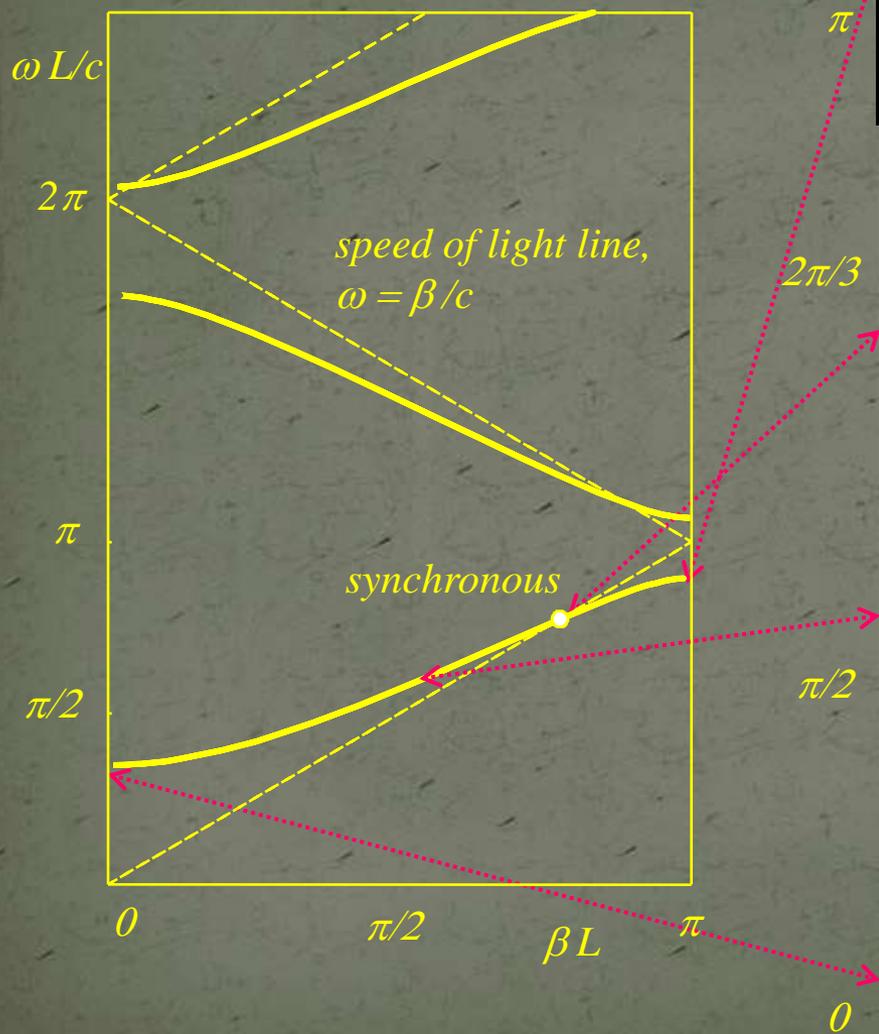


This Picture made it to the title page of *CERN Courier* vol. 41 No. 1 (Jan./Feb. 2001)

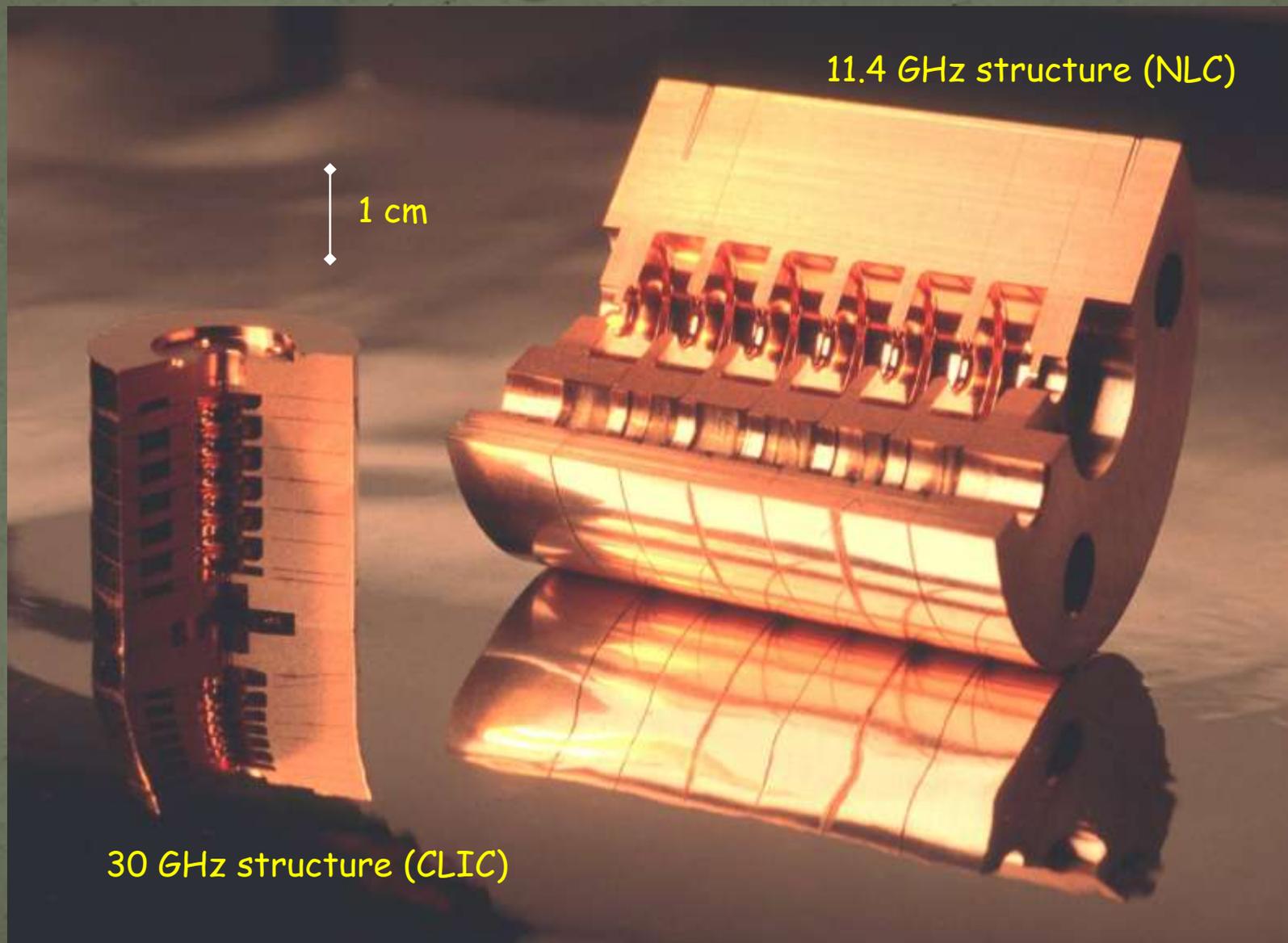
# Travelling wave structures

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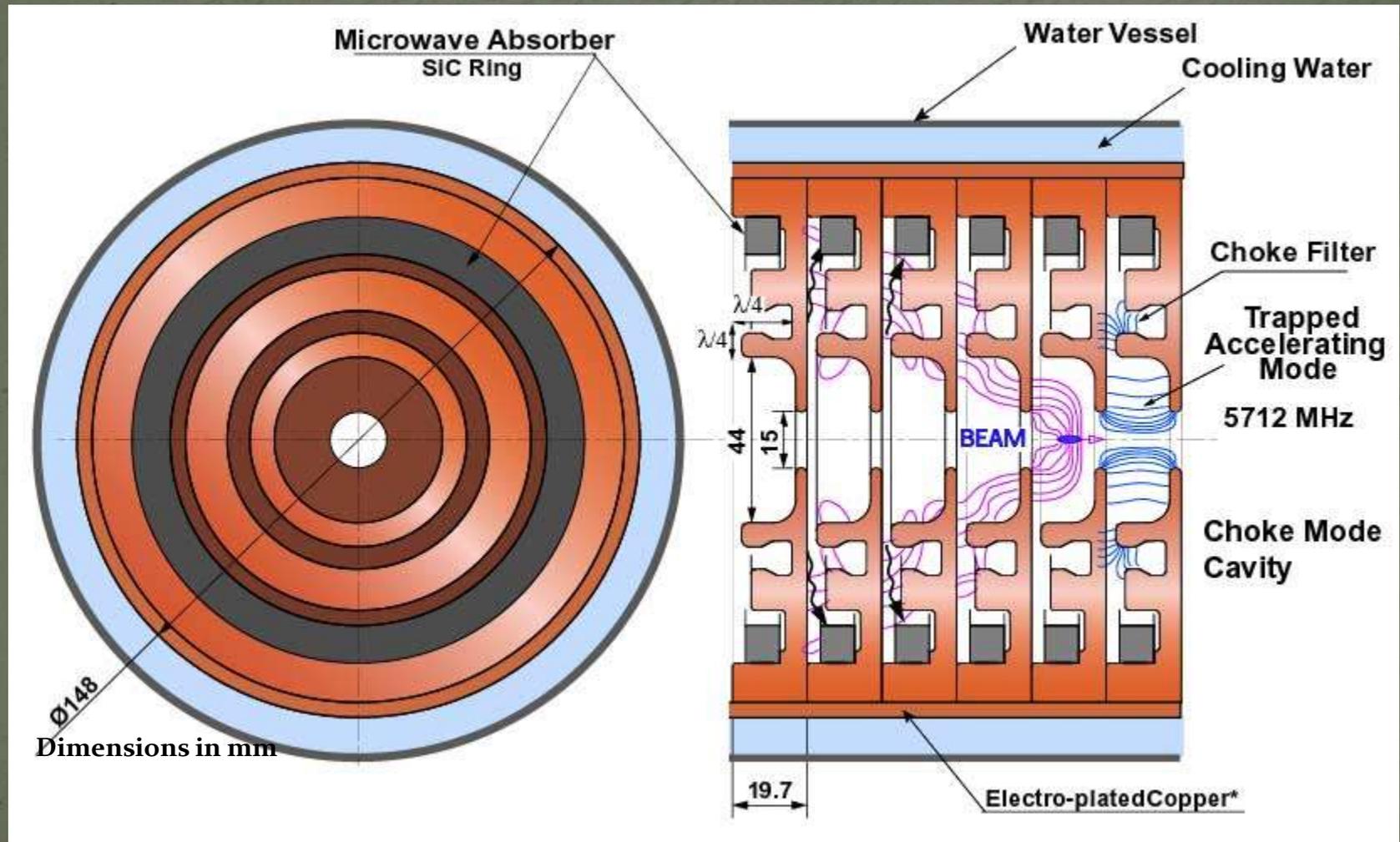
# Travelling wave structure



# Iris loaded waveguide

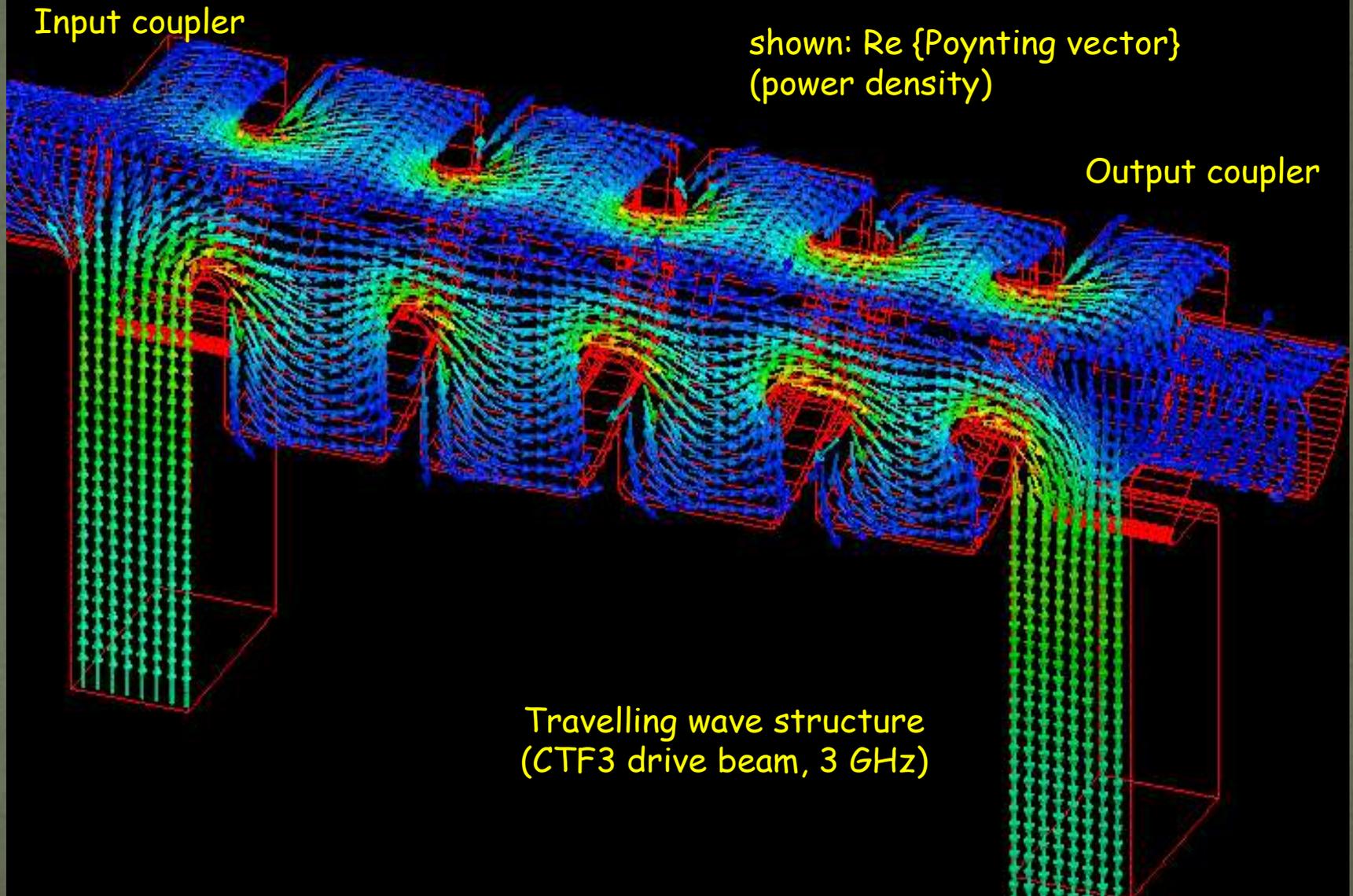


# Disc loaded structure with strong HOM damping “choke mode cavity”



# Waveguide coupling

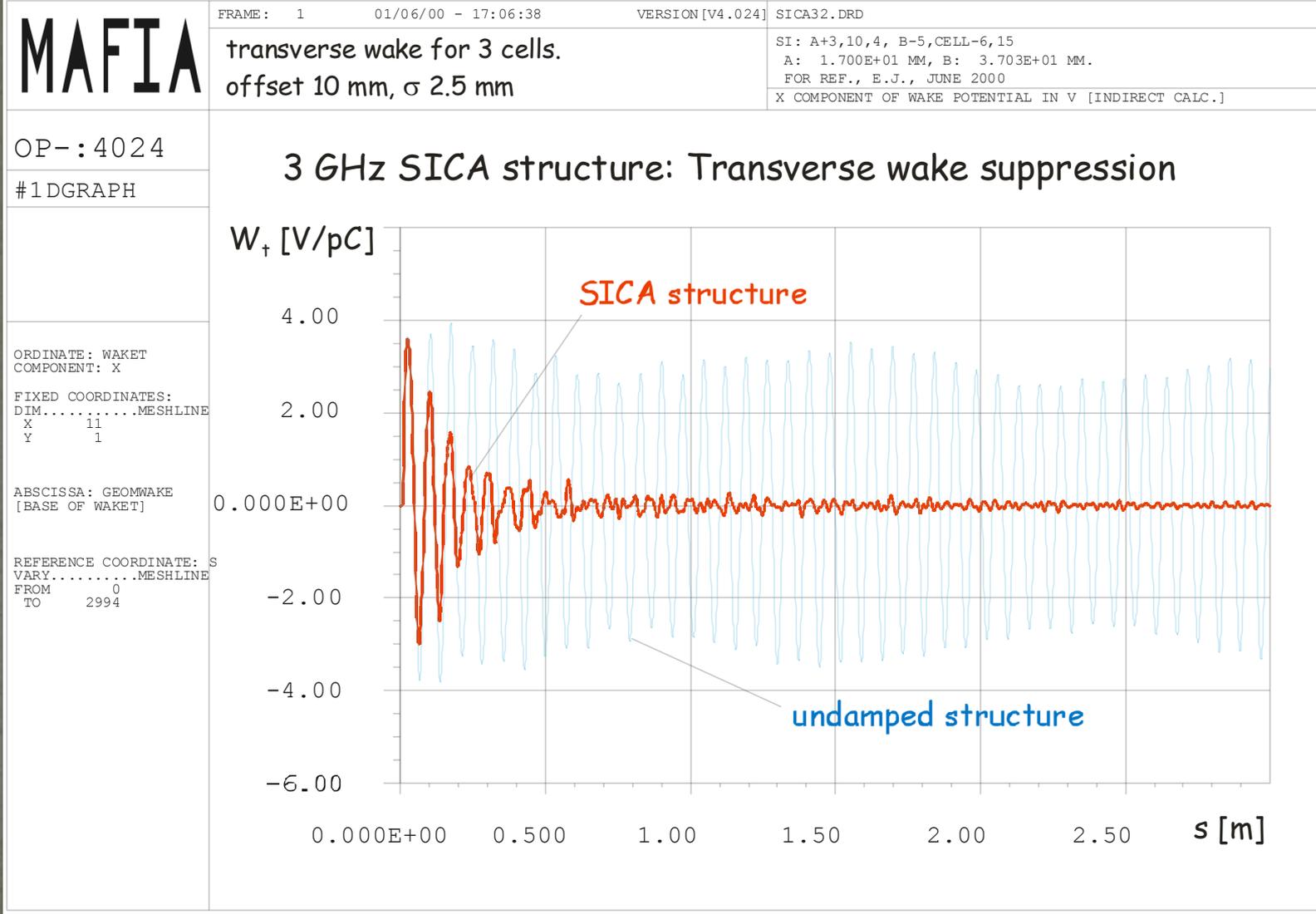
$\frac{1}{4}$  geometry shown



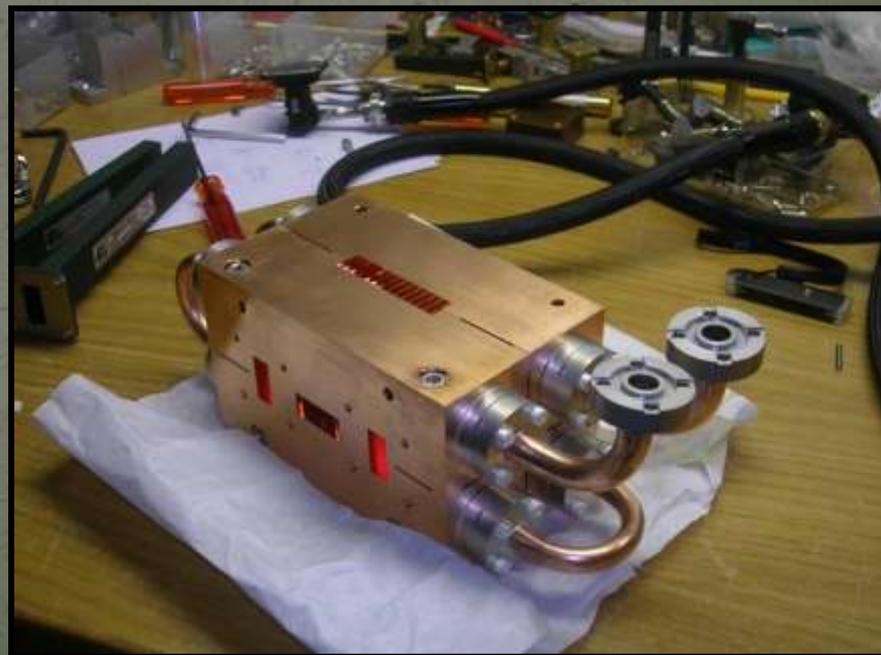
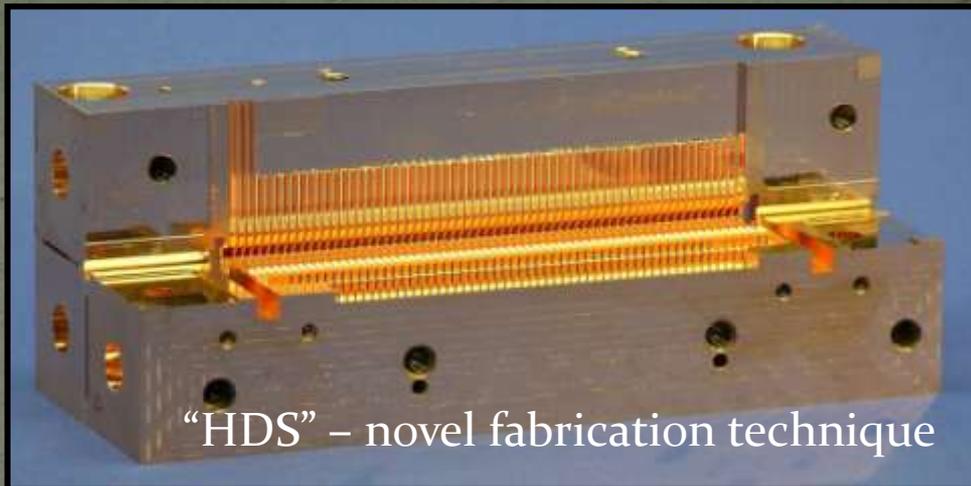
# 3 GHz Accelerating structure (CTF<sub>3</sub>)



# HOM damping at work



# Recent CLIC structures (11.4, 12 and 30 GHz)



# Superconducting Linacs

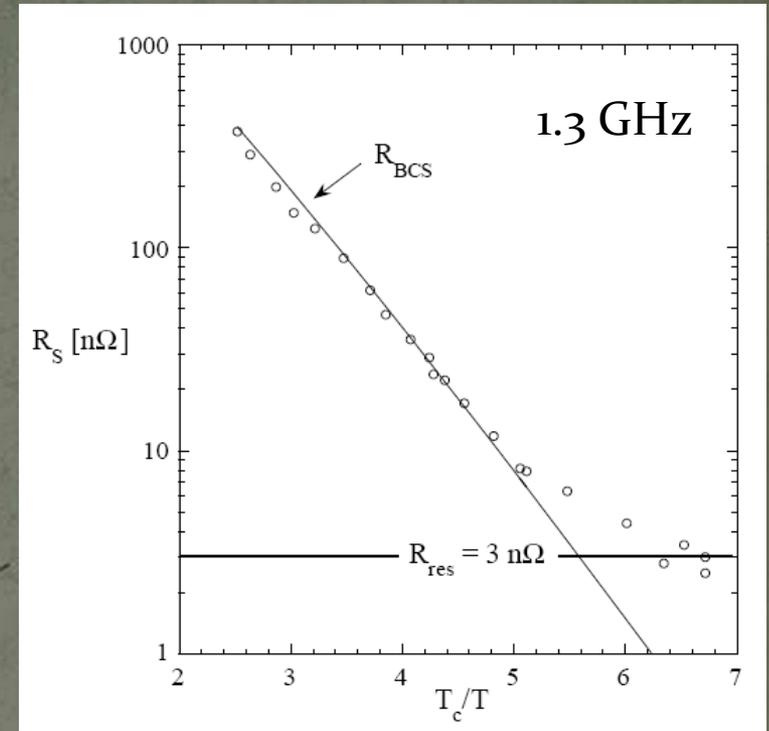
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# RF Superconductivity

- Different from DC, at RF the resistance is not exactly zero, but just very small. It is

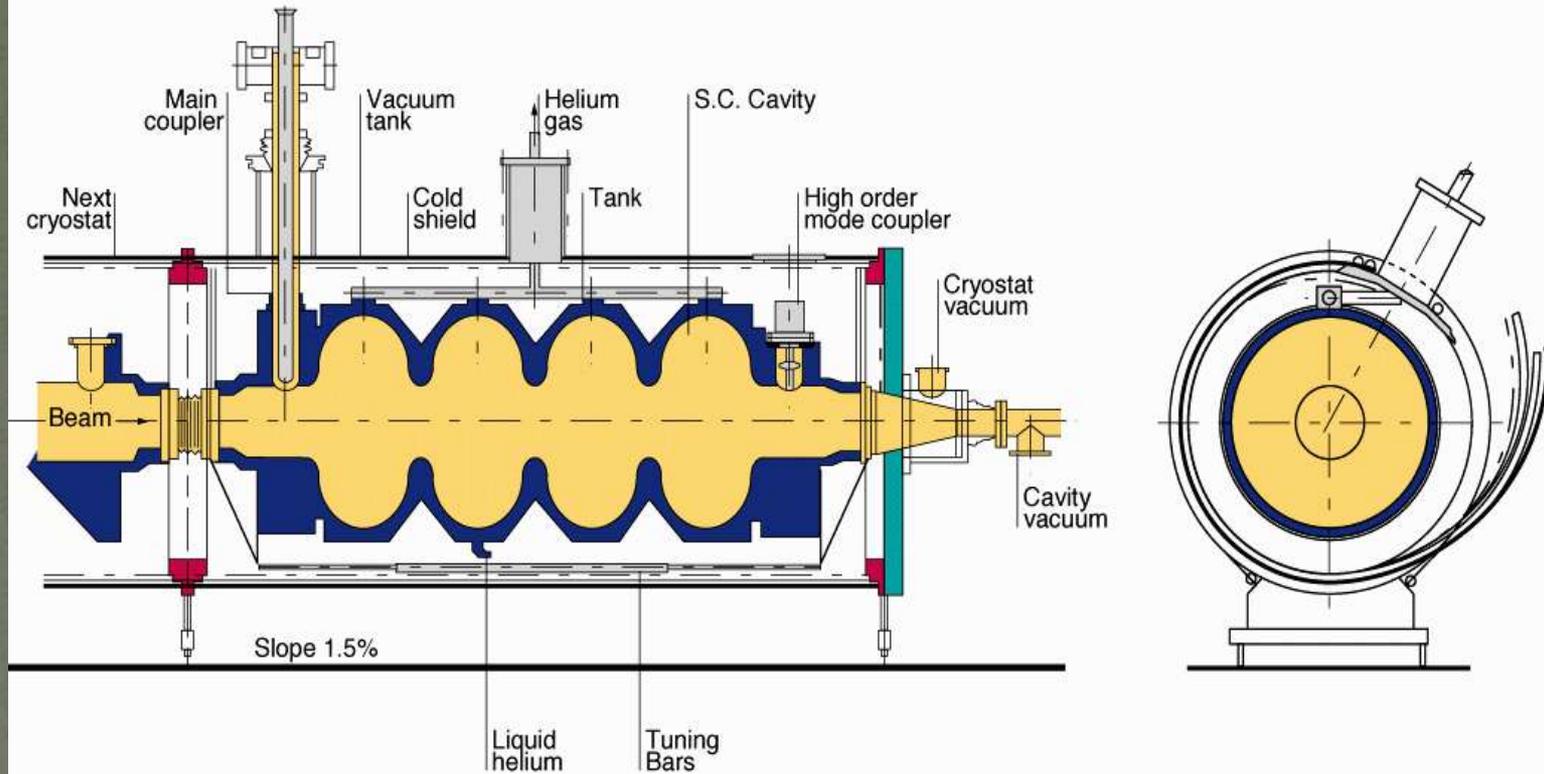
$$R_{surf} = R_{BCS} + R_{res} \quad R_{BCS} \propto \omega^2 e^{-1.76T_c/T}$$

- The maximum accelerating gradient is normally limited by the maximum possible surface magnetic field (the “superheating field”, 180 mT for Nb, 400 mT for Nb<sub>3</sub>Tn).
- Maximum acc. gradients are however obtained for Nb (ILC,  $\approx 40$  MV/m).



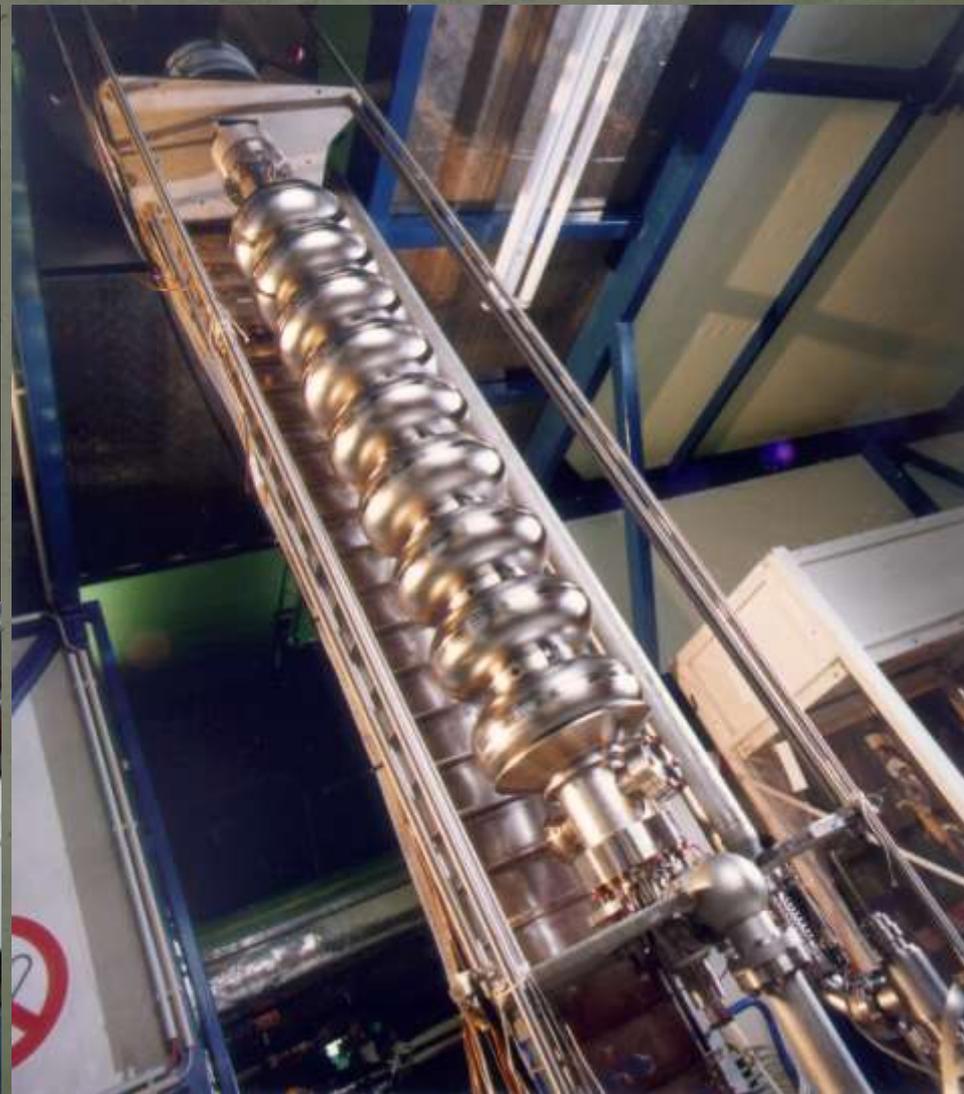
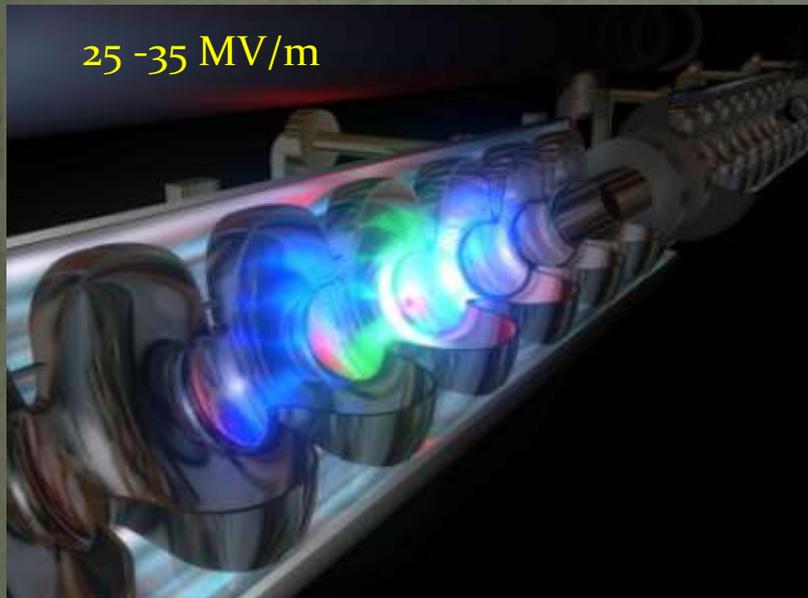
# LEP Superconducting cavities

## SUPERCONDUCTING CAVITY WITH ITS CRYOSTAT



10.2 MV/ per cavity

# TESLA/ILC SC cavities



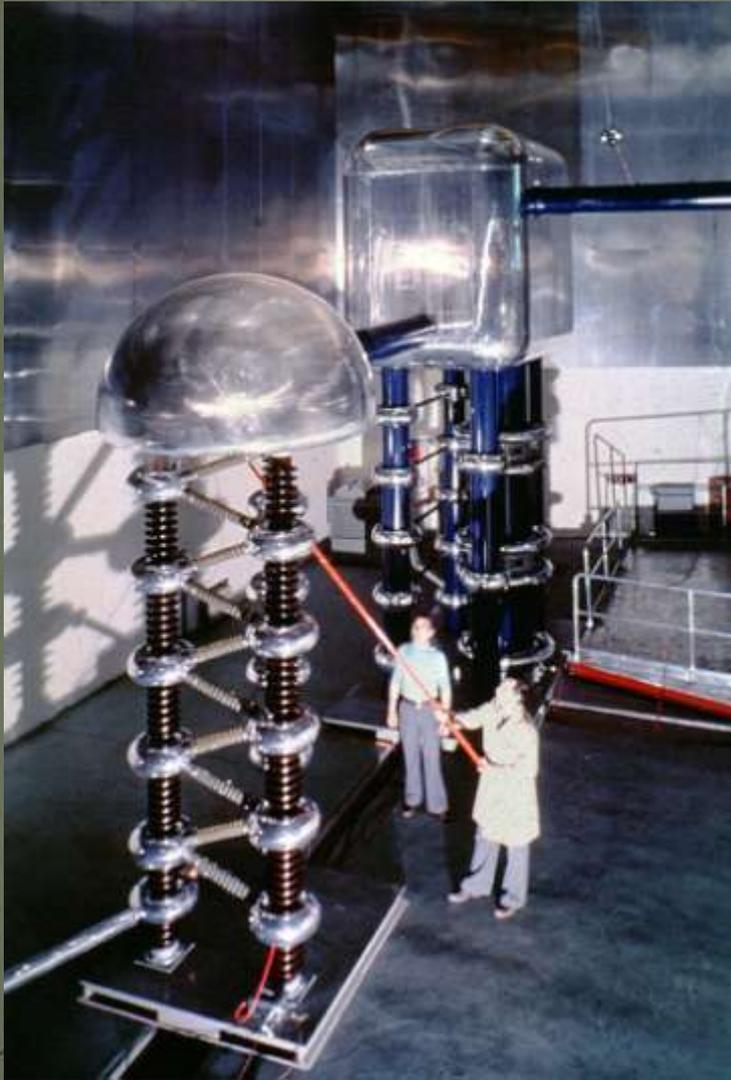
# LHC SC RF, 4 cavity module, 400 MHz



# RFQ's

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# Old pre-injector 750 kV DC , CERN Linac 2, before 1990



All this was replaced by the RFQ ...

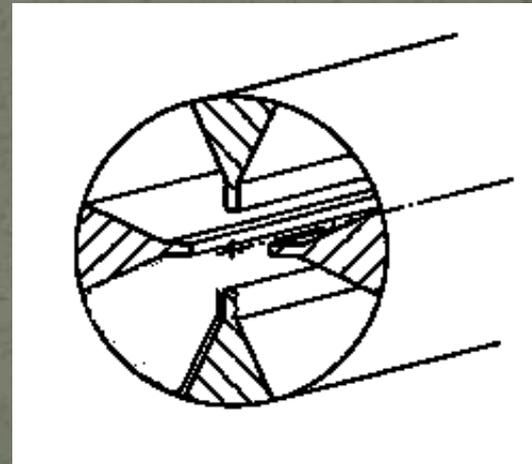
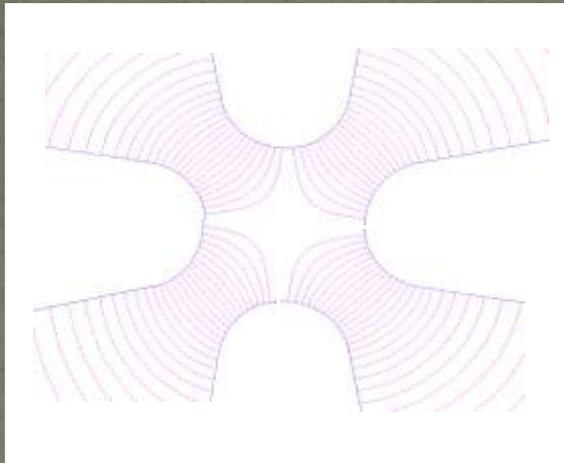
# RFQ of CERN Linac 2



# The Radio Frequency Quadrupole (RFQ)

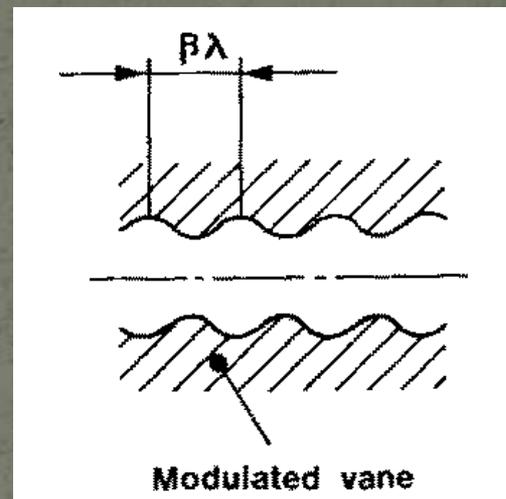
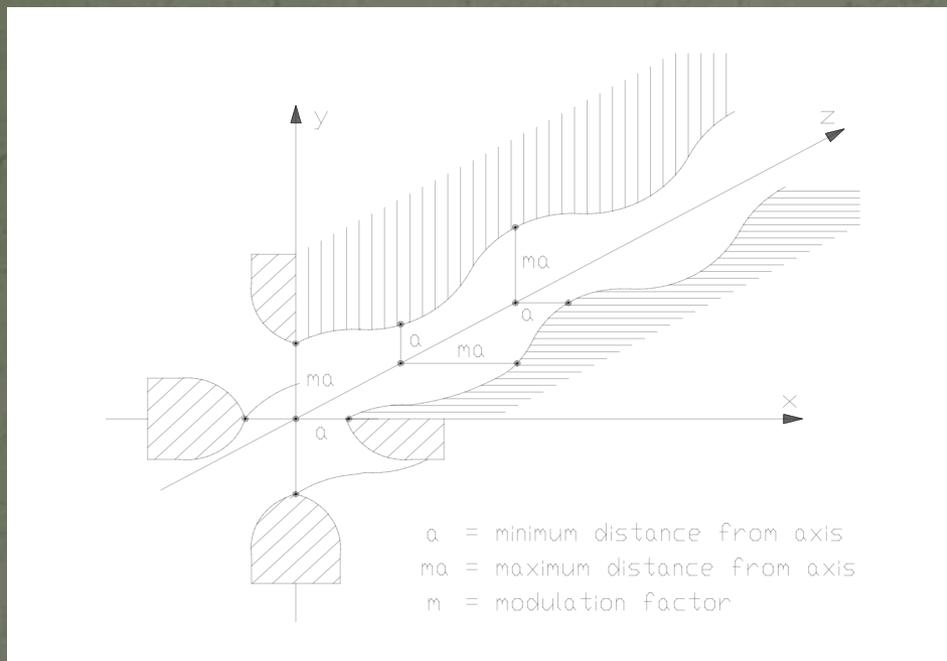
Minimum Energy of a DTL: 500 keV (low duty) - 5 MeV (high duty)  
At low energy / high current we need strong focalisation  
Magnetic focusing (proportional to  $\beta$ ) is inefficient at low energy.  
Solution (Kapchinski, 70's, first realised at LANL):

Electric quadrupole focusing + bunching + acceleration

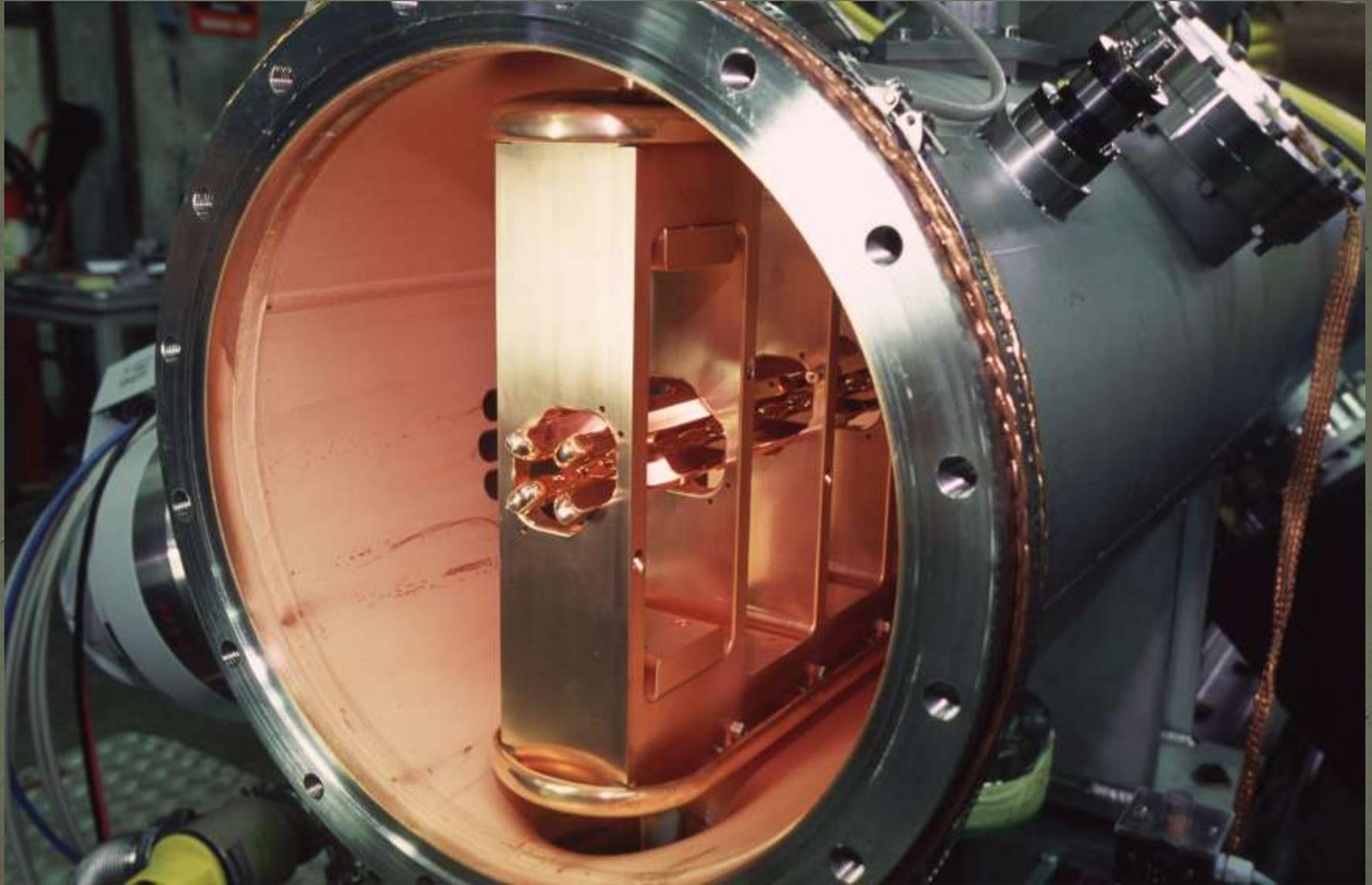


# RFQ electrode modulation

The electrode modulation creates a longitudinal field component that creates the "bunches" and accelerates the beam.



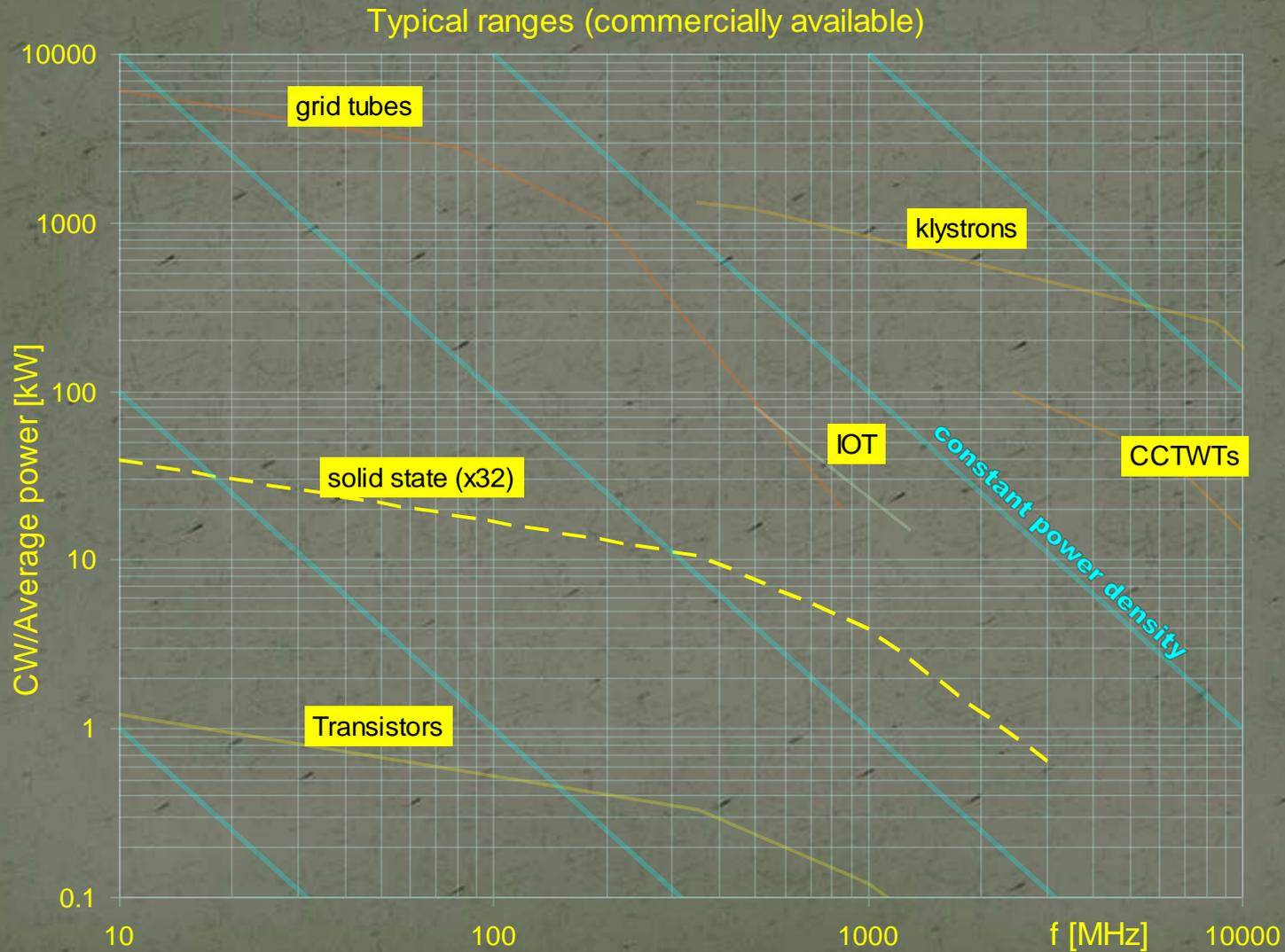
# A look inside CERN AD's "RFQD"



# RF power sources

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# RF power sources



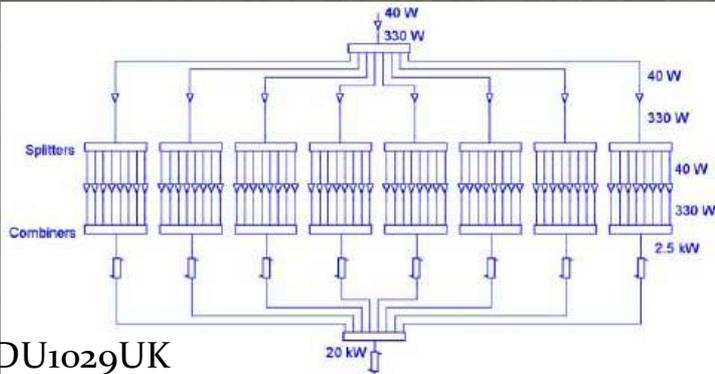
# LEIR SSPA, 1 kW, 0.2 – 50 MHz



MRF151G

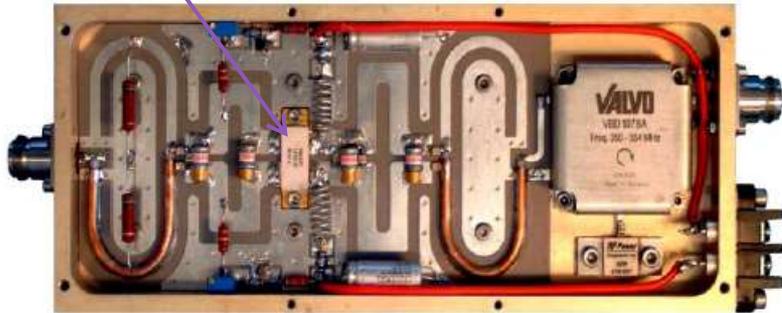
# Soleil Booster SSPA, 40 kW, 352 MHz

147 modules

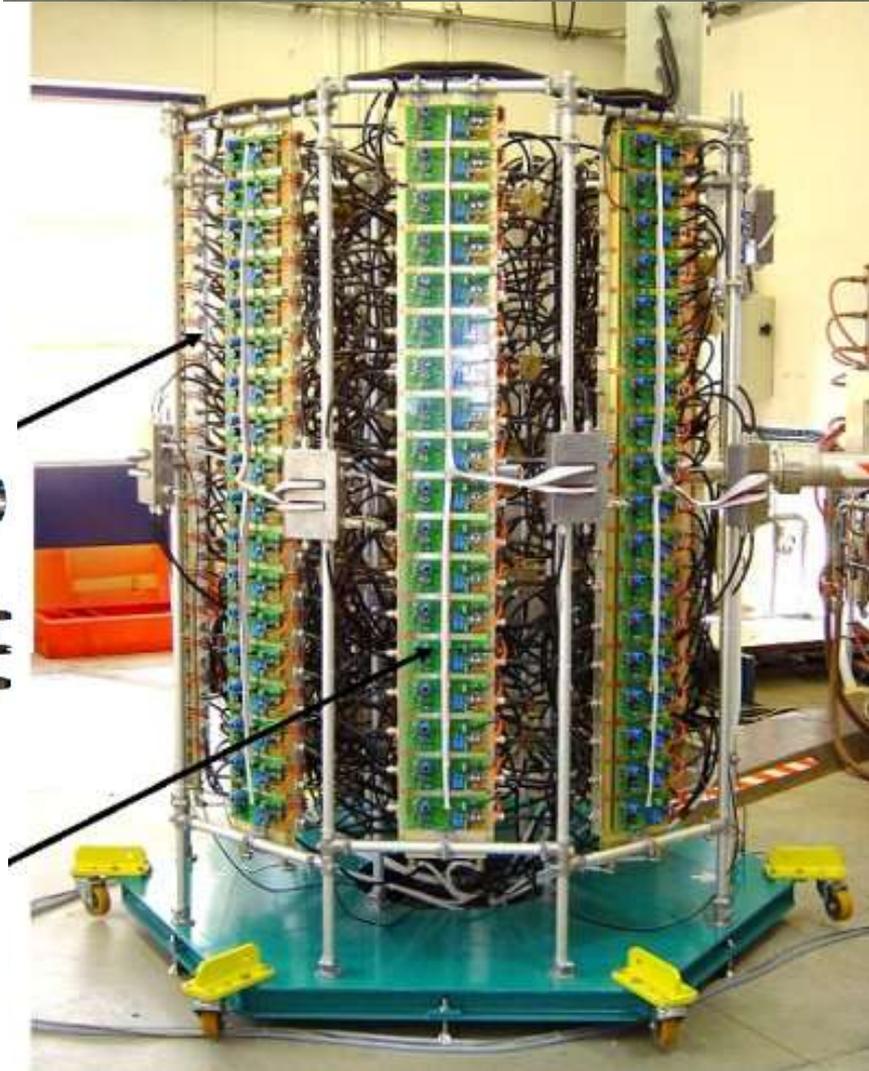


DU1029UK

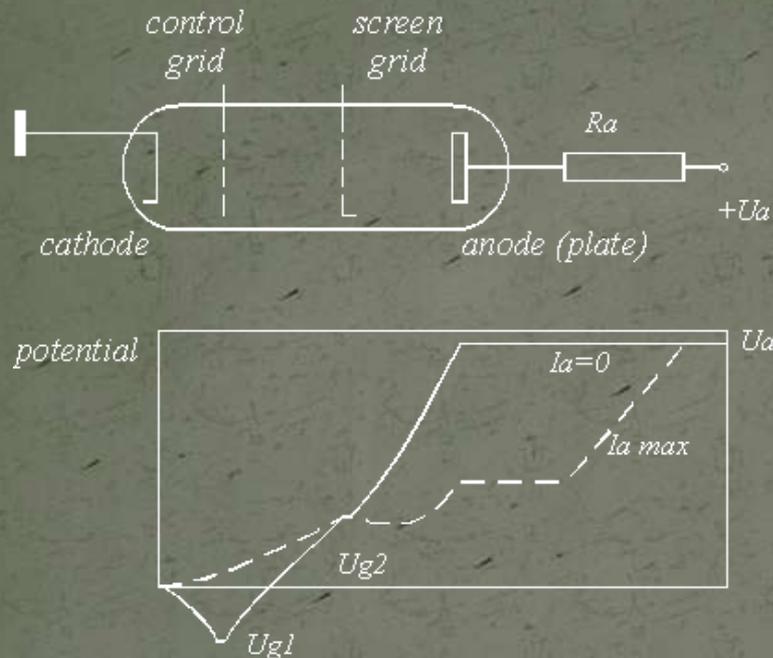
330 W amplifier module



600 W, 300 Vdc / 30 Vdc converter



# Tetrode



RS 1084 CJ (ex Siemens, now Thales),  
 $< 30$  MHz, 75 kW

4CX250B  
 (Eimac/CPI),  
 $< 500$  MHz, 600 W  
 (Anode removed)



YL1520 (ex Philips, now Richardson),  
 $< 260$  MHz, 25 kW

# High power tetrode amplifier



**CERN Linac3: 100 MHz, 350 kW**  
50 kW Driver: TH345, Final: RS 2054 SK

**CERN PS: 13-20 MHz, 30 kW**  
Driver: solid state 400 W, Final: RS 1084 CJSC

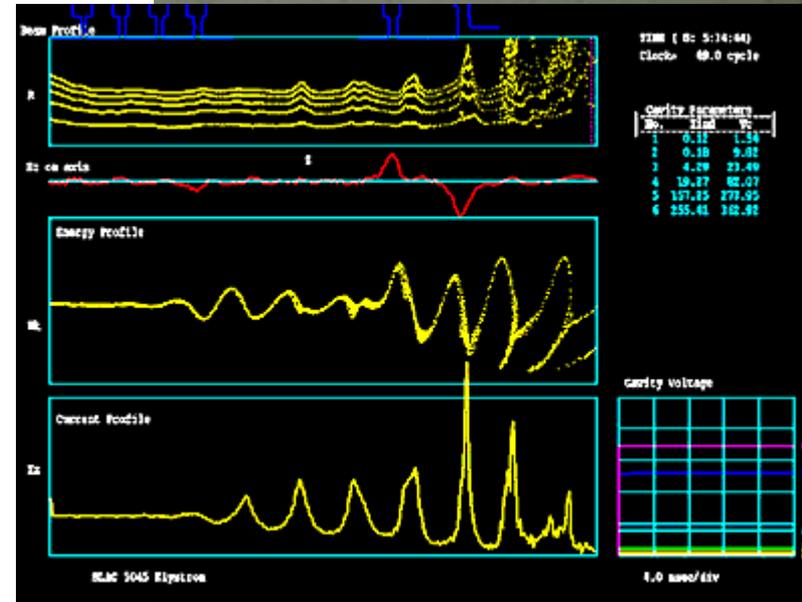
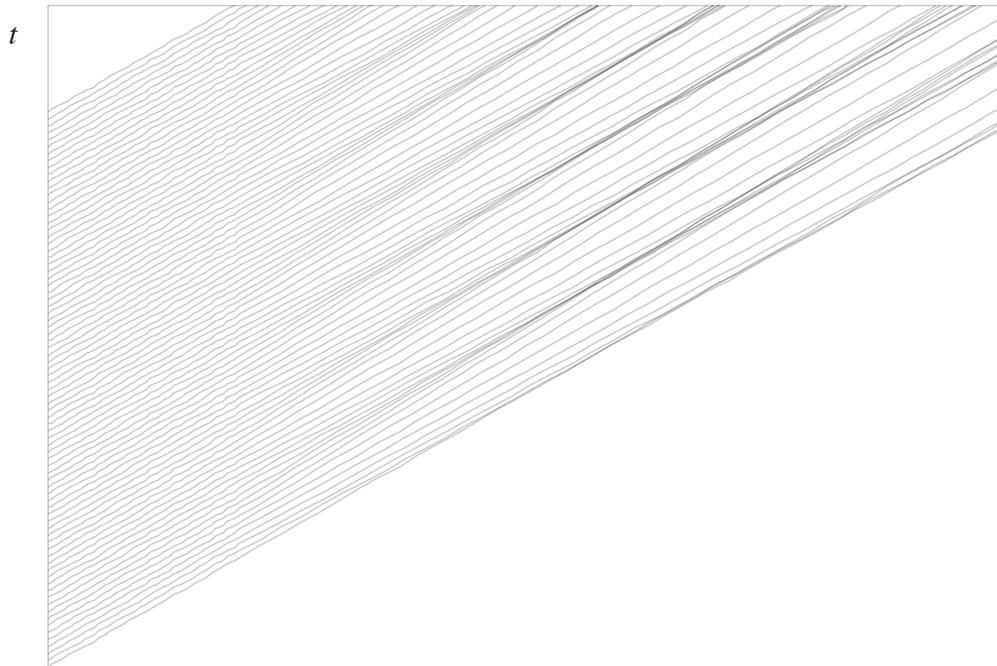


# Klystron principle

velocity  
modulation

drift

density  
modulation



RF in

RF out

z

$-V_0$

Cathode

Collector

# Klystrons



**CERN CTF3 (LIL):**  
3 GHz, 45 MW,  
4.5  $\mu$ s, 50 Hz,  $\eta$  45 %

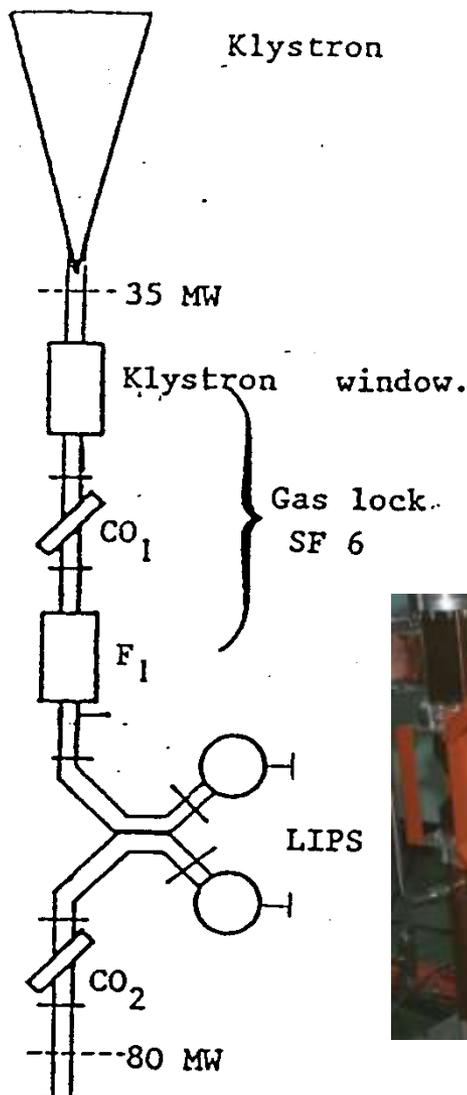


**CERN LHC:**  
400 MHz, 300 kW,  
CW,  $\eta$  62 %

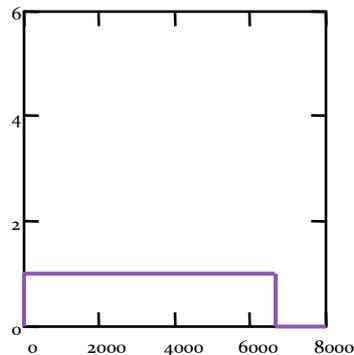
# RF pulse compression

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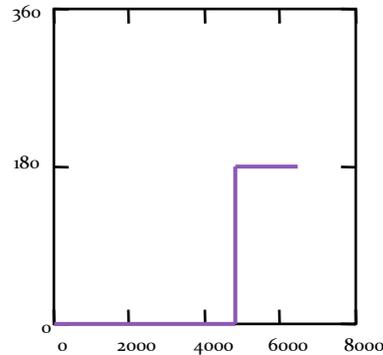
# RF Pulse Compression



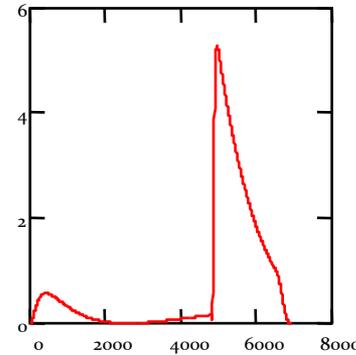
Input pulse



Input phase



"SLED" output pulse

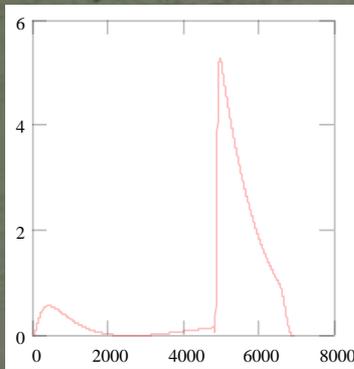


SLED: SLAC Energy Doubler    LIPS: LEP Injector Power Saver

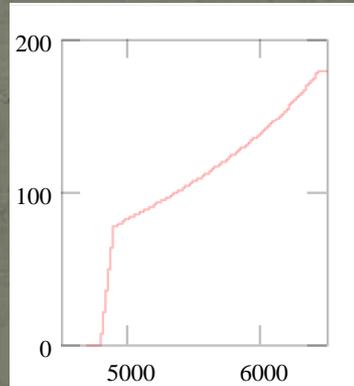


# Flat output pulses

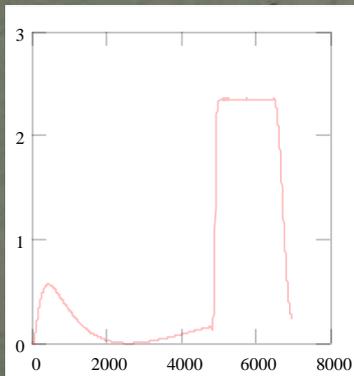
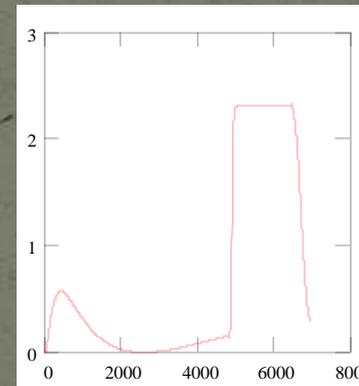
Standard "SLED" Pulse



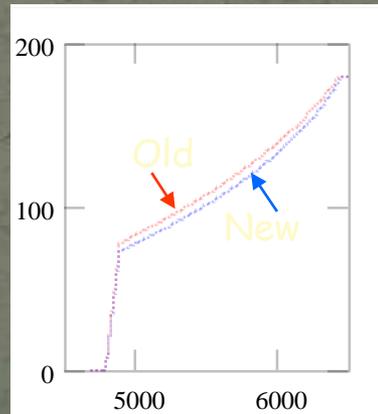
RF phase modulation



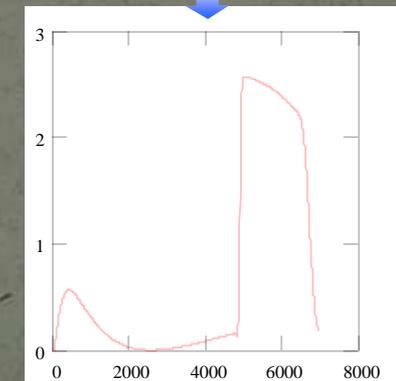
Flat pulse



Flat pulse



RF phase modulation

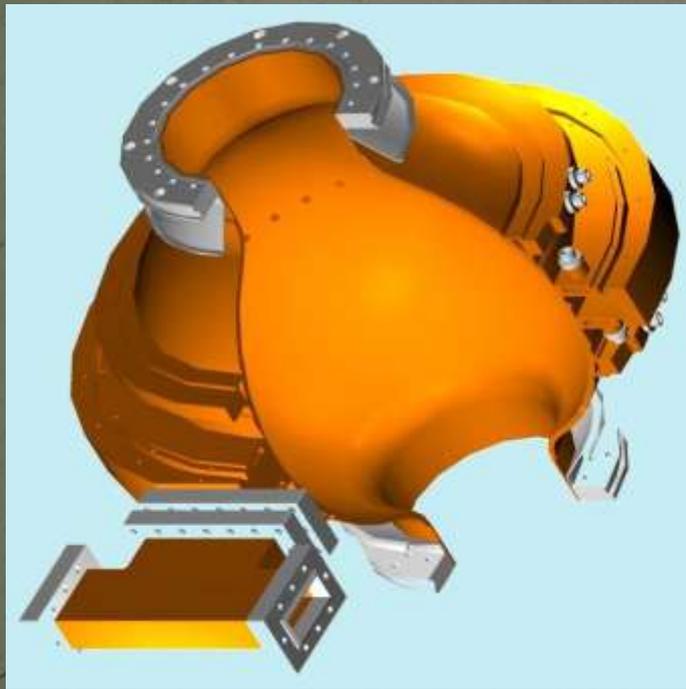


Distorted pulse

-10 kHz

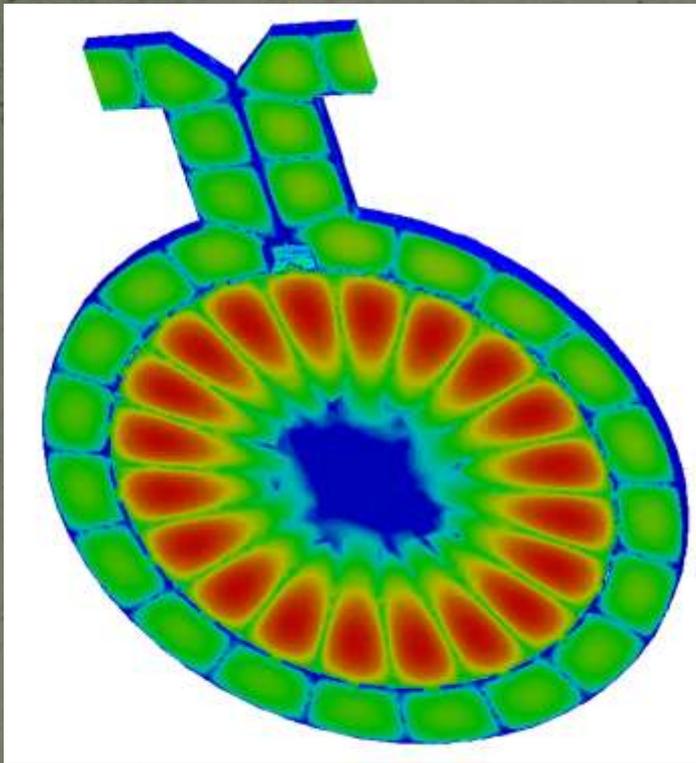
# Pulse compressor

BOC „Barrel Open Cavity“

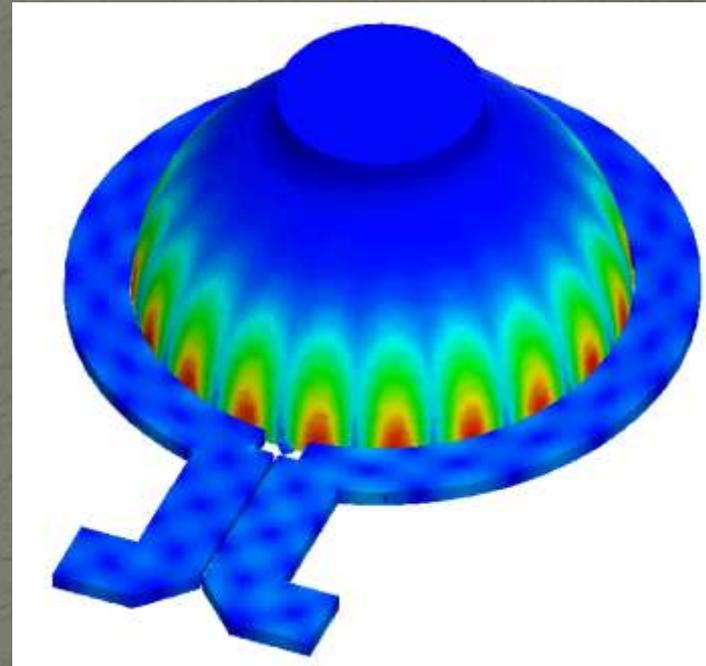


# BOC

2.99848 GHz,  
S11: -12.9 dB



Electric field, logarithmic scale



Magnetic field