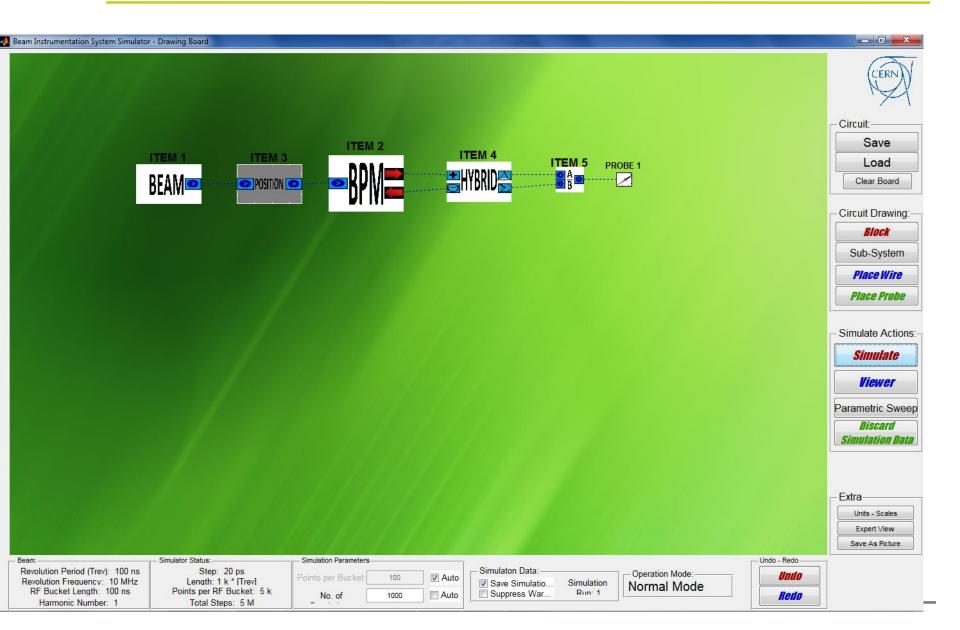
Calibration of Button Type Beam Position Monitors

Yellow: Your Tasks T1 – T4



Simulation



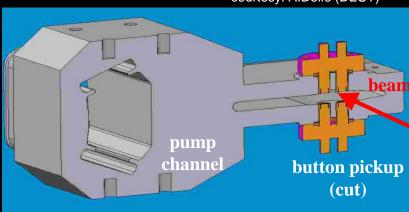


Electrostatic Pick-up - Button

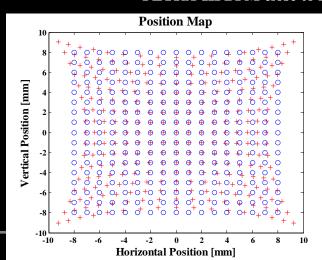
Non-linear

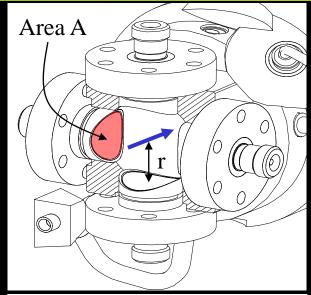
- requires correction algorithm when beam is off-centre
- vacuum chamber not rotational symmetric (SR-source)

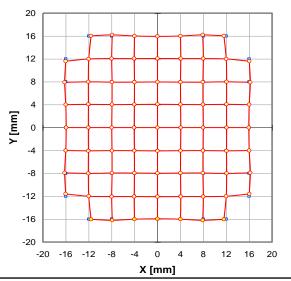
courtesy: A.Delfs (DESY)



PETRA-III BPM close to ID





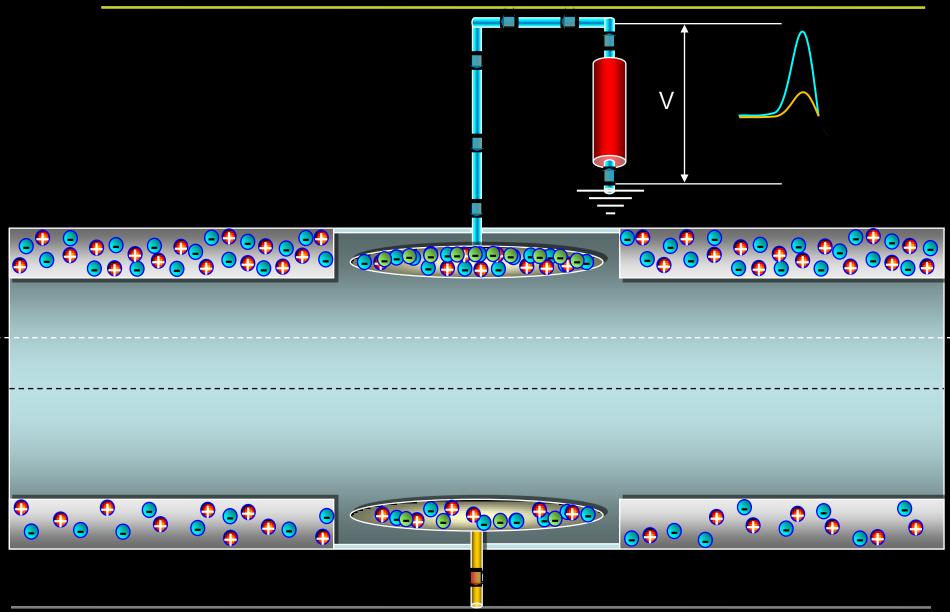


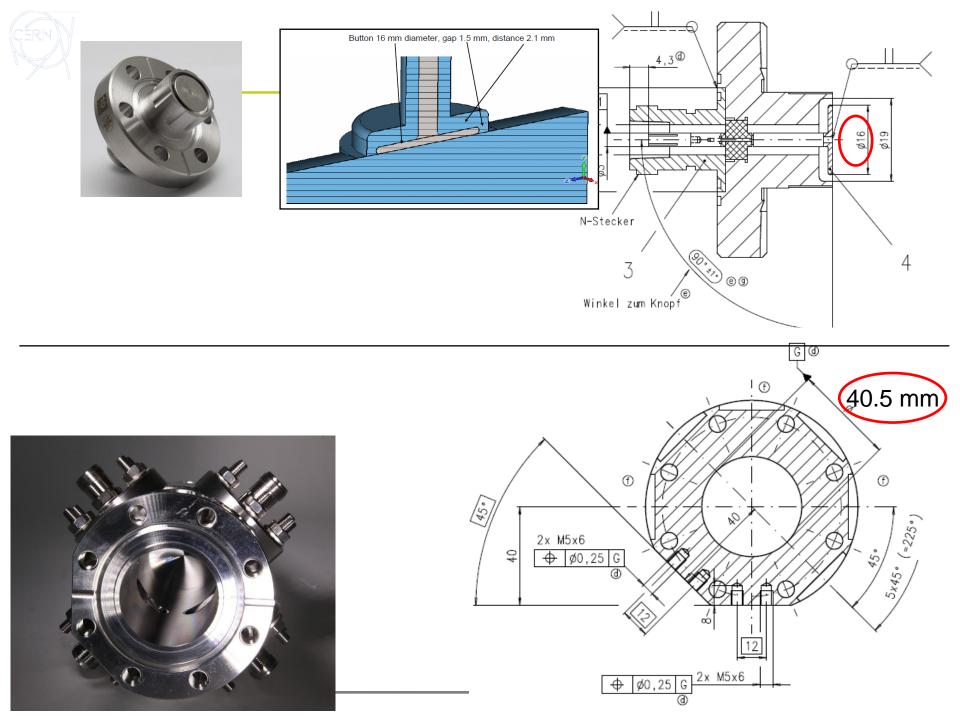
 $X = 2.30 \cdot 10^{-5} X_{1}^{5} + 3.70 \cdot 10^{-5} X_{1}^{3} + 1.035 X_{1} + 7.53 \cdot 10^{-6} X_{1}^{3} Y_{1}^{2} + 1.53 \cdot 10^{-5} X_{1} Y_{1}^{4}$

tion Group



Electrostatic Beam Position Monitor

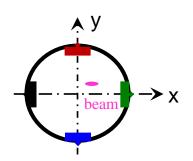




Position Reconstruction

- Two common monitor geometries
 - difference in position reconstruction

linac-type



$$\mathbf{x} = \mathbf{K_x} \cdot \frac{\mathbf{P_1} - \mathbf{P_3}}{\mathbf{P_1} + \mathbf{P_3}}$$

$$Y = K_y \frac{P_2 - P_4}{P_2 + P_4}$$

difference-over-sum or
$$Position = K \cdot \frac{\Delta}{\Sigma}$$

Position Information

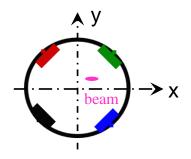
- requires knowledge of monitor constant K_x , K_v
 - \rightarrow rule of thumb (circular duct)

$$K_{x,y} = \frac{r}{2} \frac{\alpha}{\sin \alpha}$$

$$K_{x,y} = \frac{r}{\sqrt{2}} \frac{\alpha}{\sin \alpha}$$

linac-type

storage ring-type



$$x = K_x \frac{(P_1 + P_4) - (P_2 + P_3)}{P_1 + P_2 + P_3 + P_4}$$

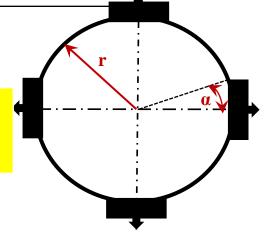
$$y = K_y \frac{(P_1 + P_2) - (P_3 + P_4)}{P_1 + P_2 + P_3 + P_4}$$

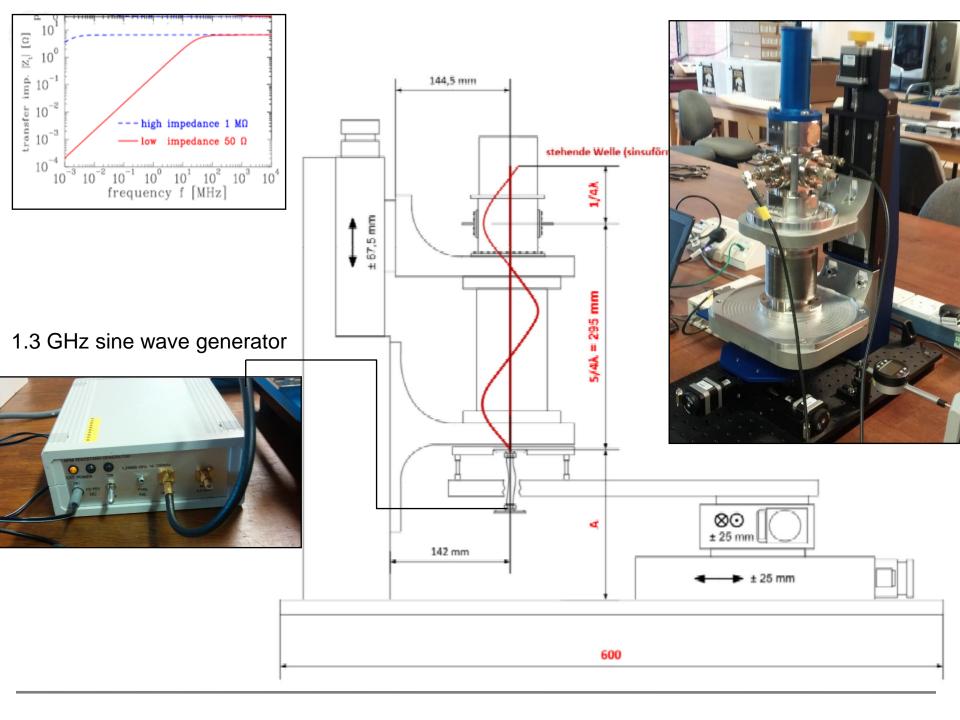
Beampipe: round: r = 20.25 mm

Button Diameter: d =16.0 mm

T1) Calculate K_x. for Linac type

$$sin(\alpha) = \alpha = K_x = K_x$$



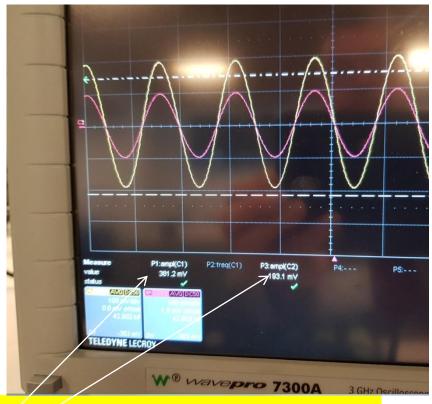


Tasks: BPMs



Signal generation by button BPM

- calculate monitor constants for BPMs
 - use rule-of-thumb formulae
- measure XFEL BPM monitor constants



- T2) define electrical center of both planes and calibrate movers
- \rightarrow T3) perform 1-dim. scan along one axis \rightarrow max. wire position: \pm 15 mm (!!!)
- \rightarrow 3a) measure signal amplitudes from each button (x-plane only)
- \rightarrow 3b) calculate Δ/Σ from measured signals
- \rightarrow 3c) plot Δ/Σ versus wire position
- T4) determine monitor constant from slope at origin and compare with rule-of-thumb

Monitor Constant Calculation



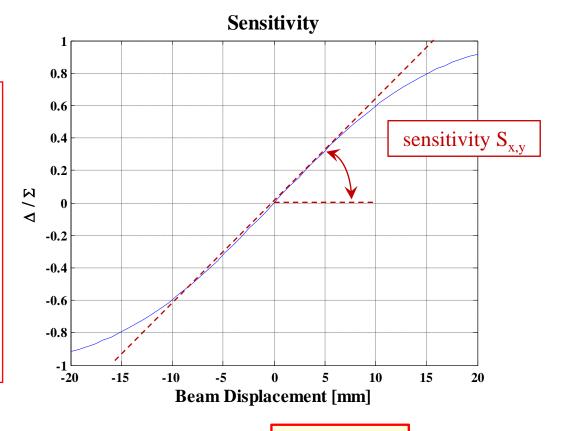
$$\mathbf{x} = \mathbf{K}_{\mathbf{x}} \frac{\mathbf{P}_1 - \mathbf{P}_3}{\mathbf{P}_1 + \mathbf{P}_3} = \mathbf{K}_{\mathbf{x}} * \Delta/\Sigma$$

> sensitivity: slope at origin

Please stay in the middle of Chamber!!!!-

Maximum ± 15 mm

(more might damage the antenna)



monitor constant:

$$\mathbf{K}_{\mathbf{x},\mathbf{y}} = \mathbf{S}_{\mathbf{x},\mathbf{y}}^{-1}$$

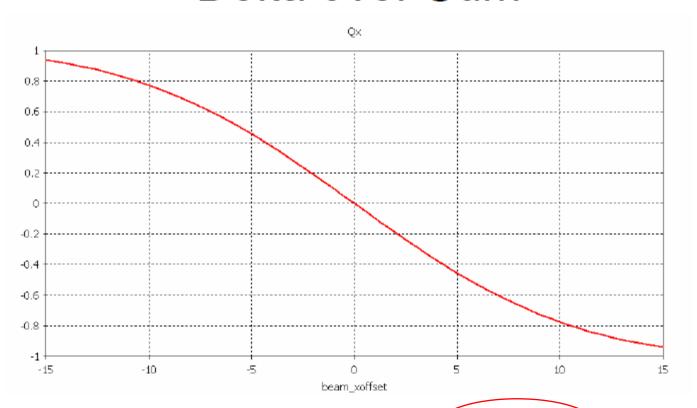


• End



From CST Simulation

Delta over Sum

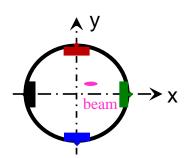


Scan in x, Sensitivity=0.0942/mm, monitor constant=10.61 mm

Position Reconstruction

- Two common monitor geometries
 - difference in position reconstruction

linac-type



$$\mathbf{x} = \mathbf{K_x} \cdot \frac{\mathbf{P_1} - \mathbf{P_3}}{\mathbf{P_1} + \mathbf{P_3}}$$

$$y = K_y \frac{P_2 - P_4}{P_2 + P_4}$$

difference-over-sum or
$$Position = K \cdot \frac{\Delta}{\Sigma}$$

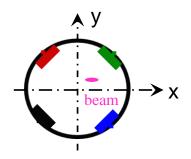
- Position Information
 - requires knowledge of monitor constant K_x , K_v
 - \rightarrow rule of thumb (circular duct)

$$K_{x,y} = \frac{r}{2} \frac{\alpha}{\sin \alpha}$$

$$K_{x,y} = \frac{r}{\sqrt{2}} \frac{\alpha}{\sin \alpha}$$

linac-type

storage ring-type



$$x = K_x \frac{(P_1 + P_4) - (P_2 + P_3)}{P_1 + P_2 + P_3 + P_4}$$

$$y = K_y \frac{(P_1 + P_2) - (P_3 + P_4)}{P_1 + P_2 + P_3 + P_4}$$

Beampipe: round: r = 20.25 mm

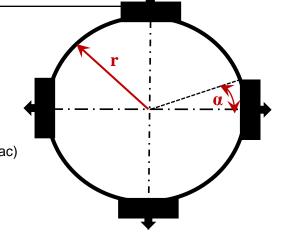
Button Diameter: d = 16.0 mm

T1) Calculate K_x for Linac type

$$\sin(\alpha) = 0.367$$

$$\alpha = 0.376$$

$$K_x = 10.367 \text{ mm (linac)}$$

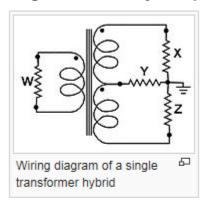




180 deg Hybrids

Input at x and z out W = x+z, out Y = x-z

Single transformer hybrid [edit]



For use in 2-wire repeaters, the single transformer version suffices, since amplifiers in the repeaters have grounded inputs and outputs. X, Y, and Z share a common ground. As shown at left, signal into W, the 2-wire port, will appear at X and Z. But since Y is bridged from center of coil to center of X and Z, no signal appears. Signal into X will appear at W and Y. But signal at Z is the difference of what appears at Y and, through the transformer coil, at W, which is zero. Similar reasoning proves both pairs, W & Y, X & Z, are conjugates.

Wiring diagram of a double transformer hybrid

Double transformer hybrid [edit]

When both the 2-wire and the 4-wire circuits must be balanced, double transformer hybrids are used, as shown at right. Signal into port W splits between X and Z, but due to reversed connection to the windings, cancel at port Y. Signal into port X goes to W and Y. But due to reversed connection to ports W and Y, Z gets no signal. Thus the pairs, W & Y, X & Z, are conjugates.

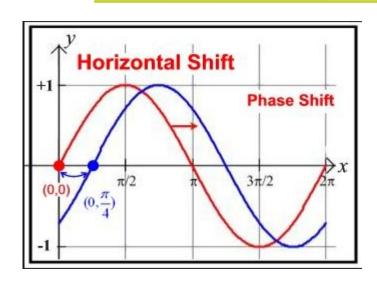


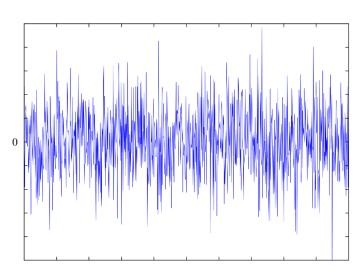
180° Hybrids Functional Description

A 180° hybrid is a reciprocal four-port device which provides two equal amplitude in-phase signals when fed from its sum port (Σ) and two equal amplitude 180° out-of-phase signals when fed from its difference port (Δ) . Conversely, signals input into ports C and D will add at the sum port (B) and the difference of the two signals will appear at the difference port (A). **Figure 1** is a functional diagram which will be used in this article to represent the 180° hybrid. Port B can be considered the sum port and port A is the difference port. Ports A and B and ports C and D are isolated pairs of ports.

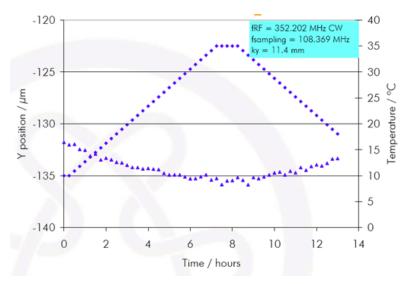


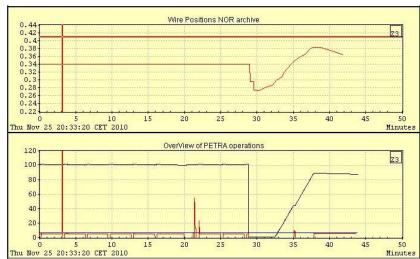
Phase, Noise, and Drifts (Stability)





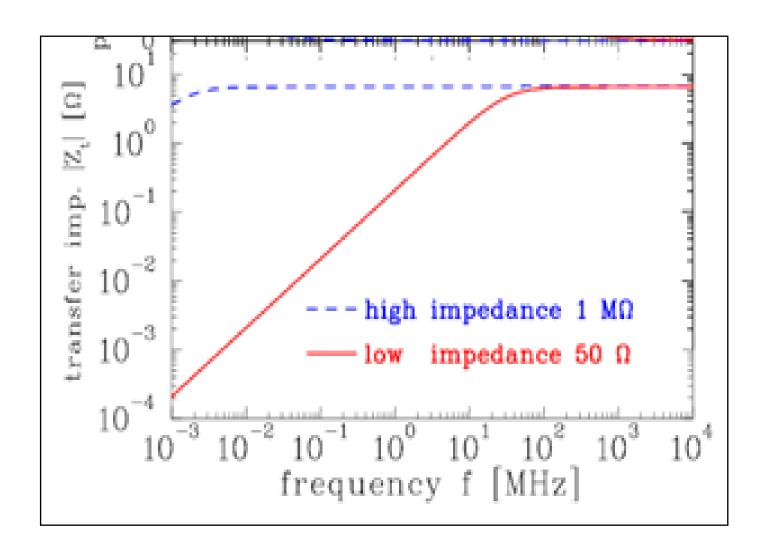
Problem: Electronic drift: 0.2 μm/°C





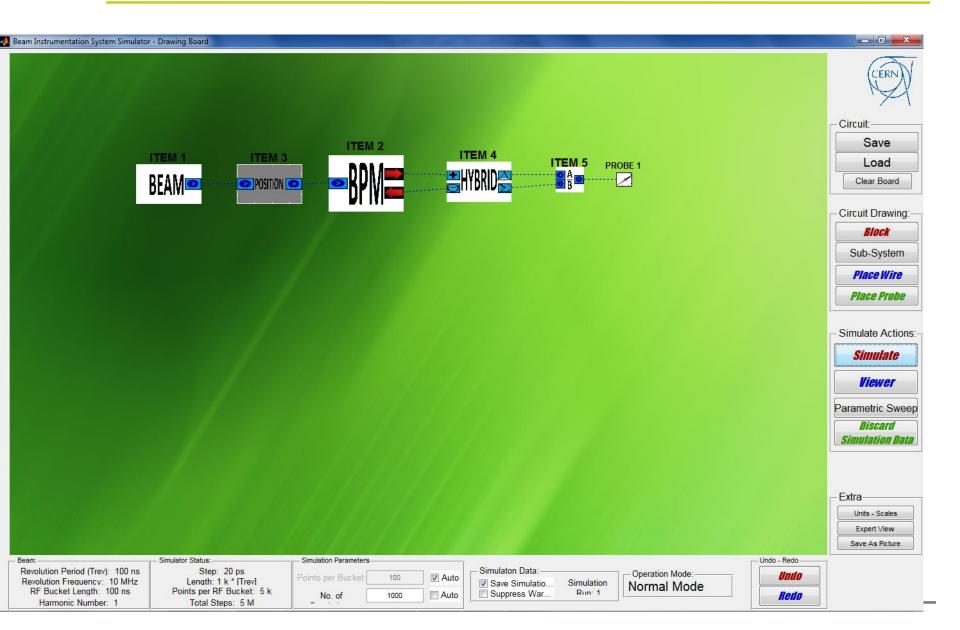


Sensitivity

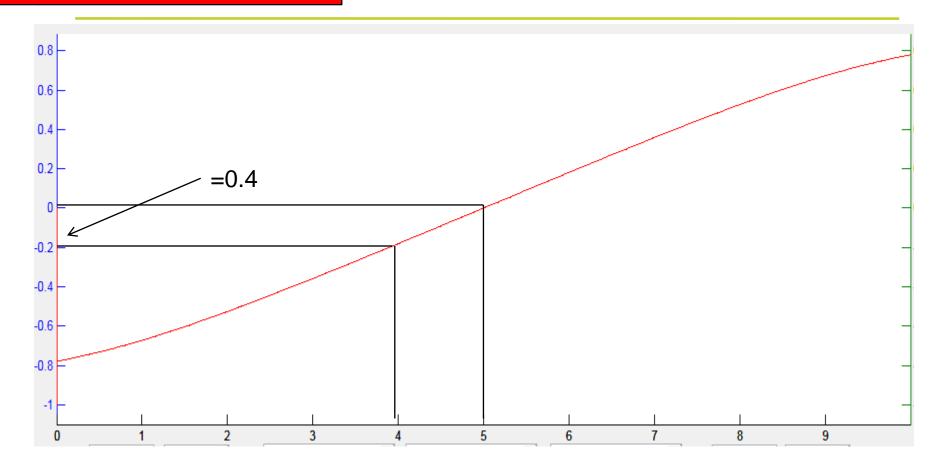




Simulation



Multiply to the Scale a factor 2!



y=S*x, $x_{full\ scale}$ = position variation, S=y/x -100% to 100% means the \pm radius => x=10 => x= 40.5 mm K_x = 1/S = 4.05 / 0.40 = 10.15