## Vacuum II

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## Index

Creating Vacuum (continuation) Measuring Vacuum Partial Pressure Measurements

# **Diffusion Ejector pump**





#### **Pump principle:**

The vacuum gas diffuses into the jet and gets kicked by the oil molecules imprinting a downward momentum

The oil jets produces a skirt which separate the inlet from the outlet





Cold surface

30/5/2011





LEYBOLD (LEYBODIFF)

with  $p_u \sim 10^{-6} \, {
m mbar}$ 

The pumping speed  ${\rm S_m}$  is proportional to the area of the inlet port

100 mm diameter  $\rightarrow$  S<sub>m</sub> = ~ 250 l/s for N<sub>2</sub>



## **Capture Vacuum Pumps**

#### **Principle**

Capture vacuum pumps are based on the process of capture of vacuum molecules by surfaces

Getter Pumps (evaporable, non-evaporable)

**Sputter ion Pumps** 

**Cryo Pumps** 

#### **Getter Pumps**



Getters are materials capable of chemically adsorbing gas molecules. To do so their surface must be clean. For <u>Non-Evaporable Getters</u> a clean surface is obtained by heating to a temperature high enough to dissolve the native oxide layer into the bulk.



P. Chiggiato

NEGs pump most of the gas except rare gases and methane at room temperature

#### **Sorption Speed and Sorption Capacity**



C.Benvenuti, CAS 2007

#### Choice of the coating technique for thin film: sputtering



> The trend in vacuum technology consists in moving the pump progressively closer to the vacuum chamber wall.

> The ultimate step of this process consists of transforming the vacuum chamber from a gas source into a pump.

One way to do this is by "ex-situ" coating the vacuum chamber with a NEG thin film that will be activated during the "in situ" bakeout of the vacuum system.
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**Dipole Coating Facility** 



#### **Quadrupole Coating Facility**



M.C. Bellachioma (GSI)

## Sputter ion pumps



#### Sputtering process



#### A glimpse to the complexity



#### **Example of Pumping speed**



**Fig. 5.67.** Volume throughput (VTP) of sputter ion pumps for nitrogen as a function of pressure. IZ270 is a pump with nominal VTP, S=270 liter s<sup>-1</sup>, diode and triode; IZ500 is a pump with nominal VTP, S=500 liter s<sup>-1</sup>, diode and triode.

J.M. Laffterty, Vacuum Science, J. Wiley & Son, 1998

## Cryo Pumps



Dispersion forces between molecules and surface are stronger then forces between molecules

Schematic of a cryo pump



Now 
$$I_w = \frac{1}{4}\tilde{n}_w v_w A \longrightarrow$$
 By using the state equation  $\longrightarrow I_w = \frac{P_w A}{4k_B T_w} v_w$   
In the same way  $\longrightarrow I_c = \frac{P_c A}{4k_B T_c} v_c$   
If  $I_c = I_w$  no pumping although  $P_c \neq P_w$ 

#### Relation between pressures

Thermal Transpiration 
$$\frac{P_c}{\sqrt{T_c}} = \frac{P_w}{\sqrt{T_w}}$$

When the two pressures breaks the thermal transpiration condition a particle flow starts

$$I_{net} = I_w - I_c = \frac{AP_w v_w}{4k_B T_w} \left[ 1 - \frac{P_c}{P_w} \frac{v_c T_w}{v_w T_c} \right]$$

We define 
$$I_{max} = \frac{AP_w v_w}{4k_B T_w}$$
 and  $P_w(ult) = P_c \sqrt{\frac{T_w}{T_c}}$   
We find  $I_{net} = I_{max} \left[ 1 - \frac{P_w(ult)}{P_w} \right]$ 

P<sub>c</sub> depends on the capture process

**Cryocondensation:**  $P_w$  is the vapor pressure of the gas at  $T_c$ 



#### Summary on Pumps



#### Gauges

**Liquid Manometers** 

**MacLeod Gauges** 

**Viscosity Gauges** 

**Thermal conductivity Gauges** 

**Hot Cathode Gauges** 

**Alpert-Bayard Gauges** 

**Penning Gauges** 

# Liquid Manometers



Relation between the two pressure

$$P_1 - P_2 = h\rho g$$

issue: measure precisely "h" by eye +/- 0.1 mm but with mercury surface tension depress liquid surface High accuracy is reached by knowing the liquid density

Mercury should be handled with care: serious health hazard

# McLeod Gauge

First mode of use:



The reservoir is raised till the mercury reaches the level of the second branch (which is closed)

$$P_2 = \rho g \frac{\Delta h^2}{h_0 - \Delta h}$$

Quadratic response to P<sub>2</sub>

Second mode of use: keep the distance  $\Delta h$  constant and measure the distance of the two capillaries  $\rightarrow$  linear response in  $\Delta h$ 

# **Viscosity Gauges**



It is based on the principle that gas molecules hitting the sphere surface take away rotational momentum



The angular velocity of the sphere decreases

$$P = \frac{\pi}{10} \rho R v_a \left( \frac{1}{\omega} \frac{d\omega}{dt} + 2\alpha \frac{dT}{dt} \right)$$

 $\rho$  = sphere density  $\alpha$  = coefficient of thermal dilatation T = temperature  $v_a$  = thermal velocity



Fig. 24: Schematic of a spinning rotor gauge. 1 rotor; 2 vacuum tube; 3 permanent magnets; 4 two coils for vertical stabilization; 5 four drive coils; 6 two detection coils; 8 four coils for horizontal stabilization. From *Wutz Handbuch Vakaumtechnik* by K. Jousten (ed.), Vieweg Verlag.

(K. Jousten, CAS 2007)



F.J. Redgrave, S.P. Downes, "Some comments on the stability of Spinning Rotor Gauges", Vacuum, Vol. 38, 839-842

# Thermal conductivity Gauges



A hot wire is cooled by the energy transport operated by the vacuum gas

$$\dot{E} = \sqrt{\frac{2k}{\pi m T_g}} \alpha (T_w - T_g) P_s$$

Accommodation factor

$$\alpha = \frac{T_d - T_g}{T_w - T_g}$$

By measuring dE/dt we measure P

# **Energy Balance**



Energy loss by gas molecules

$$\dot{E} = \sqrt{\frac{2k}{\pi m T_g}} \alpha (T_w - T_g) P_s$$

- Energy loss by Radiation
  - $W_R = \epsilon \sigma (T_w^4 T_g^4)$

$$\sigma = 5.673 \times 10^{-8} \,\mathrm{W} \;\mathrm{m}^{-2} \mathrm{K}^{-4}$$

 $\epsilon$  = emissivity

Energy loss by heat conduction

When the energy loss by gas molecule is dominant P can be predicted with contained systematic error

# Pirani Gauge



## **Ionization Gauges Principle**





#### Electrons ionization rate





## Hot Cathode Gauges



## Hot Cathode Gauges



## Limit of use



### **Alpert-Bayard Gauge**



#### Schematic of the original design (K. Jousten, CAS 2007)



Fig. 11: The original design of the Bayard-Alpert gauge. From R.T. Bayard and D. Alpert, *Rev. Sci. Instrum.* 21 (1950) 571.

#### Penning Gauge (cold cathode gauges)



Under proper condition of (E,B) electrons get trapped in the Penning Gauge





### **Ionization process**







More electrons are formed through the ionization of the vacuum gas and remains inside the trap



#### When the discharge gets saturated each new ionization produce a current



The time necessary for the discharge formation depends upon the level of the vacuum

lower pressure  $\rightarrow$  longer time of formation



J.M. Lafferty, Vacuum Science, p. 322

## Summary on Gauges

N. Marguardt



#### Partial Pressure Measurements

These gauges allow the determination of the gas components

Partial pressure gauges are composed



### Ion Sources

 $\rightarrow$ 

Vacuum gas is ionized via electron-impact

the rate of production of ions is proportional to each ion species

#### **Electron-impact ionization process**







#### The minimum energy to ionize M Xe Ion pairs/cm mm Hg is called "appearance potential" 10 Hg $S_e$ Electron $\mathbf{y}$ lon pairs/mbar-cm 1.0 IP = 15 eV $M^+ + e^-$ 0.5 15 0.3 A O<sub>2</sub>, CO, NO N<sub>2</sub> 0.2 $H_2$ He 10-1 $5 \times 10^{-2}$ He $3 \times 10^{-2}$ 103 104 20 30 50 102 10 Electron energy (eV) appearance

#### At the appearance potential the production rate is low

energy

(eV)

G. Franchetti

potential

A. von Engel, Ionized Gases, AVS Classics Ser., p. 63. AIP Press, 1994

#### lon source



# A schematic



# Ion Detection

Faraday Cup

Secondary electron Multiplier (SEM)

Idea: an ion enters into the tube, and due to the potential is accelerated to the walls. At each collision new electrons are produced in an avalanche process



J.Adams, B.W. Manley IEEE Transactions on Nuclear Science, vol. 13, issue 3, 1966. p. 88

Gain



 $G = \left(\frac{KV_0^2}{4V\alpha^2}\right)^{\left(\frac{4V\alpha^2}{V_0}\right)}$ 

- $\alpha = L/d$
- $V_0$  = applied voltage

V = initial energy of the electron

 $K = \delta V_c$ 

where

 $\delta$  = secondary emission coefficient  $V_c$  = collision energy

## Mass Analyzers

#### **Quadrupolar mass spectrometer**



By rescaling of the coordinates the equation of motion becomes

$$\frac{d^2x}{d\theta^2} = (a + 2q\cos 2\theta)x \qquad \longleftarrow \qquad \begin{array}{c} \text{Mathieu} \\ \frac{d^2y}{d\theta^2} = -(a + 2q\cos 2\theta)y \\ \frac{d^2z}{d\theta^2} = 0 \end{array} \qquad \begin{array}{c} \text{Mathieu} \\ \text{Equation} \end{array}$$

The ion motion can be stable or unstable

Stability of motion

	horizontal	vertical
q=0, a>0	unstable	stable
q=0, a<0	stable	unstable

The presence of the term q, changes the stability condition

#### **Development of stable motion**

Stable or unstable motion is referred to a channel which is infinitely long, but typically a length correspondent to 100 linear oscillation is considered enough

Example:

For N<sub>2</sub> at E<sub>k</sub> = 10 eV 
$$\rightarrow$$
 v<sub>s</sub> = 8301 m/s  
For a length of L = 100 mm  
100 rf oscillation f = 8.3 MHz f ~ 2 MHz





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q



#### **Magnetic Sector Analyzer**





The revolution time is independent from ion energy

$$\tau = \frac{2\pi}{B} \frac{M}{q}$$

If the frequency of the RF is  $1/\tau$ a resonant process takes place and particle spiral out



**Resolving power** 

$$\frac{M}{\Delta M} = 4.8 \times 10^{-5} \frac{R_0 B^2}{E_0} \frac{e}{M}$$

# Conclusion

Creating and controlling vacuum will always be a relevant part of any accelerator new development.

#### THANK YOU FOR YOUR ATTENTION

These two lectures provides an introduction to the topic, which is very extensive: further reading material is reported in the following bibliography



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Thermal Physics, Charles Kittel, (John Wiley and Sons, 1969).

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- The Physical Basis of Ultrahigh Vacuum, P. A. Redhead, J. P. Hobson, E. V. Kornelsen, AIP, 1993, ISBN 1-56396-122-9
- Foundation of Vacuum Science, J.M. Lafferty, Wiley & Sons, 1998
- Vacuum in accelerators, CERN Accelerator School, CERN-2007-003 11 June 2007
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