

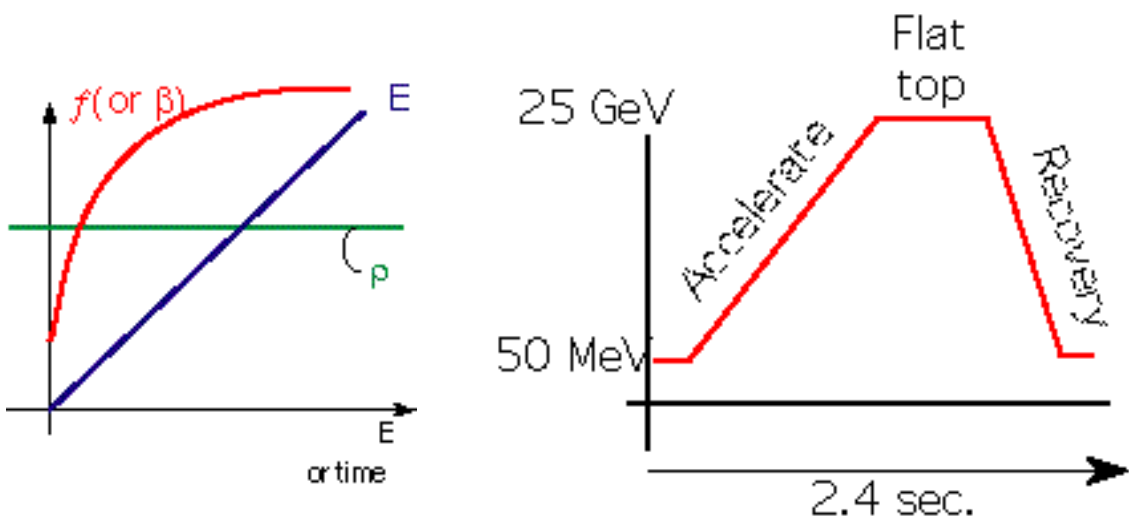
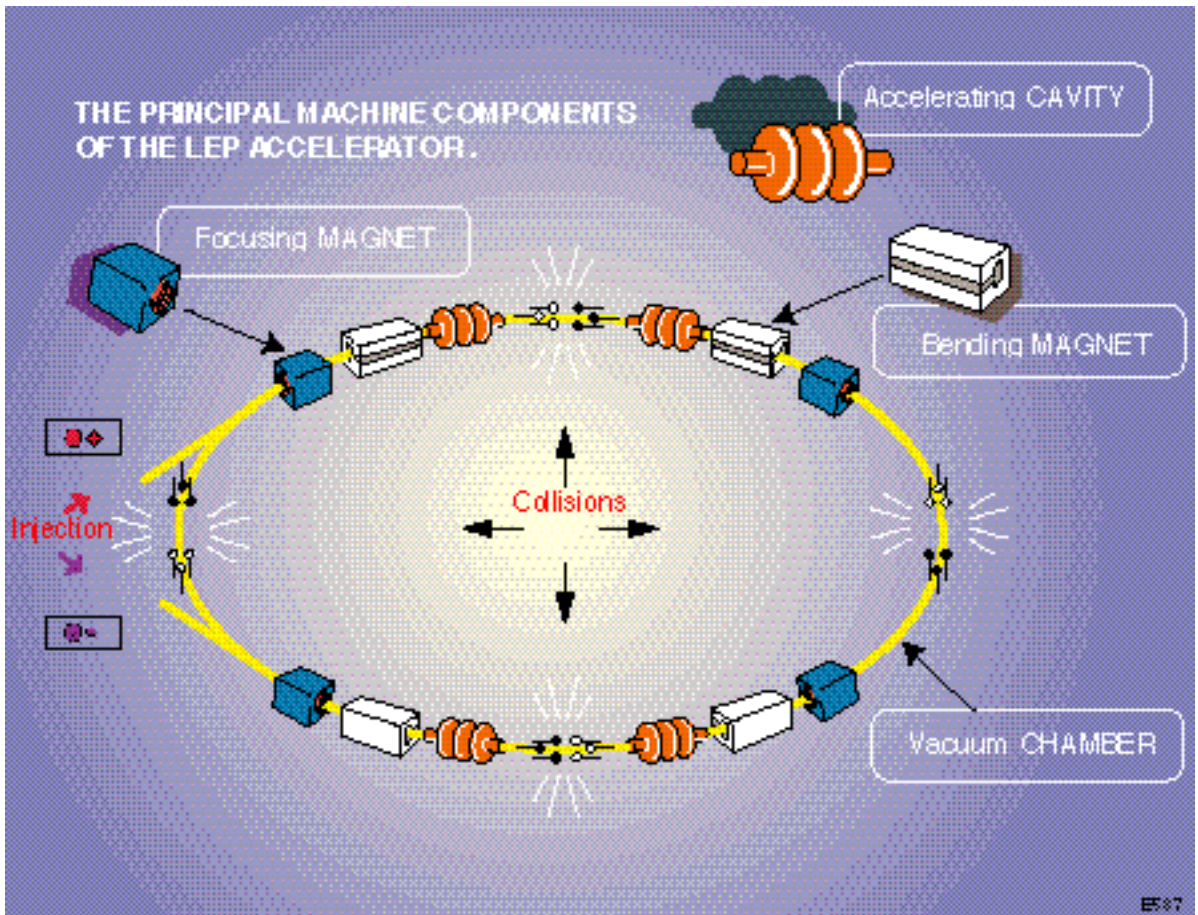
# **Transverse Dynamics**

## *E. Wilson - CERN*

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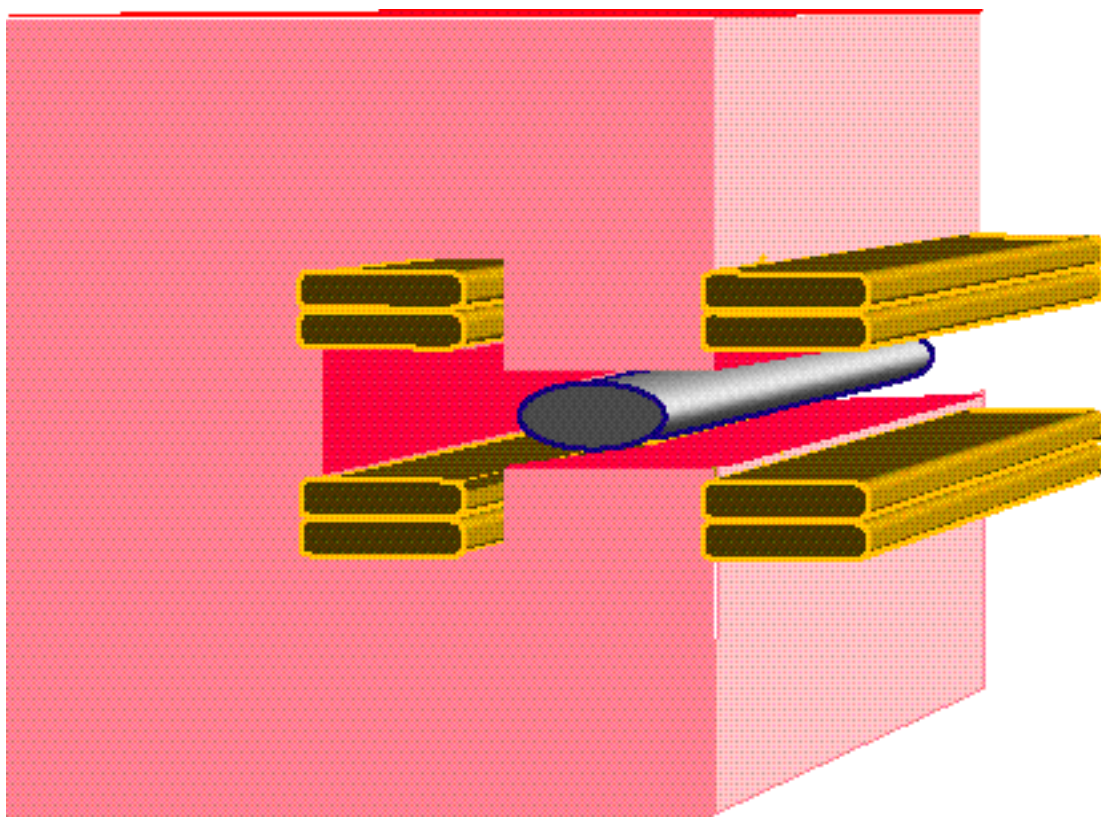
- ◆ **Components of a synchrotron**
- ◆ **Dipole Bending Magnet**
- ◆ **Magnetic rigidity**
- ◆ **Bending Magnet**
- ◆ **Weak focusing - gutter**
- ◆ **Transverse ellipse**
- ◆ **Fields and force in a quadrupole**
- ◆ **Strong focusing**
- ◆ **Equation of motion in transverse co-ordinates**
- ◆ **Twiss Matrix**
- ◆ **The lattice**
- ◆ **Dispersion**
- ◆ **Chromaticity**

# Components of a synchrotron

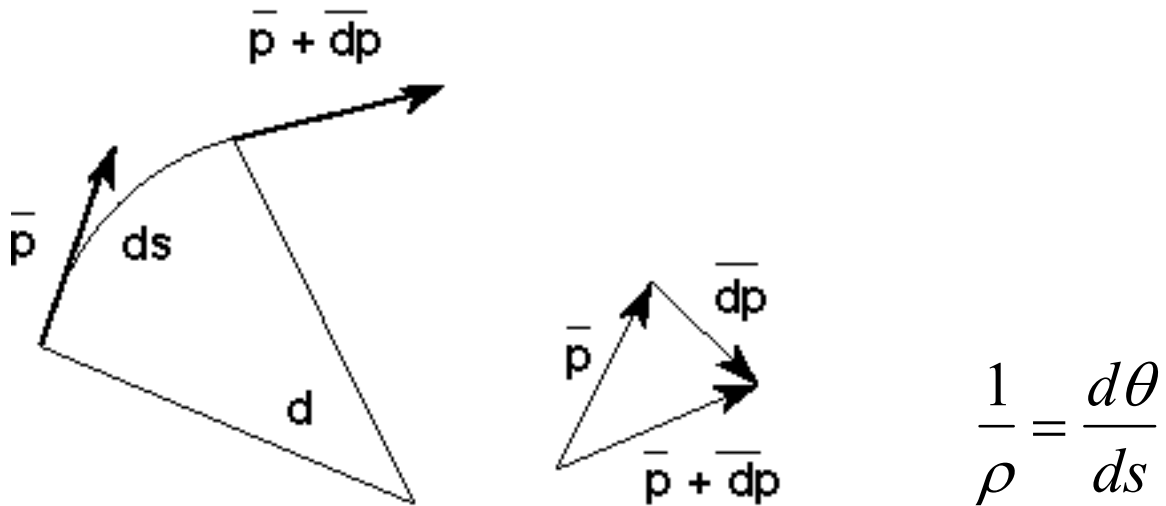


# Dipole Bending Magnet

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# Magnetic rigidity (*vectors*)

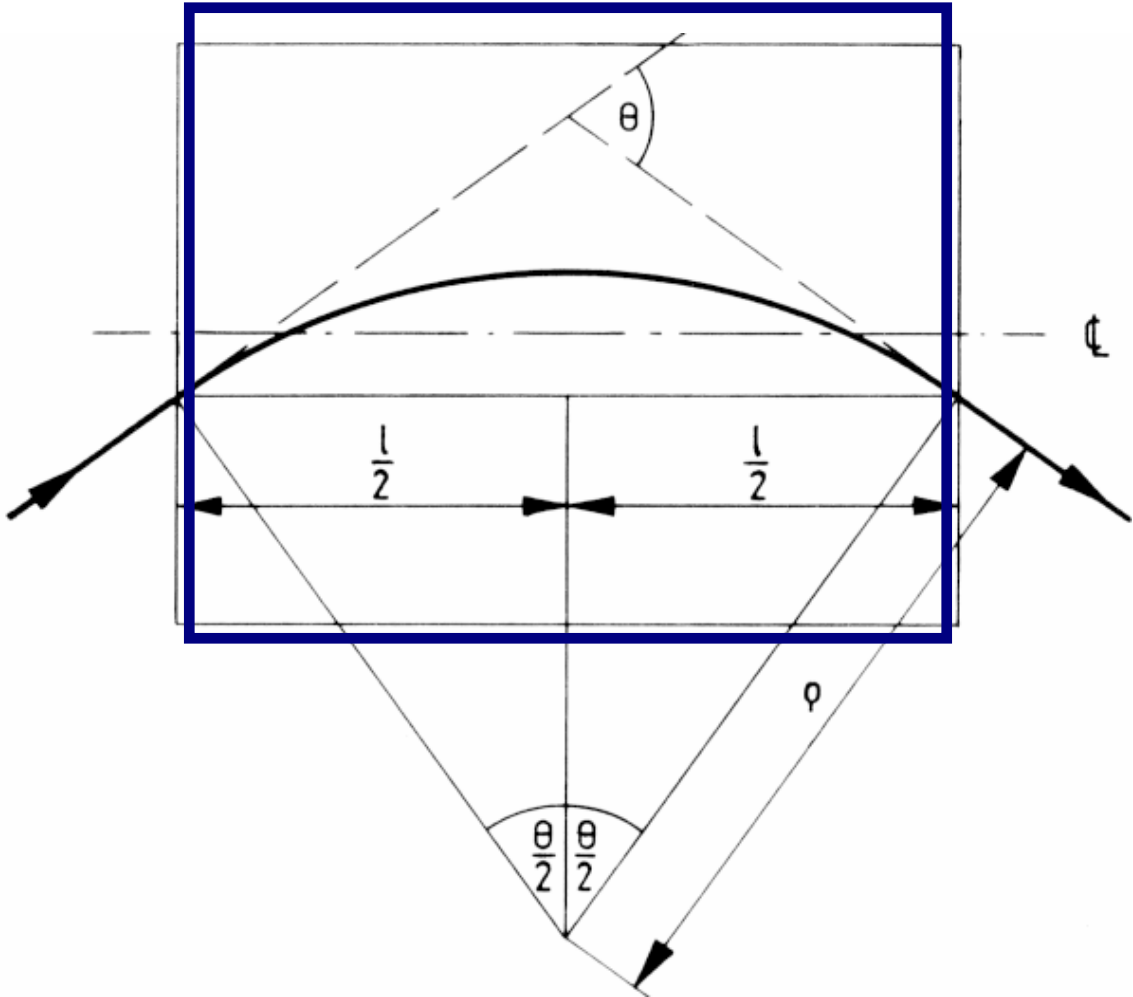


$$\begin{aligned} \frac{d\mathbf{p}}{dt} &= |\mathbf{p}| \frac{d\theta}{dt} = |\mathbf{p}| \frac{d\theta}{ds} \frac{ds}{dt} = \frac{|\mathbf{p}|}{\rho} \frac{ds}{dt} \\ &= e\mathbf{v} \times \mathbf{B} = e \frac{ds}{dt} B \end{aligned}$$

$$(B\rho) = \frac{p}{e} = \frac{pc}{ec} = \frac{\beta E}{ec} = \frac{\beta\gamma E_0}{ec} = \frac{m_0 c}{e} (\beta\gamma)$$

$$(B\rho)[T.m] = \frac{pc[eV]}{c[m.s^{-1}]} = 3.3356(pc)[GeV]$$

# Bending Magnet



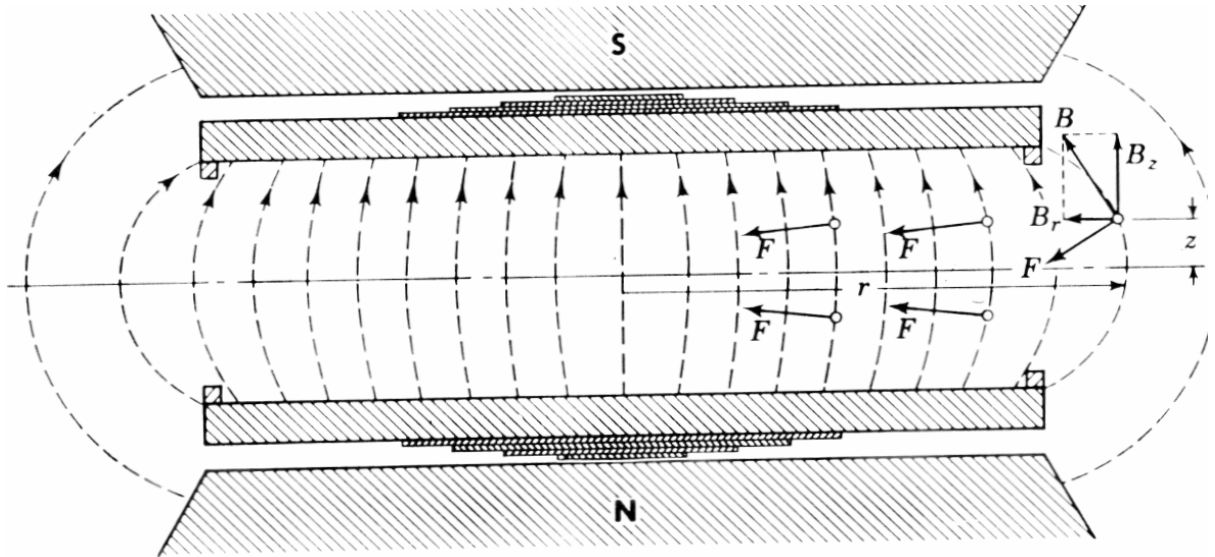
- ◆ Effect of a uniform bending (dipole) field

$$\sin (\theta / 2) = \frac{1}{2\rho} = \frac{1B}{2(B\rho)}$$

- ◆ If  $\theta \ll \pi / 2$  then  $\theta \approx \frac{1B}{(B\rho)}$

- ◆ Sagitta  $\pm \frac{\rho}{2} (1 - \cos (\theta / 2)) \approx \pm \frac{\rho \theta^2}{16} \approx \frac{1}{16} \theta$

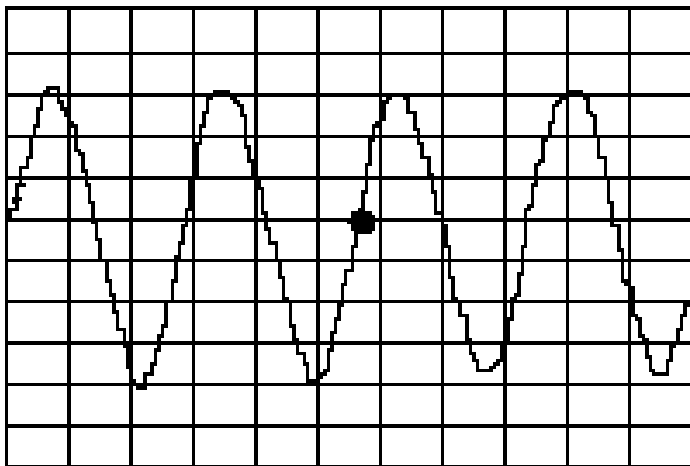
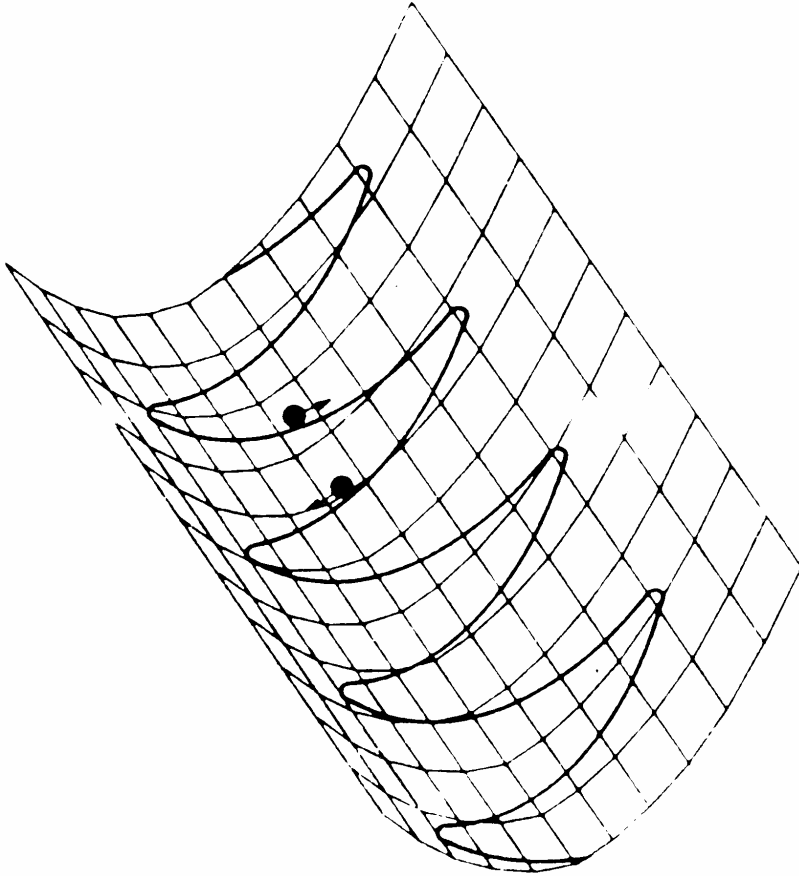
# Vertical Focusing



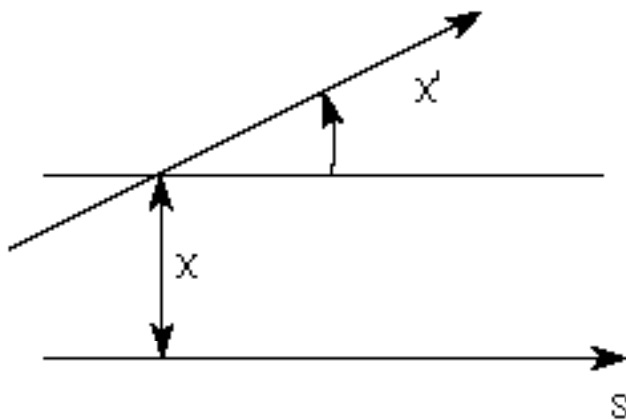
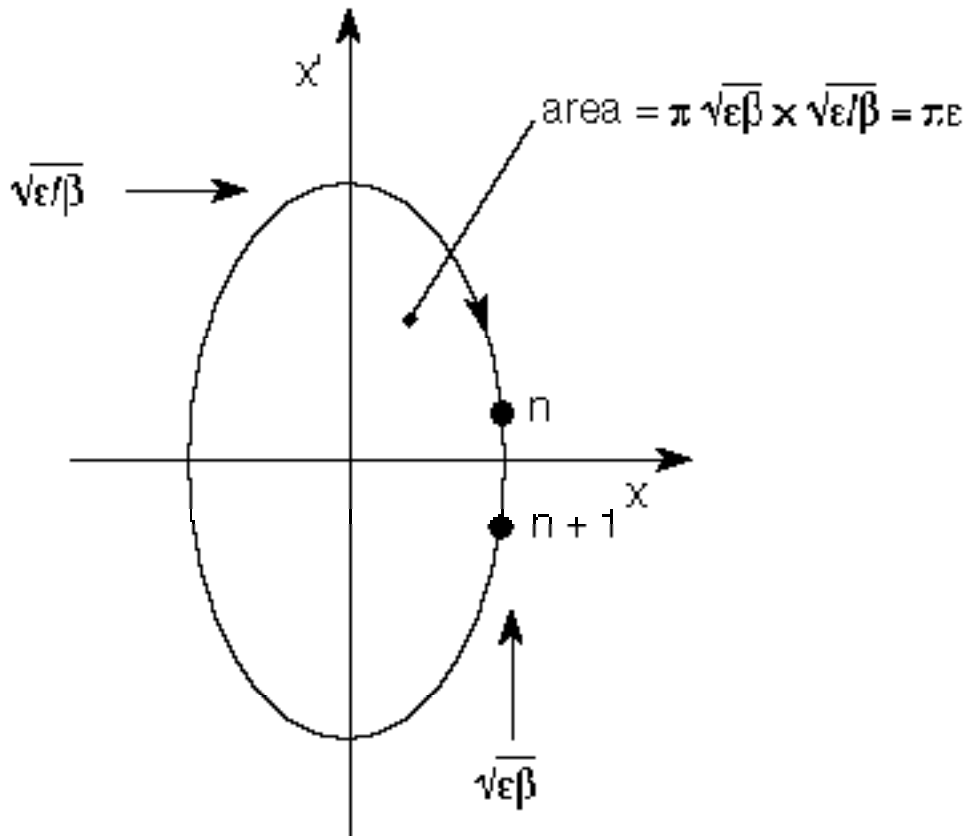
- ◆ People just got on with the job of building them.
- ◆ Then one day someone was experimenting
- ◆ Figure shows the principle of vertical focusing in a cyclotron
- ◆ In fact the shims did not do what they had been expected to do
- ◆ Nevertheless the cyclotron began to accelerate much higher currents

# Gutter

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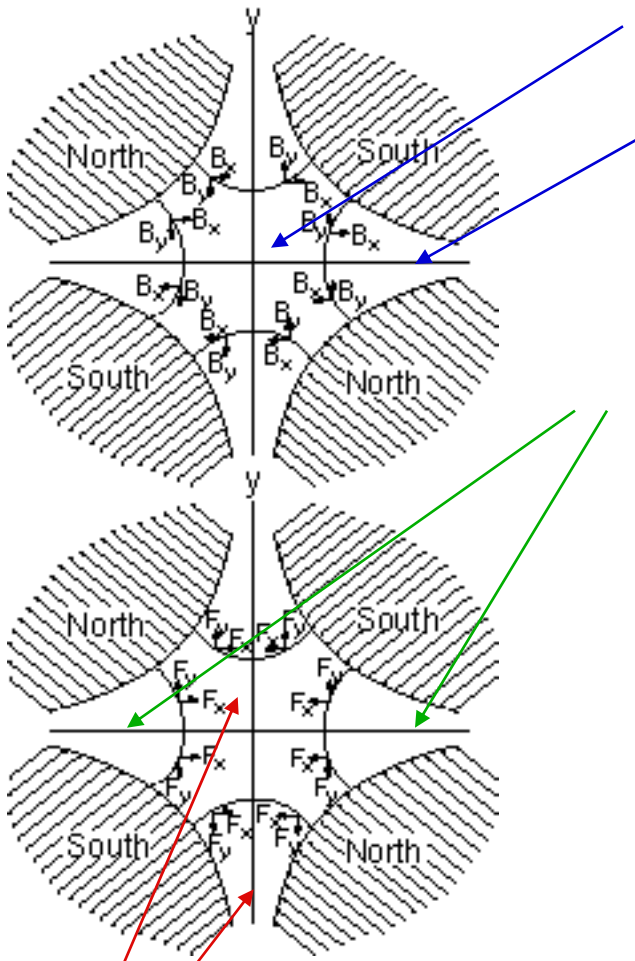


# Transverse ellipse





# Fields and force in a quadrupole



**No field on the axis**  
**Field strongest here**

$$B \propto x$$

**(hence is linear)**

**Force restores**

**Gradient**

$$\frac{dB_z}{dx}$$

**Normalised:**

$$k = -\frac{1}{(B\rho)} \frac{dB_z}{dx}$$

## POWER OF LENS

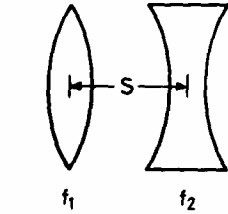
$$lk = -\frac{l}{(B\rho)} \cdot \frac{\partial B_z}{\partial x} = \frac{1}{f}$$

**Defocuses in vertical plane**

**SOLUTION IS TO ALTERNATE THE GRADIENTS OF A SERIES OF QUADS**

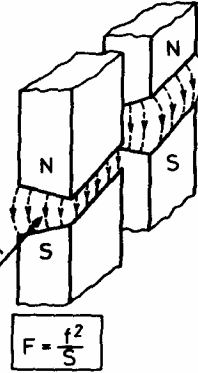
# Strong focusing

Positive-Negative Lens



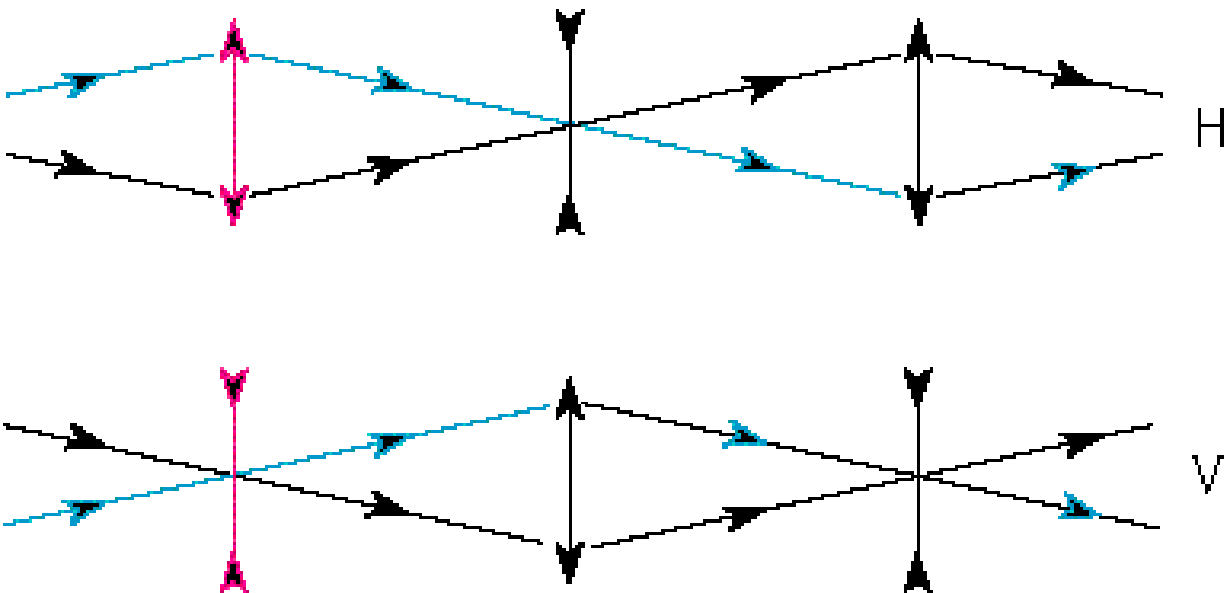
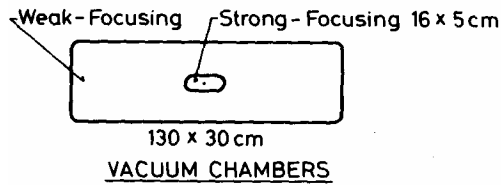
$$\frac{1}{F} = \frac{1}{f_1} + \frac{1}{f_2} - \frac{S}{f_1 \cdot f_2}$$

$$f = f_1 = f_2$$



$$F = \frac{f^2}{S}$$

$n \gg 0$      $n \ll 0$     Alternating Gradient, AG  
 $|n| \gg 1$



# Equation of motion in transverse coordinates

- ◆ Hill's equation (linear-periodic coefficients)

$$\frac{d^2 y}{ds^2} + k(s)y = 0$$

where  $k = -\frac{1}{(B\rho)} \frac{dB_z}{dx}$  at quadrupoles

like restoring constant in harmonic motion

- ◆ Solution (e.g. Horizontal plane)

$$y = \sqrt{\beta(s)} \sqrt{\varepsilon} \sin[\phi(s) + \phi_0]$$

- ◆ Condition

$$\phi = \int \frac{ds}{\beta(s)}$$

- ◆ Property of machine  $\sqrt{\beta(s)}$

- ◆ Property of the particle (beam)  $\varepsilon$

- ◆ Physical meaning (H or V planes)

Envelope

$$\sqrt{\varepsilon\beta(s)}$$

Maximum excursions

$$\hat{y} = \sqrt{\varepsilon\beta(s)}$$

$$\hat{y}' = \sqrt{\varepsilon / \beta(s)}$$

# Twiss Matrix

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- ◆ All such linear motion from points 1 to 2 can be described by a matrix like:

$$\begin{pmatrix} y(s_2) \\ y'(s_2) \end{pmatrix} = \begin{pmatrix} a & b \\ c & d \end{pmatrix} \begin{pmatrix} y(s_1) \\ y'(s_1) \end{pmatrix} = \mathbf{M}_{12} \begin{pmatrix} y(s_1) \\ y'(s_1) \end{pmatrix} .$$

- ◆ We define the “Twiss” parameters:

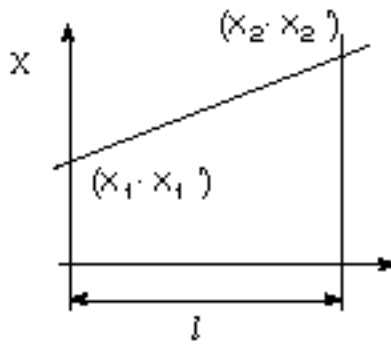
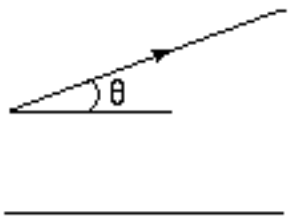
$$\beta = w^2, \quad \alpha = -\frac{1}{2}\beta', \quad \gamma = \frac{1 + \alpha^2}{\beta}$$

- ◆ Giving the matrix for a ring (or period)

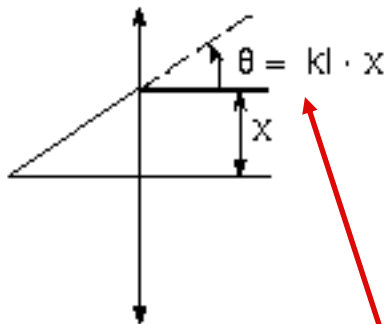
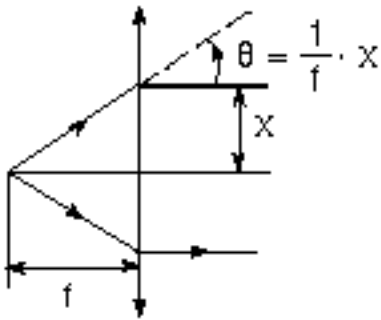
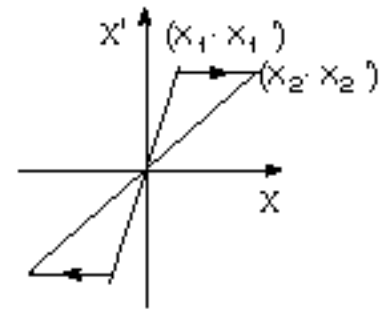
$$M = \begin{pmatrix} \cos \mu + \alpha \sin \mu, & \beta \sin \mu \\ -\gamma \sin \mu, & \cos \mu - \alpha \sin \mu \end{pmatrix}$$

# Effect of a drift length and a quadrupole

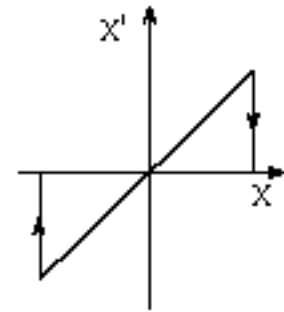
$$\begin{pmatrix} x_2 \\ x_2' \end{pmatrix} = \begin{pmatrix} 1 & 1 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x_1' \end{pmatrix}$$



(a)



(b)

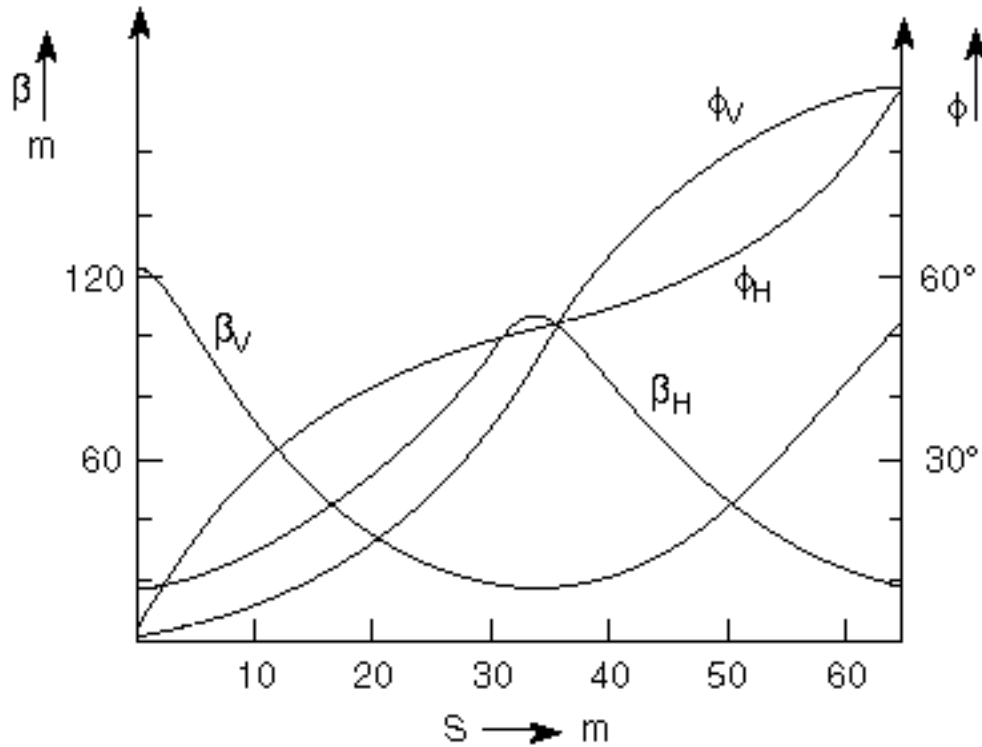


$$\theta = \frac{1}{f} \cdot x$$

$$\begin{pmatrix} x_2 \\ x_2' \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ -1/f & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x_1' \end{pmatrix}$$

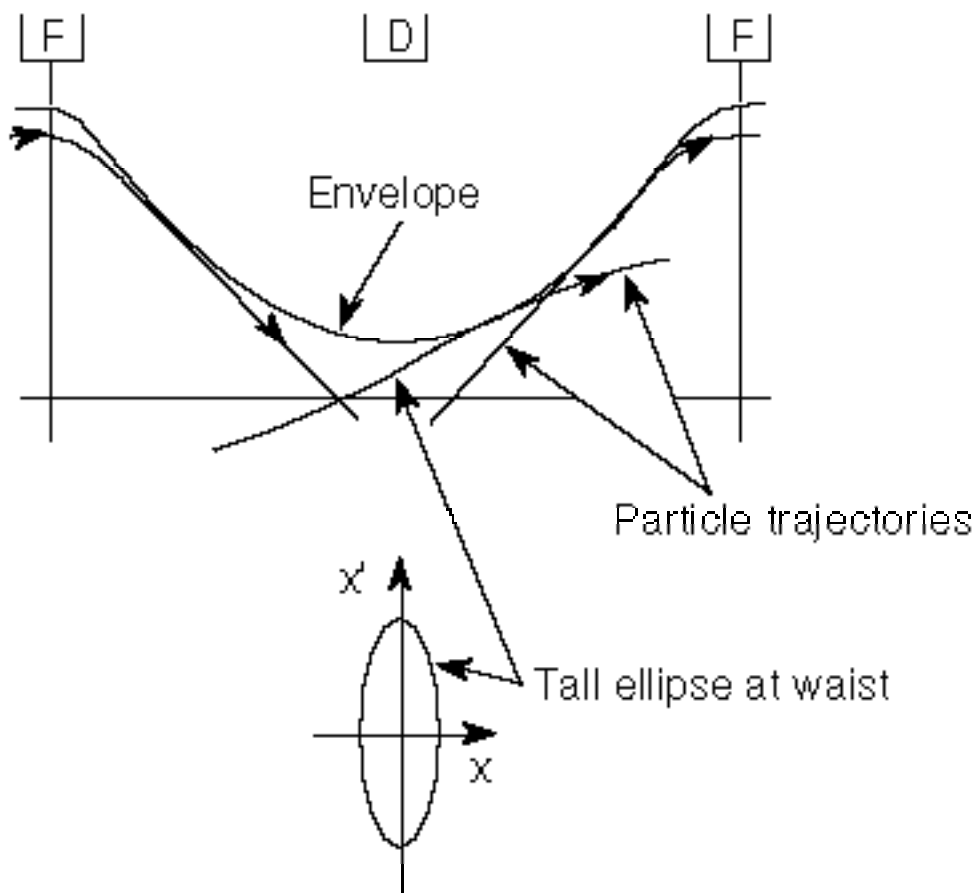
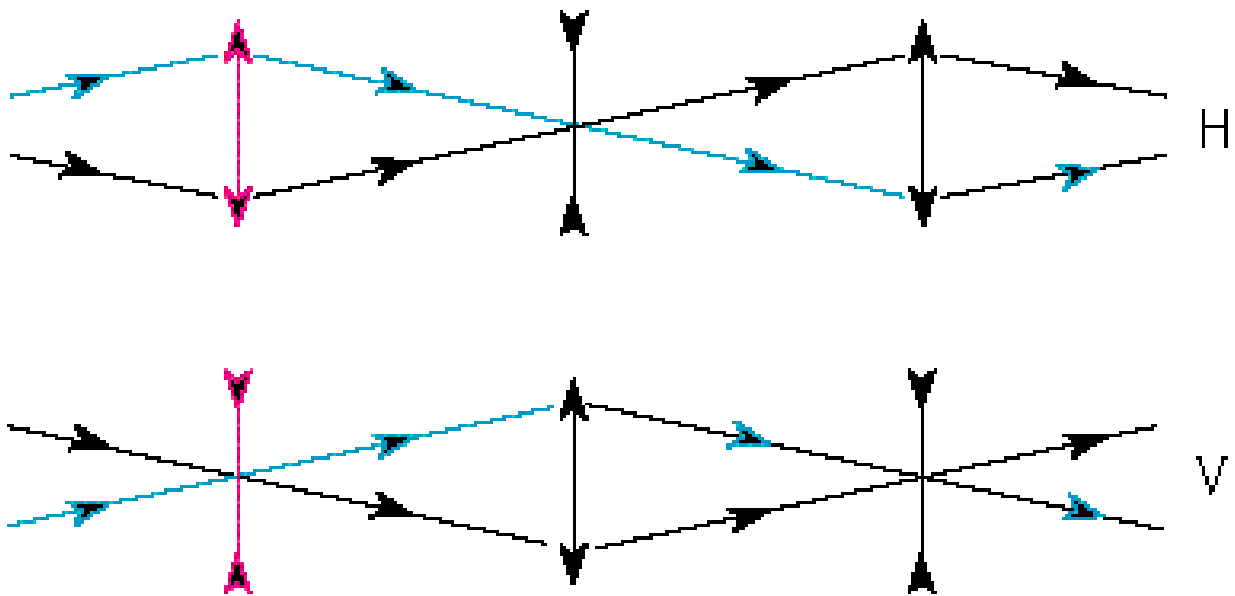
$$\begin{pmatrix} x_2 \\ x_2' \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ -kl & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x_1' \end{pmatrix}$$

# The lattice

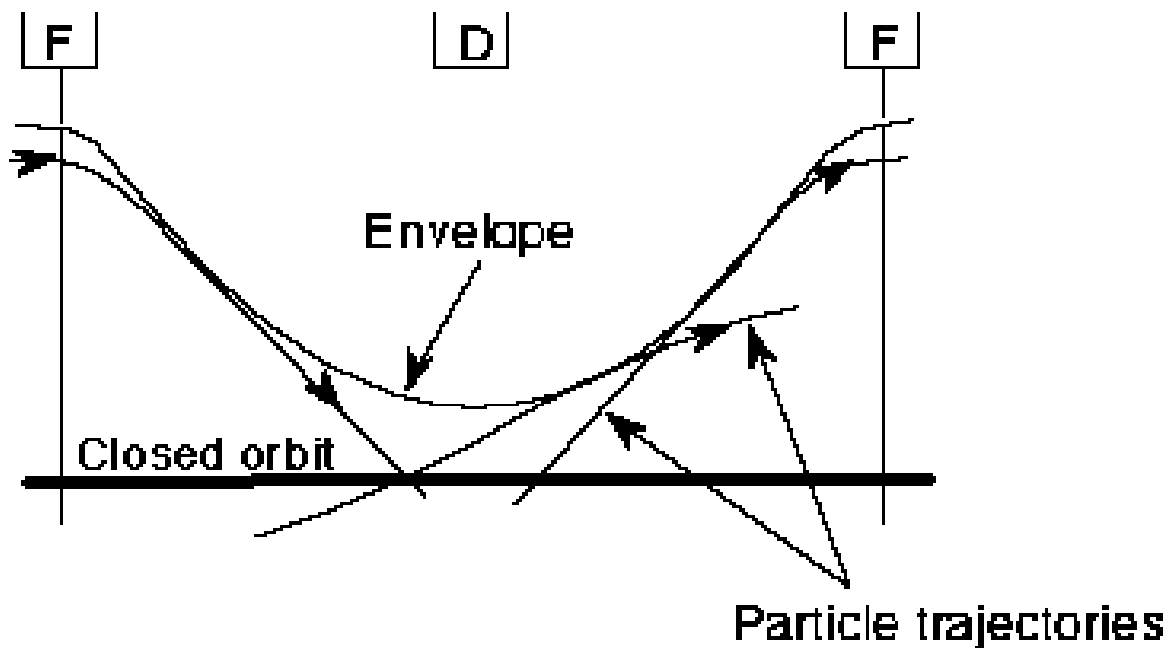


LENGTH	ANGLE	K(V)	ALPHA(P)	BETA(H)	ALPHA(H)	MUH/2PI	BETA(V)	ALPHA(V)	MUH/2PI	AH/2	AV/2
01	3,085000	0,000000	=,015063	1,386440104,884855	2,452160	,004571	19,011703	=,520345	,028571	65,715663	9,917560
2	3,360000	0,000000	0,000000	1,374053103,127965	2,428089	,005122	19,395014	=,544408	,029555	64,547513	10,017039
03	0,260000	,008445	0,000000	1,196124 75,348859	2,009521	,016433	28,828710	=,962519	,072198	64,004371	12,212911
4	4,400000	0,000000	0,000000	1,186405 73,751941	1,982775	,017287	29,609417	=,989248	,074377	64,751341	12,376828
05	0,260000	,008445	0,000000	1,060742 51,548094	1,564207	,033474	44,610910	=1,407071	,101988	54,174091	15,192432
6	3,390000	0,000000	0,000000	1,054559 50,338182	1,538130	,034692	45,718685	=1,433122	,103302	45,428661	15,379447
07	0,260000	,008445	0,000000	,981762 33,701223	1,119563	,058975	66,274961	=1,850527	,181441	44,905056	18,517478
8	3,800000	0,000000	0,000000	,978948 32,860011	1,094154	,060793	67,691002	=1,875896	,182344	36,980337	18,713705
09	0,260000	,008445	0,000000	,959017 21,751569	,875586	,098381	93,787676	=2,292753	,334861	36,534921	22,028267
10	2,342700	0,000000	0,000000	,961450 18,983146	,518942	,116788	104,896272	=2,449038	,338621	30,069327	21,295624
11	3,085000	0,000000	,018037	1,034354 18,983068	=,518916	,143368	104,901820	2,447388	,343191	28,349412	23,716825
12	3,350000	0,000000	0,000000	1,030730 19,354500	=,542318	,146275	103,196611	2,424067	,343726	28,638028	23,296218
13	0,260000	,008445	0,000000	1,370047 28,764399	=,968079	,189011	75,452122	2,007802	,355027	35,089639	23,106121
14	3,800000	0,000000	0,000000	1,391035 29,504322	=,986287	,191088	73,935822	1,982463	,358836	35,546047	19,787412
15	0,260000	,008445	0,000000	1,763219 44,472640	=1,404847	,218731	51,724094	1,655610	,371975	43,780575	19,557880
16	3,390000	0,000000	0,000000	1,788053 45,578591	=1,430924	,220109	50,513067	1,539589	,373169	44,298587	16,388398
17	0,260000	,008445	0,000000	2,213103 66,113699	=1,849484	,238298	33,849177	1,122280	,397377	53,470174	16,165782
18	4,400000	0,000000	0,000000	2,241952 67,603985	=1,876229	,239251	32,962034	1,095579	,399283	64,079136	13,233307
19	0,260000	,008445	0,000000	2,719888 93,714254	=2,294790	,251780	21,889390	,677943	,40745	63,830251	13,058741
20	2,352700	0,000000	0,000000	2,909420104,882261	=2,452099	,255558	19,038995	,520847	,405140	67,892709	10,634409
21	3,085000	0,000000	=,015063	2,946010104,882266	2,452098	,260189	19,038106	=,520546	,401673	68,853088	9,924676
22	3,360000	0,000000	0,000000	2,925443103,125421	2,428027	,260680	19,421551	=,544879	,404653	67,668889	10,023890
23	0,260000	,008445	0,000000	2,594240 73,347037	2,009467	,271992	28,854181	=,962177	,407246	67,105194	12,218305
24	4,400000	0,000000	0,000000	2,574765 73,750162	1,982722	,272846	29,634602	=,988874	,409424	67,546939	12,382087
25	0,260000	,008445	0,000000	2,296428 51,546933	1,564162	,289032	44,628208	=1,406185	,406955	66,950187	15,195377
26	3,390000	0,000000	0,000000	2,280734 50,337057	1,538085	,290251	45,735180	=1,432204	,405331	47,899567	15,382338
27	0,260000	,008445	0,000000	2,055284 33,700612	1,119525	,314534	66,276862	=1,849098	,376466	47,356928	18,517444
28	3,800000	0,000000	0,000000	2,043182 32,859428	1,094117	,316382	67,691805	=1,874435	,377389	39,127022	18,713817
29	0,260000	,008445	0,000000	1,870577 21,751395	,875557	,353941	93,786993	=2,290792	,389888	38,663082	22,028836
30	2,342700	0,000000	0,000000	1,815875 18,983101	,518917	,378318	104,865902	=2,446675	,393648	31,892336	23,292251
31	3,085000	0,000000	,015037	1,873603 18,983178	=,518943	,398928	104,662544	2,447912	,398220	30,027986	23,712598

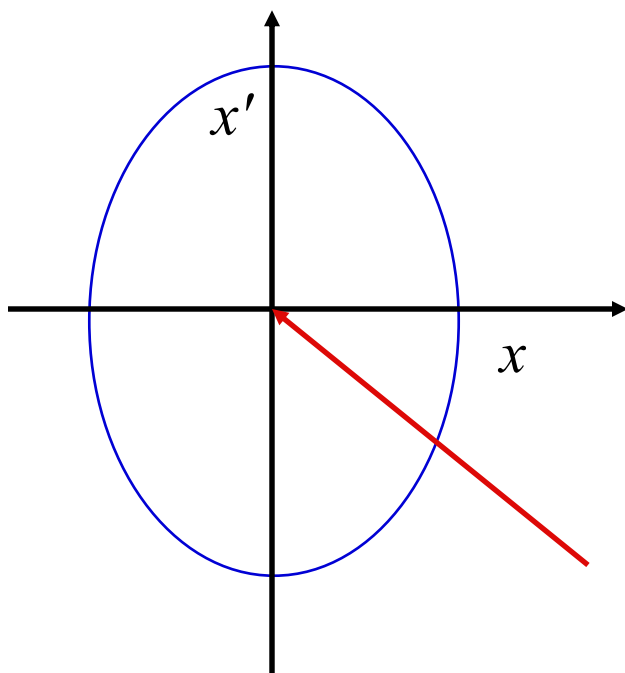
# Envelope and trajectories



# Closed orbit of an ideal machine



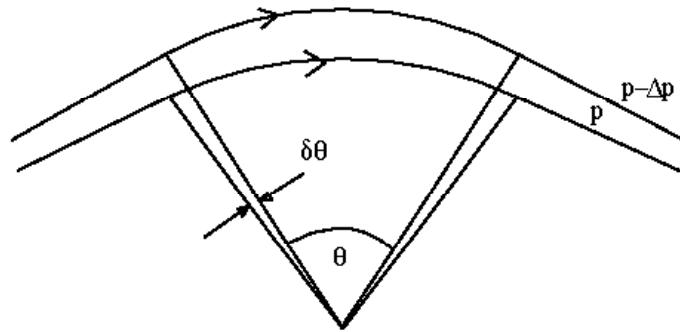
- ◆ In general particles executing betatron oscillations have a finite amplitude
- ◆ One particle will have zero amplitude and follows an orbit which closes on itself
- ◆ In an ideal machine this passes down the axis



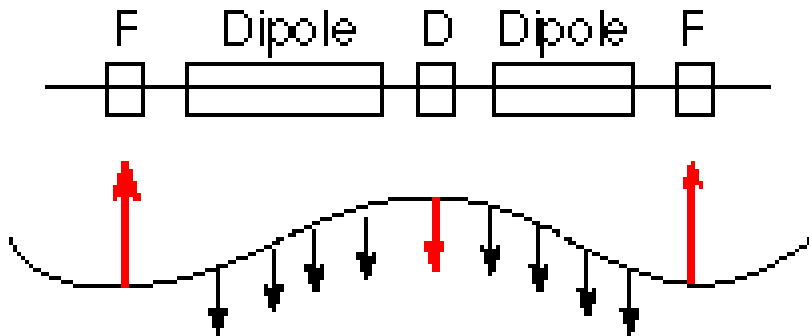
**Closed orbit  
Zero betatron  
amplitude**



# Dispersion



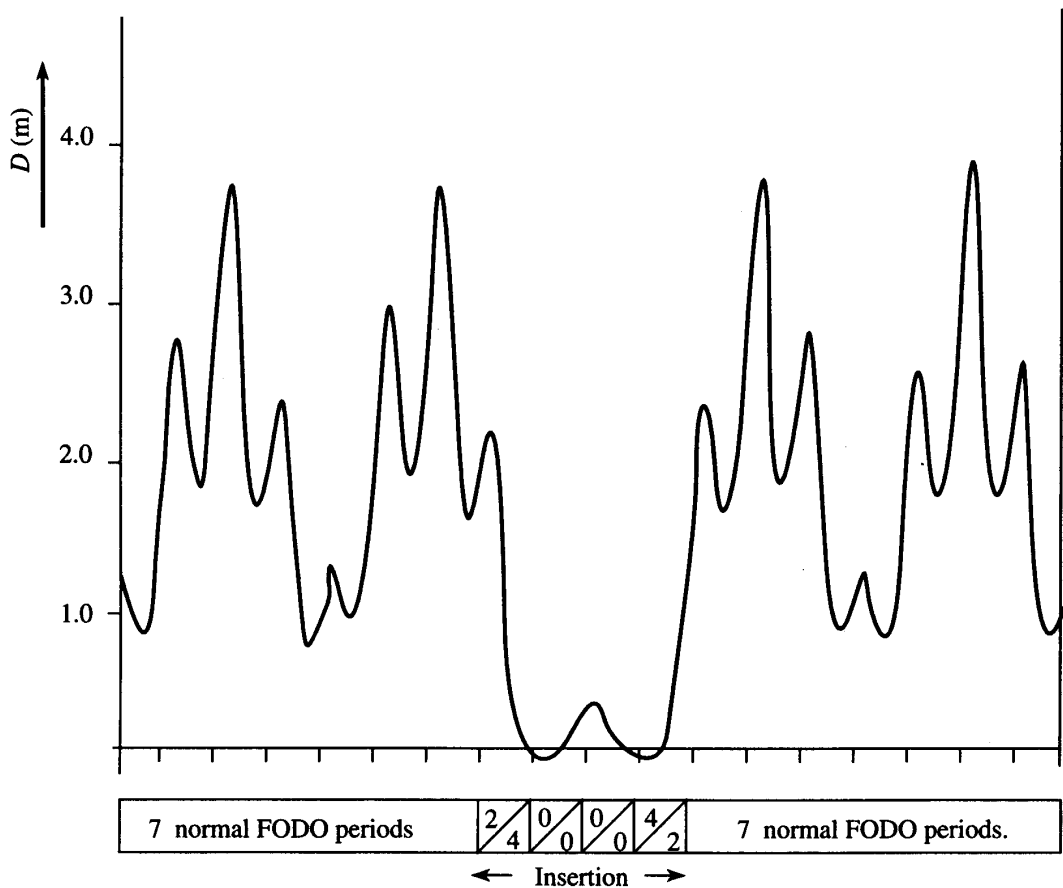
- ◆ Low momentum particle is bent more
- ◆ It should spiral inwards but:
- ◆ There is a displaced (inwards) closed orbit
- ◆ Closer to axis in the D's
- ◆ Extra (outward) force balances extra bends



- ◆  $D(s)$  is the “dispersion function”

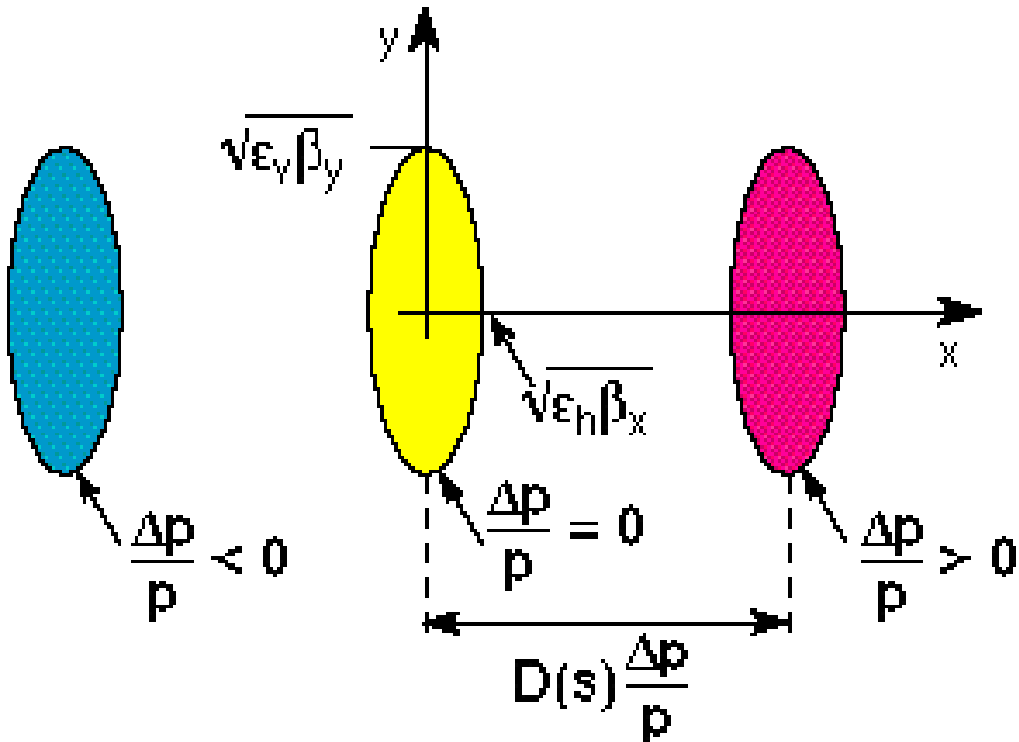
$$x = D(s) \frac{\Delta p}{p}$$

# Dispersion in the SPS



- ◆ This is the long straight section where dipoles are omitted to leave room for other equipment - RF - Injection - Extraction, etc
- ◆ The pattern of missing dipoles in this region indicated by “0” is chosen to control the Fourier harmonics and make  $D(s)$  small
- ◆ It doesn't matter that it is big elsewhere

# Dispersed beam cross sections



- ◆ These are real cross-section of beam
- ◆ The central and extreme momenta are shown
- ◆ There is of course a continuum between
- ◆ The vacuum chamber width must accommodate the full spread
- ◆ Half height and half width are:

$$a_V = \sqrt{\beta_V \epsilon_V} \quad , \quad a_H = \sqrt{\beta_H \epsilon_H} + D(s) \frac{\Delta p}{p} \quad .$$

# Physics of Chromaticity

- ◆ The  $Q$  is determined by the lattice quadrupoles whose strength is:

$$k = \frac{1}{(B\rho)} \frac{dB_z}{dx} \propto \frac{1}{p}$$

- ◆ Differentiating:

$$\frac{\Delta k}{k} = -\frac{\Delta p}{p} .$$

- ◆ From gradient error analysis

$$\delta Q = \frac{1}{4\pi} \beta \delta(kl)$$

Giving by substitution

$$\Delta Q = \frac{1}{4\pi} \int \beta(s) \delta k(s) ds .$$

$Q'$  is the chromaticity

- ◆ “Natural” chromaticity

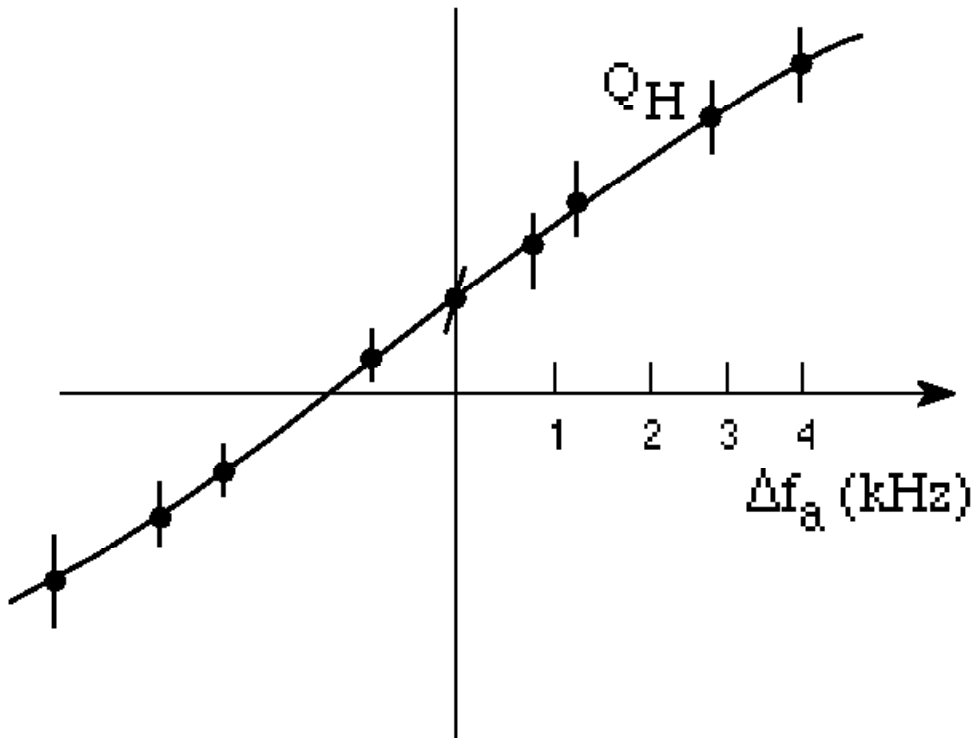
$$\Delta Q = \frac{1}{4\pi} \int \beta(s) \Delta k(s) ds = \left[ \frac{-1}{4\pi} \int \beta(s) k(s) ds \right] \frac{\Delta p}{p} .$$

$$\Delta Q = Q' \frac{\Delta p}{p}$$

$$Q' = -\frac{1}{4\pi} \oint \beta(s) k(s) ds \approx -1.3Q$$

**N.B. Old books say**  $\xi = \frac{p}{Q} \frac{dQ}{dp} = \frac{Q'}{Q}$

# Measurement of Chromaticity



- ◆ We can steer the beam to a different mean radius and a different momentum by changing the rf frequency and measure  $Q$

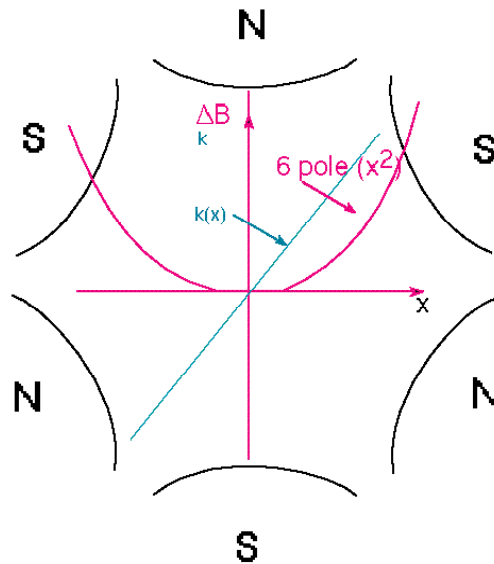
$$\Delta f_a = f_a \eta \frac{\Delta p}{p} \quad \Delta r = D_{av} \frac{\Delta p}{p}$$

- ◆ Since

- ◆ Hence 
$$\Delta Q = Q' \frac{\Delta p}{p}$$

$$\therefore Q' = f_a \eta \frac{dQ}{df_a}$$

# Correction of Chromaticity



- ◆ Parabolic field of a 6 pole is really a gradient which rises linearly with  $x$
- ◆ If  $x$  is the product of momentum error and dispersion
- ◆ The effect of all this extra focusing cancels **chromaticity**

$$\Delta k = \frac{B'' D \Delta p}{(B\rho) p} .$$

- ◆ Because gradient is opposite in  $v$  plane we must have two sets of opposite polarity at F and D quads where betas are different

$$\Delta Q = \left[ \frac{1}{4\pi} \int \frac{B''(s)\beta(s)D(s)ds}{(B\rho)} \right] \frac{dp}{p} .$$

# **Transverse dynamics - Summary**

## *E. Wilson - CERN*

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- ◆ **Components of a synchrotron**
- ◆ **Dipole Bending Magnet**
- ◆ **Magnetic rigidity**
- ◆ **Bending Magnet**
- ◆ **Weak focusing - gutter**
- ◆ **Transverse ellipse**
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